



Laser for Califes

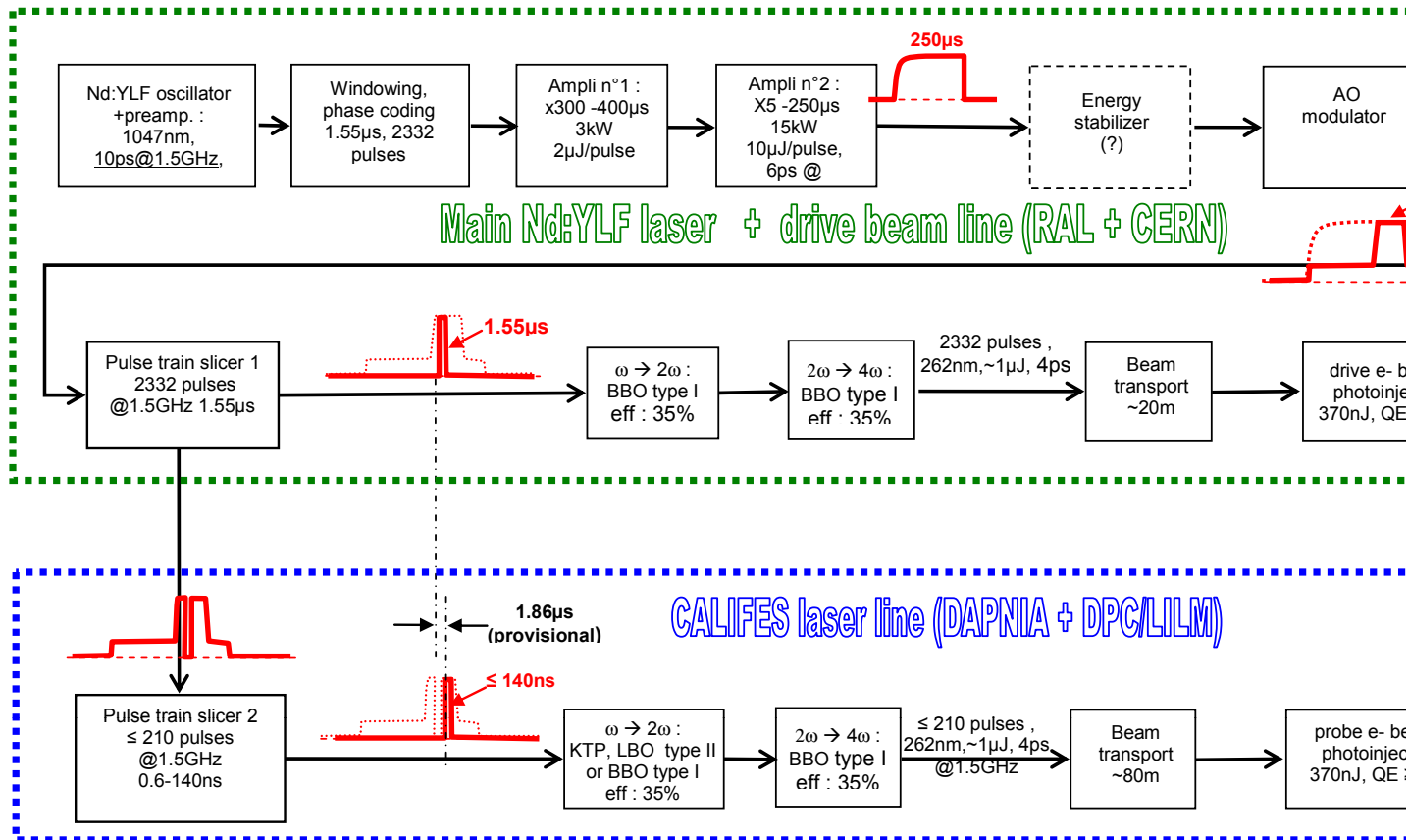
M Gilbert - P.Y Thro - G.Cheymol

Laboratoire Interaction Laser Matière/SCP/DPC/DEN/DANS/CEA Saclay

F Gobin - P Girardot and all

SIS/DAPNIA/DSM/CEA Saclay

Global Scheme



Pulse picker: scheme

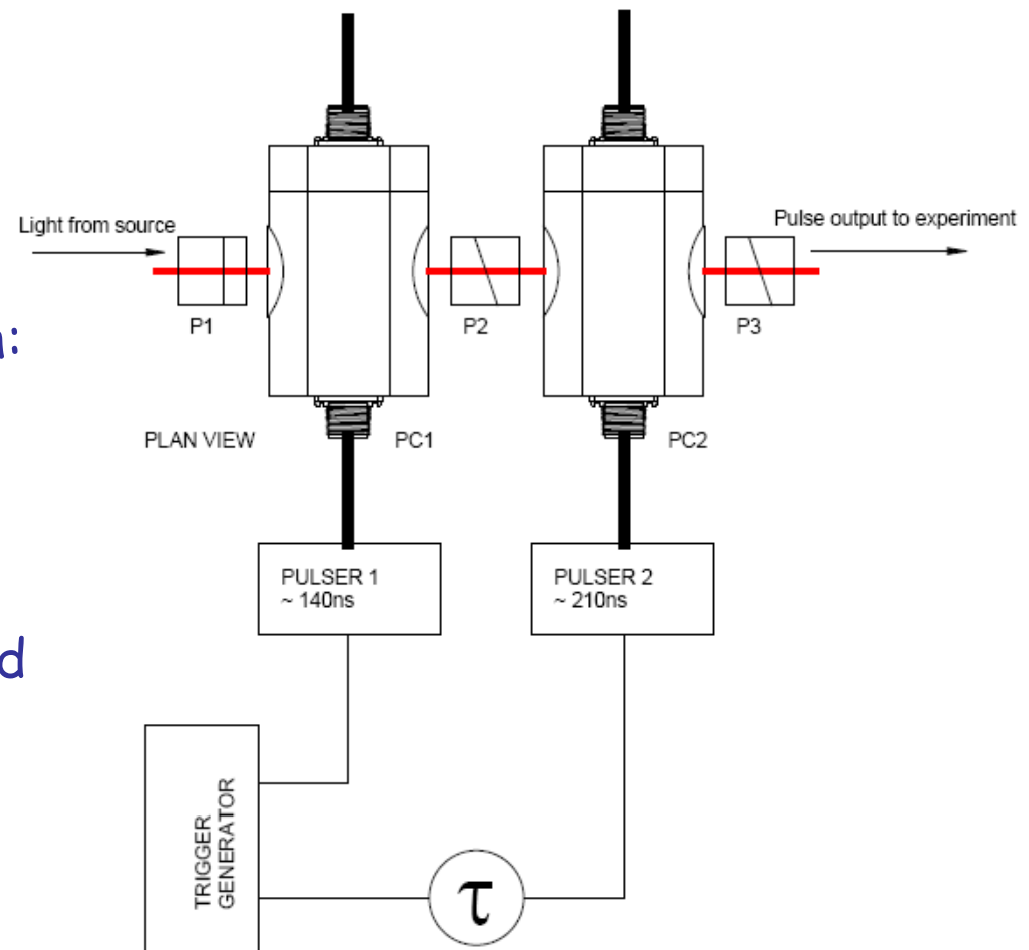


The pulse picker is made with:

- 2 pockels cells
- 3 polarisers

Each pockels cell is triggered by a HV pulser

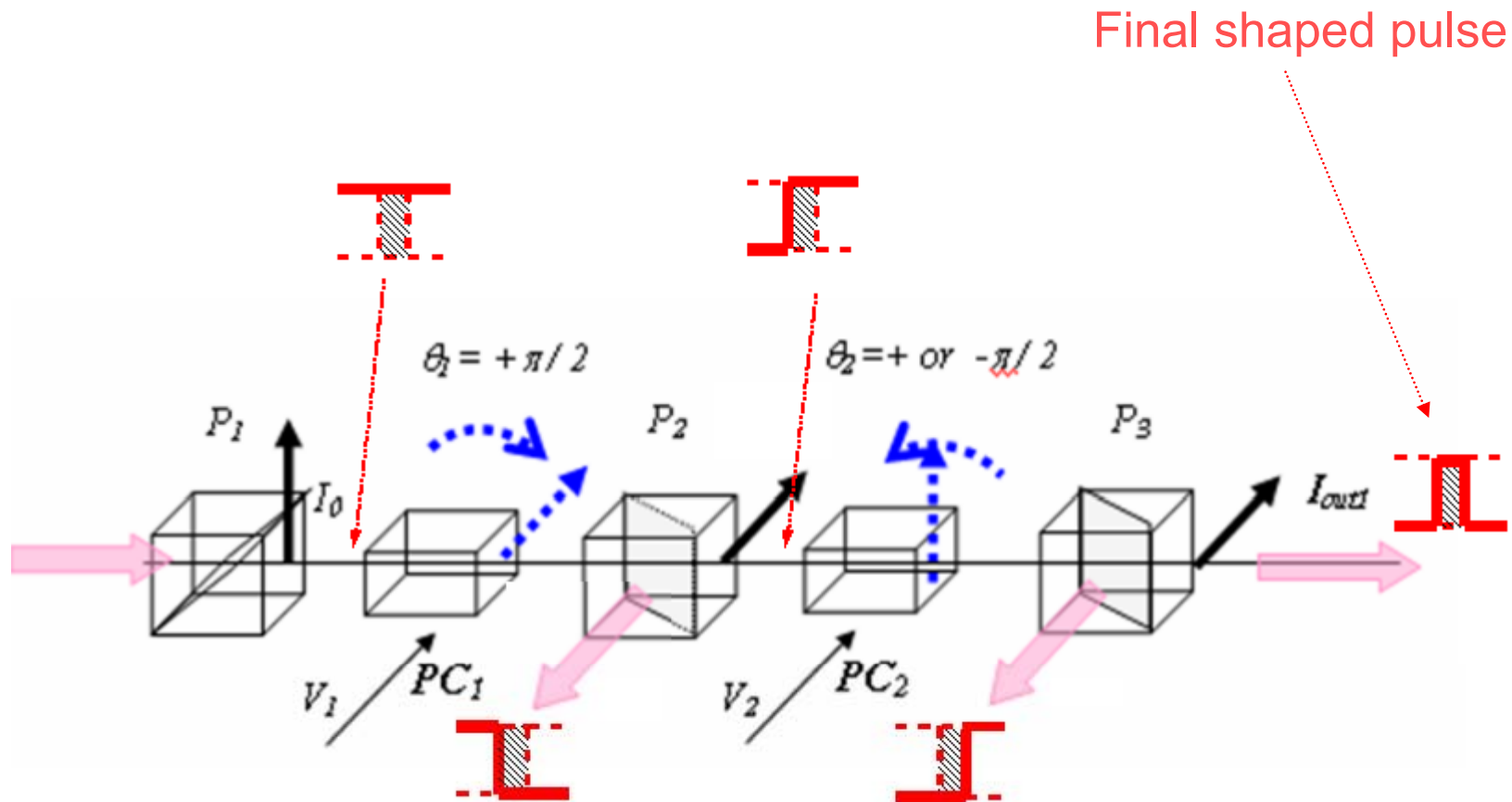
Both HV pulsers are triggered by a generator



Pulse picker: how it works?



In red: the different temporal shapes of the pulse

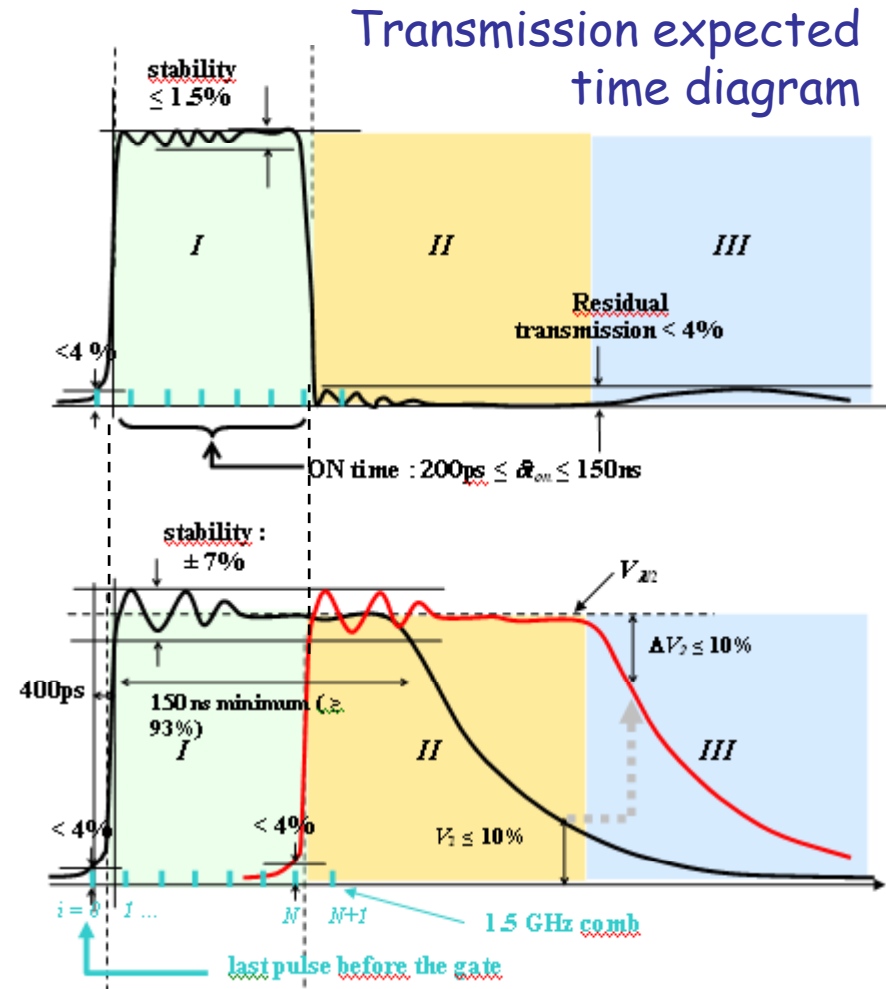


Pulse picker ordered to Leysop Ldt : specifications



Mains specifications for the pulse picker:

- sharp rise time and fall time: less than 666ps \rightarrow \sim 400 ps
- duration \sim 0.5 ns to 140 ns
- with stability better than \pm 1.5%
- low transmission ($<$ 4%) out of the pulse selected
- need for high transmission during the pulse



Related specifications HV pulse

Pulse picker: Test Report on HV pulsers - Temporal response

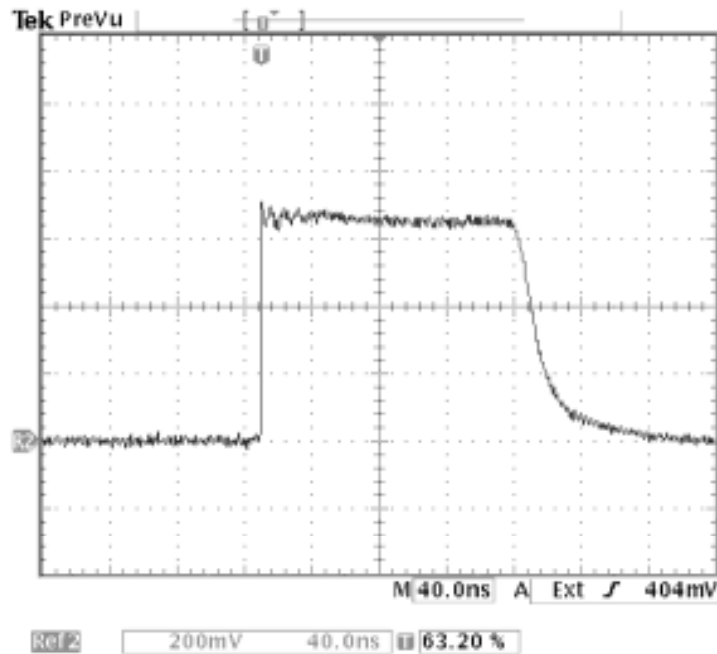


Figure 1: 140ns Long Pulse

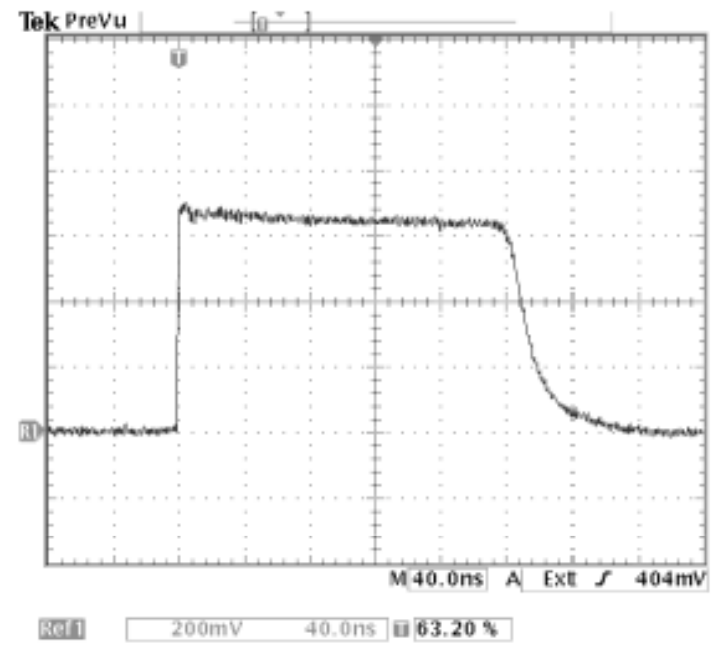
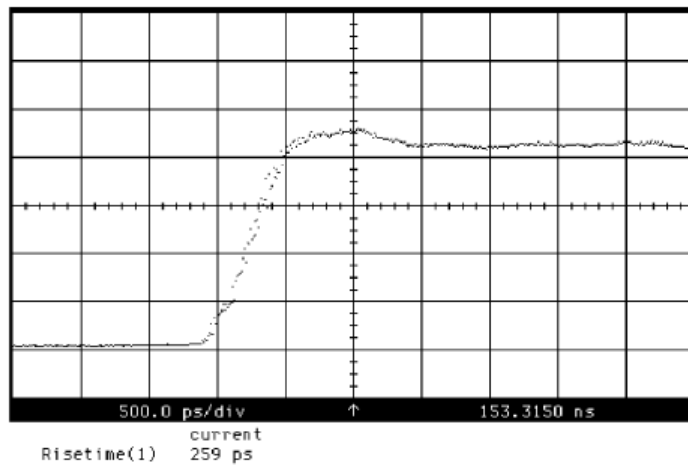


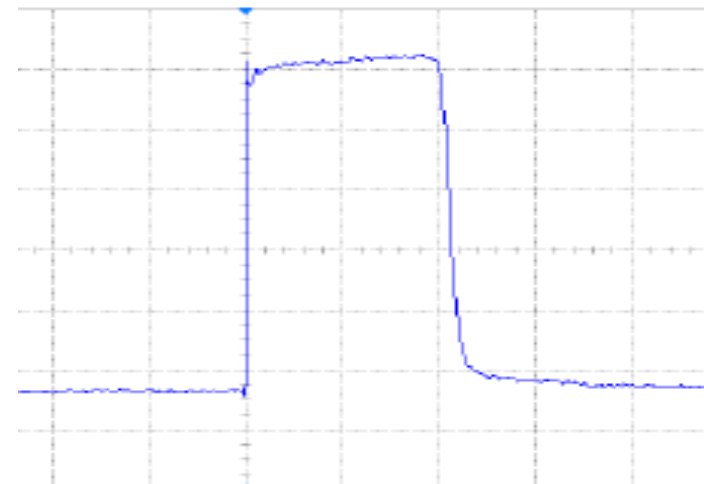
Figure 2: 210ns Long Pulse

The HV pulsers are in good agreement with specifications

Pulse picker: Test Report-Temporal rise time

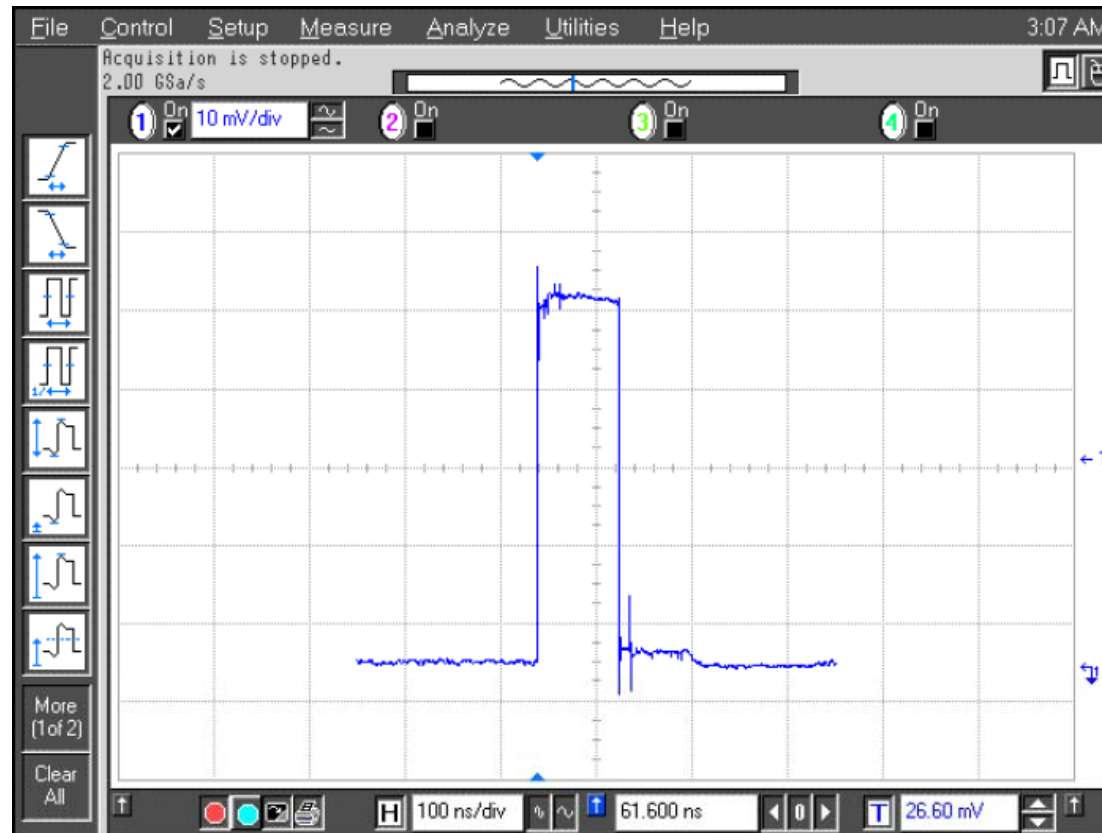


Out of the pulser:
measured rise time
~260ps



Out of one pockel cell:
measured rise time:
less than ~ 350ps

Pulse picker: Test Report- Chopped pulse



100ns Duration Chopped Pulse

Pulse picker: chose dry cell /fluid



Dry cell was finally preferred:

- less transmission (around 1% less per cell)
- theoretically less impedance adaptation, but tests in Leysop showed good performing of dry cell
- but no degradation of the fluid with peak power, (especially for a long running time).

Pulse picker: total transmission



Transmission:

- Transmission of Pockels cell was measured around 92% per cell, less than expected.
 - Transmission of plate polariser: $T_p > 95\%$ (exact value to be confirmed)
- Total transmission for the pulse picker: ~ 75%

Frequency conversion - crystals considered

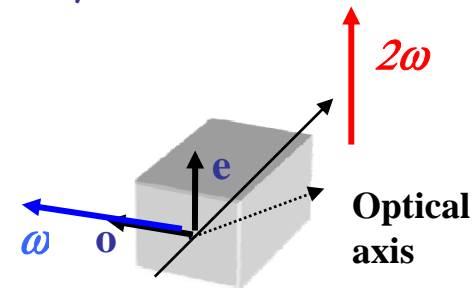


With only one direction of polarisation (since the 3 GHz option has been given up), we can now choose either a Type 1 or Type 2 crystal for doubling:

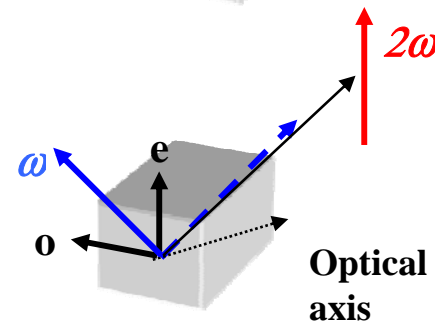
$$\begin{aligned}\omega &\rightarrow 2\omega \\ 2\omega &\rightarrow 4\omega\end{aligned}$$

type II: KTP, LBO ; type I: BBO, LBO
type I: BBO, CLBO, KDP

TYPE I :



TYPE II :



Frequency conversion - 1047→523 - calculations



Nominal parameters for optimisation:

- entering beam parameters: 10μJ, 6ps, 1047 nm, M^2 (beam quality factor) = 1
- CE (conversion efficiency) = 35% (\rightarrow 12% for $\omega \rightarrow 4\omega$)



	KTP (II)	LBO (I)	BBO (I)
λ_ω incident (nm)	1047	1047	1047
d_{eff} : non linearity coeff (pm.V)	3.0	0.83	2
L : length of crystal (cm)	0.6	1.5	0.8
Φ_{1/e^2} : diameter (mm)	1.8	1.5	1.8
Tolerance: <i>Critical if tolerance parameter approach 1.</i>			
Angular acceptance: $\xi_\theta = 2\theta / \Delta\theta_{acc}$	0.028	0.106	0.36
Walk-off : $\xi_\alpha = 2\alpha_{max} \cdot L / \Phi$	0.038	0.17	0.5
GVM: $\xi_{GVM} = GVM \cdot L / Dt_{1/2}$	0.44	0.267	0.79

Frequency conversion - 523→262 - calculations



Typical parameters and tolerances

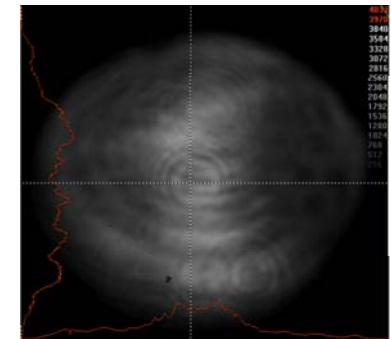
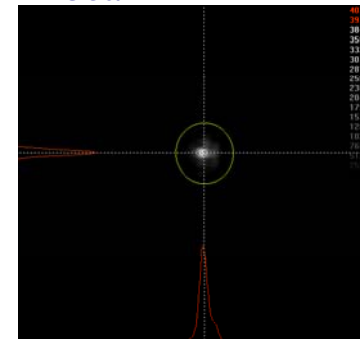
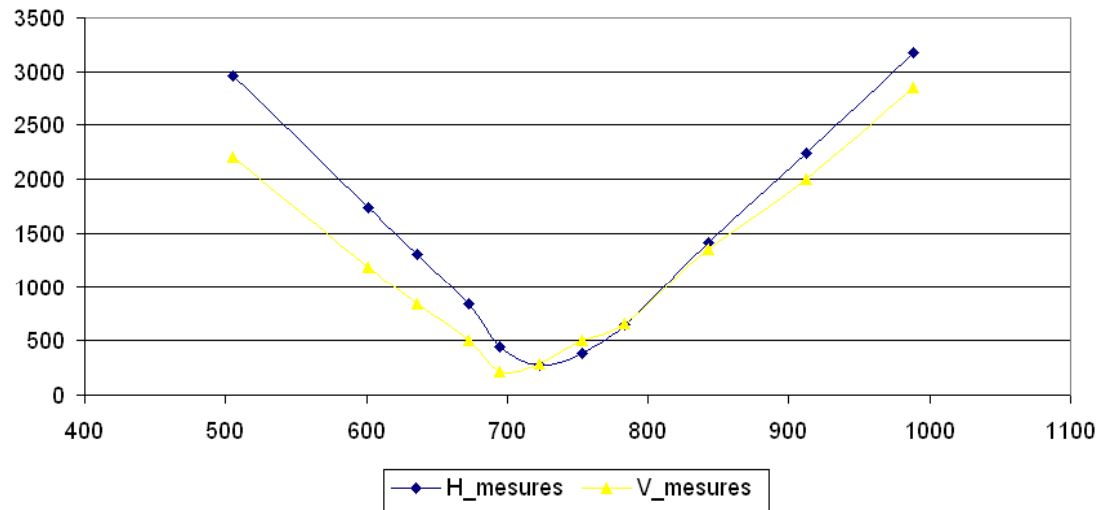
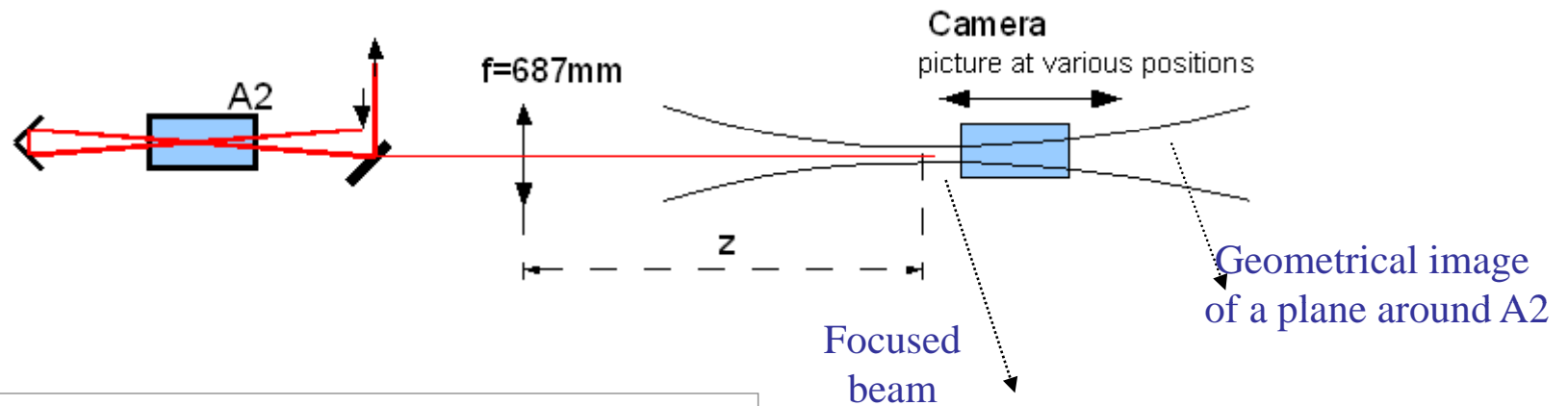
calculations for entering beam parameters: 10μJ, 6ps, 1047 nm, M² (beam quality factor) =1

and for CE (conversion efficiency) =35% (→ 12% for ω → 4ω)



	BBO (I)	CLBO (I)	KDP
λ_{ω} incident (nm)	523	523	523
d_{eff} : non linearity coeff (pm.V)	1.74	0.8	0.47
L : length of crystal (cm)	0.8	1.5	2
Φ_{1/e^2} : diameter (mm)	2.04	2.1	0.94
Tolerance: <i>Critical if tolerance parameter approach 1</i>			
<i>Angular acceptance: $\xi_{\theta} = 2 \theta / \Delta\theta_{acc}$</i>	0.48	0.32	0.2
Walk-off : $\xi_{\alpha} = 2 \cdot \alpha_{max} \cdot L / \Phi$	0.67	0.44	0.285
GVM : $\xi_{GVM} = GVM \cdot L / Dt_{1/2}$	0.97	1.04	1.24

M^2 measured out of A2 amplifier



$M^2 \sim 2$ (1.5 to 2.6)
for the beam out of A2

Frequency conversion - crystal ordered



Crystals ordered:

- KTP (10mm)
- BBO (12mm)

Detailed calculations on the Report:

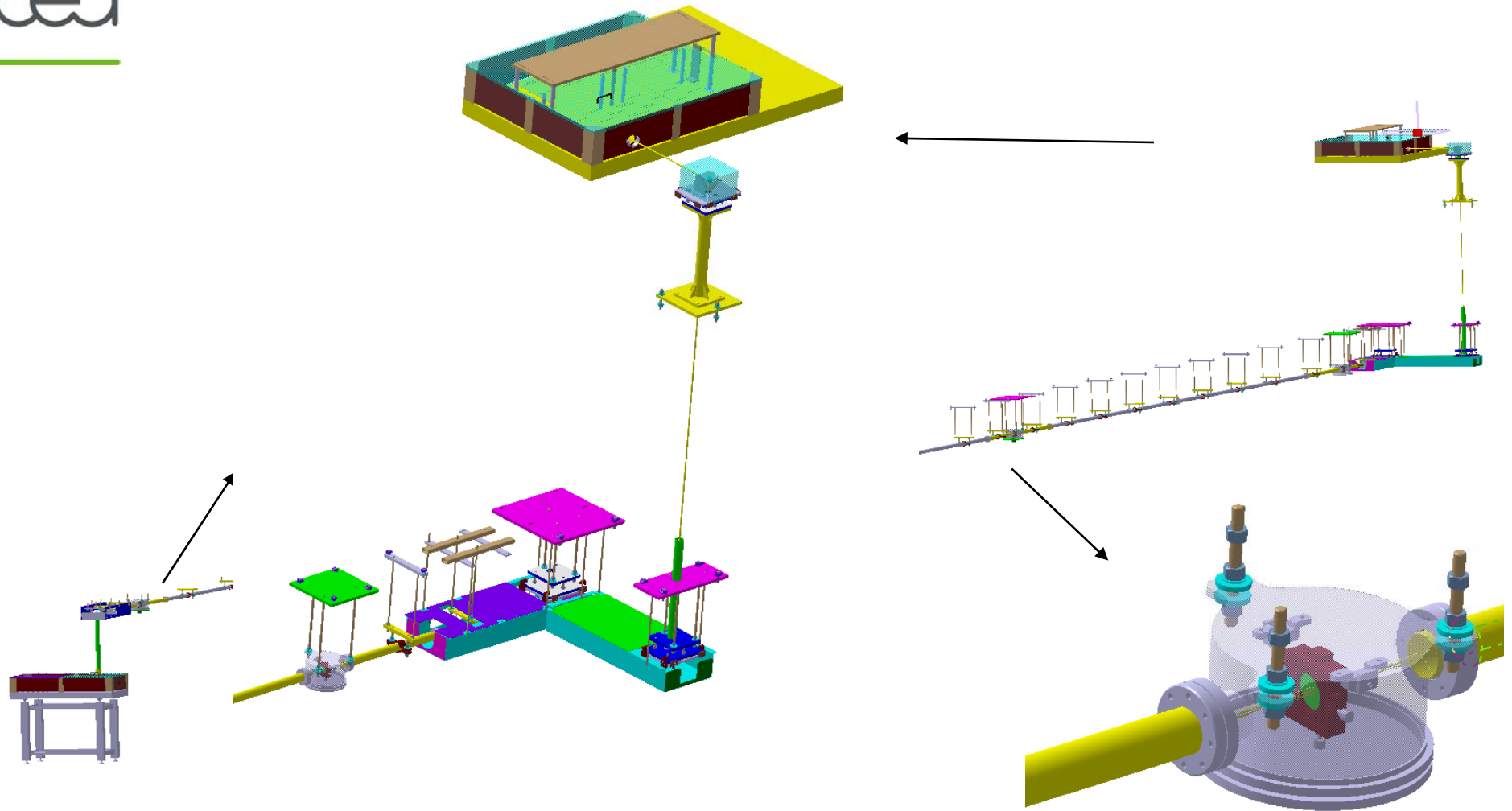
Ligne laser du photoinjecteur CALIFES (CERN).

Sélection d'impulsions (pulse picker)

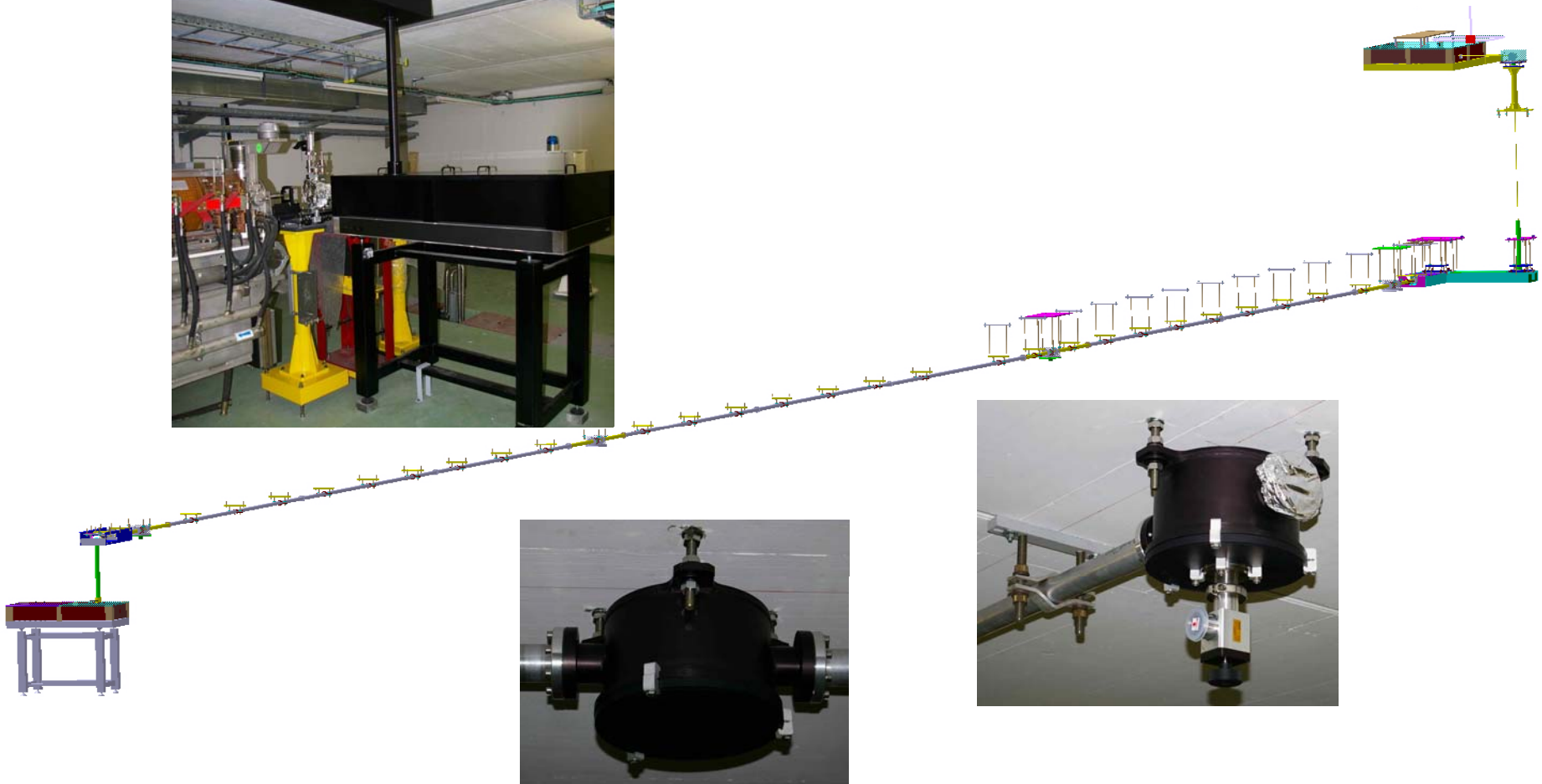
et conversion non-linéaire 1047nm → 262nm.

M.GILBERT, G.CHEYMOL

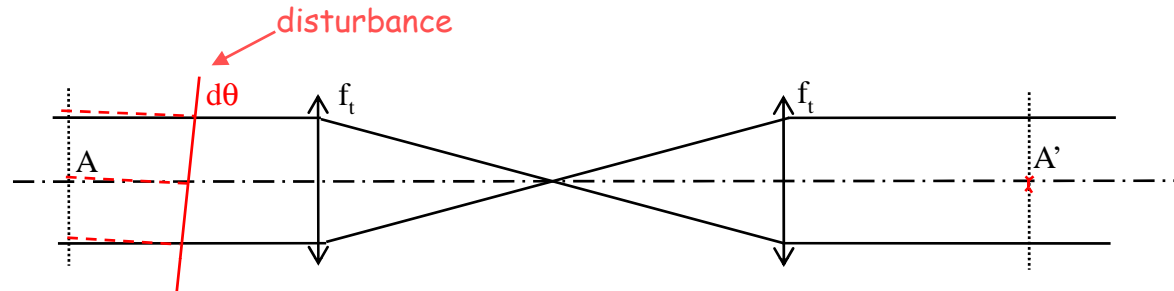
Transport- tables and mechanical supports



Transport- tables and mechanical supports

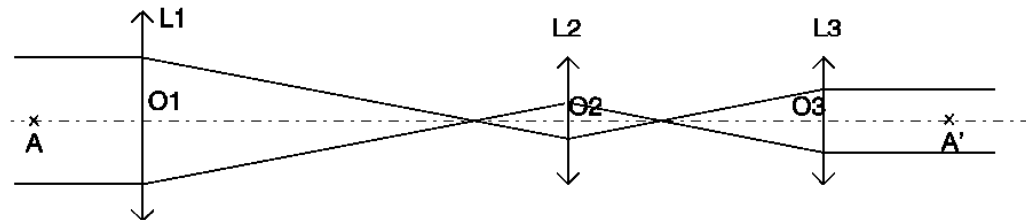


Optical relay /afocal system



Optical relay reduce consequences of mirror vibration, air turbulence in plane A'

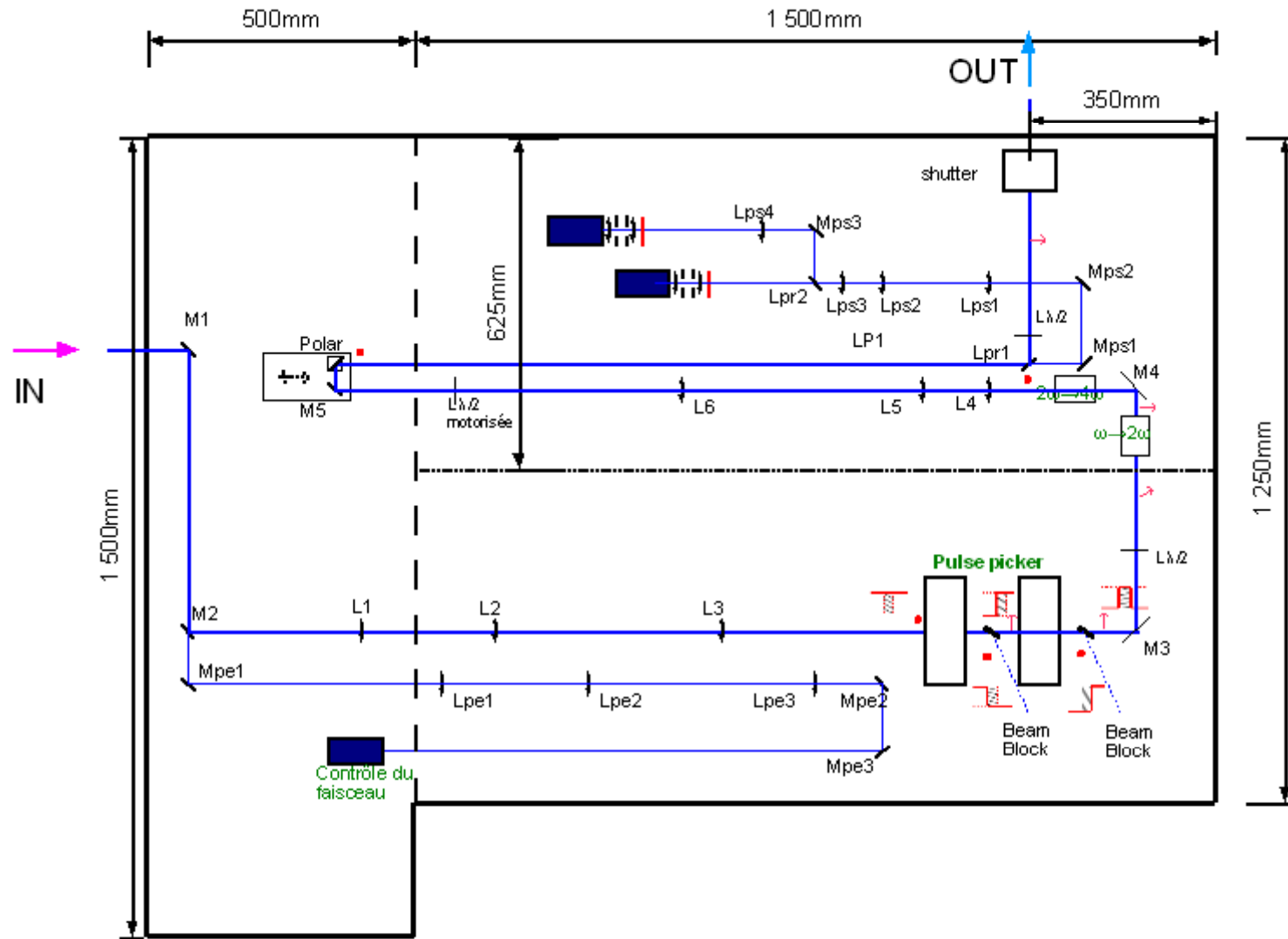
(A' geometrical image of A)



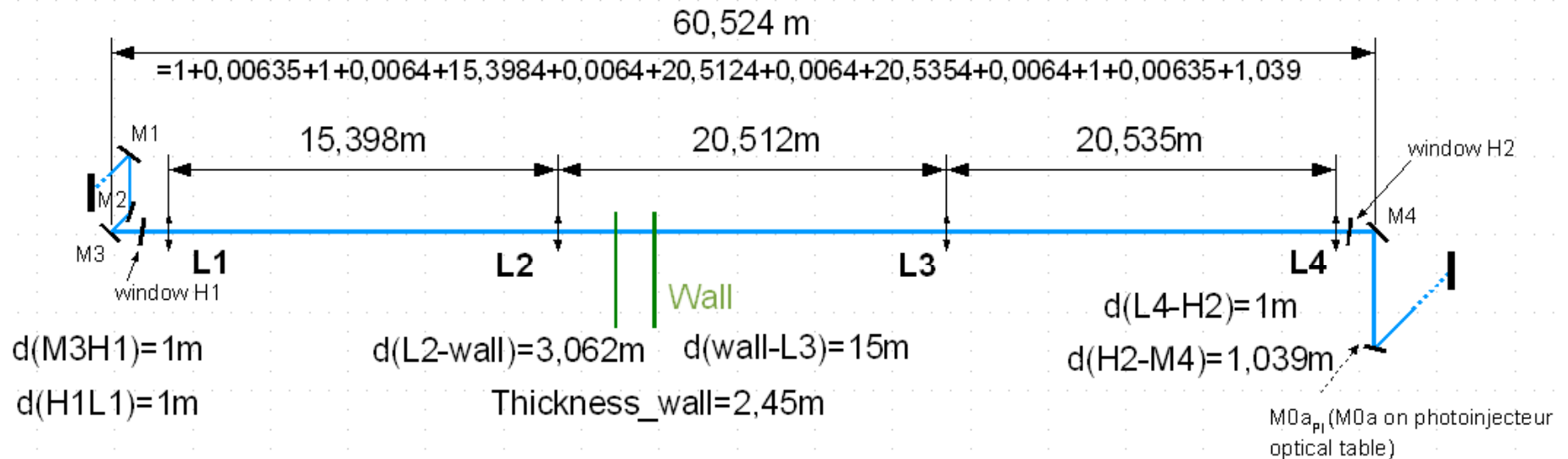
3 lenses afocal system allows to:

- decrease the footprint of the optical system for a given relay distance.
- change zoom factor and relay distance (to some extent)

Optical path on « laser table »



« under the roof » long distance beam delivery



2 afocal optical relay:
 L1-L2 with $f \sim 10$ m
 L3-L4 with $f \sim 7.5$ m

« photoinjector » optical table

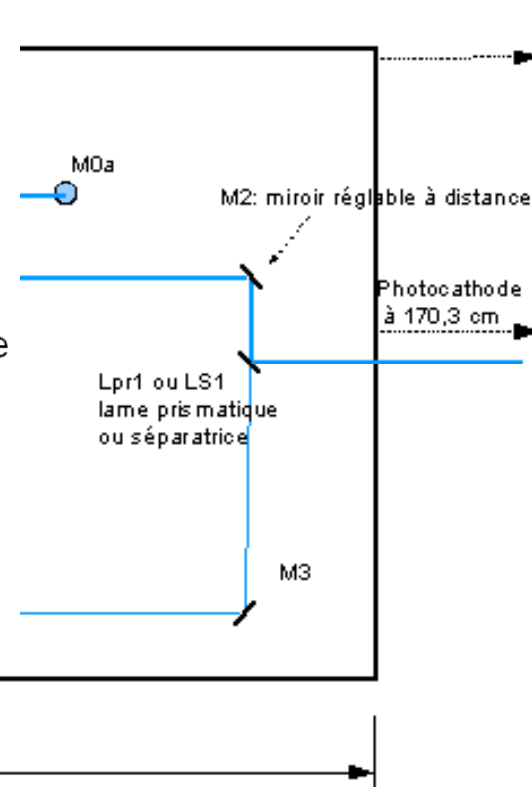


Photodiode
to measured the pulse energy
continuously

Variable optical density

Caméra controlling the
position on photocathode

LP1:
Phosphorous plate
(virtual cathode)



Photoinjector

Around 25 optical components on the whole transport



- Pulse picker quite correct
- Frequency conversion to be tested soon
- Total transmission and energy delivered to the photoinjector to be checked



End