

# Design and Operation of a Cryogenic Nitrogen Pulsating Heat Pipe

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# Overview

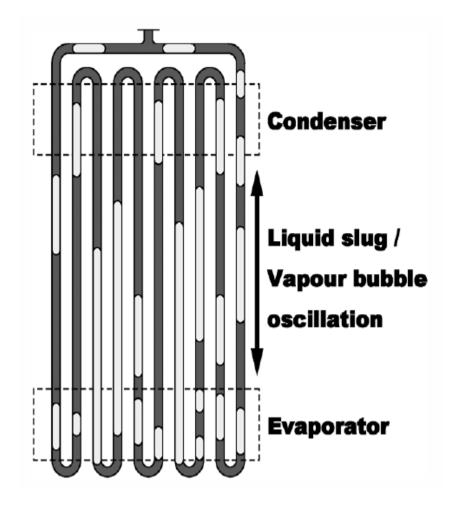


- Concept
- Main Design Parameter
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- Results
- Future Improvements
- Questions

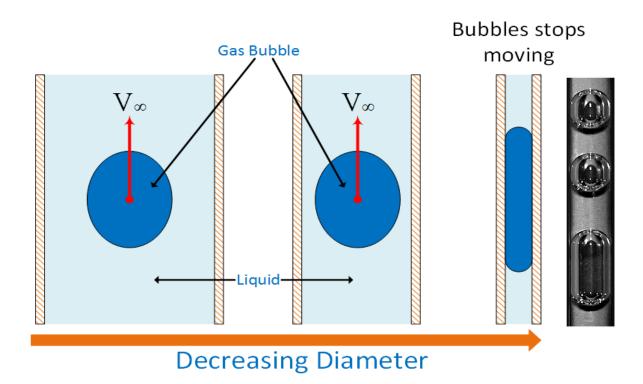
### **PHP Concept**



- Pulsating Heat Pipes: oscillations/pulsations are cause by the change in volumetric expansion and contraction in evaporator and condenser.
- Liquid plugs and vapor bubbles are formed.







$$Re = \frac{F_i}{F_\mu} = \frac{\rho_L V_\infty D}{u_L}$$

$$We = \frac{F_i}{F_S} = \frac{\rho_L V_{\infty}^2 D}{\sigma}$$

$$Fr = \frac{F_i}{F_b} = \frac{\rho_L V_{\infty}^2}{(\rho_L - \rho_g)gD}$$

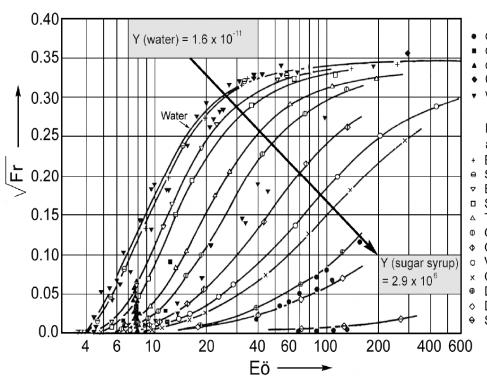
$$Ps = \frac{F_{\mu}}{F_b} = \frac{\mu_L V_{\infty}}{(\rho_L - \rho_a)gD^2}$$

$$Eo = \frac{F_b}{F_s} = \frac{(\rho_L - \rho_g)gD^2}{\sigma}$$

$$Bo = \sqrt{Eo}$$



Air bubbles through different fluids in vertical plates White and Beardmore (1962).



- oils by Foust
- oils by Barr
- oils by Abrams et al.
- CCl4 by Harmathy
- various liquids by Hattori

Results of White and Beardmore

- + Ethanol
- Sucrose solution
- ▼ Ethylene glycol
- Sucrose solution
- △ Tellus Oil
- Glyserol solution
- Glyserol solution
- Voluta oil
- X Glyserol
- Diluted sugar syrup
- ♦ Diluted sugar syrup
- ♦ Sugar syrup

$$Fr = \frac{F_i}{F_b} = \frac{\rho_L V_{\infty}^2}{(\rho_L - \rho_g)gD}$$

$$Ps = \frac{F_{\mu}}{F_b} = \frac{\mu_L V_{\infty}}{(\rho_L - \rho_a)gD^2}$$

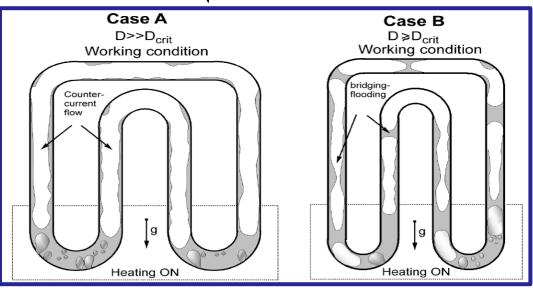
$$Eo = \frac{F_b}{F_s} = \frac{(\rho_L - \rho_g)gD^2}{\sigma}$$

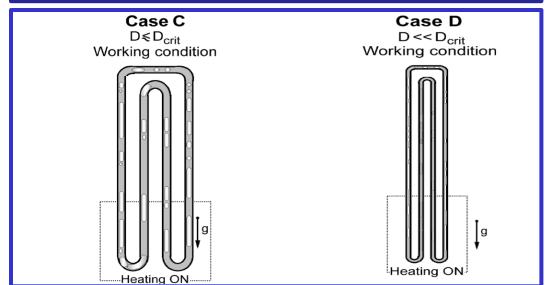
$$Y = \frac{Ps^4 Eo^3}{Fr^2} = \frac{g\mu_L^4}{\rho_L \sigma^3}$$

$$Eo = Bo^{2} = \frac{(\rho_{L} - \rho_{g})gD_{crit}^{2}}{\sigma} \le 4 \longrightarrow D_{crit} \le 2\sqrt{\frac{\sigma}{(\rho_{L} - \rho_{g})g}}$$



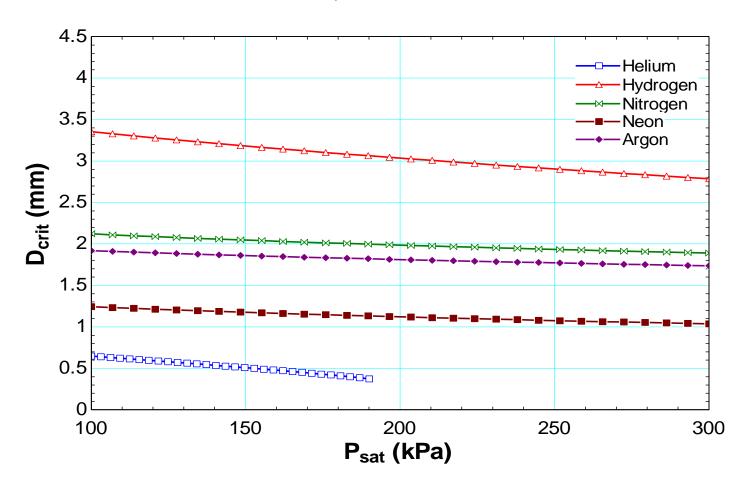
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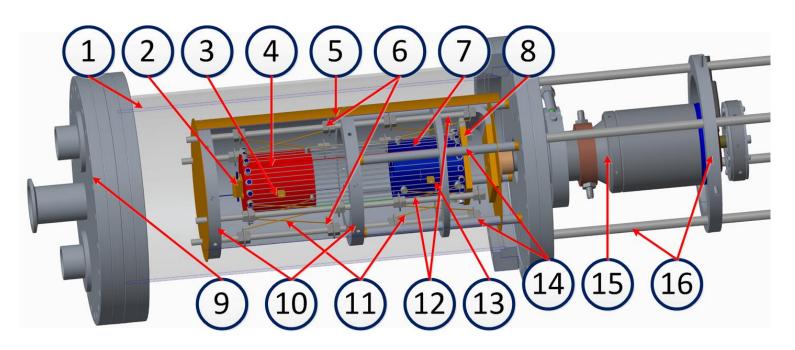
### **Experimental Setup**



#### Main Components:

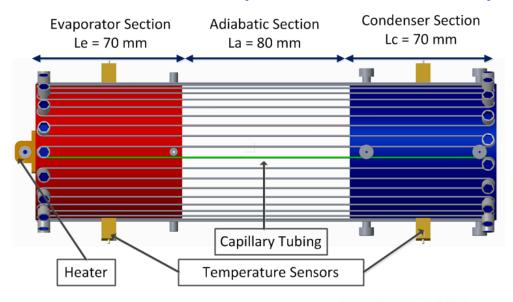
- 20 cm OD Vacuum Nipple.
- PHP heat at Evaporator.
- PT-103 temperature casing at evaporator.
- Evaporator Section.
- Thermal Jacket: Cu 110 Grade.
- Wire Support Tensors.
- Condenser Section.

- Thermal Bus: from <u>cryocooler</u> to condenser.
- 9) Vacuum and temperature feedthrough flange.
- 10) AL 6061 Circular Supporting Plates.
- Supporting Wires for condenser and evaporator sections.
- 12) Threaded rod to fix circular supports (10).
- 13) PT-103 temperature casing at condenser.
- 14) SSL support tubes for circular support. Bolted from bottom flange to circular support.
- 15) <u>Sunpower CT cryocooler</u>. Nominal operation: 10 W at 77 K.
- 16) Support Structure for cryocooler.

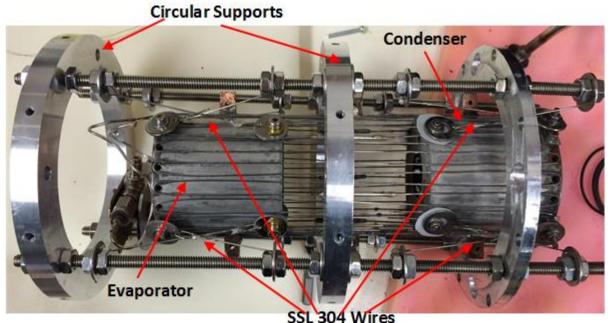


# **Experimental Setup: PHP Core**



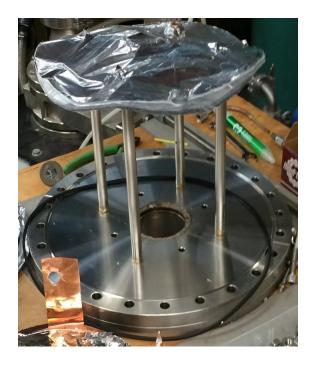


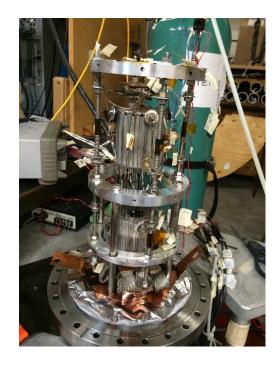
- Condenser section have an OD of 65 mm.
- Capillary tubing are soldered to both sections.
- PHP core are supported by SSL 304 Wires.

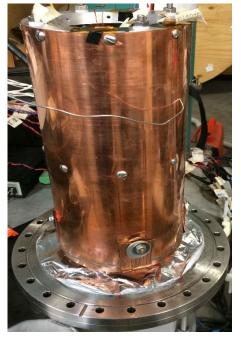


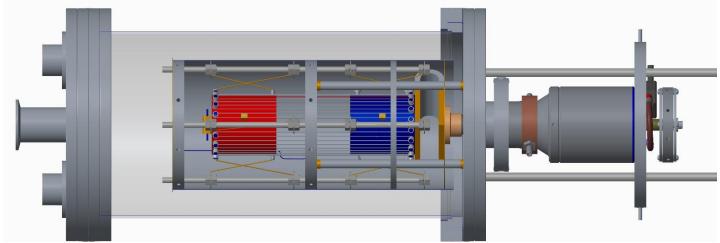
# **Experimental Setup: Support Structure**





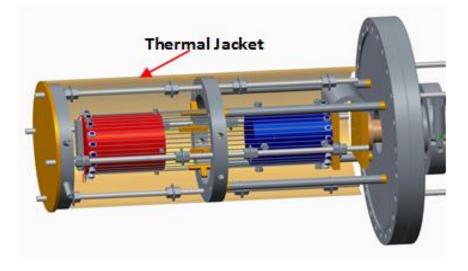




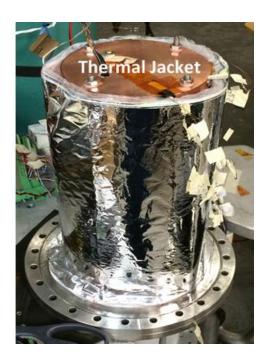


# Experimental Setup: Thermal Jacket and MLI



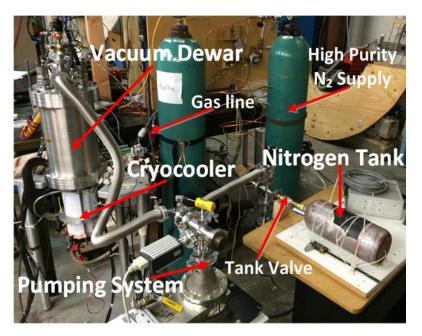


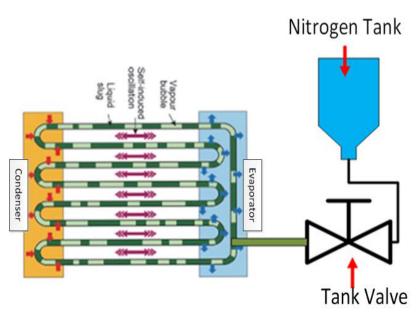


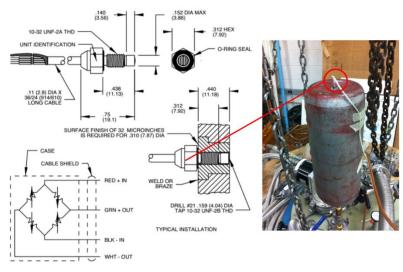


# **Experimental Setup: Vacuum Pumps**







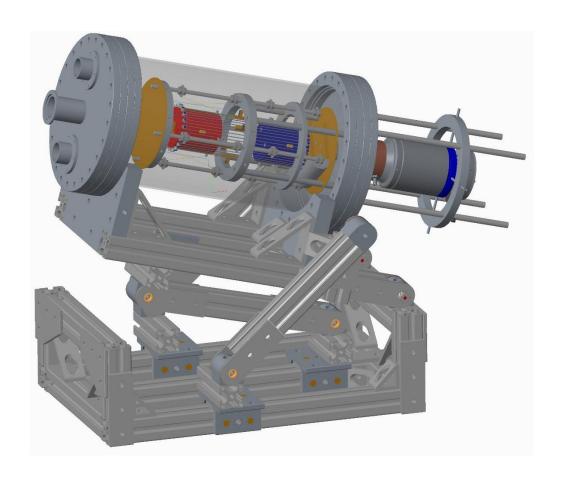


STANDARD TOLERANCE INCHES (MILLIMETERS) .XX = +/- .03 (.X = +/- .8) .XXX = +/- .010 (.XX = +/- .25)

# Experimental Setup: Future Test Bed

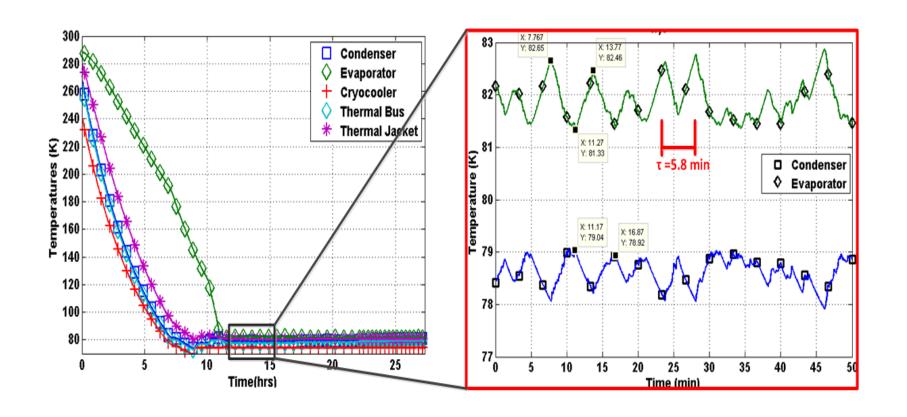


Inclination test bed to run PHP at different orientation angles.



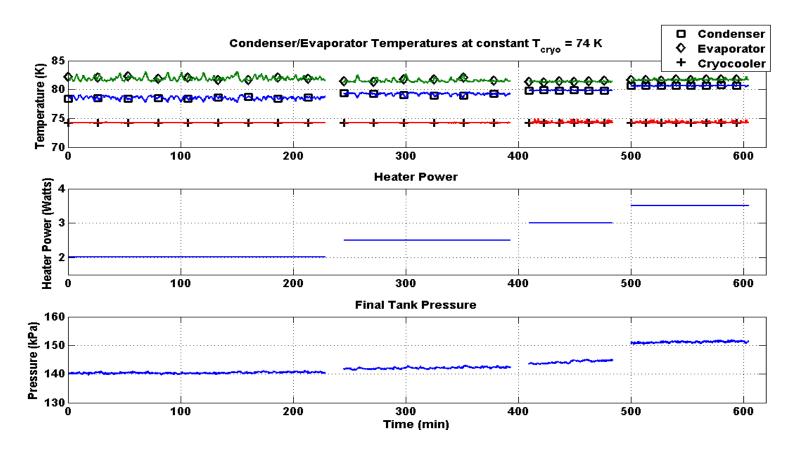


- Horizontal orientation.
- Cooldown curve took 12 hours to reach saturation temperatures.
- Pressure in PHP around 140 kPa.
- At heat load below 2 W, time periods reached 5.8 min.





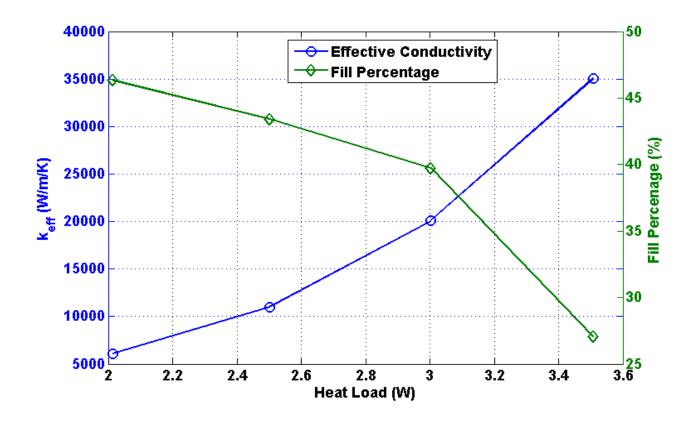
- Horizontal orientation.
- Maintained constant cryocooler temperature of 74 K.
- Increased heat load from 2 W to 3.5 W.
- ΔT between sections decreased from 3.3 K to 1 K.
- Oscillations periods decreased dramatically, most frequent were between 18 and 42 seconds.





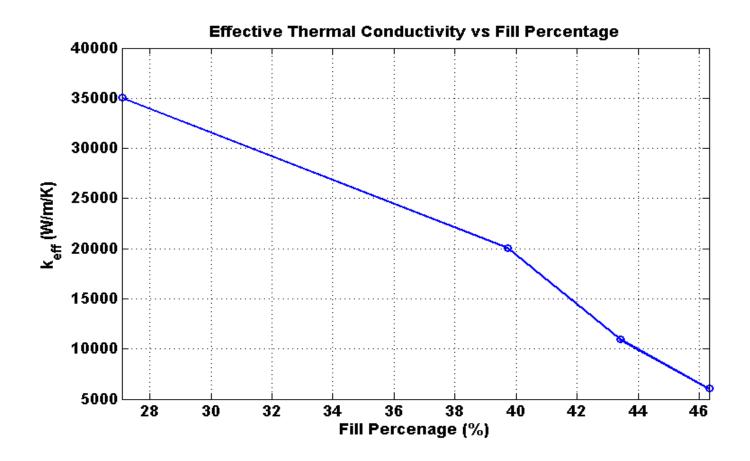
• As heat load increases effective thermal conductivity  $k_{eff}$  increases but Fill Percentage  $f_{liq}$  decreases.

$$N_{total} = \frac{P_{final}V_{tank}}{RT_{amb}} + \frac{P_{final}V_{gas-lines}}{RT_{gas-lines}} + \overline{r}_{l,sat}V_l + \overline{r}_{v,sat}\left(V_{PHP} - V_l\right) \qquad f_{liq} = \frac{V_l}{V_{php}}$$





 it should be noted that the effective thermal conductivity is higher at low fill percentages at a constant cryocooler cold tip of 74 K.



#### **Future Work**



- Build inclination test bed.
- Test different adiabatic lengths.
- Divide evaporator section in 3 sections to have 3 independent heaters.
- Test experiment in a zero gravity environment (Parabolic Flight) to verify usage for space applications. NASA's flight opportunity program.
- Currently building another PHP to test more than one cryogen: Argon, Nitrogen, Helium, Neon and Hydrogen. (Supported by Sumitomo)

# **Special Thanks**



• Sunpower Inc. for all their help and consulting of the operation of the CT cryocooler.

# Questions?

