

# Considerations on the module vacuum

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## •Summary

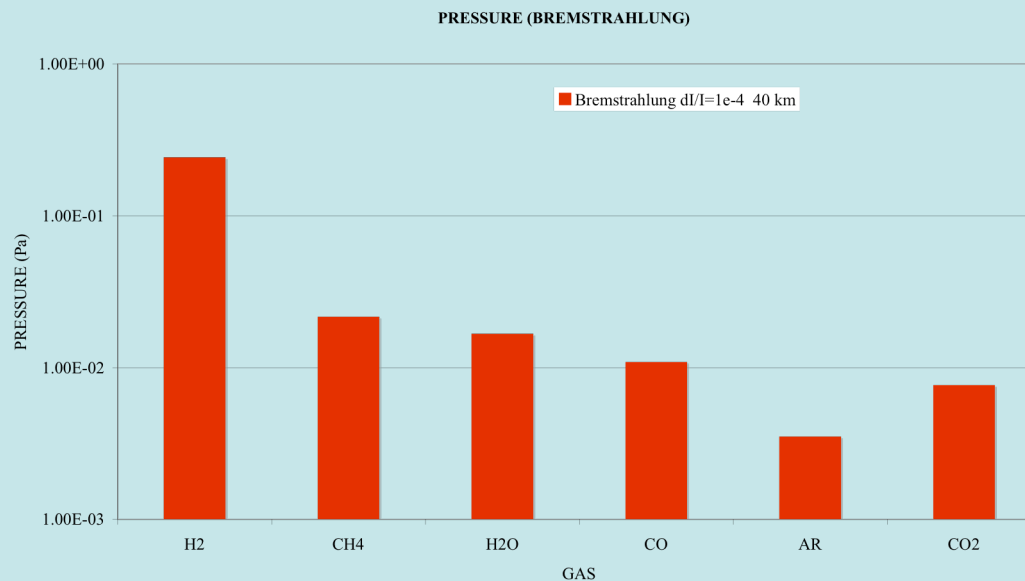
- Specifications: P
- Key points: Gasloads
- A scheme for the vacuum system

# What Pressure??

See D. Schulte talk: Fast ion instabilities

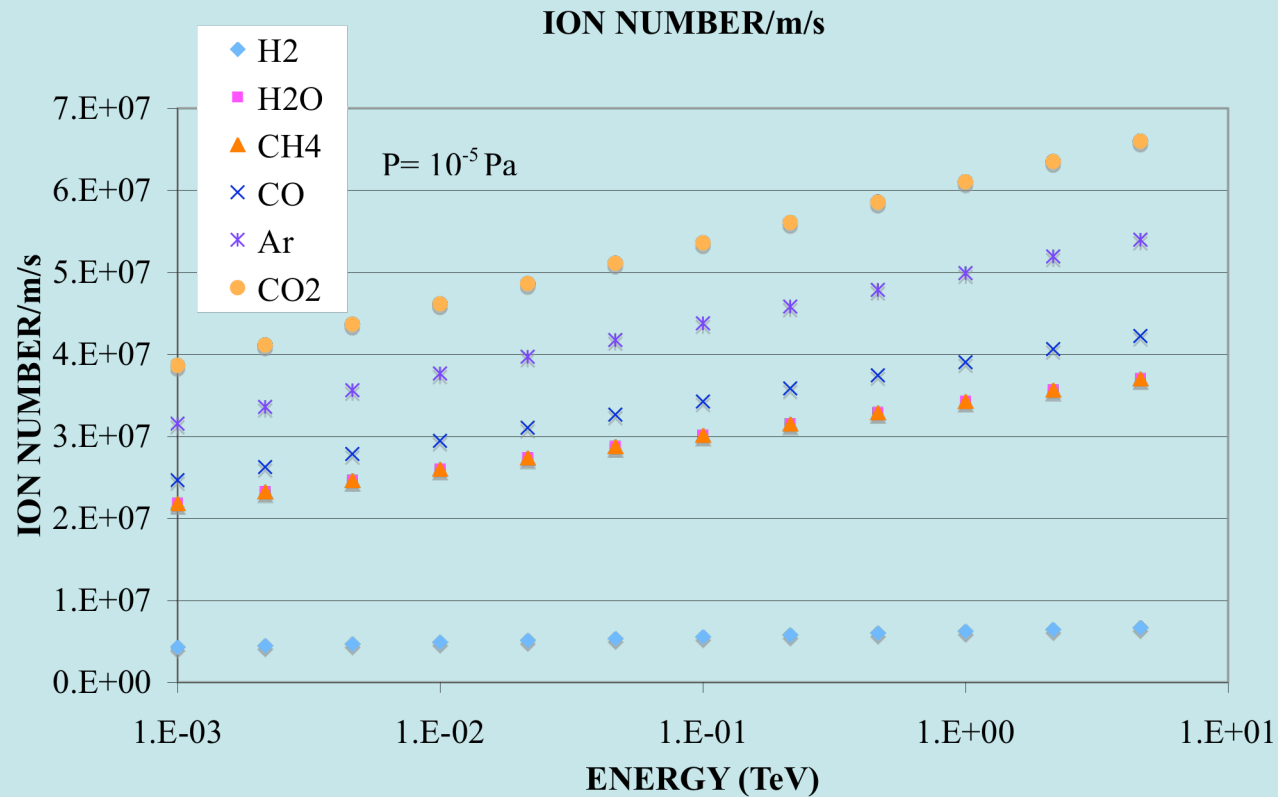
Drive beam: 1nTorr

Main beam: still uncertain



# What Pressure??

- Production of ions (neutralisation)?

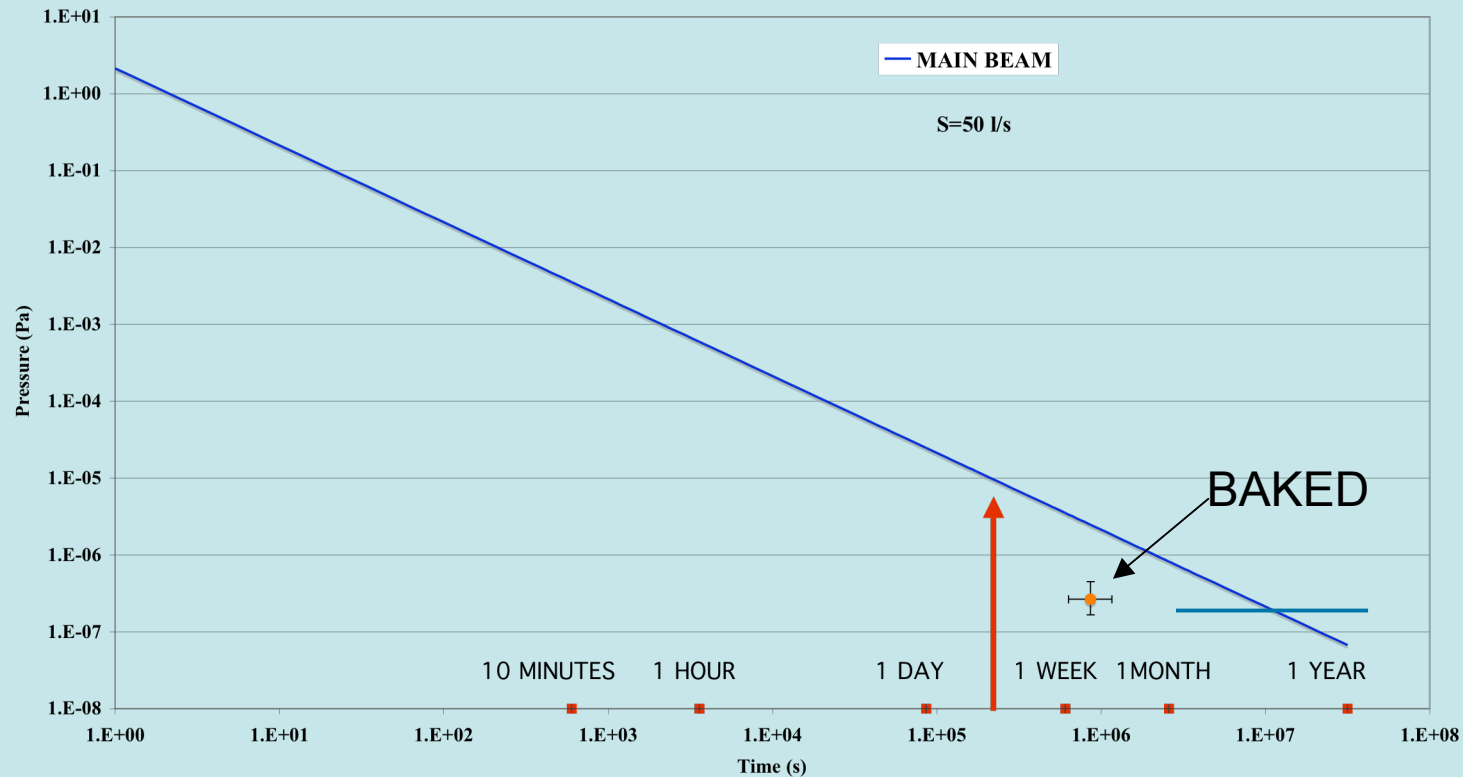


# What Pressure??

- Users requirements: RF:
  - No influence of bake out on conditioning
  - Model developed for breakdown in agreement with experimental results: no vacuum depending parameters
  - Tradition?=>  $10^{-6}$  Pa
  - Doubts with “Fast Ion Instabilities”  $10^{-8}$  Pa?

# GAS LOAD

- Unbaked system=> Water predominates
  - $S \sim 10 \text{ m}^2/\text{module MB}$  ,  $S=50 \text{ l/s}$



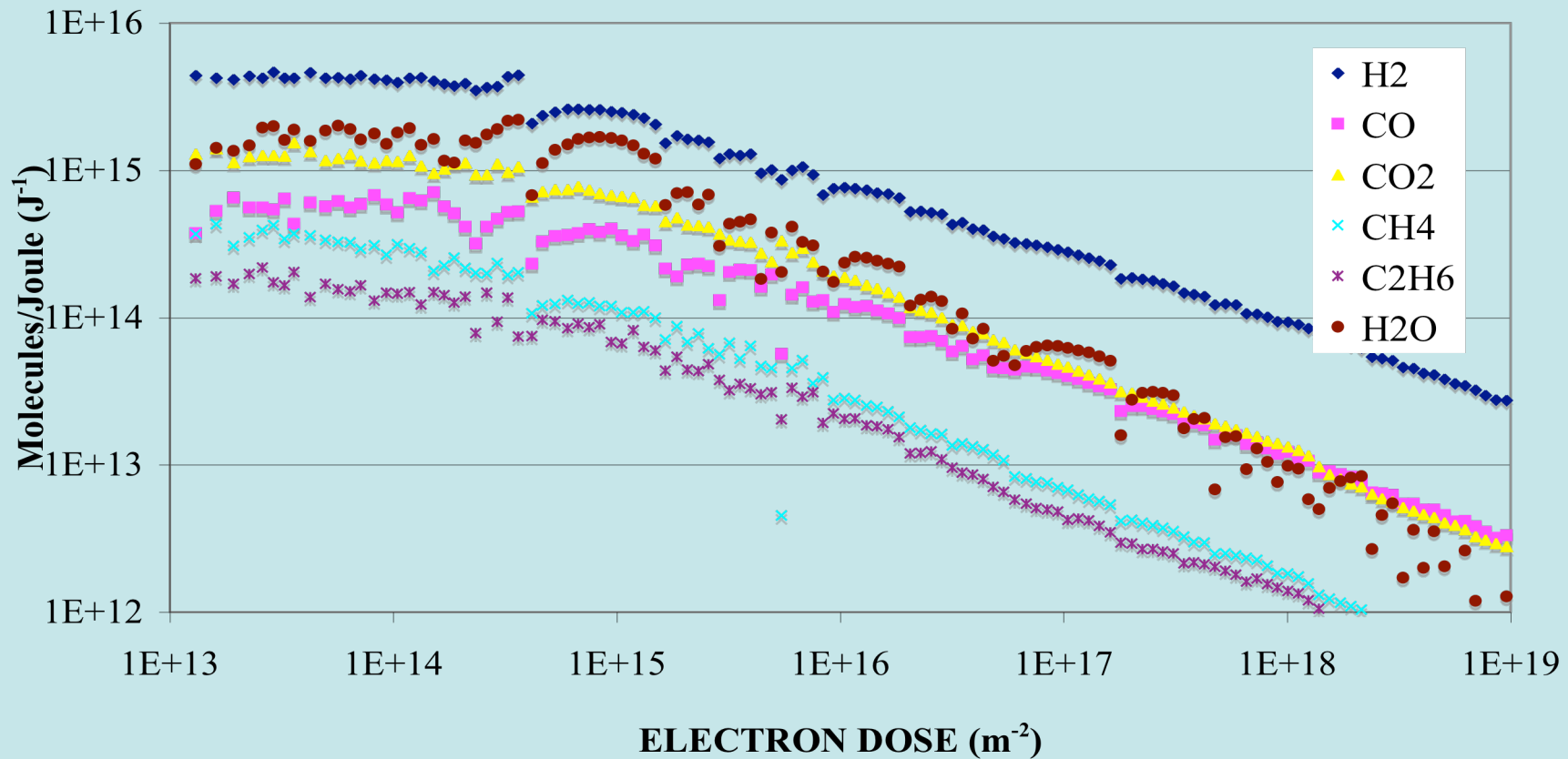
# GAS LOAD

- Baked
  - Expensive
  - Mechanical constraints (thermal elongation)
  - Extra space needed for bellows
  - Space in quadrupoles?
  - Lower pressure in shorter time
- Unbaked
  - More demanding in terms of materials/cleanliness (ferrite excluded)
  - Longer time to achieve “good” pressure
  - Reduced thermal elongation=> less constraints on bellows=> more space
  - Cheaper operation
  - Less constraints on Quad aperture

# Gas Load

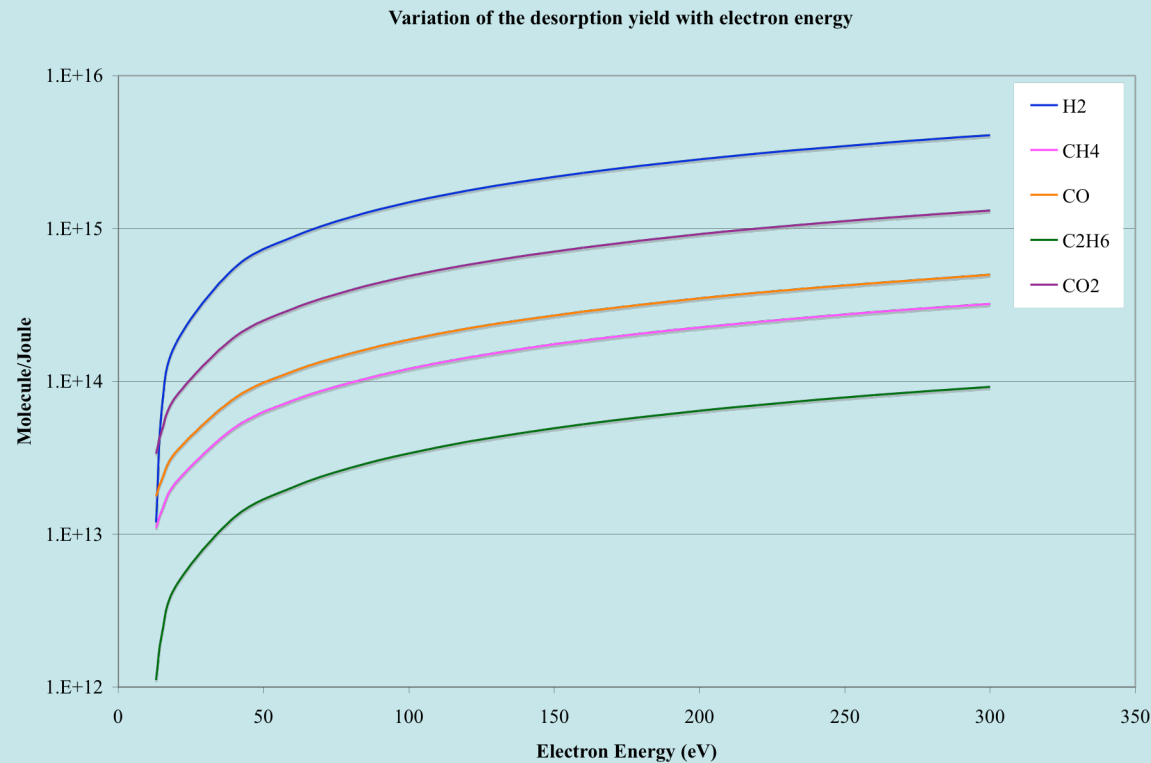
- Dynamic: e<sup>-</sup> induced desorption?
  - 10J/breakdown (Walter)

Molecules/Joule



# Gas Load


- Dynamic: e<sup>-</sup> induced desorption? 10J/breakdown (Walter).  
Electron Energy: 100 keV: stopping force reduced by ~10 (compared to 300 eV)
- => Breakdown liberate ~ 10<sup>15</sup> mol/breakdown ( 4x10<sup>-6</sup> Pa.m<sup>3</sup>)





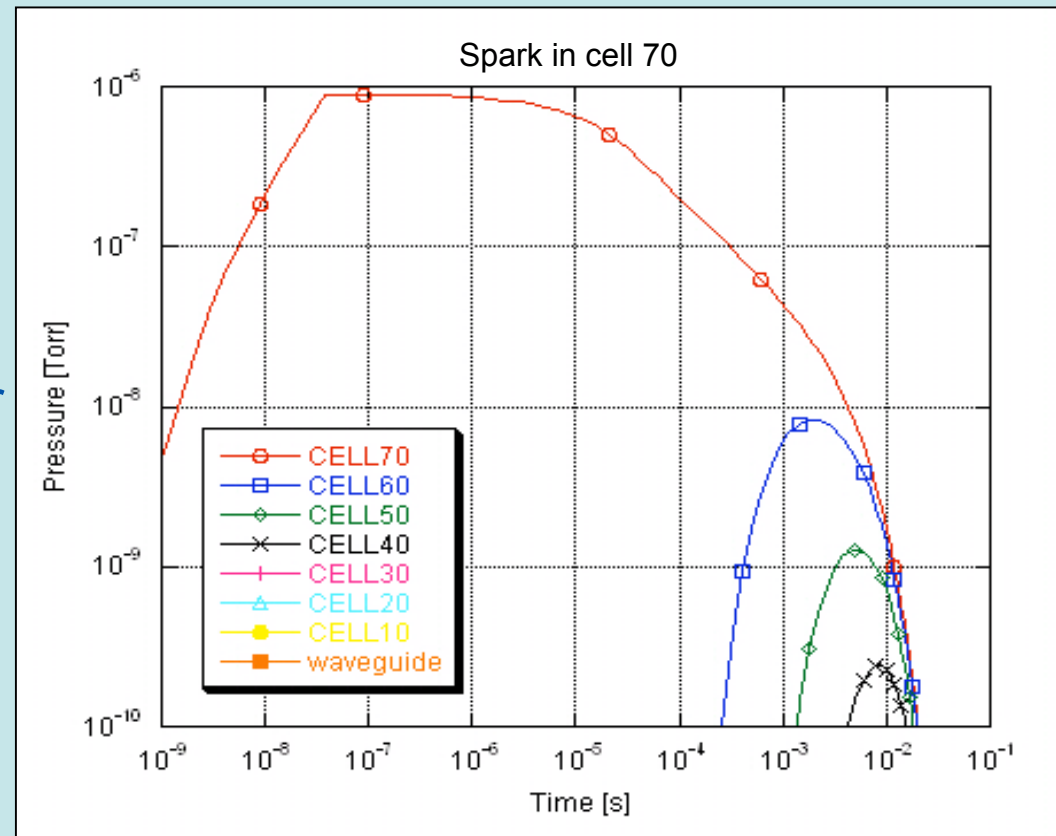
# Gas Load

- Dynamic: irrelevant for vacuum design
  - Cell Pressure entirely determined by structure design

Simulation for HDS  
(30GHz) 

For 11GHz structures  
conductance per cell is ~30x higher  
Per structure ~4x higher

	30GHz	11GHz	increase
	S[l/s]	S[l/s]	
H2/cell	0.02	0.56	28.9
CO/cell	0.01	0.15	27.5
H2/struct	10.934	45.15877	4.1
CO/struct	3.035658	11.90549	3.9



# Gas Load

- Dynamic: irrelevant for vacuum design  
(If no influence of bake out)
  - Gas load during breakdown : pretreatments
  - Pumping speed independent of pumps (conductance)
  - Breakdowns transients pumped by container volume:  
 $VdP/dt$

# PUMPS

- MAIN PUMPS:

- Pumping during breakdown:

- holes in the structure

- P recovery between breakdowns:

- Volume of the vacuum tank

- Mean pressure

- External pumps

- Example:

Breakdown  $dP/dt=10^{-6}Pa/ms$ ,  $P=10^{-6} Pa$

- Q pump:  $P=10^{-6} Pa$ ,  $1000l/s \Rightarrow Q=10^{-3}Pa.l/s$

- Q vol (200l)  $\Rightarrow Q= 2 \cdot 10^{-1} Pa.l/s$

# PUMPS

- Preevacuation: Mobile TM stations (access??)
- Holding pumps: Ion+ Capture pumps
  - Ion: 50 l/s =>
    - Pump ignition ~ 1day
    - start up of structure operation (1 week)
  - Su pumps for hard conditioning/ operation (~1000 l/s)
    - Cheap reliable
    - Efficient after ~ 2 weeks
    - Tests needed (speed/capacity for water?)
  - Alternate: Cryogenic pumps/TM pumps
    - Expensive (very)
    - Reliability ? (expensive maintenance)

# Sectorisation

- Each quadrupole is a barrier (0.4 l/s conductance)
- Length of sector determined by:
  - Money (1 valve~ 20kCHF)
  - Space lost (~ 10 cm minimum)
  - Operation: in case of failure or modification all the length vented=> reconditioning. Failure rate?
  - Guess :
    - 1% total length (20km=>200m)
    - lost space ( $\geq 100$  mm)
    - 100 sectors=> 10m
  - 200m long sectors: 1% of the accelerator opened (i.e. reconditionned) per failure

# Vacuum monitoring

- One valve (manual) on vacuum envelope per girder
- Ion pump used for vacuum measurement (reliable above  $10^{-6}$  Pa) $\Rightarrow$  provides VAC interlocks
- When problems: magic box connected to the valve: (gauge, RGA...)
- Leak check made per girder (lengthy)
  - Possibly by-pass between two tanks

# Miscellaneous

- Construction element: 1 girder (~2m)
- In case of problem transported as a block to the lab
- Avoid any unnecessary constraints :
  - Cheap (hopefully) welded vacuum tank
    - Geometry  $\pm$ some mm
    - Tank cover with bellows at the beam pipe (no load on the fragile beam tube)
    - Welded beam tube junction (no flange but space for automatic welding machine)
- Possibility to bake each girder before installation?

# Possible quad chamber design

- Produced in 2 halves
- Machined (accurate parts)
- Longitudinal weld between 2 profiles
- NEG strips in the appendixes (Pumping and heating elements)
- To be adapted to actual quad design
- Integrated pump~ 10l/s/m
- To be checked for feasibility, cost and performance





# CONCLUSIONS

- Most important question: design pressure?
- =>Choice between baked/unbaked system
- Achievable pressure in cells determined only by geometric constraints
- Connexion between module/BPM/quadrupoles must be studied: space, technique...