



LHC CRAB CAVITY WITH REDUCED OUTER DIAMETER

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FNAL

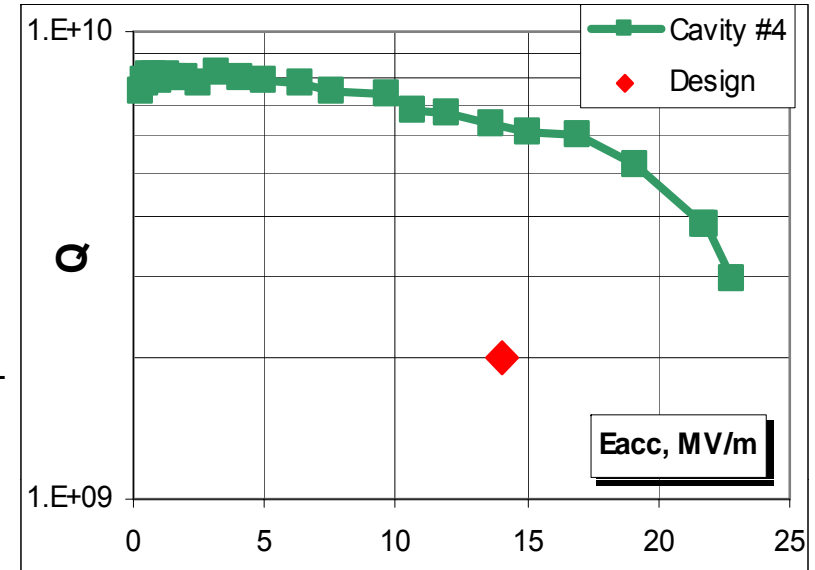
LHC CC08 meeting, BNL, Feb. 25-26, 2008



FNAL SRF infrastructure

FNAL SRF Projects:

- ❑ CKM – 3.9 GHz deflecting cavity
 - 13 cells; 5MV/m (reached ~7.5 MV/m)
- ❑ 3.9 GHz accelerating cavity (3rd harm)
 - 9-cells, 8 cavities built
 - Eacc=25MV/m; E_{pk}=60 MV/m; B_{pk}~120mT
- ❑ 1.3 GHz ILC (TESLA) cavity
- ❑ 1.3 GHz beta=0.81 cavity design
 - built, tested by MSU
- ❑ 325 MHz spoke cavity
 - 2 cavity built, under test
- ❑ Couplers, HOM couplers, tur
- ❑ Cryomodule (CM1, CM-3rd h



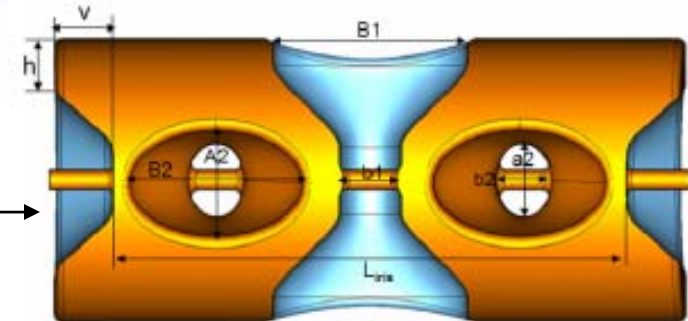
Spoke
325 MHz



3.9GHz deflecting

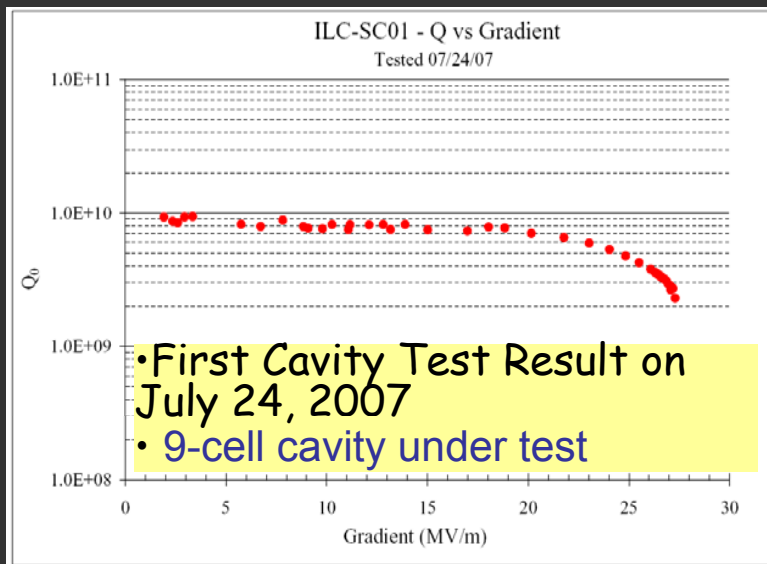


3.9GHz deflecting





Cavity Vertical Test Stand



- VTS-1 Upgrades:
 - Vacuum pumping
 - Variable coupler
 - Two cavity operation
 - T-mapping
- To increase capacity of the VTS
 - Add 2 more VTS pits (~200test/yr)
 - Upgrade cryogenic 125W→300W

Cavity Testing Infrastructure



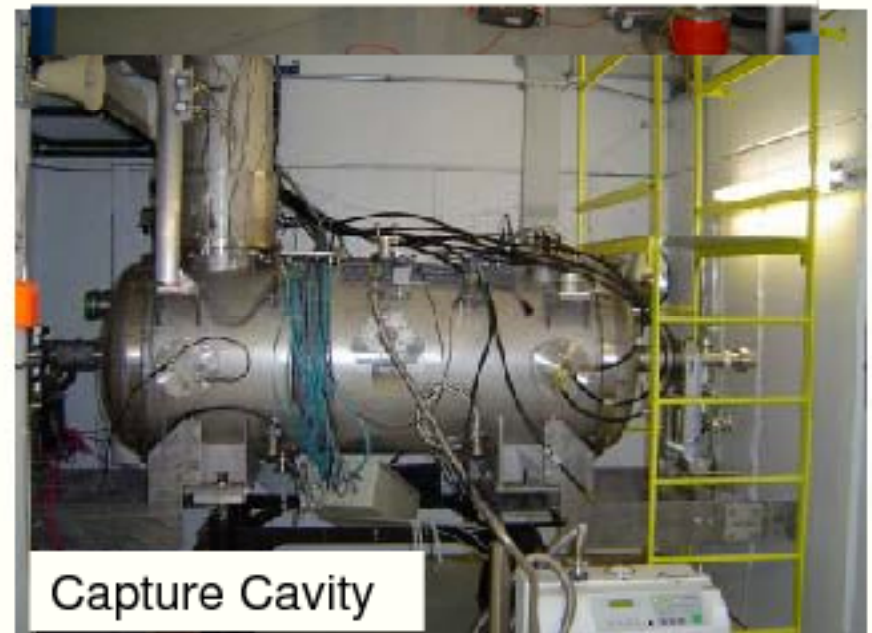
RF Power for HTS



Cryogenics for HTS ready at 2 K



Cryogenics for HTS getting ready for 2 K



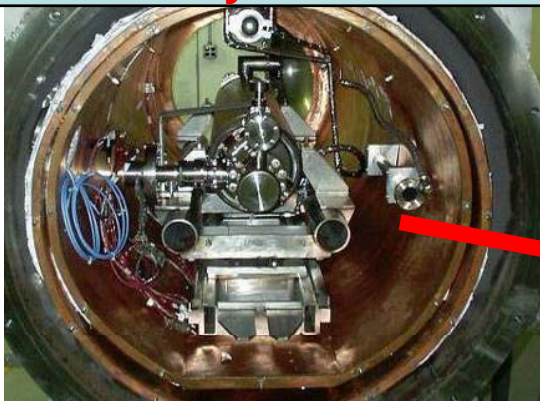
Capture Cavity



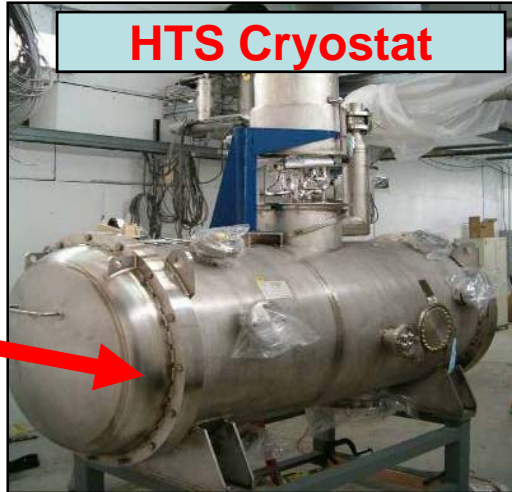
Horizontal Test System

- HTS facility is completed and commissioned
 - First test of the cavity with high pulsed RF power
 - R&D Test bed: tuners (slow), couplers, LLRF, etc
 - 1.3 GHz capture cavity
 - 3.9 GHz accelerating cavity,

1.3 GHz Cavity in HTS Cryostat



HTS Cryostat



RF Power for HTS

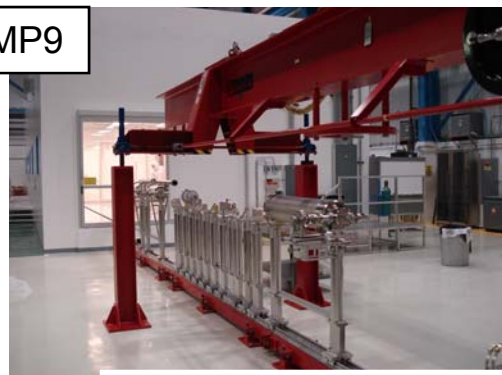




TD-MP9 CRYOMODULE ASSEMBLY FACILITY



CAF-MP9



1.3GHz bare cavity hydrogen degas bake at CAF-IB4



- Cavity string and Cold mass Assembly Areas

- Fully Operational (June 2007)



1.3GHz dressed cavity



3.9GHz Cryomodule Mockup Assembly



Clean room technicians from FNAL & DESY working together during CM1 string assembly



Cleanroom Class 10 area



Cryomodule #1 (CM1) string assembly in the cleanroom



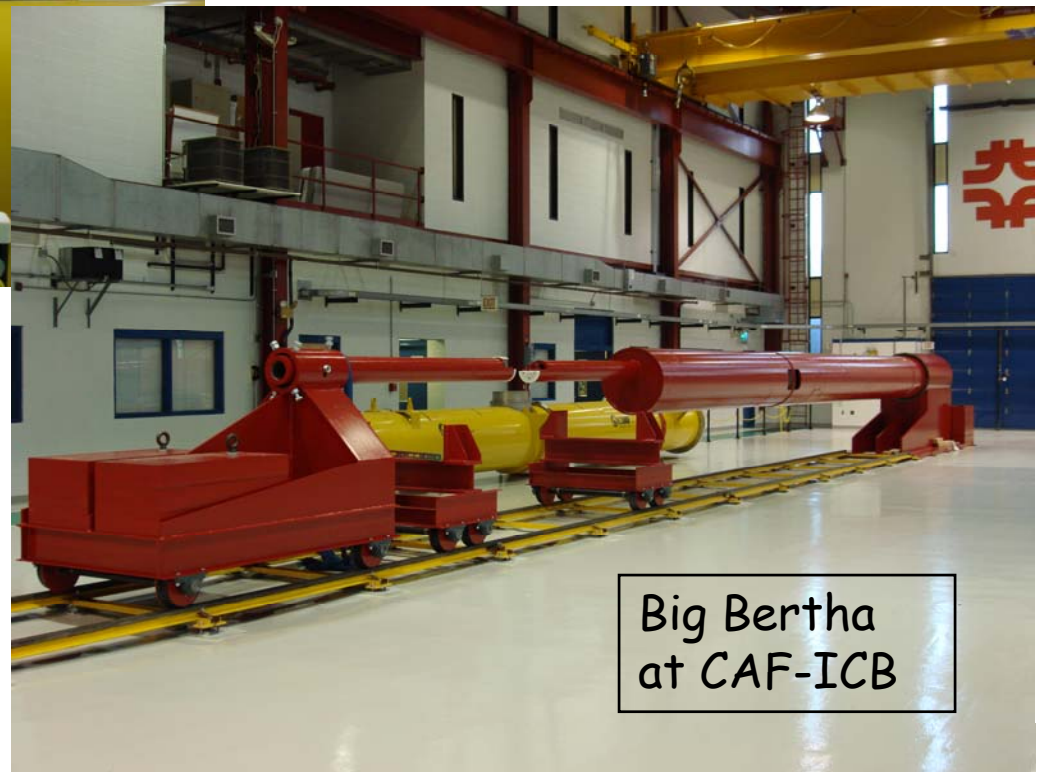


CRYOMODULE ASSEMBLY FACILITY

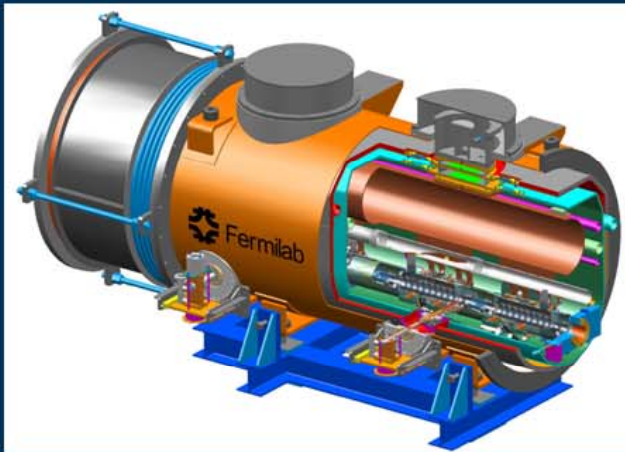


CM1 -Assembly schedule

- String Assembly: mid-Sept.
- Cold Mass Assembly: mid Oct.
- Final Assembly: Nov.
- 3rd Harm Cryomodule: Jan 2008



3rd Harmonic SRF Cryomodule



Cryomodule design completed in May 2007.

1st successful cavity test in Spring 2007!

Fabrication in process at MP9.

2008 delivery to DESY.





LHC Crab Cavity: Design Constrains

- General:
 - Frequency 800 MHz; $Q_L \sim 10^6$ (beam transverse jitter)
 - Dipole HOM: $Q_L \sim 10^2 \div 10^3$ - TCBI (Transv. Coupled Bunch Instability)
 - Monopole modes: $Q_L \sim 10^2$ - Power dissipation in load

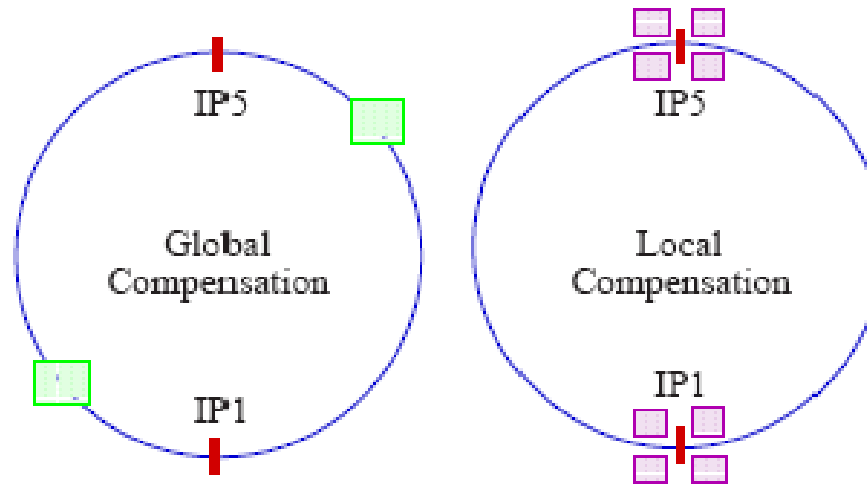


Figure 3: Schematic of global and local crab compensation at two IPs for LHC upgrade.

Global scheme:

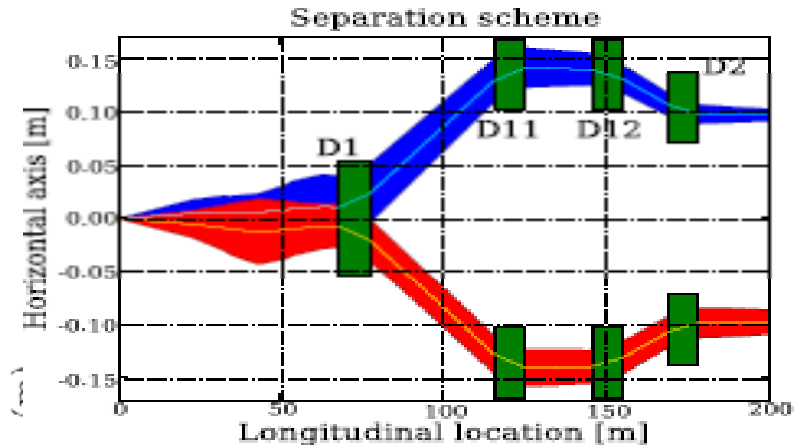
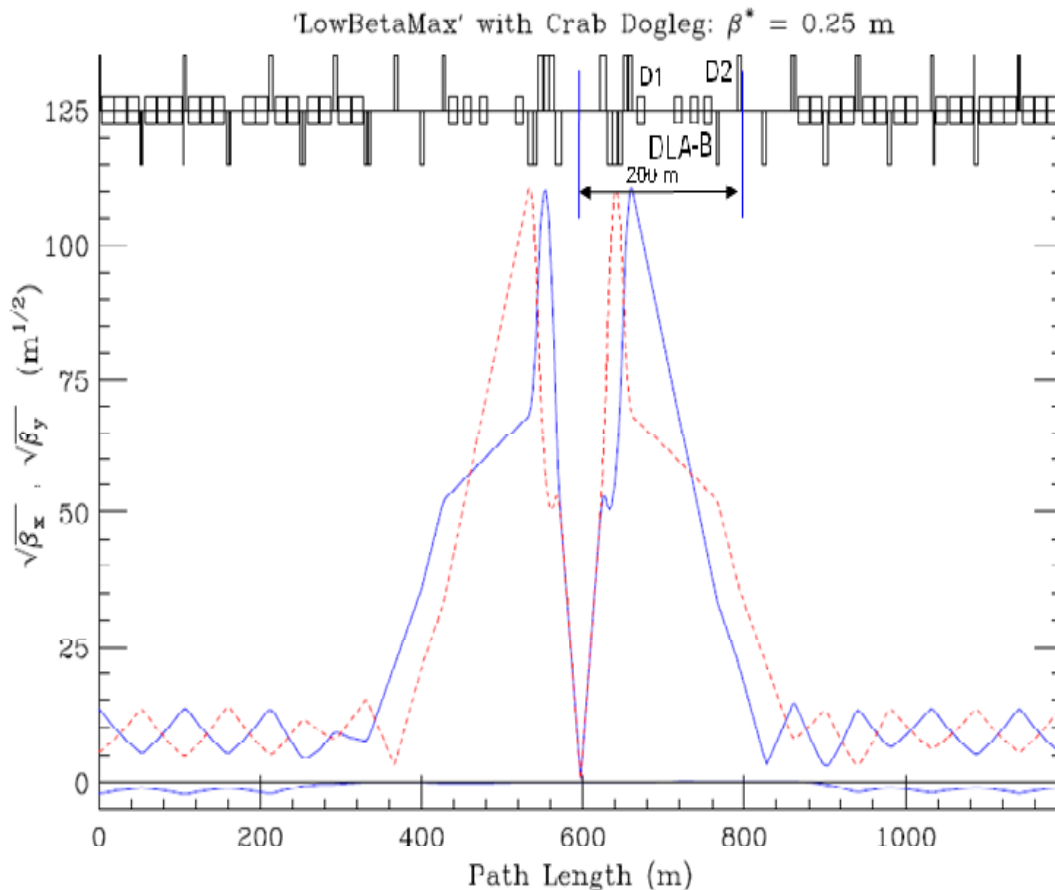
Beam separation ~ 40 cm
Beta function ~ 100 m (?)
Longitudinal space $\sim 5-10$ m

Local scheme
(preferable choice)

Beam separation ~ 30 cm
Beta function $\sim 3-4$ km
Longitudinal space ~ 10 m



Local Scheme for Crab Cavity



Magnet	L (m)	B (T)	Position (m)	Separatic (mm)	β_x (m)	β_y (m)
D1	9.45	8.473	70.447	0	11103	4685
			79.897	32.4	9721	4552
DLA	9.45	8.473	116.229	281.6	5266	4059
			125.679	314.0	4329	3935
MID-DL			130.679	314.0	3870	3870
DLB	9.45	8.473	135.679	314.0	3437	3806
			145.129	281.6	2689	3687
D2	9.45	8.473	153.175	226.4	2125	3586
			162.625	194.0	1547	3470

Optical functions of the 'LowBetaMax' Phase I upgrade option. To create the beam separation for insertion of crab cavities the baseline D1 separation magnet comprising 6 conventional magnet modules must be replaced by a single SC dipole. The remaining 3 separation dipoles in the dogleg are all superconducting.

Beam separation ~ 30 cm at 10 m

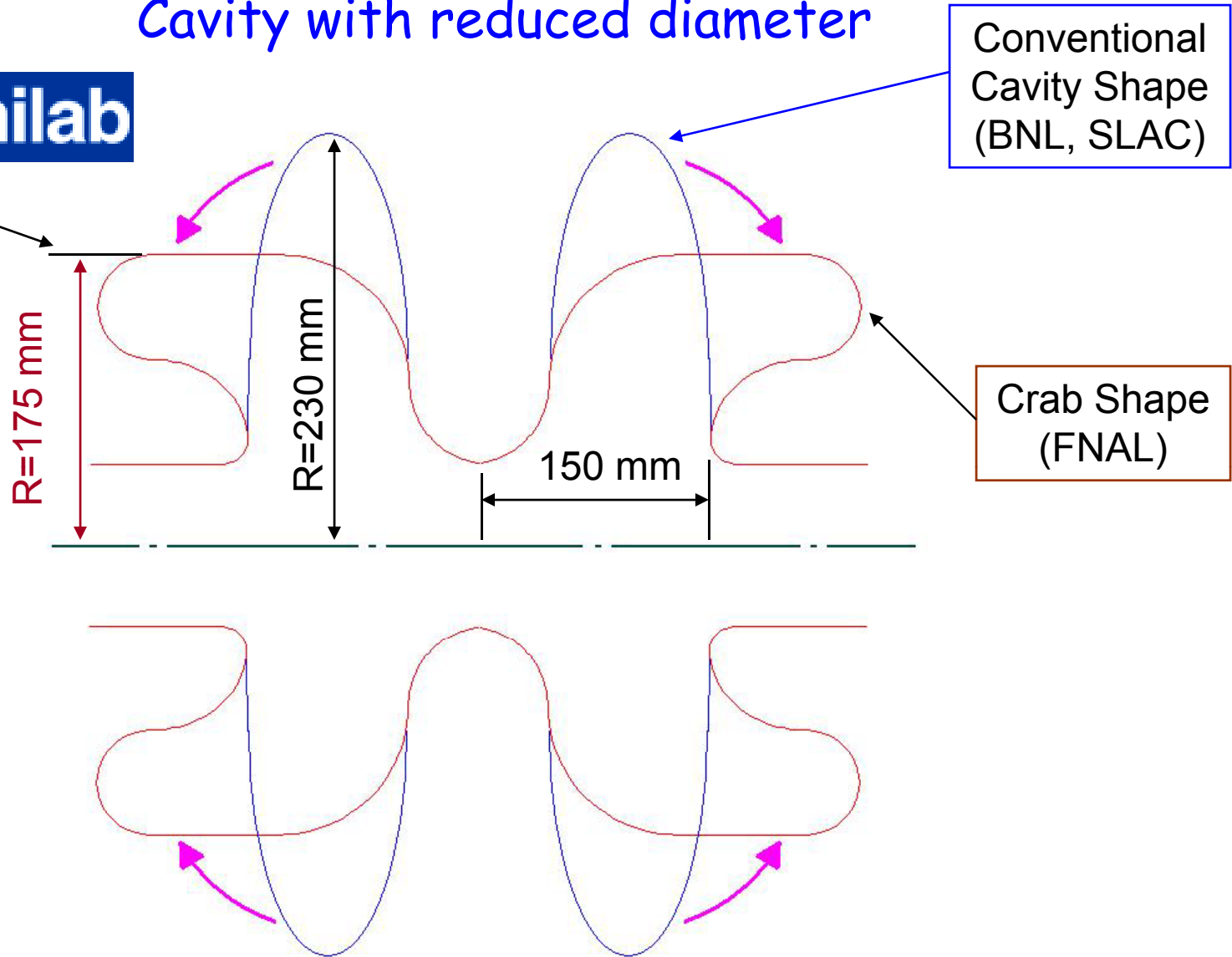
D1 - single aperture. DLA,DLB, and D2 are all double bore.

In straight section $\beta_x = \beta_y$.

(J.Johnstone and P.Limon (FNAL))



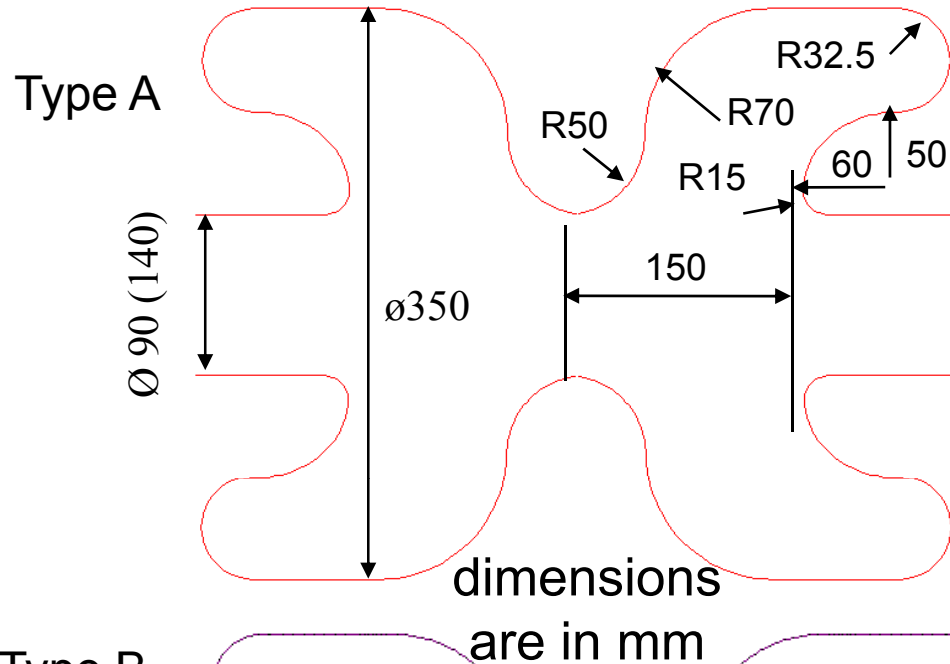
Cavity with reduced diameter



Idea of the LHC Crab cavity with reduced outer diameter to fit 30cm bunch separation. Conventional cavity (blue) vs. the cavity with reduced diameter (red)

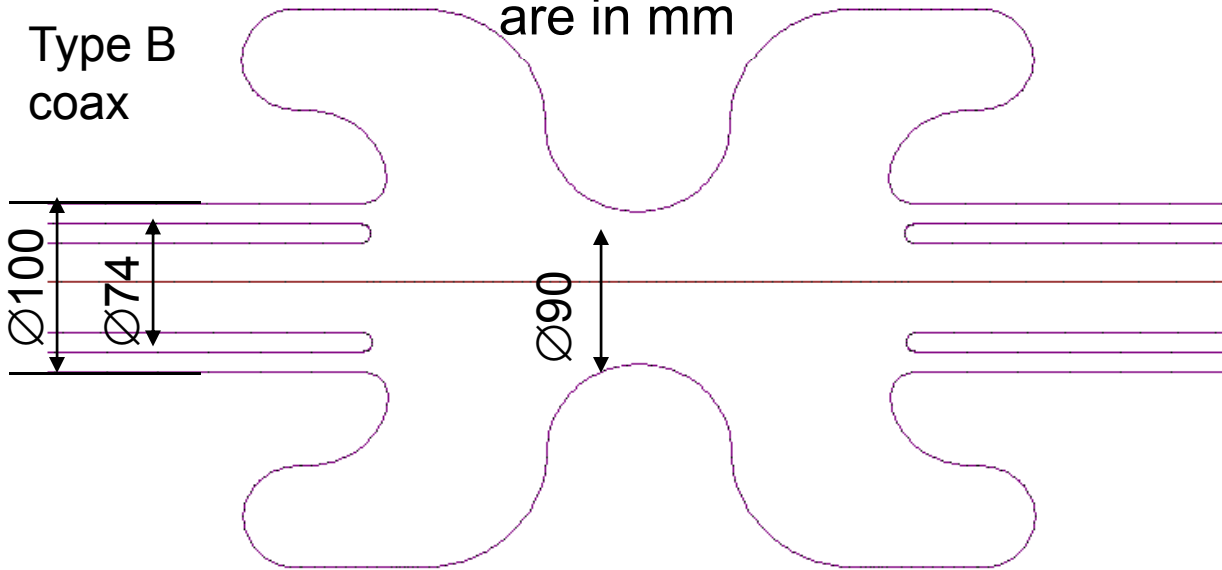


Cavity Shape



ILC-like

- Few monopole and dipole modes are trapped in cavity
- Needs **LOM**, **HOM** and **SOM** couples to damp all these modes



KEKB-like

Coaxial coupler

All monopole modes are propagating in coaxial line

Only working dipole mode (800 MHz) are trapped in cavity.

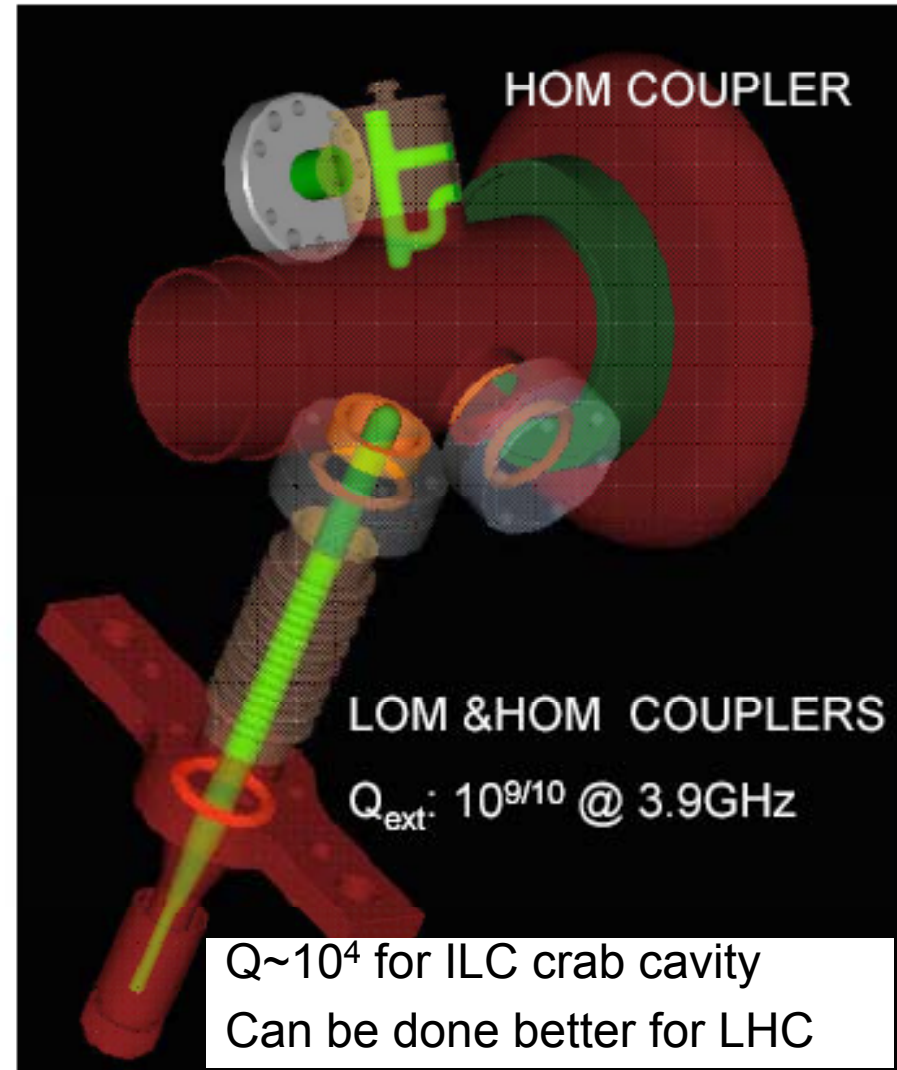
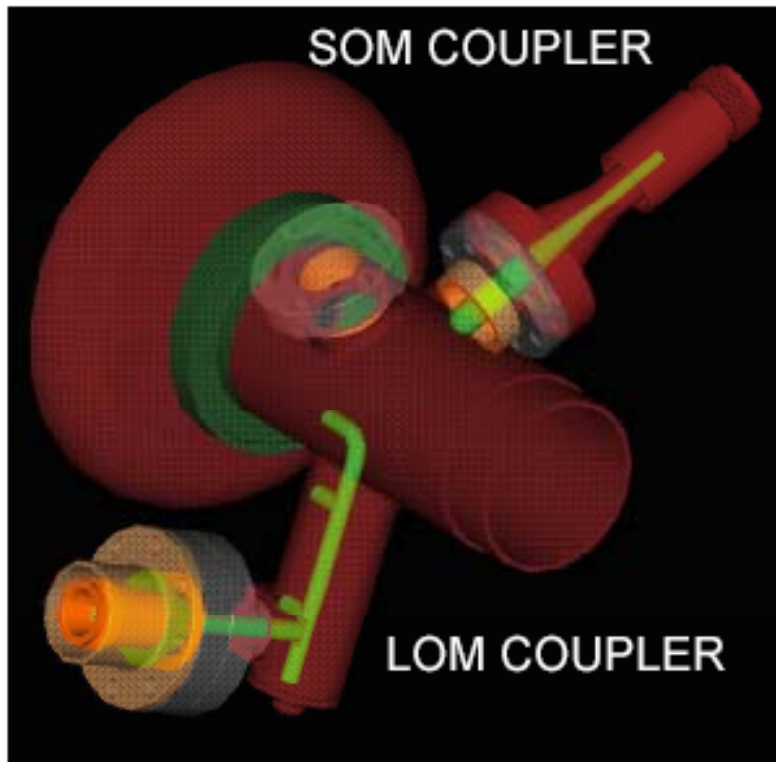
All other dipole modes are well damped. $f_c > 1097\text{MHz}$

LOM, SOM, HOM COUPLERS

HOM coupler a modification of DESY design

SOM coupler will be mechanically adjusted to find the node of the TM_{110} mode

LOM at opposite end of input coupler





Mode damping in KEKB crab cavity

Crab Cavity Conceptual Design

Squashed cell

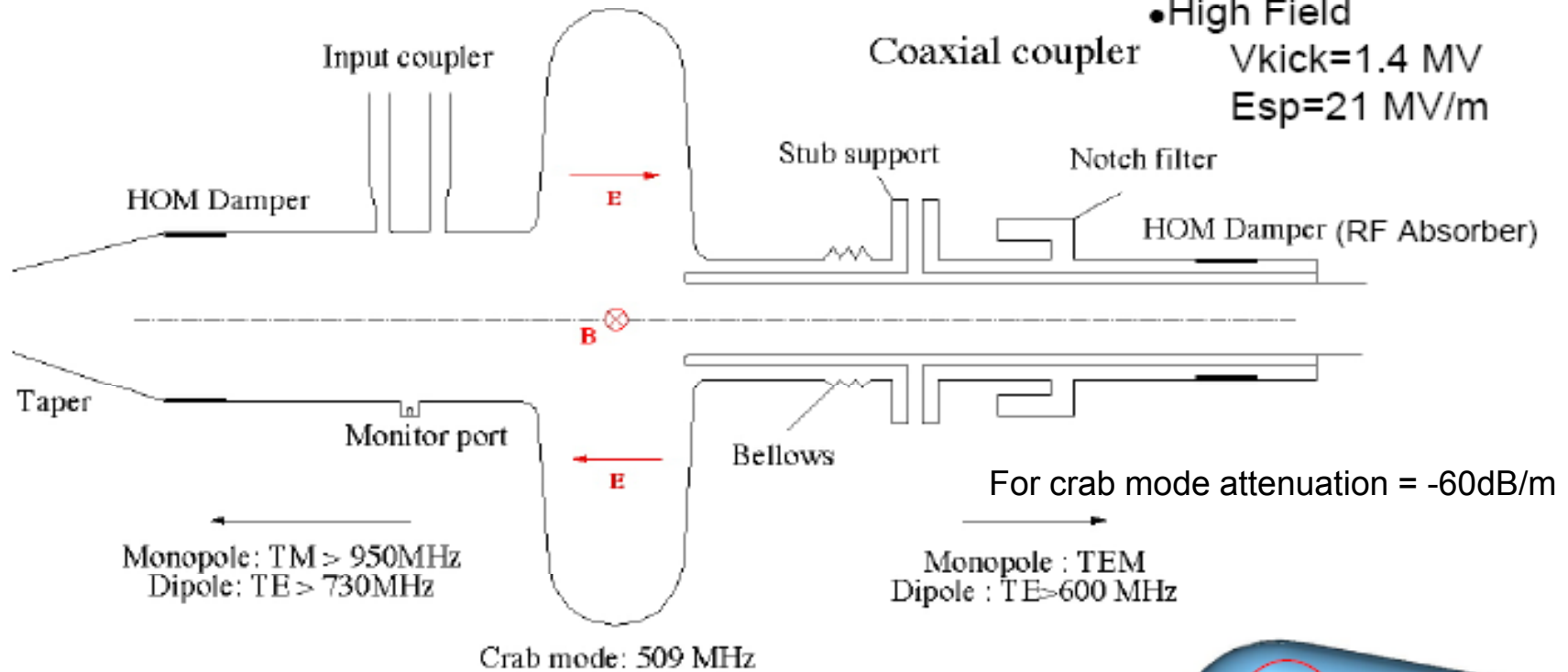
K. Akai

Unique characteristics

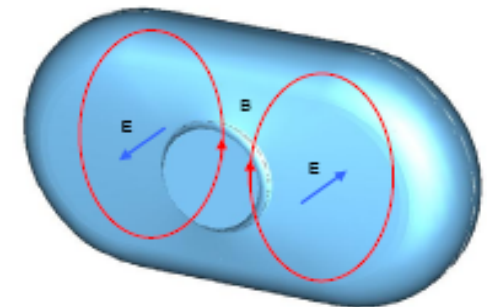
- Coaxial Coupler
- Squashed Cell
- High Field

$V_{kick} = 1.4 \text{ MV}$

$E_{sp} = 21 \text{ MV/m}$

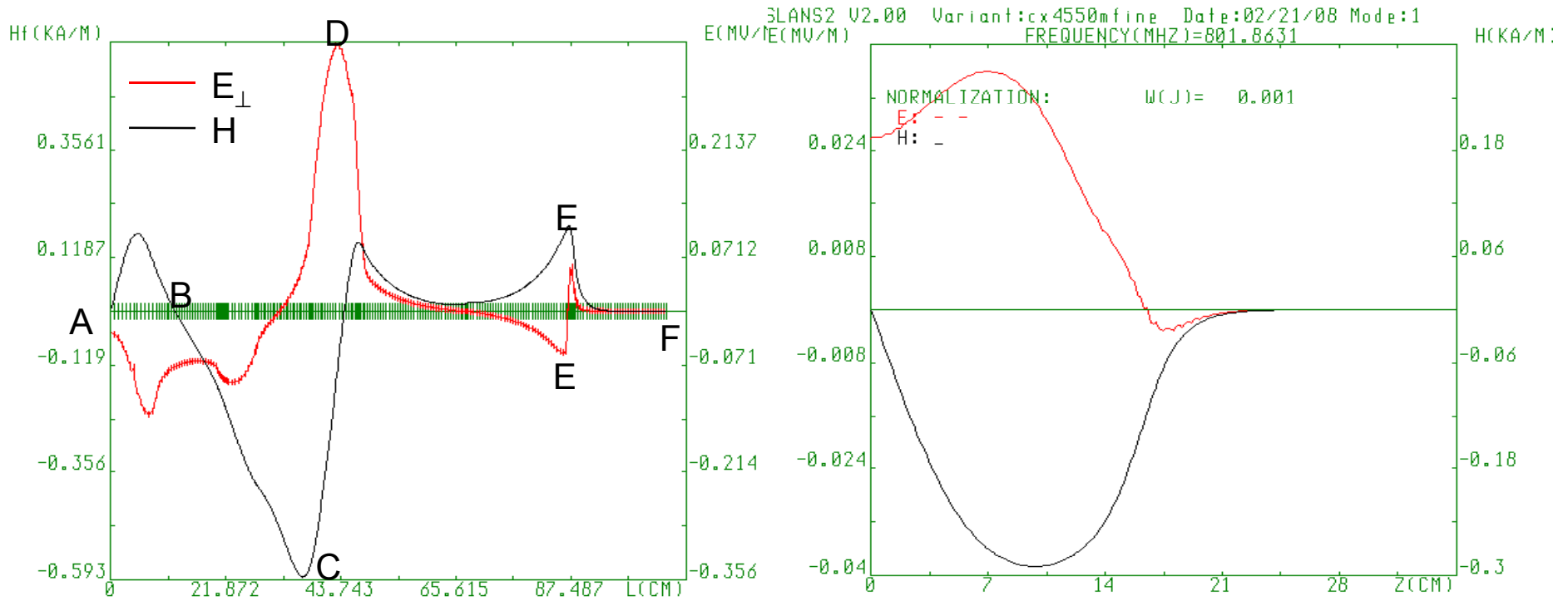
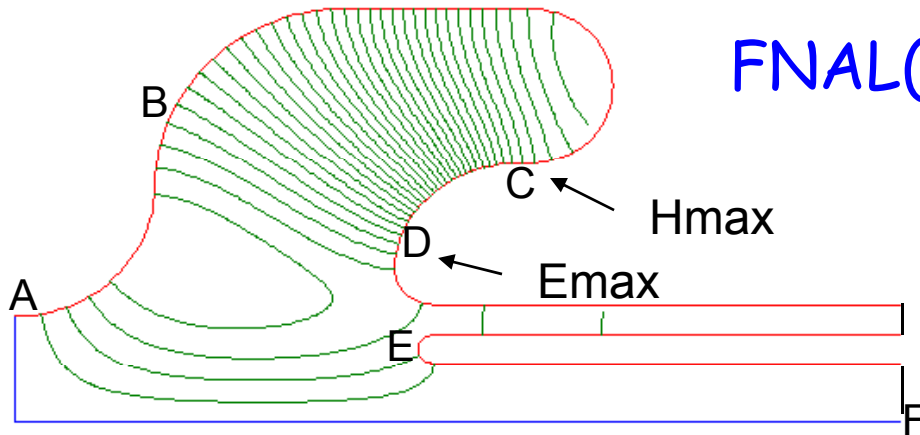


- Crab Mode: TM₁₁₀-like mode (high R/Q)
- Coaxial coupler: LOM damping
- Squashed cell: UWP > 600 MHz
- Notch filter: TEM-coupled Crab mode rejection
- Stub support: support for inner conductor





FNAL(B): Half-cavity



Distribution of electric and magnetic fields along cavity surface (left) and at the axis (right).



Main parameters of the crab cavities

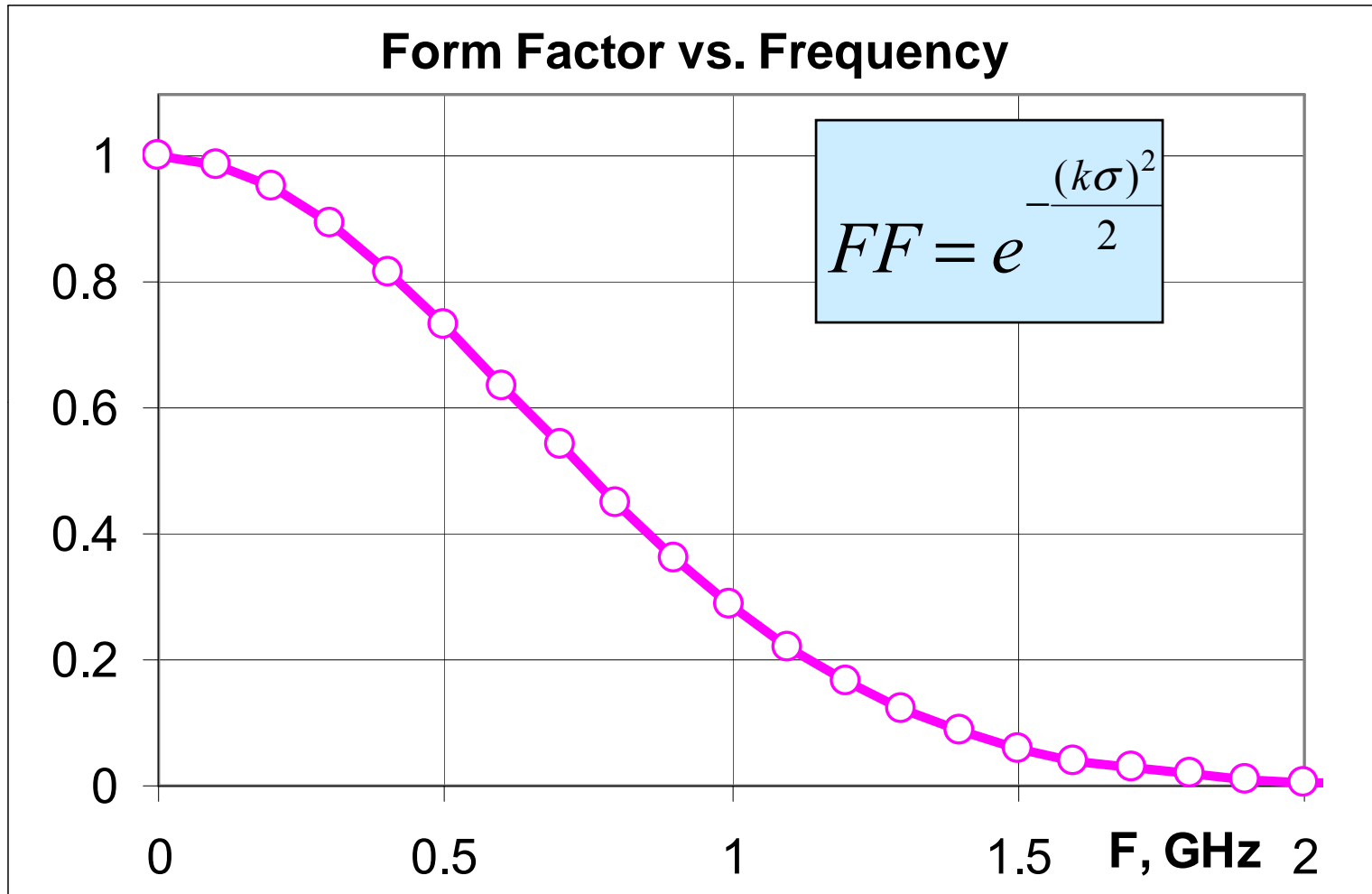
	BNL	SLAC	FNAL(A)	FNAL(B)
V_{\perp} , MV	5	5	5	5
B_{peak} , mT	386	189	150	152.1
E_{peak} , MV/m	66.2	47.5	68.6	72.4
r_{\perp}/Q , Ohms**	41	56	61	58.7
\emptyset iris, mm	160	140	90	100x74 (coax)
\emptyset cavity, mm	460	460	350	350

* $V_{\perp} = \Delta p_{\perp} c / e$;

** $(R_{\perp}/Q) = V_{\perp}^2 / 2\omega W$

(Form factor not included)

- Crab frequency 800 MHz
- All cavities in simulations not squashed
- SLAC squashed cavity: $H_s = 165.5$ mT; $E_s = 49.4$ MV/m



Bunch length $\sigma = 7.55$ cm

$$(R/Q)_{\text{eff}} = FF * (R/Q)$$



Monopole modes in Crab Cavities

	BNL		SLAC		FNAL(B)	
	0 - π modes		0- π modes		0- π modes	
Beam pipe \varnothing (mm)	160		140		100	
$F_{\text{cut-off}}$, MHz	1435.4		1640.4		0	
TM010: Freq, MHz	582	590	556	560	520.5	520.6
FF*(R/Q), Ω	12	6	16.5	63	20	73
TM020: Freq, MHz	1219	1256	1242	1264	1087.2	1087.8
FF*(R/Q), Ω	0.15	0.04	0.6	0.4	6.8	2.1
TM011: Freq, MHz	1384	1429	1440	1453	1675	1680
FF*(R/Q), Ω	0.06	0.6	0.08	0.7	0.02	0.3
TM030: Freq, MHz	1454	1457	1660	1661	1844.3	1843.6
FF*(R/Q), Ω	1.9	1.3	0.88	0.08	0.2	0.02

In squashed cavity (ratio=0.8)

TM010 moves up 30 MHz

Three monopole modes need to be damped in BNL, SLAC designs.

Higher frequencies (>1.5 GHz) are suppressed by form-factor



Dipole modes in Crab Cavities

	BNL		SLAC		FNAL(B)	
	0 π modes		0 π modes		0 π modes	
Beam pipe \varnothing (mm)	160		140		Coax: 74x100	
$F_{\text{cut-off}}$ MHz	1098		1255		1097	
TM110: Freq, MHz	828	800	811	800	801.3	800
FF*(R/Q), Ω	0.36	18.6	0.08	25	0.17	26.4
TM111: Freq, MHz	980	877	1069	981	1142	1145
FF*(R/Q), Ω	1.0	0.86	0.98	0.2	0.6	0.01
TM120: Freq, MHz	1185	1164	1353	1309	1291	1286
FF*(R/Q), Ω	0.003	0.009	0.07	0.0002	1.4	1.3
Freq, MHz	1355	1293	1495	1426	1309	1302
FF*(R/Q), Ω	0.004	0.003	0.06	0.1	0.22	0.05

↑
In squashed cavity SOM
(800MHz) moved up ~89 MHz

In FNAL(B) design squashing can move up frequency of other polarization (800MHz), higher than cut-off frequency in coaxial line



Damping

Monopole modes

Freq MHz	FF*(R/Q) Ohm	Q
520.6	20	440
520.7	73	420
1087.2	2.1	330
1087.2	6.8	350
1675.1	0.3	120
1679.6	0.02	115

Dipole modes

Freq MHz	FF*(R/Q) Ohm	Q
800	26.4	
801.3	0.17	
1144.6	0.01	61
1144.9	0.6	60
1285.5	1.3	509
1291.4	1.4	150
1302	0.05	18.8
1309	0.22	18.4
1412.3	0.5	28
1434.9	0.5	32

Stronger damping is possible changing position of the coaxial.

Crab mode is attenuated in coaxial line -136 dB/m



Requirements for HOM damping

HOM impedances should not be worse than for the acceleration cavity (?). For LHC acceleration cavity:

- *The total power of monopole HOMs dissipated < 800 W.*
- *Impedance of the two lowest dipole modes should not be 1.5 k Ω*
 - *Total transverse impedance is dominated by collimators*

Table 2: Estimated impedance budget for the LHC in the vertical plane.

Element	Inner radius [mm]	β/β_{av}	Z_T [k Ω /m]
Beam screen			
pumping holes	18	1.25	500
200 MHz cavities	50	3	155
400 MHz cavities	150	2.9	11
Shielded bellows	20	1.25	265
Vacuum valves	40	1.25	35
Collimators	8	4.3	2300
BPMs [6]	25	1.25	300
BI instruments	40	2.15	12
Total			3578

(D. Boussard, et al, "The LHC Superconducting Cavities, PAC 1999.)

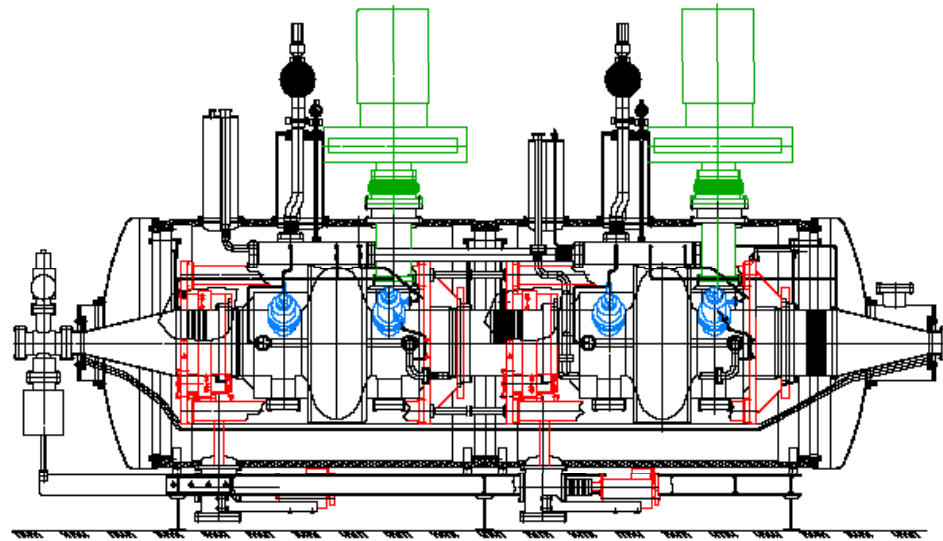
For 800 MHz crab cavity if the same requirements:

Monopole modes: $FF^*(R/Q)_{\max} \sim 70 \text{ Ohms} \rightarrow Q \sim 30$

Dipole HOMs: $FF^*(R/Q)_{\max} \sim 1 \text{ Ohms} \rightarrow Q \sim 100$ ($\beta \sim 4 \text{ km}$)



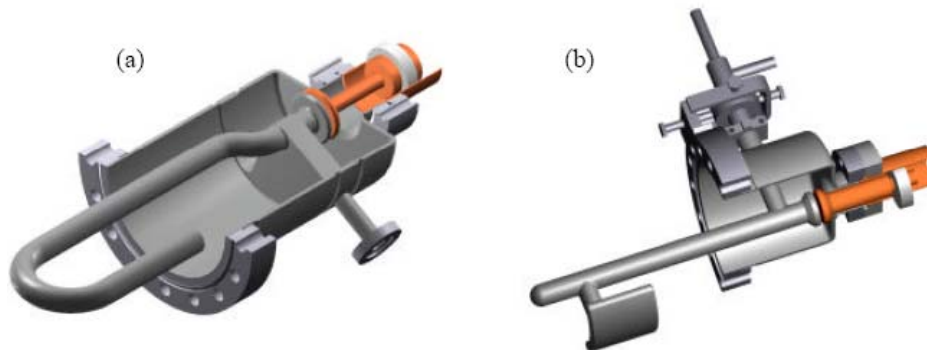
HOM damping in the LHC accelerating cavities.



$F(TM_{010}) = 400 \text{ MHz}$

Beam pipe = 300mm

The cryomodule with two cavities. HOM couplers are shown in blue.



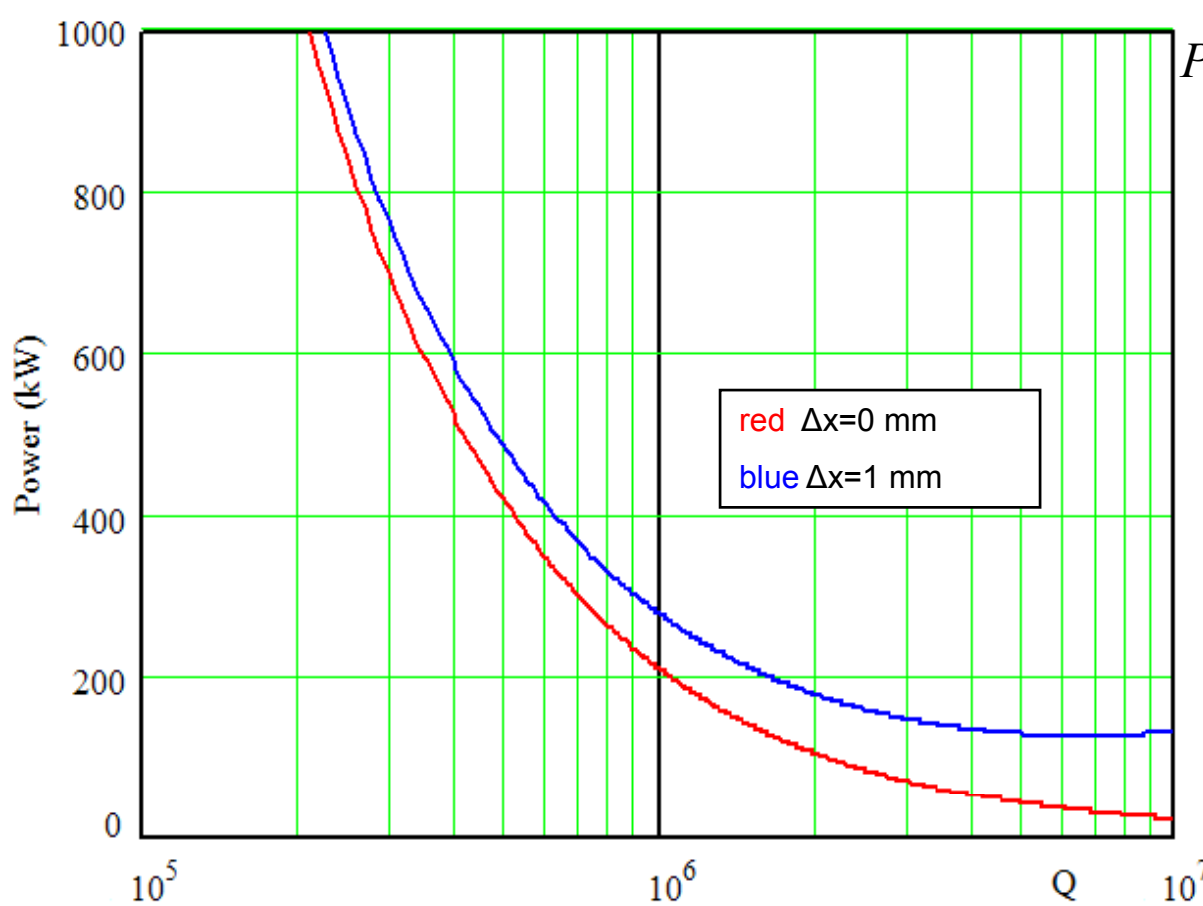
(a) Narrow band dipole mode HOM coupler;
 (b) Broad band HOM coupler

Frequency (MHz)	Undamped Q	Damped Q
500 (TE_{111})	38000	137
534 (TM_{110})	40000	93
779 (TM_{011})	50000	270
1184	50000	1000
1238	50000	400

HOM damping on a single-cell cavity by one dipole mode and one broadband coupler



Power requirements. Beam jitter



$$P = \frac{(V_{\perp} + 2I_b FF \cdot (R_{\perp} / Q) \cdot Q \cdot k \Delta x)^2}{2(R_{\perp} / Q) \cdot Q}$$

$$V_{\perp} = 5MV,$$

$$I_b = 0.84A,$$

$$R_{\perp} / Q^* = 60 Ohms,$$

$$k = 2\pi / \lambda_{RF},$$

$$\lambda_{RF} = 37.5cm(800MHz)$$

FF is form-factor,

$$FF \sim e^{-\frac{(k\sigma)^2}{2}}$$

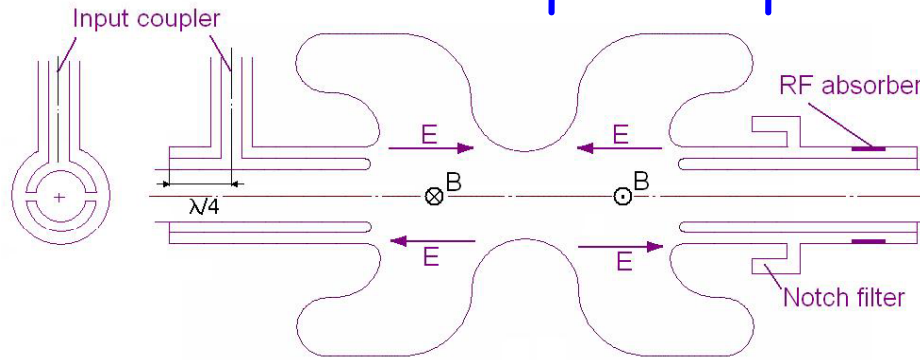
$$* R_{\perp} / Q \equiv \frac{V_{\perp}^2}{2\omega W},$$

ω is cyclic frequency, W is stored energy.

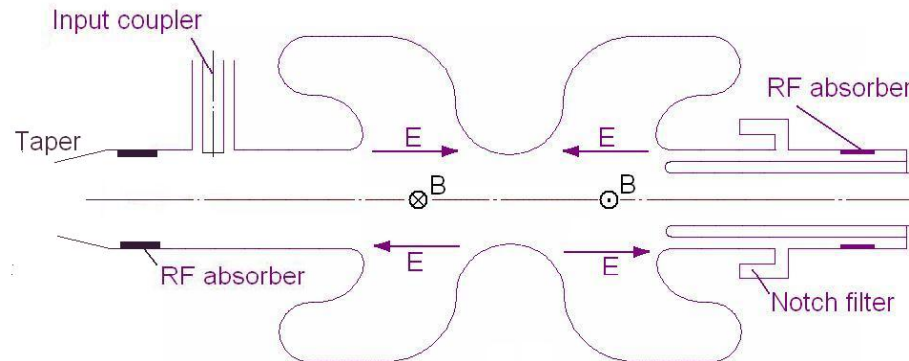


Different options for the HOM damping and the input coupler

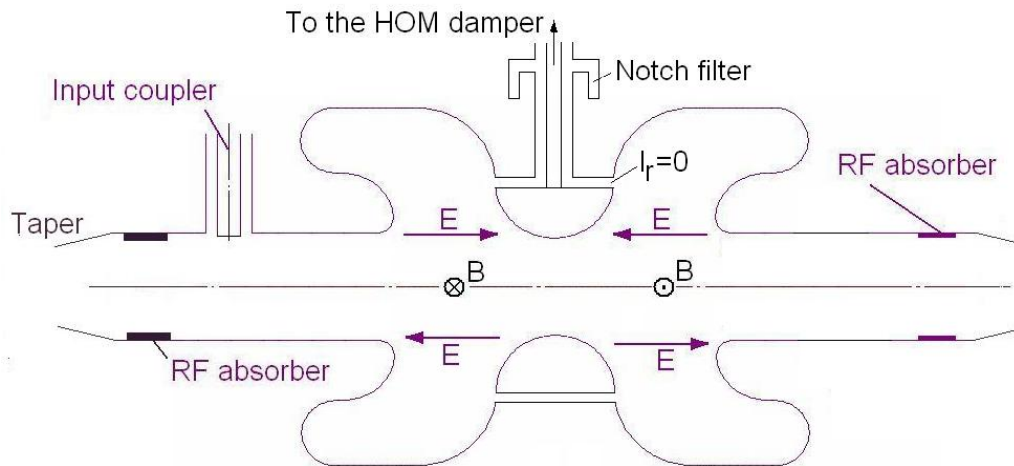
a)



b)



c)





Conclusions

- Preliminary results of R&D
 - Crab-like shape for crab cavity to reduce cavity outer diameter
 - Coaxial damping works for all modes
- Next to do:
 - Requirements (Q_{load} , beam-pipe diameter, etc.)
 - Optimize cavity shape
 - Squashed cavity design
 - Input coupler design
 - Study other options