





# Dimensional Changes of Nb<sub>3</sub>Sn Cables during Heat Treatment

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\* This work was supported by the Director, Office of Science, High Energy Physics, U.S. Department of Energy under contract Nos. DE-AC02-05CH11231 and DE-AC02-98CH10886



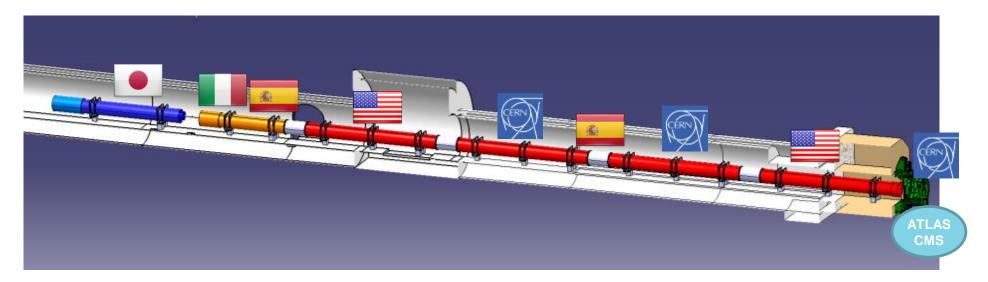
# Outline

- Introduction
- Motivation
- Experiments
- Results
- Conclusion
- Acknowledgement: Hugh Higley (LBNL), LARP, GARD, Toohig Fellowship



## Introduction

- The <u>LHC-Accelerator Research Program (LARP)</u> has been designing and fabricating R&D magnets for the <u>High</u> <u>Luminosity Upgrade</u> for over ten years
- Inner triplet quadrupoles using Nb<sub>3</sub>Sn. US in-kind contribution.
- "MQXF"



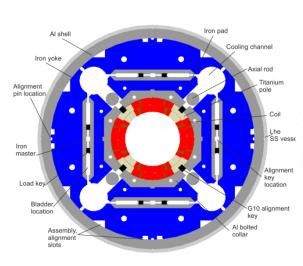


# MQXF - Magnet



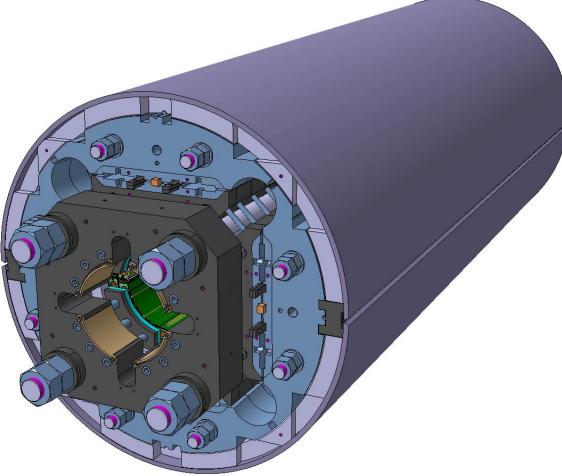
#### THE TRIPLET

- Main parameters [LHC today]
  - Aperture 150 mm [70 mm]
  - Gradient 140 T/m [200 T/m]
  - Lengths 8.0 m/6.8 m [6.2/5.5 m]
  - Peak field 12.1 T [8.6/7.7 T]
  - Current 17.45 kA [7.2 kA/12 kA]
  - 80% on the loadline [80%, 84%]
  - To be installed in '23-'24 [2007-8]
  - Temp margin ~4.5 K [1.5-2.0 K]



QXF cross-section [G. Ambrosio, P. Ferracin]

- $j_{overall} \sim 500 \text{ A/mm}^2$  [380-420 / 480-590 A/mm<sup>2</sup>]
- $j_{sc} \sim 1600 \text{ A/mm}^2$  [800-1600 / 1000-1500 A/mm<sup>2</sup>]
- 16 units needed (IR1 and IR5) plus spares [we do not touch IR2 and IR8]



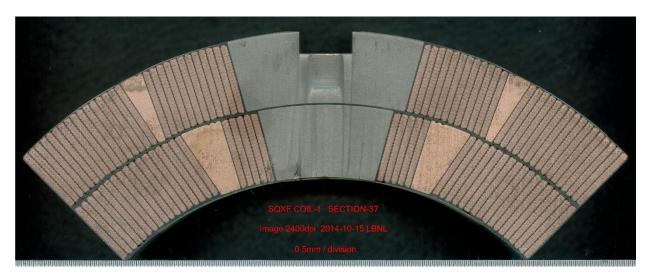
E. Todesco HL LHC magnets roadmap - 4

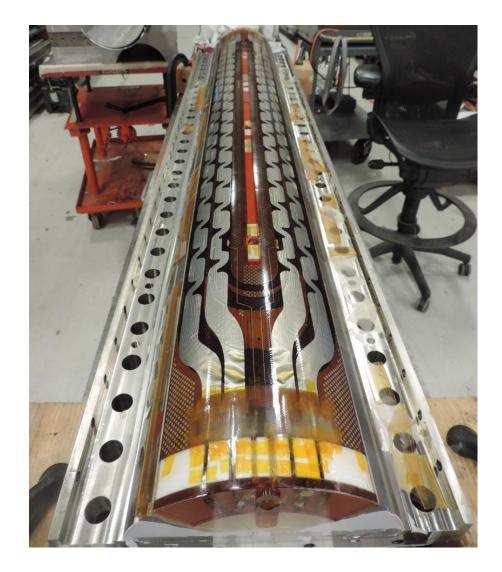


# MQXF - Coil

- Two layers
- Four blocks
- No grading









# **MQXF** Conductor

- 108/127 stack Nb<sub>3</sub>Sn wires
  - 0.850 mm diameter, uncoated
- 40-strand cable UL ~500 m
  - 18.15 mm wide
  - 1.525 mm thick
  - 0.40° keystone ("2nd generation")
  - With stainless steel core
  - Unannealed strands

U.S.
HiLum
Project

#### Specification for Quadrupole Magnet Conductor

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US-HiLumi-doc.40 Rev. No. Original Release Date: 04-May-2015 Page 15 of 15

#### ANNEX – SUMMARY OF PERFORMANCE REQUIREMENTS

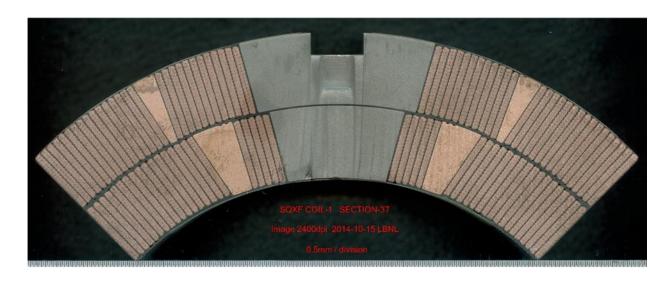
Parameter or characteristic	Value	Unit
Superconductor composition	Ti-alloyed Nb <sub>3</sub> Sn	
Strand Diameter	$0.850 \pm 0.003$	mm
Critical current at 4.2 K and 12 T	> 632	A
Critical current at 4.2 K and 15 T	> 331	A
n-value at 15 T	> 30	
Count of sub-elements	≥ 108	
(Equivalent sub-element diameter)	(< 55)	(µm)
Cu : Non-Cu volume Ratio	≥ 1.2	
Variation around mean	± 0.1	
Residual Resistance Ratio RRR for reacted final-size strand	≥ 150	
Magnetization* at 3 T, 4.2 K	< 240	kA m <sup>-1</sup>
	(<300)	(mT)
Twist Pitch	19.0 ± 3.0	mm
Twist Direction	Right-hand screw	
Strand Spring Back	< 720	arc degrees
Minimum piece length	550	m
High temperature HT duration	≥ 40	Hours
Total heat treatment duration from start of ramp to power off and furnace cool	≤ 240	Hours
Heat treatment heating ramp rate	≤ 50	°C per hour
Rolled strand (0.72 mm thk.) critical current at 4.2 K and 12 T	> 600	A
Rolled strand RRR after reaction	> 100	
	> 100	<u> </u>

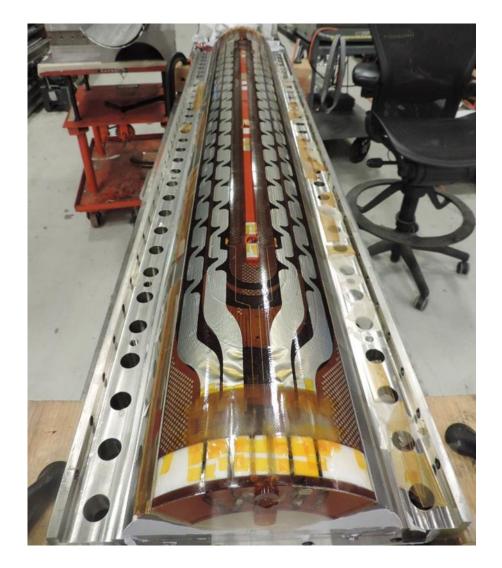
<sup>\*</sup>Magnetic moment (A m²) divided by the volume (m³) of a strand piece in transverse magnetic field, without removing copper

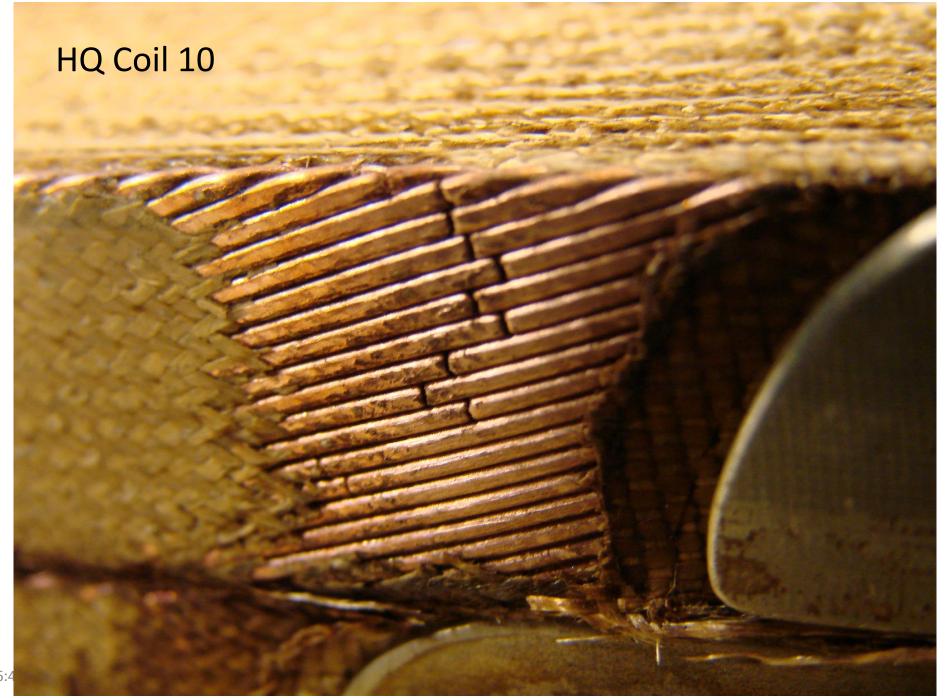


## Motivation

Nb<sub>3</sub>Sn: wind & react → impact on coil due to cable dimension change during heat treatment, esp. length, width, and thickness?









# Complication

### Cable insulation







- AGY S2-glass fibers 66 tex with 933 silane sizing
- 32 (CERN, CGP) or 48 (LARP, NEW) coils (bobbins)
  - · Variables: # of yarn per coil and of picks/inch
- Target: ≤ 150 µm per side (145 ±5 µm) at 5 MPa, average 3 cycles





Paolo Ferracin

10/12/2014

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Cable insulation changes cable behaviour!

LBNL experience shows that dimension change is different between confined and unconfined cables



# Past Experience

- Unconfined cables
  - Cables are free to expand or contract in width, thickness, and length
- Confined cables
  - Width and thickness defined by tooling that is bolted together
    - Cable width and thickness are determined by CME at 17 MPa
    - Insulation thickness are determined at a reference pressure
  - Length is not confined.



# **Unconfined Cables**



Figure 7: a) Measuring cable length, b) in the unconfined case, the cables are placed between siderails, top & bottom plates are tied together



# **Confined Cables**

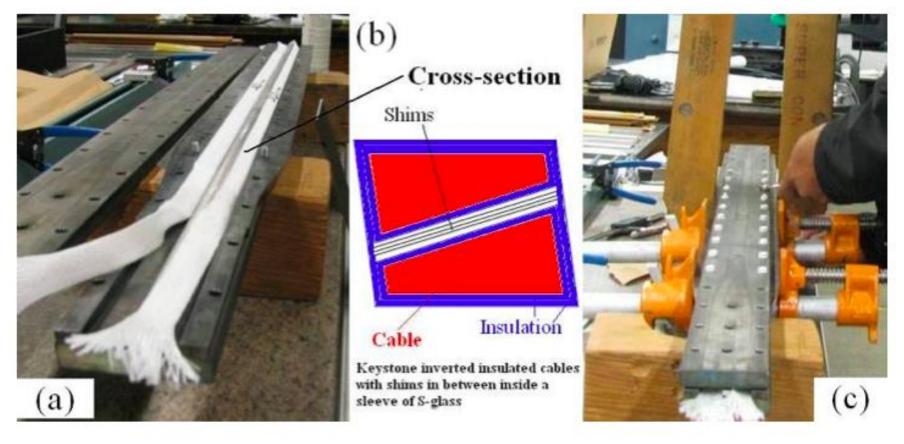
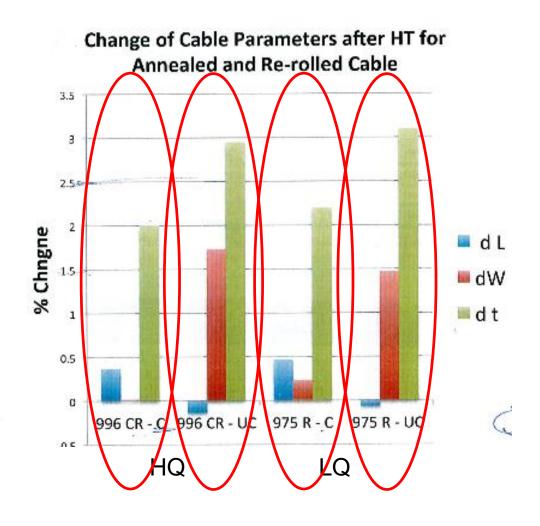


Figure 6: a) & b) The cables in the tooling, c) top plate is bolted on while the width is maintained by wooden blocks



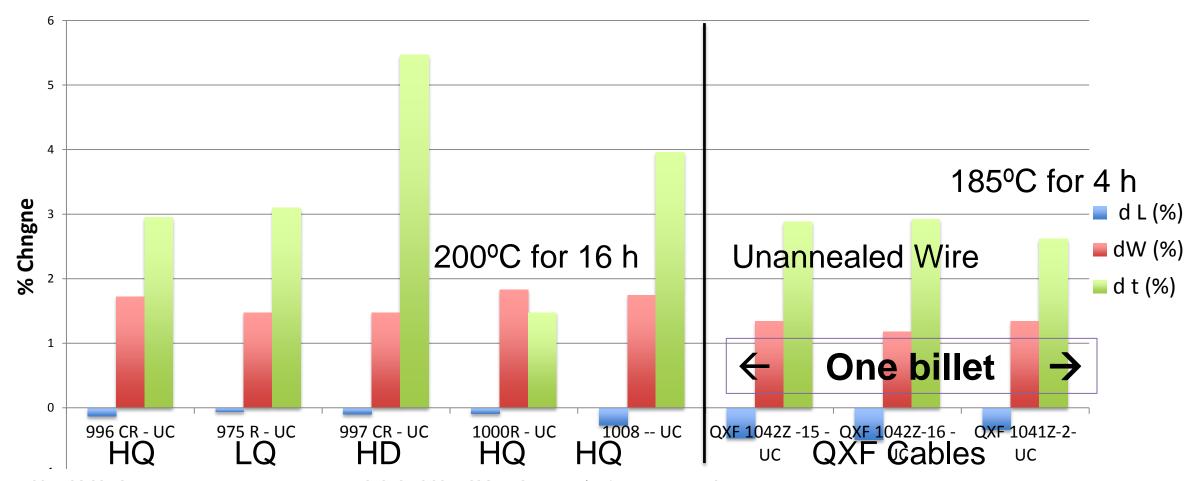
# Confined vs. Unconfined Cables





## **Unconfined Cables**

Change of Cable Parameters after HT for Annealed and Re-rolled Cable + QXF Cables with Annealed and Un-annealed





# **Materials**

#### Cable Samples ("1st Generation")

- SQXF03 Inner P33OL1053CB(70)B\*
- SQXF-PC01b P35OL1056AB(70)B
- SQXF04 Inner P33OL1057AA(00)B
- SQXF05 Outer P33OL1057AD(40)B

#### **Details**

- 108/127, Ti-doped, reduced-Sn, 0.55° KS;
   annealed prior to cabling
- 132/169, Ti-doped, Standard-Sn, 0.55° KS; annealed prior to cabling
- 108/127, Ti-doped, reduced-Sn, 0.55° KS; annealed prior to cabling
- 108/127, Ti-doped, reduced-Sn, 0.55° KS; annealed prior to cabling

<sup>\*</sup> This cable was test-wound on a Selva winder and subsequently straightened. It had matrix painted on the insulation every ~24" in 6 to 12" painted sections.



# **Reaction Method**

- S2-glass Sleeve
- S2-glass Braid
- S2-glass Braid + CTD-1202 Matrix



#### CTD-1202 Polymer-Derived Ceramic Insulation

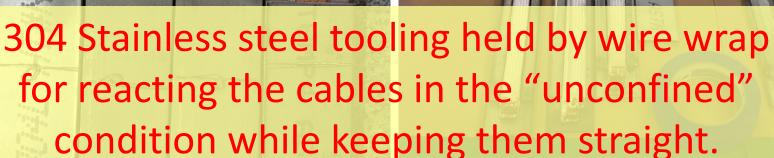
**Electrical Insulation for Superconducting Magnet Applications** 

- A Polymer-Derived Ceramic (PDC) resin system for use in a wide range of service temperatures and conditions.
- Resin is first cured, or green staged, to form a polymer. Thereafter, pyrolysis converts
  the green polymer to a ceramic.
- · Processing characteristics: low viscosity and long pot-life.
- · High dielectric breakdown strength.
- Extremely low toxicity resin system. No harmful volatiles are evolved during pyrolysis.

Green Cure:

1 hour at 80°C; 2 hours at 150°C Do not heat at rates exceeding 5°C/min May be cured in a closed mold







## **Heat Treatment**

- 210°C for 72h + 405°C for 50h + 654°C for 50h and furnace cooled
- ± 5°C and ± 5 h at dwell; under flowing Ar



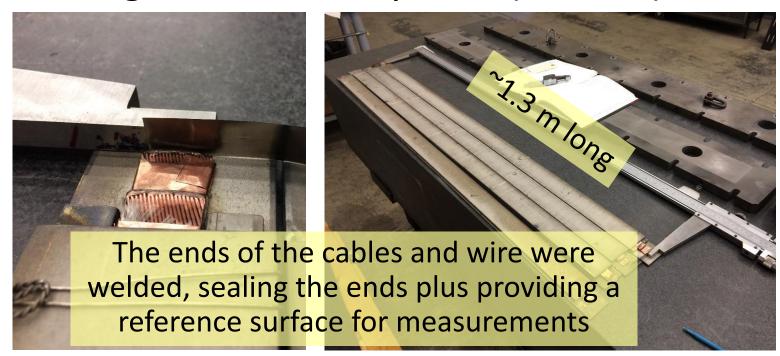


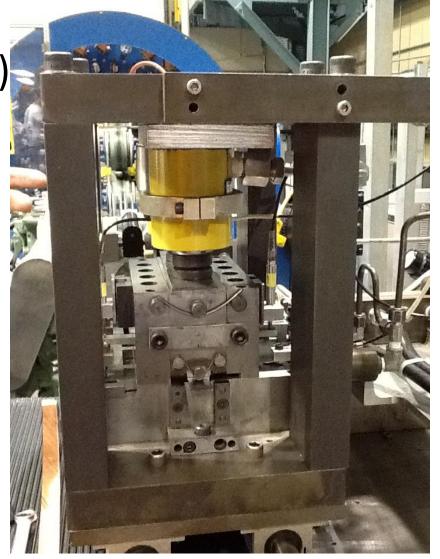


# Measurement Methods

Length measured with a caliper (±0.002")

 Mid-thickness, width, and keystone angle measured by CME (17 MPa)

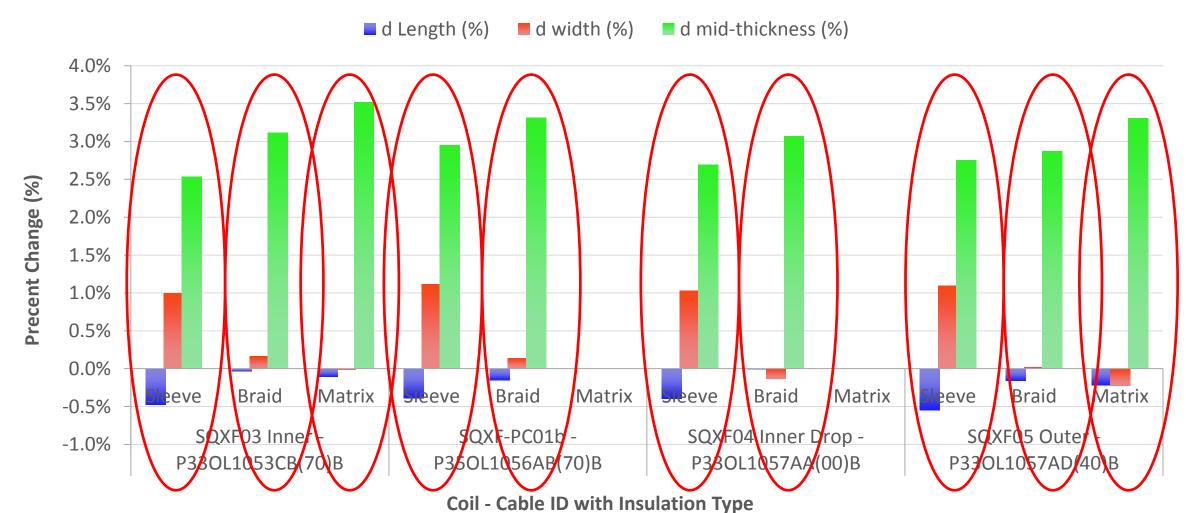






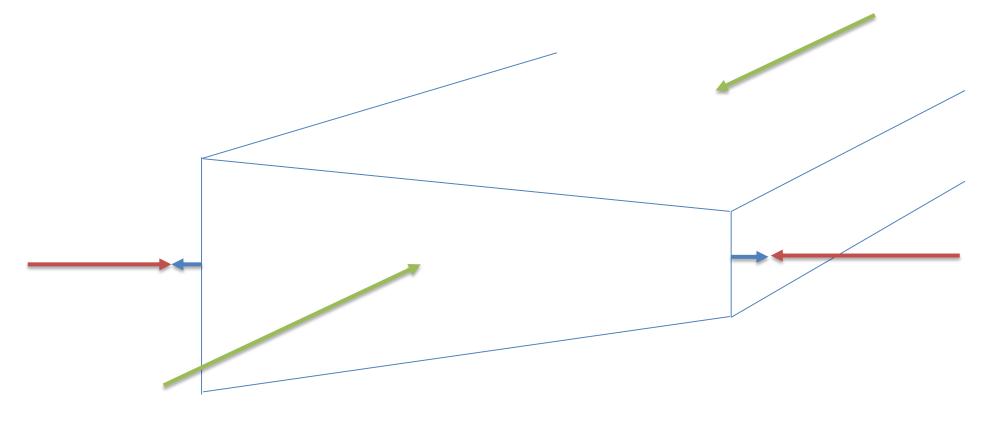
# Results

Cable Expansion Experiment 2015





Large Hadron Collider Accelerator Research Program





# Conclusion

- Confined and unconfined cables behave differently
  - Length shrinks with greater width and thickness increase when unconfined; whereas cable elongates when confined
- Braid and sleeve have different effect on cable dimension change during heat treatment 

  impact of insulation
  - braid is like a cable with width and thickness confined
  - Slight length shrinkage and slightly larger thickness increase than C
- "Matrix material" degrades the braid but the effect on cable dimension change is similar: ~3% increase in mid-thickness



# Coil Cross Section Analysis

- Direct coil cross section analysis comparison is difficult due to many reasons
  - Cable parameter definitions
  - Thickness variation
  - Core folding
  - etc. etc.
- Future papers:
  - MT24 (abstract 01010P0696 by Holik et al.)
  - EuCAS (abstract A51662EH by Pong et al.)

