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Nuclear Energy Agency



Fifth International Workshop on the Utilisation and Reliability of High Power Proton Accelerators

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Reliability of a s.c. linac from the ADS perspective

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Revised version for:

CARE-HHH-APD BEAM'07



with many contribution from DM1/WP1.3-Accelerator (IPNO/CEA/IBA/IAP/INFN) and ENEA



Forschungszentrum Karlsruhe
in der Helmholtz-Gemeinschaft



AnsaldoNucleare
Una Società Finmeccanica



EUROTRANS EUROPEAN RESEARCH PROGRAMME FOR THE TRANSMUTATION OF HIGH LEVEL NUCLEAR WASTE IN AN ACCELERATOR DRIVEN SYSTEM

In the 6th Framework Programme of EC (2005-2008)
Expands 5th FP PDS-XADS Project (2001-2004)

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4 year research budget 42.3 M€ (23 M€ from EU funds)

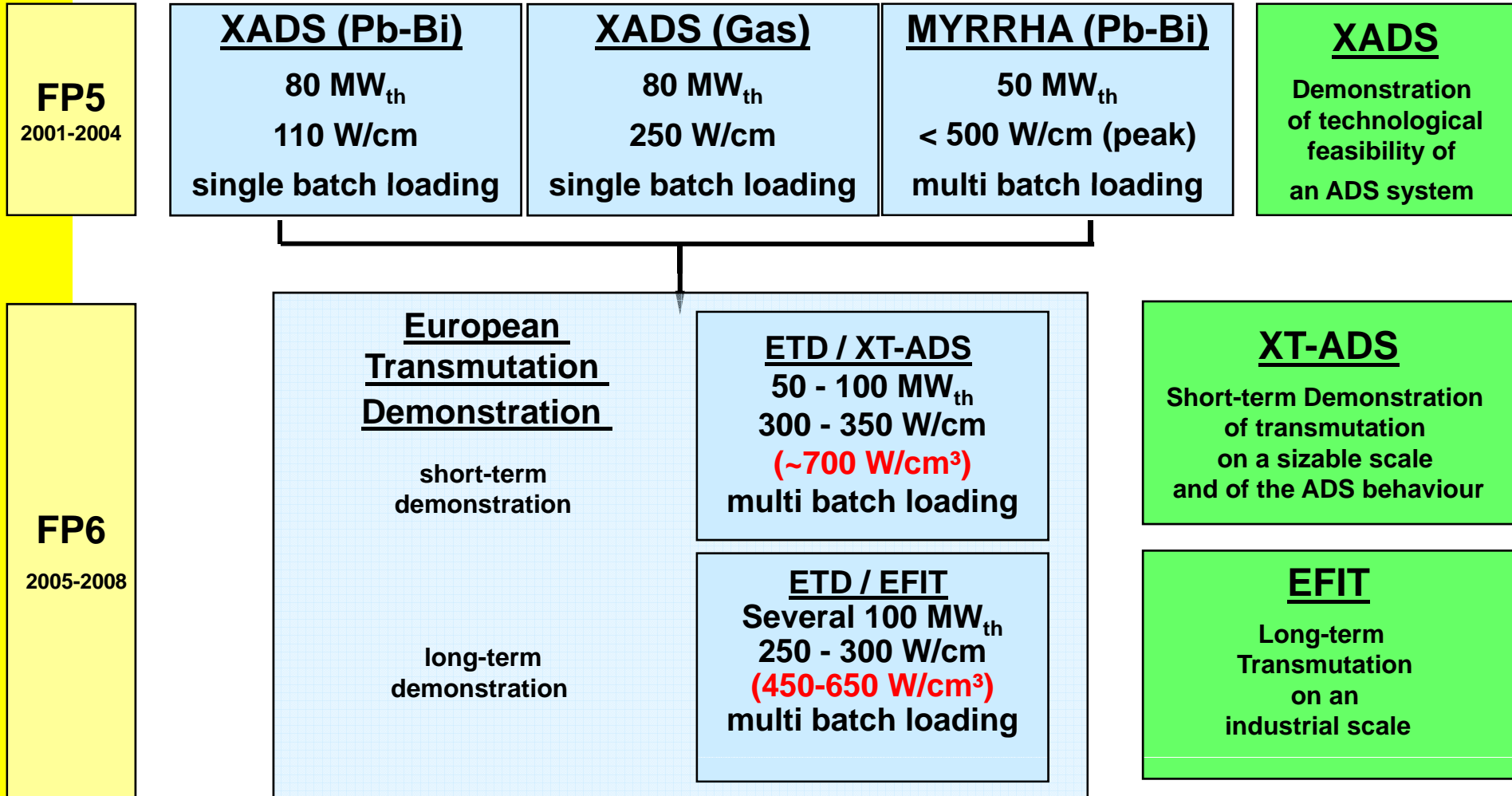
CERN, 1-5 October 2007

- Work towards a **European Transmutation Demonstration** (ETD) in a step-wise manner
- Advanced design of a 50 to 100 MWth eXperimental facility demonstrating the technical feasibility of Transmutation in an **Accelerator Driven System (XT-ADS)**
 - realization in a short-term, say about 10 years
- Generic conceptual design (several 100 MWth) of a modular **European Facility for Industrial Transmutation (EFIT)**
 - realisation in the long-term

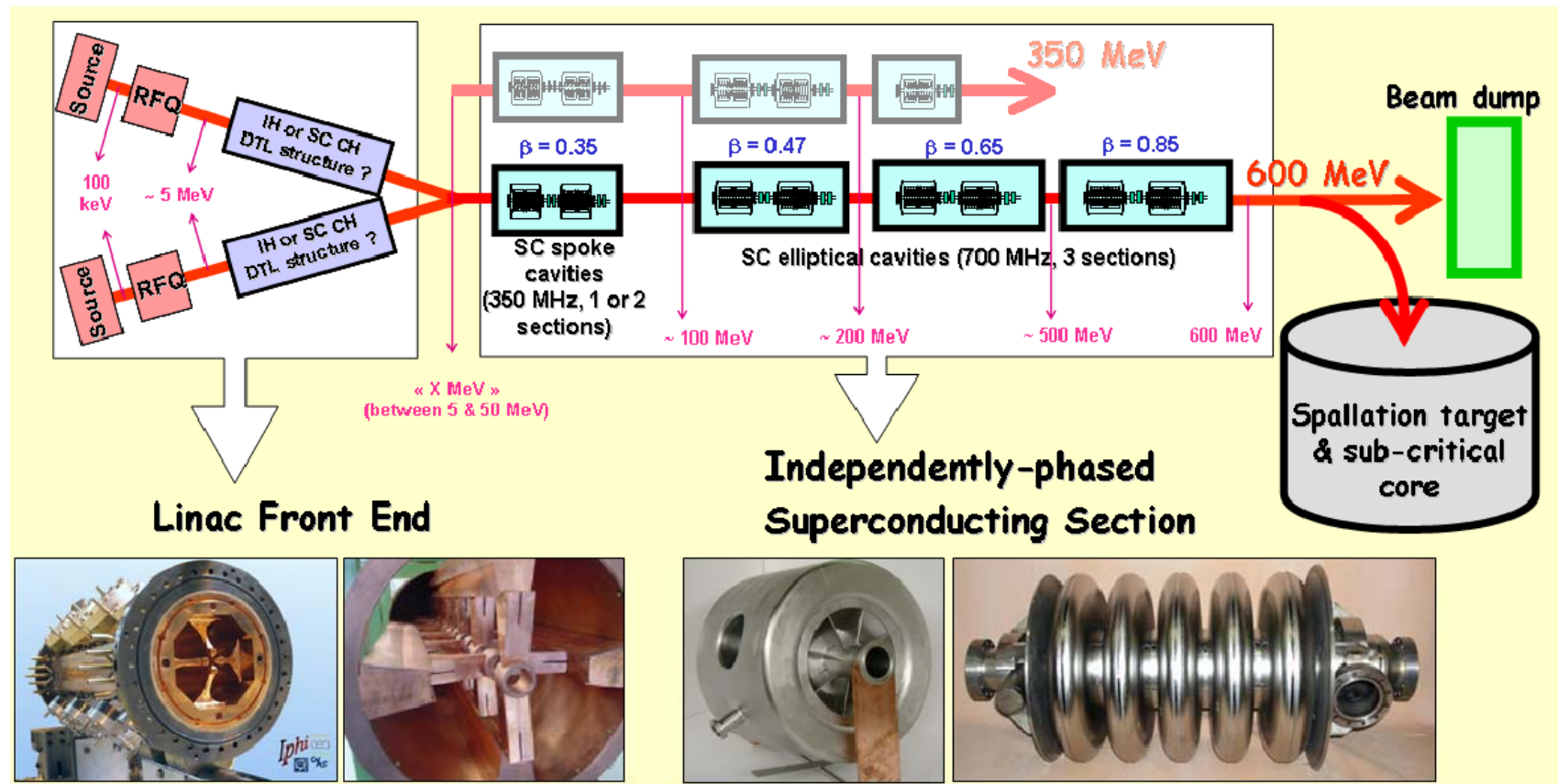
FP

Design Concepts

Objectives



- Accelerator design performed in the PDS-XADS program
 - Choice of **superconducting linac**
 - Modular: same concept for Prototype and Industrial scale



- Specific challenges for ADS:
 - **High reliability and availability**
 - Less than a few unexpected beam shutdowns per year
 - trips longer than 1 s duration induce stresses on fuel and assembly
 - Component design and operation following the reliability-oriented procedures used in the nuclear reactor community
 - strong design
 - planning of redundance and fault tolerance capabilities
 - **High power CW operation**
 - But with the possibility for beam holes (200 μ s) at low duty cycle for on-line reactivity measurements of the subcritical assembly
- For every linac component (in the high-energy, mid-energy and low-energy sections) in the EUROTRANS program a prototype will be designed, built and tested

How reliability has been implemented



- **Reliability guidelines extensively used in the linac design**
 - Derating
 - Redundancies
 - Fault tolerance
- **Provide redundancy in the most critical items**
 - Source, RFQ, low energy stage
 - Achieved by injector **duplication**!
- **Handle the “natural” redundancy in the superconducting linac**
 - A SC linac has a **high degree of modularity**
 - The whole beamline is an array of nearly identical “periods”
All components are derated with respect to technological limitations
 - A high degree of fault tolerance with respect to cavity/magnets can be expected in the SC linac
 - Implies a reliable and sophisticated digital RF **control system** with preset set points for implementation

- Starting with **FP5 PDS-XADS** we have started developing a qualitative FMEA + a lumped-component reliability model of the driver superconducting linac
 - preliminary “parts count” assessment presented at HPPA4
- Extended study to variety of linac configurations
 - » L.B., P.P., *Rel. Eng. System Safety* **92** (2007) 449-463
 - concentrate on **design issues rather than component data**
 - **fault tolerance implementation**
 - **missing of a exhaustive and representative reliability parameter database**
- **FP6 EUROTRANS** assumes the same linac layout
- Study extended to show sensitivity to component reliability characteristics

Outcome of FP5 PDS-XADS activities



- Three project deliverables dedicated to reliability assessments
 - Qualitative **FMEA**
 - RBD** analysis
 - Assessment of (lack of) existing **MTBF** database for components
 - Identification of **redundant and fault tolerant linac configurations** intended to provide nominal reliability characteristics

CONTRACT N°: FIKW-CT-2001-00179		FP5
ISSUE CERTIFICATE		
PDS-XADS Preliminary Design Studies of an Experimental Accelerator-Driven System		
Workpackage N° 3 Identification: N° DEL/04/063 Revision: 1		
Definition of the XADS-class reference accelerator concept & needed R&D		
Dissemination level: PU Issued by: CNRS Reference: XADS-DEL04-063 Status: Final		

4 Failure Mode and Effect Analysis

1.3 – Radio Frequency Cavity

1.3.1 - RF Cavity

Function: Provide initial acceleration
 Originated by: RF/DS
 Institution: CEA/INFN

Failure Mode	Cause
Failure to reach design RF field	Broken Pickup and/or connectors
Failure to reach design RF field	RF instability due to field emission
Failure to reach design RF field	Failure in RF feed
Failure to reach design RF field	Failure in LLRF control system
Failure to reach design RF field	Cavity detuning due to wrong cooling (water flow)
Failure to reach design RF field	Cavity detuning due to wrong cooling (water temperature)
Vacuum leak	Leak in welds

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Rev. 0

FIKW-CT-2001-00179

CONTRACT N°: FIKW-CT-2001-00179		FP5
ISSUE CERTIFICATE		
PDS-XADS Preliminary Design Studies of an Experimental Accelerator-Driven System		
Workpackage N° 3 Identification: N° DEL/03/057 Revision: 0		
Potential for Reliability Improvement and Cost Optimization of Linac and Cyclotron Accelerators		
Dissemination level: RE Issued by: INFN Reference: INFN/TC_03/9 (July, 23 rd , 2003) Status: Final		
Summary: This document identifies the suitable design strategies that have been followed in order to meet the reliability and availability specifications for the XADS accelerator outlined in Deliverable 1. The document describes also how these strategies can be applied in the different components of the XADS accelerator design, and how design iterations can lead to reliability improvements. The Failure Mode and Effect Analysis (FMEA) methodology has been used on the suggested design for highlighting the reliability critical areas. Finally, a first rough cost estimation of the XADS accelerator is also provided.		
23/07/2003	Paolo Pierini, INFN 	Alex C. Mueller, CNRS
	WVP LEADER Name/Company Signature	Bernard Carlucci, Framatome ANP SAS
DATE	RESPONSIBLE Name/Company Signature	COORDINATOR Name/Company Signature

assessment	operate	4	RFQ off	4	delivery	3	RF-control	repair	solution and test switching capabilities
LLRF system reliability assessment	Cavity cannot operate	4	RFQ off	4	No beam delivery	3	Machine control system	Repair	No effect for a double injector solution and fast switching capabilities
ong 									

- Define a **Mission Time**, the operation period for which we need to carry out estimations
 - Depends on design of subcritical assembly/fuel cycle
 - big difference w.r.t. HEP context, no weekly maintenance
- Define **parameter** for reliability goal
 - **Fault Rate**, i.e. Number of system faults per mission
 - **Availability**
 - No concern on **R** parameter at mission time
 - R is the survival probability
 - relevant for mission critical (non repairable environments, satellites!)
- Provide **corrective maintenance** “rules” on elements
 - Components in the accelerator tunnel can be repaired only during system halt
 - Personnel protection issues in radiation areas
 - Components in shielded areas can be repaired immediately

- Assumed XT-ADS
 - 3 months of continuous operation with < 3 trips per period
 - 1 month of long shutdown
 - 3 operation cycles per year
 - 10 trips per year (*i.e. beam interruptions longer than a second*)
 - no constraints on R

Mission Time	2190 hours
Goal MTBF	~ 700 hours
Goal number of failures per mission	~ 3
Reliability parameter	Unconstrained

- Baseline idea: use a commercial available RAMS tool for formal accelerator reliability estimations
 - Powerful RBD analysis
 - Montecarlo evaluation
 - Elaborated **connection configurations**
 - Hot parallelism
 - Standby parallelism
 - Warm parallelism
 - “k/n” parallelism
 - Many options for **maintenance schemes** and actions (both **preventive & corrective**, “kludge fixes”, etc.)
 - Eg: fix when system fails or fix when component fail (it’s the same only for series connection)
 - can easily account for maintenance cost and repair and spare logistics
 - Not used at all in accelerator community (or at least very rarely!)

What kind of faults are in component MTBF?



- ***MTBF means only random failure events***
- **Every failure that is highly predictable should get out of the MTBF estimations, and goes into the (preemptive) maintenance analysis**
 - eg. Components wear out, failures related to bad design, Aging (if we perform a constant failure rate analysis)
- **Example:** CRT Monitor in a RBD block
 - MTBF of 100.000 h
 - But we know that CRT phosphors do not last 11 years! Monitors need to be changed after 5.000 h of operations or so.
 - The “bath-tub” curve...
- **Trivial concepts within communities where reliability standards have been applied since decades**
 - Not so clear in accelerator community, hence confusing DB
 - Accelerators are now in a similar situation of NPP in the '70s

- Often many “reliability” problems can be truly identified as component design issues (weak design) or improper operation (above rated values)
- e.g. very successful SNS operation
 - concerns due to components providing non critical functionalities but with failure modes with drastic consequences

Operations of SNS SRF

- **Cold Cathode Gauges**
 - Degradation of response and decreasing reliability (interlock replacement)
- **HOM Filters**
 - Distorted transmitted power waveforms
 - Feedthrough and attenuators failures
- **Field emission**
 - Relationship to quench, HOM, FPC
 - Field emission cross talk
 - Field emission cryogenic load



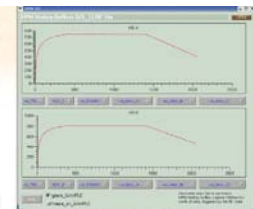
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Fermilab April 23-26, 2007
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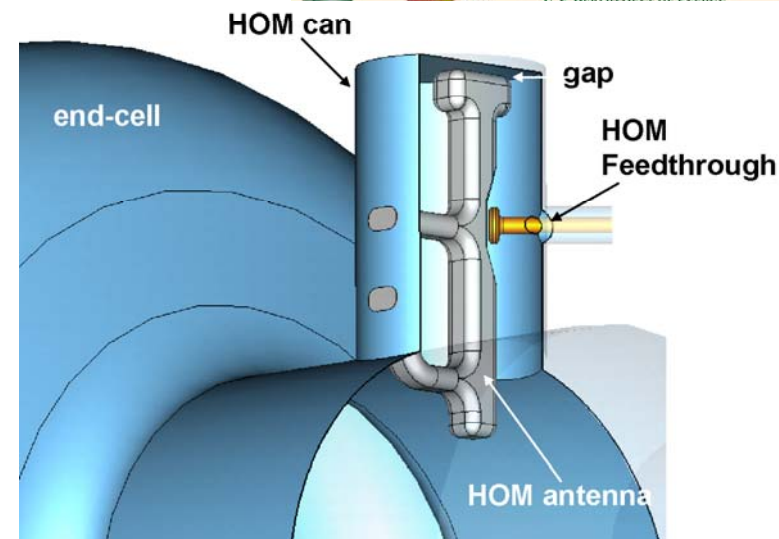
HOM couplers

- At Jlab
 - 2 feedthroughs leaked after testing
- At SNS
 - 11b (HOMB), 19b (HOMA) off due to excessive fundamental mode coupling
 - ~10 cavities show deformed transmitted power waveforms
 - Most inline attenuators were damaged during turn on and operation (transient power surge, related to field emission bursts)
 - Operational gradients limited and some cavities are off to prevent possibility of HOM feedthrough failure



HOM transmitted power curves (log)

HFIR SNS
TESLA Technology Collaboration Meeting
Fermilab April 23-26, 2007
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CHL event

- On February 25th a loss of communication between an IOC and a PLC in the CHL resulted in over pressurization of the He return header and of all the cavities to 2.2 atm.
- Negative impact: three tuners were damaged (being repaired as we speak)
- Positive impact: the system was pressure tested a significant fraction of the pressure vessel code requirements



TESLA Technology Collaboration Meeting
Fermilab April 23-26, 2007
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Fermilab Update on Inner Triplet Magnets at LHC

On Tuesday, March 27, a Fermilab-built quadrupole magnet, one of an "inner triplet" of three focusing magnets, failed a high-pressure test at Point 5 in the tunnel of the LHC accelerator at CERN. Since Tuesday, teams at CERN and Fermilab have worked closely together to address the problem and have identified the cause of the failure. Now they are at work on a solution.

The asymmetric force generated by the pressure of the test broke the supports in magnet Q1 that hold the magnet's cold mass inside the cryostat, which also resulted in damage to the electrical connections. The status of the Q1 cold mass itself is still being determined, as is the status of the other two magnets in the triplet, Q2 and Q3. Also under investigation is the status of a distribution feed box, or DFBX, designed to provide cryogenic fluids and electrical power for the inner triplet magnets.

The magnet supports are made of a material called G-11, a glass cloth-epoxy laminate. The specifications for the magnet designate 20 atmospheres as the design pressure criterion and 25 atmospheres as the acceptance test criterion. However, computer-aided engineering calculations completed independently by Fermilab and CERN on March 28 show that the G-11 support structure in the magnets was inadequate to withstand the associated longitudinal forces. CERN and Fermilab now know that this is an intrinsic design flaw that must be addressed in all triplet magnets assembled at Fermilab.

Review of engineering design documentation reveals that the longitudinal force generated by asymmetric loading was not included in the engineering design or identified as an issue in the four design reviews that were carried out.



Q1 Quadrupole Magnet – CERN and Fermilab are working to identify repairs to the structures that hold the cold mass (blue) in place within the cryostat (orange) in each magnet of the triplet on either side of the LHC's four interaction points. The Q1 magnet of each triplet is the magnet closest to the interaction point (IP).



Longitudinal force during a pressure test broke the G-11 support structure (green) securing the cold mass (blue) inside the magnet cryostat (not shown).

Also design reviews and risk analysis procedures are different in the 2 communities

March 2007
LHC magnet failure in tunnel

a foreseen test condition was not in the design specs

But also cases of significant design effort



- LHC Machine Protection system
 - Energy stored in each of the 2 proton beams will be 360 MJ
 - If lost without control serious damage to hardware
 - 1 kg of copper melts with 700 kJ
 - Analysis meant to trade off safety (probability of undetected beam losses leading to machine damage) and availability (number of false beam trips per year induced by the system)
 - Complete reliability modeling
- LHC magnets
 - Huge energy stored in SC magnets (10 GJ)
 - Needs to be gracefully handled

Proceedings of 2005 Particle Accelerator Conference, Knoxville, Tennessee

RELIABILITY ASSESSMENT OF THE LHC MACHINE PROTECTION SYSTEM

R. Filippini, B. Dehning, G. Guaglio, F. Rodriguez-Mateos, R. Schmidt, B. Todd, J. Uythoven, A. Vergara-Fernandez, M. Zerlauth, CERN, Geneva, Switzerland

Abstract

A large number of complex systems will be involved in ensuring a safe operation of the CERN Large Hadron Collider, such as beam dumping and collimation, beam loss and position monitors, quench protection, powering interlock and beam interlock system. The latter will monitor the status of all other systems and trigger the beam abort if necessary. While the overall system is expected to provide an extremely high level of protection, none of the involved components should unduly impede machine operation by creating physically unfounded dump requests or beam inhibit signals. This paper investigates the resulting trade-off between safety and availability and provides quantitative results for the most critical protection elements.

MACHINE PROTECTION AND DEPENDABILITY CONCERNS

The Machine Protection System (MPS) [1,2] guarantees safe conditions in the LHC by 1) checking the status of the equipment before every new fill and 2) preventing damage to the machine by safely stopping operation once the beam is circulating, either at the end of

Interlock Controllers (PIC), 36 in total. More details on each system may be found in [1]. Figures of safety and unavailability due to false dumps will be given for one year of operation under different operational scenarios.

MPS MODELLING ASPECTS

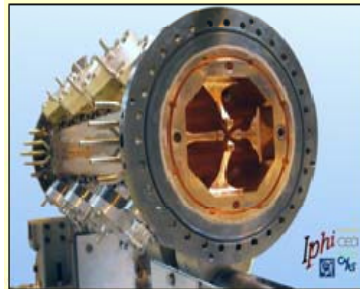
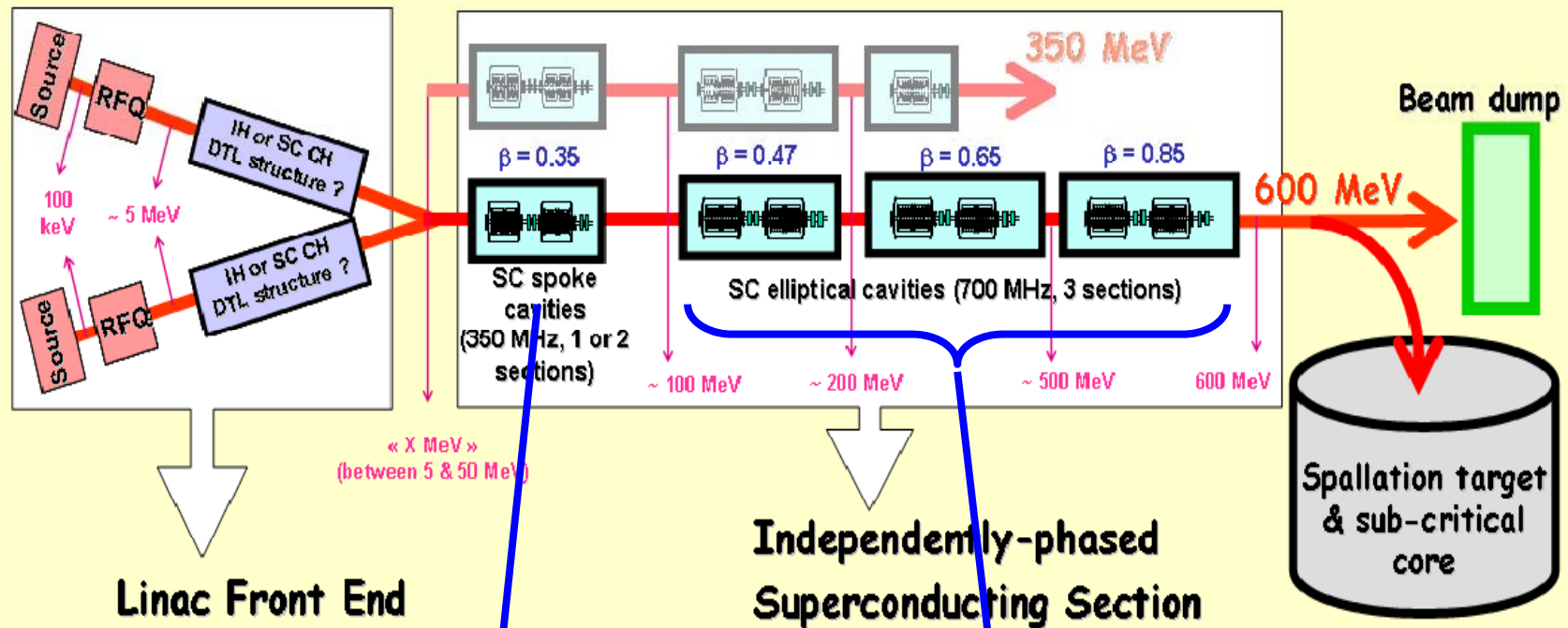
The system is studied in two steps. Firstly, safety and unavailability due to false dumps have been evaluated for each system of the simplified MPS, passing through the definition of the functional architecture, Failure Modes, Effects and Criticality Analysis (FMECA) [5] and reliability prediction at component level. This has been the most time-consuming part of the study because for all system components the failure modes needed to be defined and therefore classified with respect to the consequences, including the means to prevent them. Failure rates were deduced from literature [6] or experience (historical CERN databases), in both cases adopting conservative criteria (e.g. overestimating the component mean lifetime).

An second step, results obtained for the individual systems have been arranged into the simplified MPS model with the sources of dump requests and their

- Reduce the accelerator complexity to a simple system
- System composed of “lumped” components
 - Various sources: IFMIF, SNS, APT estimates, internal eng. judg.
 - + a bit of optimism and realism

System	Subsystem	MTBF (h)	MTTR (h)
Injector	Proton Source	1,000	2
	RFQ	1,200	4
	NC DTL	1,000	2
Support Systems	Cryoplant	3,000	10
	Cooling System	3,000	2
	Control System	3,000	2
RF Unit	High Voltage PS	30,000	4
	Low Level RF	100,000	4
	Transmitters	10,000	4
	Amplifier	50,000	4
	Power Components	100,000	12
Beam Delivery System	Magnets	1,000,000	1
	Power Supplies	100,000	1

- We cannot rely on MTBF data sources for typical accelerator components (usually special components)
- The set of data is used to develop a system scheme that guarantees the proper reliability characteristics with the given components by using
 - **fault tolerance** capabilities
 - **redundancy** patterns
- Experimental activities foreseen within EUROTRANS will provide more knowledge on some of the reliability characteristics of the key components
- Also SNS operational experience is very relevant

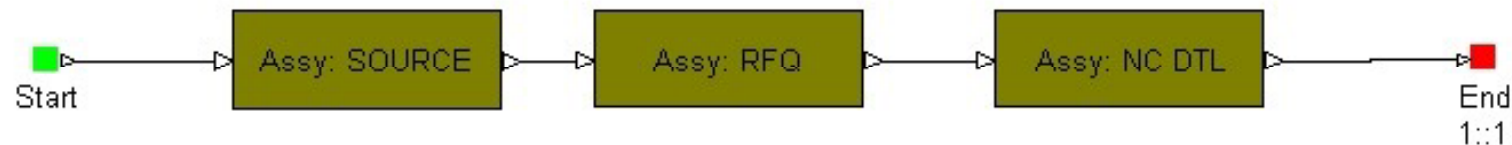


96 RF units

92 RF units

- With a “parts count” estimate we come to an obviously short MTBF ~ 30 h
- Split into:
 - Injector: 7.7%
 - Spoke linac: 45.4%
 - High energy linac: 43.5%
 - Beam line: 0.6%
 - Support systems: 2.7%
- Of course, the highest number of components is in the linac (nearly 100 RF units each, with each RF units having an MTBF of 5700 h...
- ***That already suggests where to implement strategies for redundancy and fault tolerance implementation***

Injector

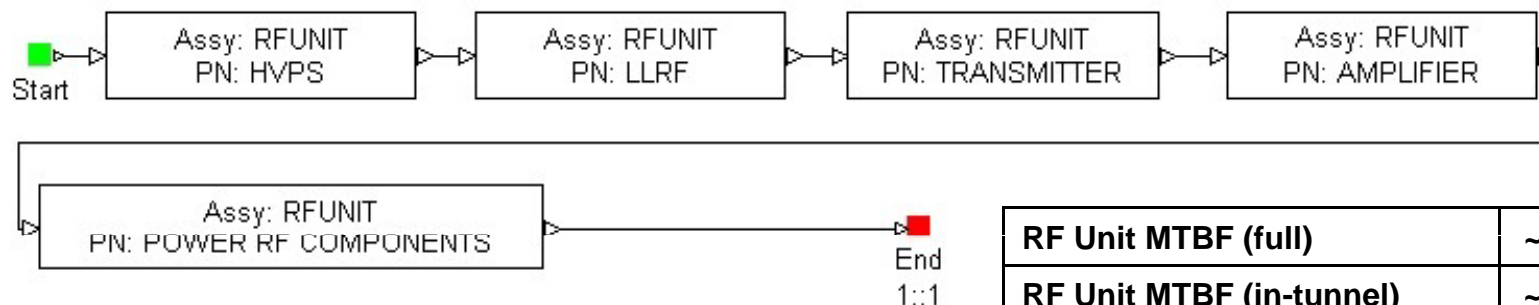


Support Systems

Standard support systems, with MTBFs only moderately tailored to mission time. Each system $R(\text{Mission time}) = 0.48$.



RF Units

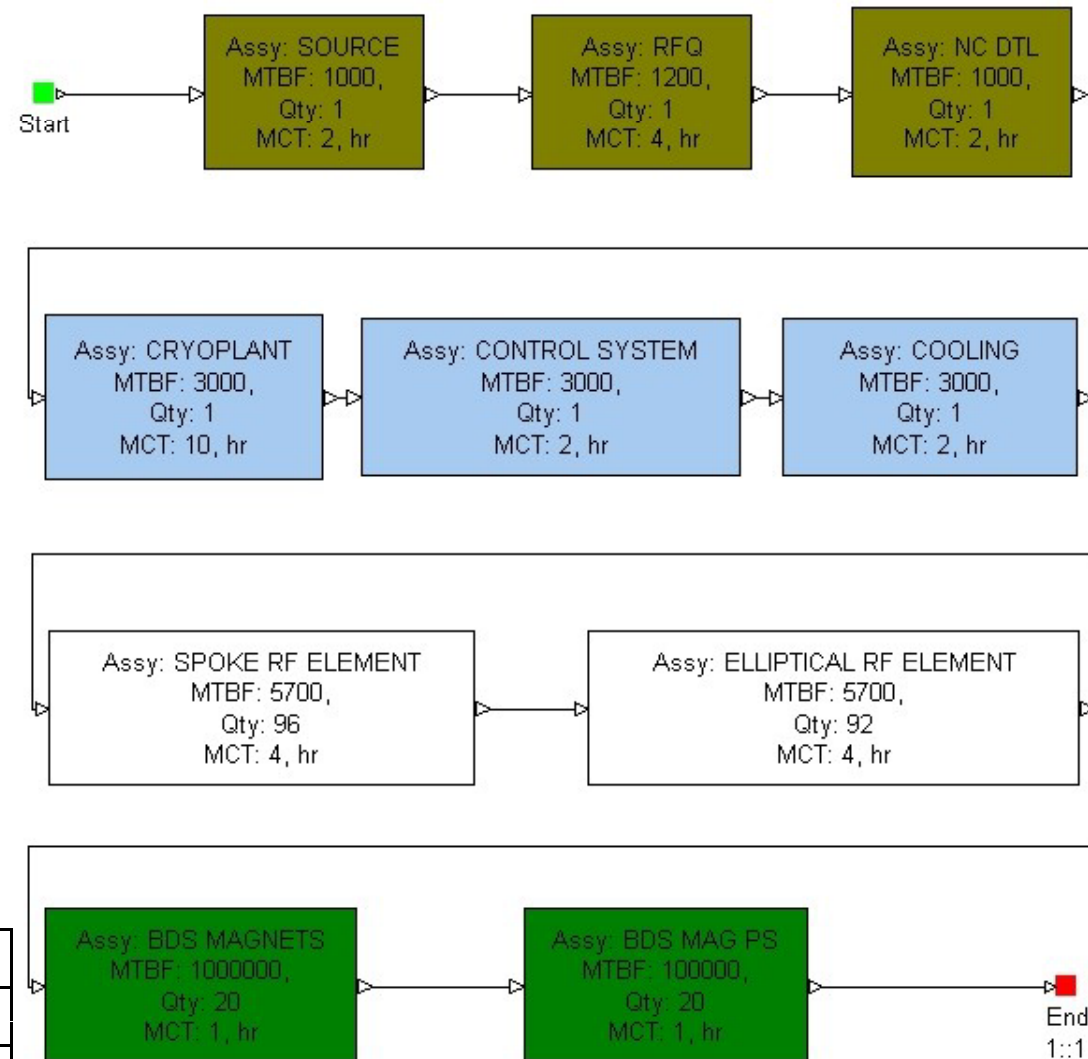


RF Unit MTBF (full)	~ 5700 hours
RF Unit MTBF (in-tunnel)	~ 6100 hours

Initial Scenario – All Series, no redundancy



- Worst possible case
 - similar to parts count
- All component failures lead to a system failure
- Poor MTBF
- Too many failures per mission
- Mostly due to RF units
- $5700/188 = 30.32 \text{ h}$



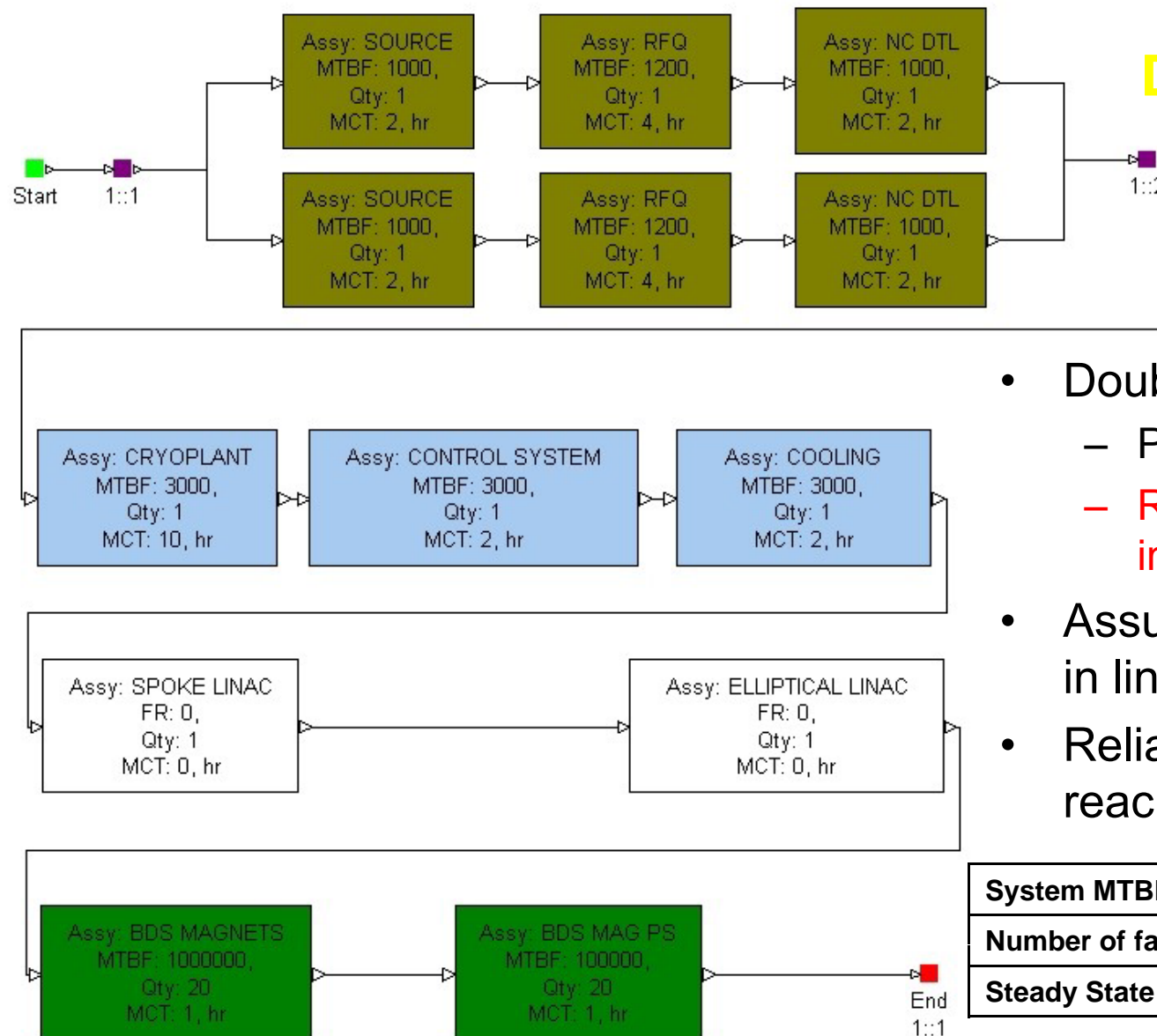
System MTBF	31.2 hours
Number of failures	70.23
Steady State Availability	87.2 %

- Clearly, in the region where we are driven by *high number of moderately reliable components* we don't want a series connection (where each component fault means a system fault)
 - Need to provide **fault tolerance**
- Luckily, the SC linac has ideal perspectives for introducing tolerance to RF faults:
 - highly modular pattern of repeated components providing the same functions (beam acceleration and focussing)
 - individual cavity RF feed, digital LLRF regulation with setpoints and tabulated procedures
- In the injector low fault rates can be achieved by redundancy

2 Sources - ∞ Fault Tolerant SC section



Dream Linac



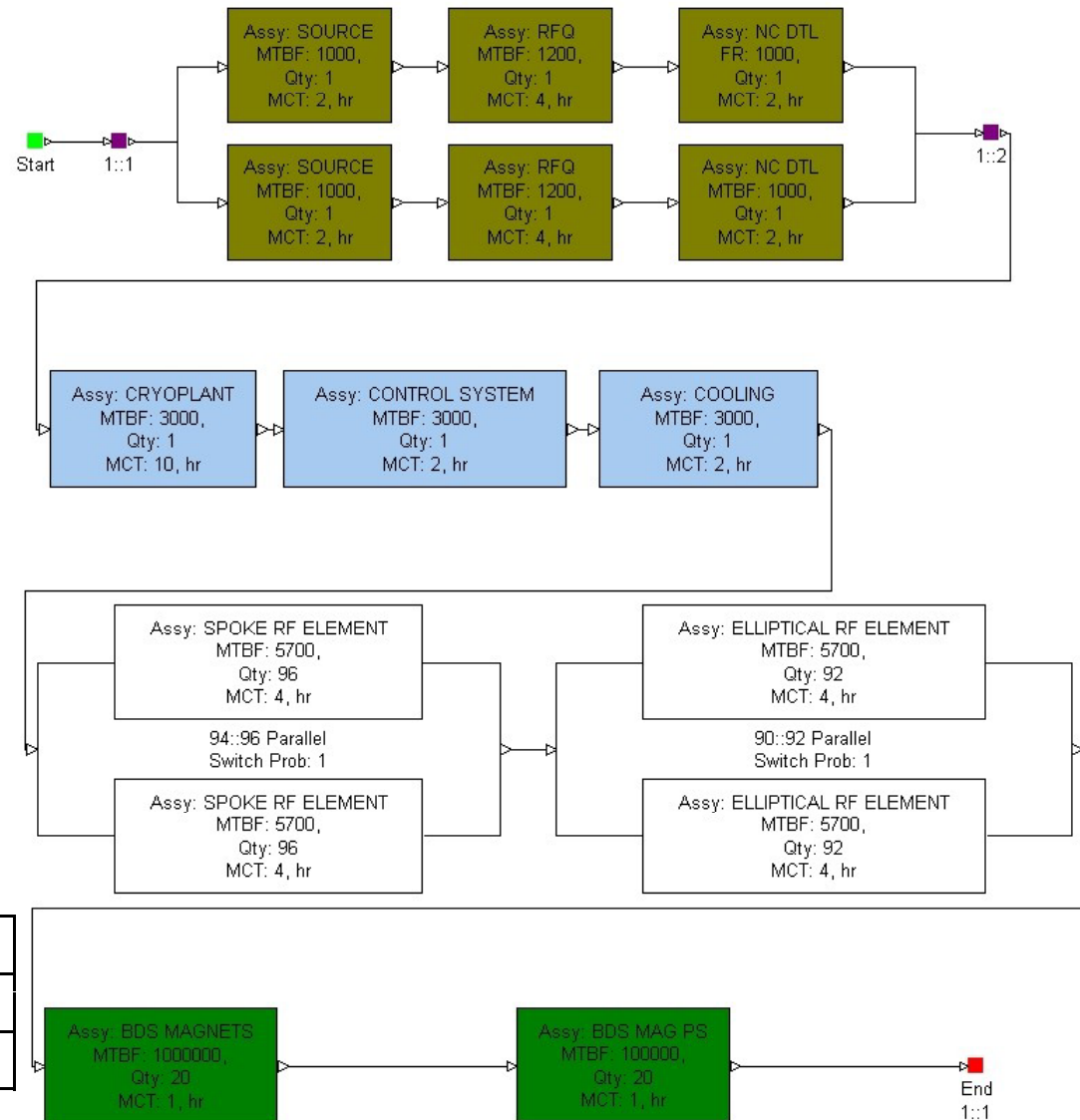
- Double the injector
 - Perfect switching
 - **Repair can be immediate**
- Assume infinite FT in linac section
- Reliability goal is reached!

System MTBF	796.91 hours
Number of failures	2.75
Steady State Availability	99.5 %

2 Sources – Redundant RF Systems



- Keep 2 sources
- Assume that we can deal at any moment with any 2 RF Units failing at any position in the SC sections
 - Maintenance can be performed on the failing units while system is in operation
 - ideal detection and switching
- Still within goals



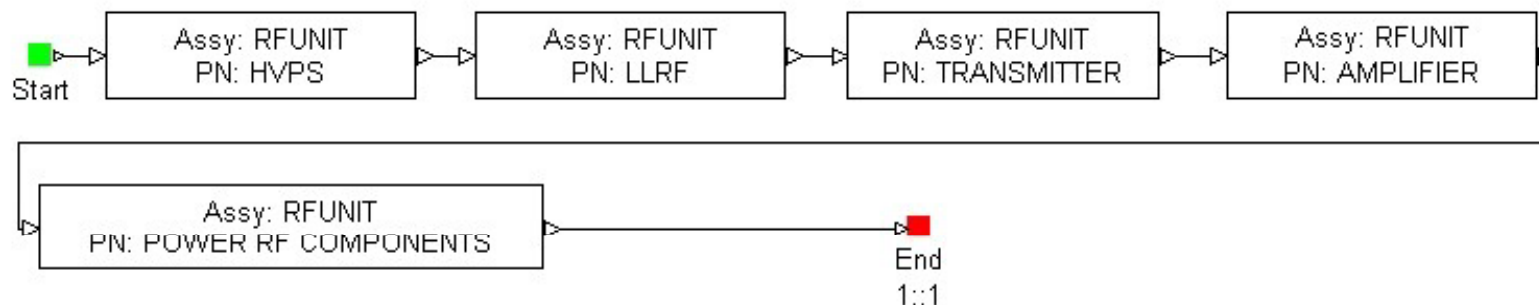
System MTBF	757.84 hours
Number of failures	2.89
Steady State Availability	99.5 %

CERN, 1-5 October 2007

Realistic RF Unit correction provisions



- When assuming parallelism and lumped components we should be consistent in defining **repair provisions**
- For example, the components in the RF system that are out of the main accelerator tunnel **can be** immediately repairable, but certainly **not** all RF power components that are inside the protected-access tunnel
 - Even if the in-tunnel component can be considered in parallel (we may tolerate failures to some degree), all repairs are executed **ONLY** when the system is stopped
 - This greatly changes system MTBF



Final Scheme – Split RF Systems



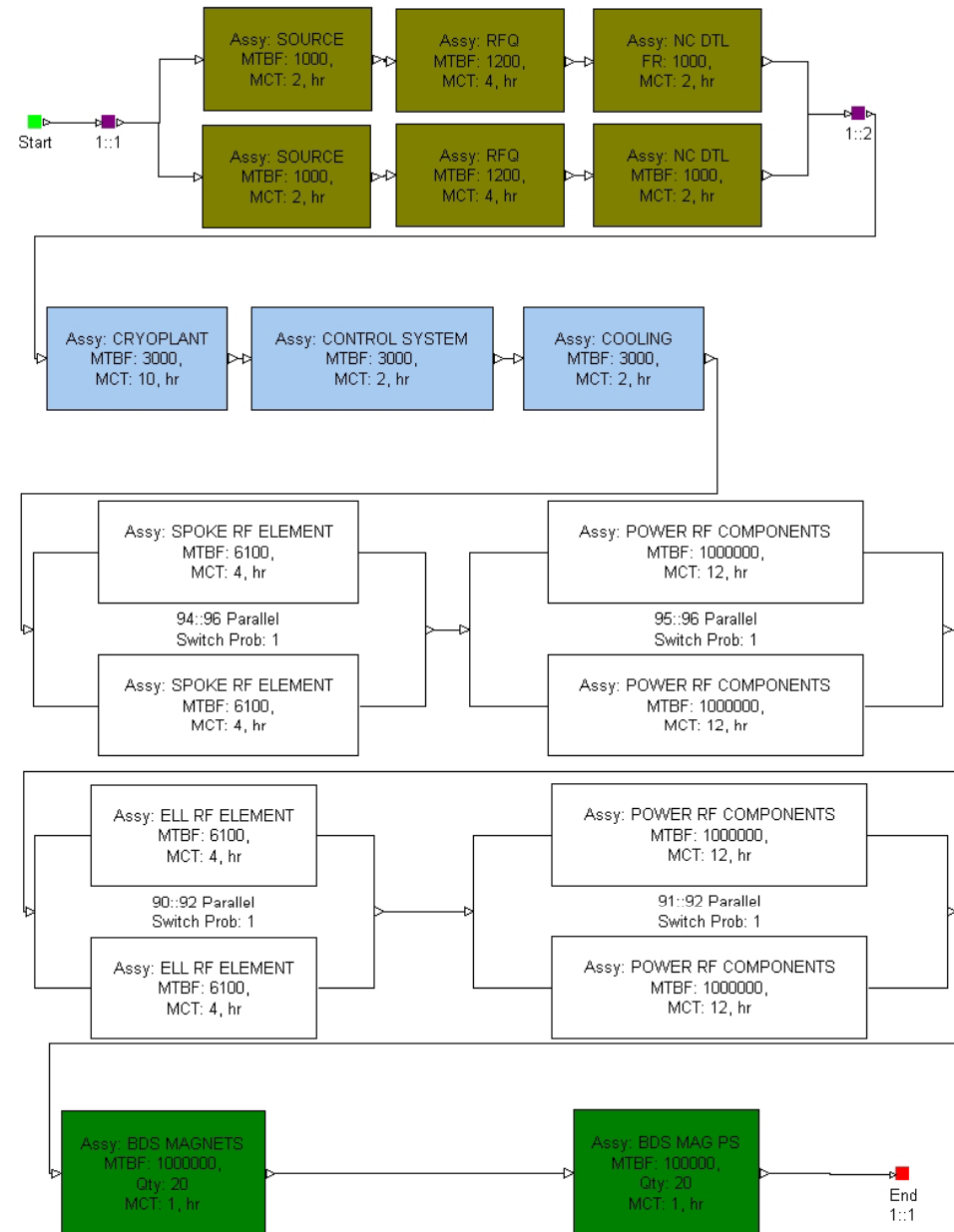
- Keep 2 sources
- Split RF Units
 - Out of tunnel
 - Immediate repair
 - Any 2 can fail/section
 - In tunnel
 - 1 redundant/section
 - Repair @ system failure

System MTBF	550 hours
Number of failures	3.8
Steady State Availability	97.9 %

- Increasing only MTBFx2 of support systems

System MTBF	720 hours
Number of failures	2.80
Steady State Availability	99.1 %

CERN, 1-5 October 2007



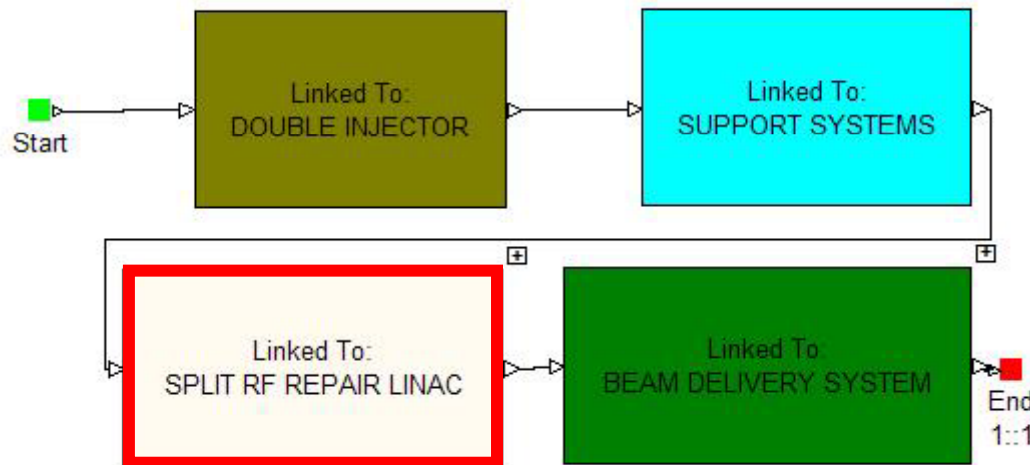
System MTBF “evolution”



# Inj.	Fault Tolerance degree	RF unit repair	System MTBF
1	None, all in series	At system stop	31
2	Infinite	Immediate	797
2	94/96 in spoke, 90/92 in ell are needed	Immediate	758
2	94/96 in spoke, 90/92 in ell are needed, more realistic correction provisions, by splitting the RF system	<ul style="list-style-type: none"> • Immediate for out of tunnel • at system stop for in tunnel 	558
2	94/96 in spoke, 90/92 in ell are needed, split RF SUPPORT SYSTEM MTBF * 2	<ul style="list-style-type: none"> • Immediate for out of tunnel • at system stop for in tunnel 	720
2	94/96 in spoke, 90/92 in ell are needed, split RF IN-TUNNEL MTBF * 10	<ul style="list-style-type: none"> • Immediate for out of tunnel • at system stop for in tunnel 	760

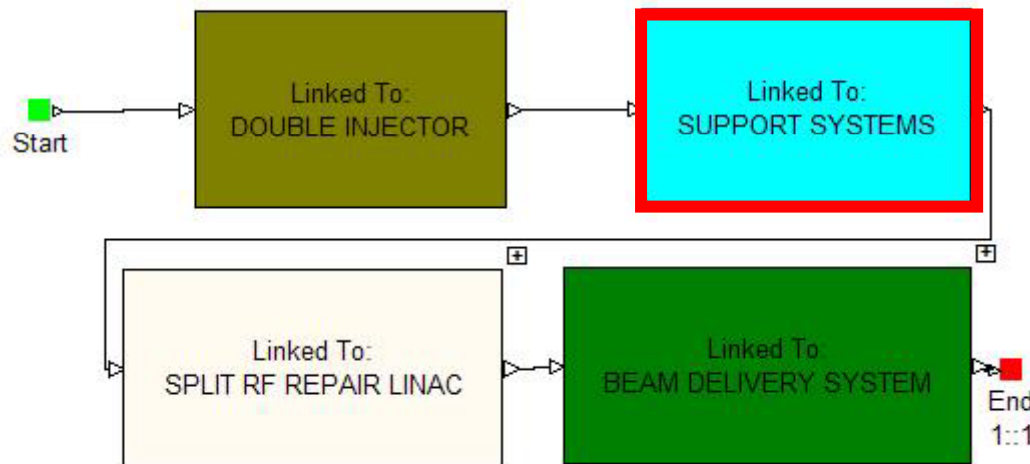
- Type of connection & corrective maintenance provisions change dramatically the resulting system reliability, independently of the component reliability characteristics
- This analysis allows to identify **choices of** components for which we need to guarantee high MTBF, due to their criticality or *impossibility of performing maintenance*
 - in-tunnel components/more robust support systems
- Analysis here is still crude, while similar MTBF values are reported in literature, the MTTR are inserted mainly for demonstration purposes
 - several issues ignored: decay times before repair, logistic issues, long times if cooldown/warmup is needed...

Example: acting on in-tunnel components



- In terms of fault rates in mission (2.9 total)
 - Injector contributes to 3%
 - Support systems amounts to **75%!**
 - Linac is down to 5%
 - BDS is 17%
- Clearly longer MTBF in the conventional support systems is desirable...

Example: acting on support systems



Here MTBF*2 in the support systems

- In terms of fault rates in mission (2.8 total)
 - Injector contributes to 3%
 - Support systems amounts to 35%
 - Linac is 45%
 - BDS is 16%
- More balanced share of fault areas
- MTBF increase only in conventional support facilities

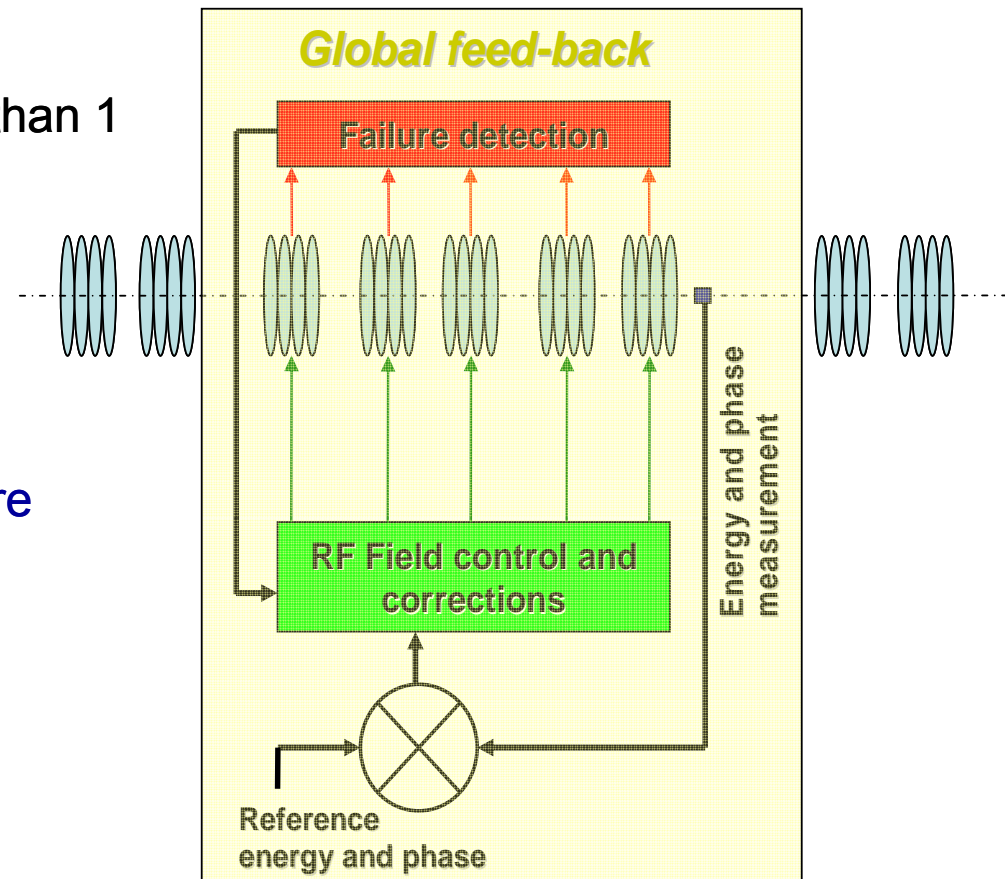
- Still, analysis assumes a high degree of fault tolerance, where the failure of an RF unit is automatically recovered without inducing beam trips on target in timescales ~ 1 s
 - challenging technical issue in LLRF and beam control systems
- Two tasks of the EUROTRANS accelerator program (Tasks 1.3.4 and 1.3.5) are dedicated to reliability analysis and LLRF issues for providing fault tolerance in the high power linac

GOAL

- Recover most of the SCRF cavities (spoke/elliptical) fault conditions
- Without stopping the beam more than 1 second

STRATEGY

- Use the “local compensation method” in the case of a cavity failure
- Adjacent cavities are retuned to provide the missing energy gain to the beam
- Performed using a pre-tabulated set-points database (or fast beam diagnostics ideally)



SCENARIO n°1: STOPPING THE BEAM FOR 1 SEC

DEMONSTRATED ON THE BEAM DYNAMICS POINT OF VIEW

- Proven during PDS-XADS by systematic simulations [Biarrotte et al., HPPA04, EPAC04]

- using the local compensation method with 4 to 8 cavities
- requiring up to ~30% margin on powers and fields
- for all energies from 5 to 600 MeV, but with less good results below 10 / 15 MeV

- Demonstrated on-line at SNS [Galambos et al., ICANS07, HPPA07]

- at high energy (> 200 MeV) & low mean current
- using the “global compensation method”
- recovery procedure duration = a few minutes

- Work still to be done on technical issues:

- fast fault detection, LLRF communication procedures, cold tuner fast management

SCENARIO n°2: WITHOUT STOPPING THE BEAM

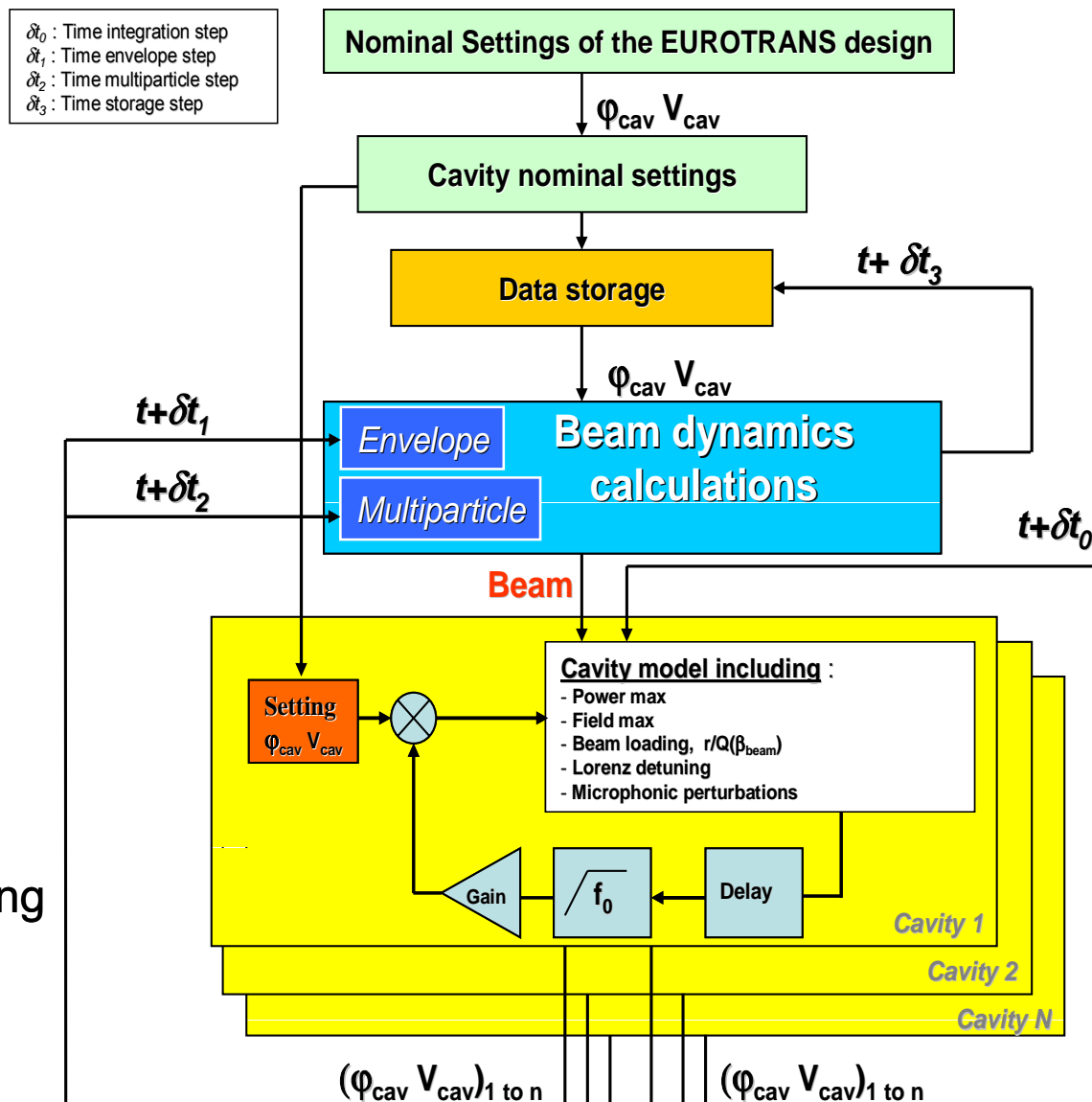
**Fast
enough to
avoid
significant
beam loss**

- fast fault detection;
- fast access to a predefined set-point general database;
- fast update and tracking of the new field and phase set-points, based on the foreseen failed cavity transient behaviour (pre-calculated tables), to recover quickly the nominal beam transmission and energy;
- slow update and tracking of new field and phase set-points with the same method while detuning the failed cavity to avoid beam loading effects

TO BE DEMONSTRATED ON THE BEAM DYNAMICS POINT OF VIEW

• IMPLEMENTATION IN THE TRACEWIN / PARTRAN CEA CODE

- Implementation of cavity model with RF control loop in the whole linac
- Crosscheck with Simulink simulations
- Implementation of the option “transient calculation”: Enveloppes/MP are simulated every Δt
- Can be very consuming depending on the choice of the time steps



Failure of a cavity

Beam envelopes at different t

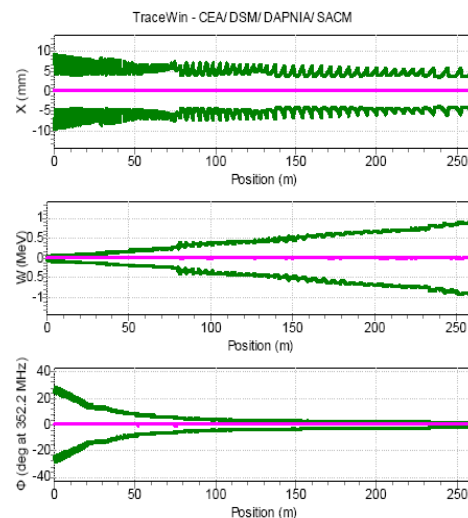


Figure 8 : Envelopes at 0 μ s, reference linac

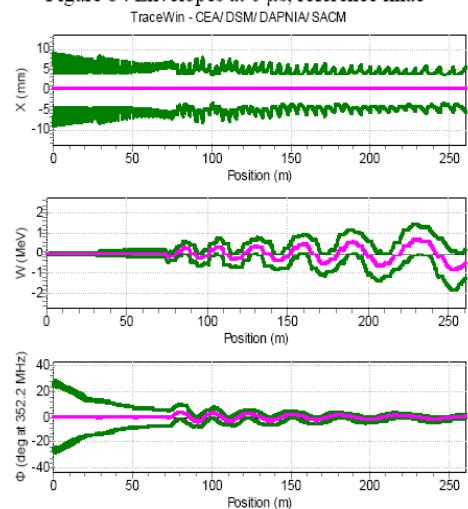


Figure 10 : Envelopes at 50 μ s

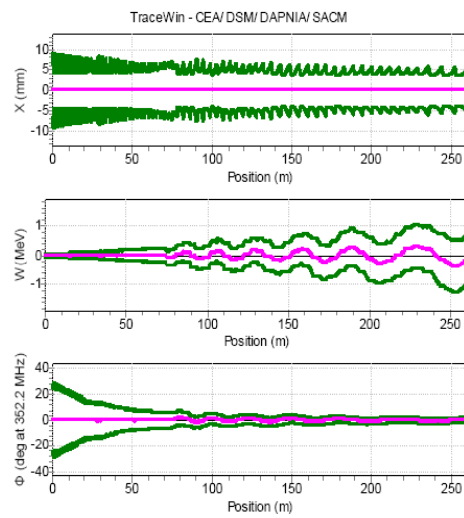


Figure 9 : Envelopes at 20 μ s

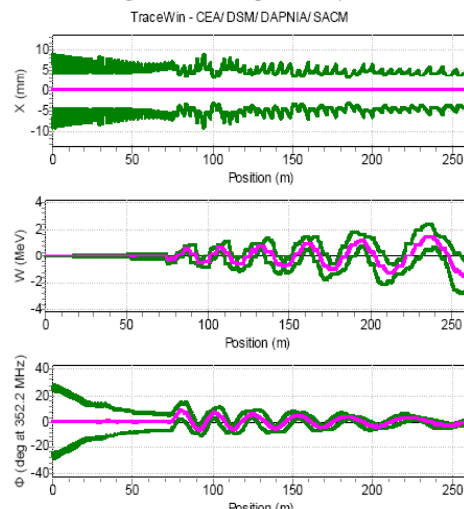


Figure 11 : Envelopes at 100 μ s

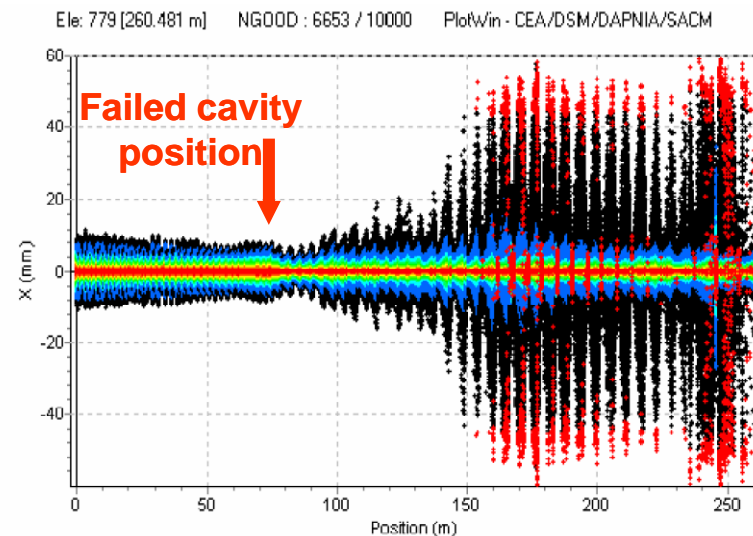


Figure 12 : Transverse beam distribution at 220 μ s, in red are plotted the losses

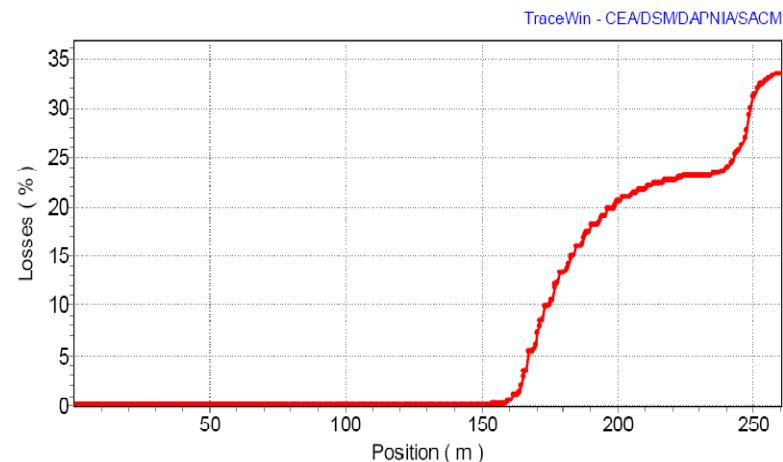


Figure 13 : Losses along the linac at 220 μ s.

EXAMPLE : @ $t=0$, the last spoke cavity fails

- $t_1 = 75 \mu\text{s}$ (detection time), $t_2 = 75 \mu\text{s}$ (correction step)
- Good emittance behaviour, no beam losses during the procedure

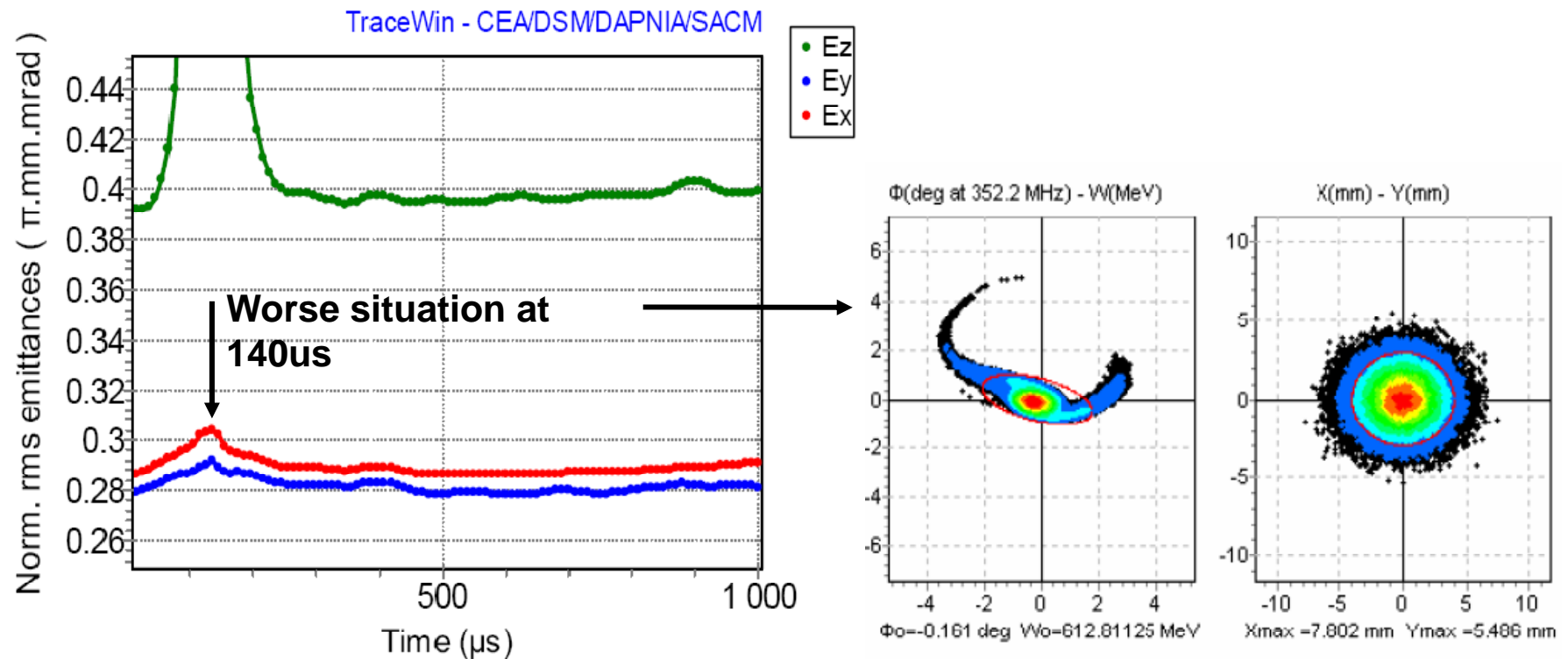


Figure 20 : Emittance evolution during the first ms

- Even in the absence of a validated reliability database for accelerator components the standard reliability analysis procedures indicate where design effort should be concentrated:
 - **providing large degree of fault tolerance whenever possible**
 - Meaning: fault detection, isolation and correction procedures
 - providing additional design effort aimed at **longer MTBF only in critical components**
- Study here is an illustration of how, with minimal “tweaking” of the component MTBF, a simple model for an accelerator system can be altered (adding redundancy and fault tolerance capabilities) in order to meet the ADS goals