

# Transverse, axial and torsional strain in REBCO tapes; experiments and models

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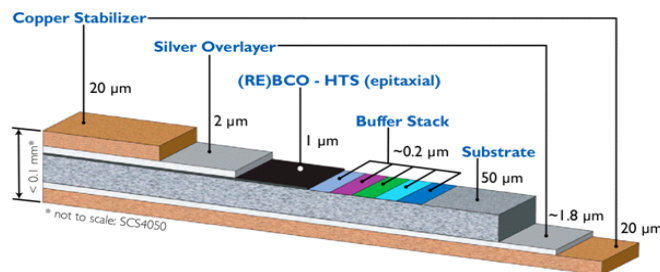
<sup>3</sup> US Air Force Research Laboratory, USA

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# Outline

- Introduction
- Tape model and experiments
- CORC cable model, work in progress
- Summary



All samples - SuperPower SCS 4050 tape

# CORC cable FE modeling steps

Step 1

- Tape material thermal-mech properties

Step 2

- Tape production (different  $T$  process)

Step 3

- Tape winding to CORC @ RT

Step 4

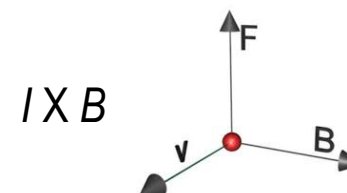
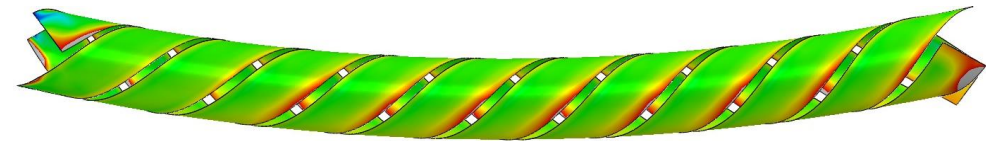
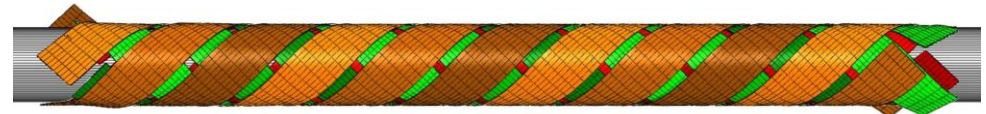
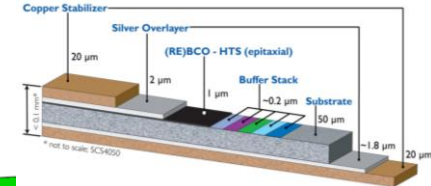
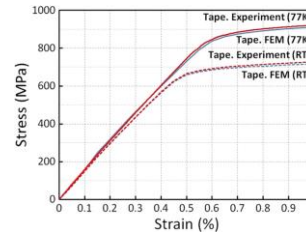
- CORC bending to coil @ RT

Step 5

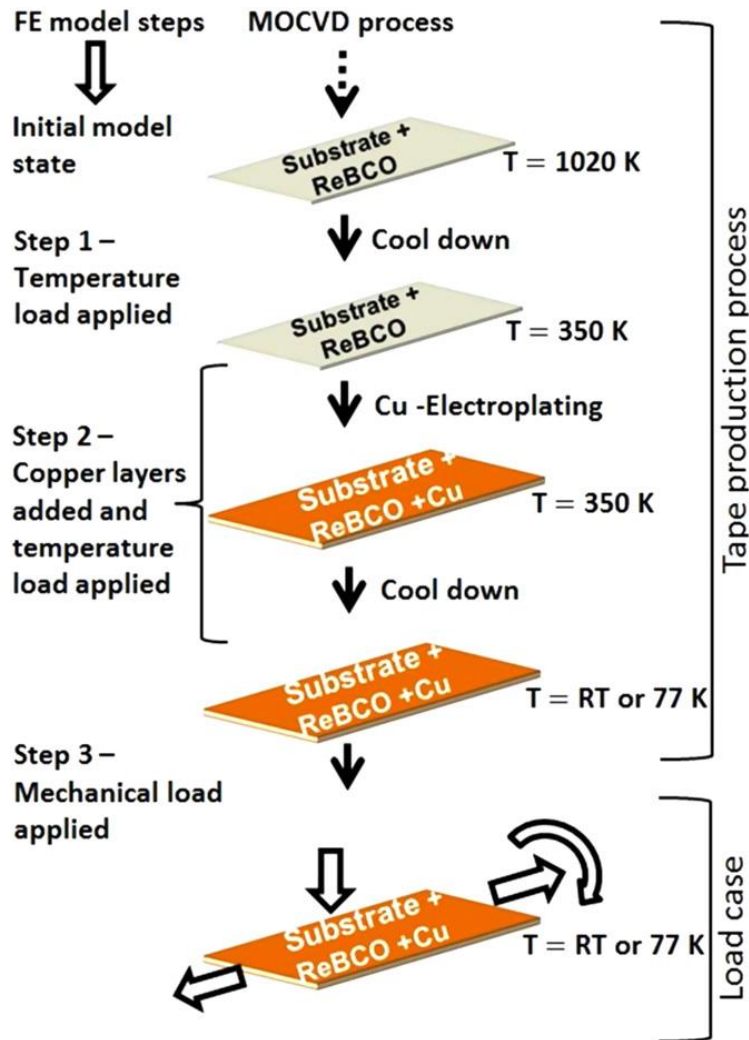
- Cooling to operating  $T_{op}$  (77 K)

Step 6

- Electromagnetic load @  $T_{op}$

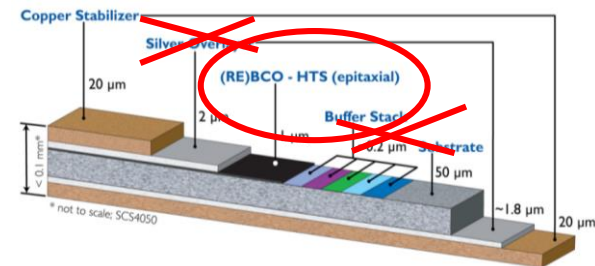


# Modeling: tape initial state



- Substrate (Hastelloy C-276)
- Copper (Electroplating)
- REBCO

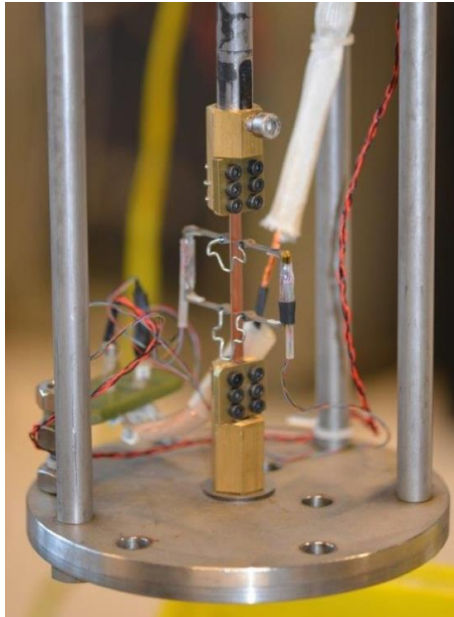
Buffer and silver layers excluded from model  
(minor influence on tape mechanical behavior)



Model: residual strain in REBCO layer at RT –  $0.17\text{ }\%$ .

Cooling down to  $77\text{ K}$  increases compressive strain further to  $\sim -0.24\text{ }\%$ .

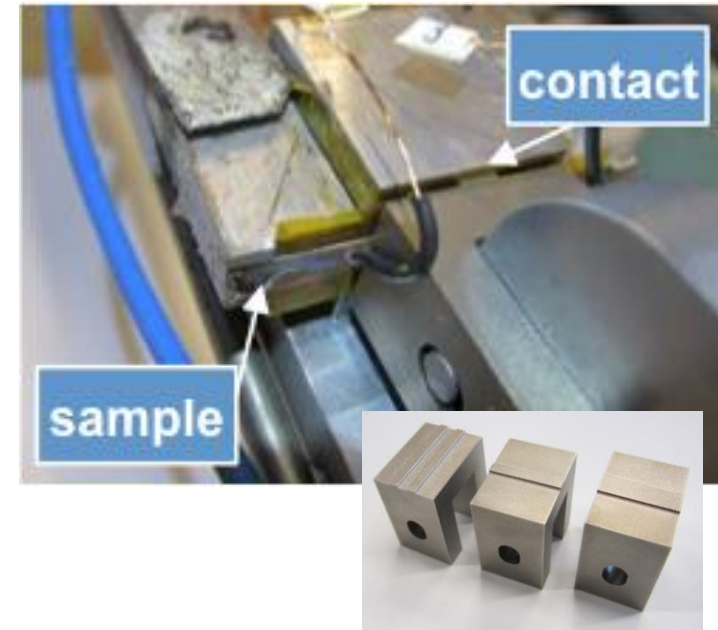
# Tape strain test setups



Tensile axial stress-strain for thermo-mechanical material properties of tape components (copper, hasteloy)



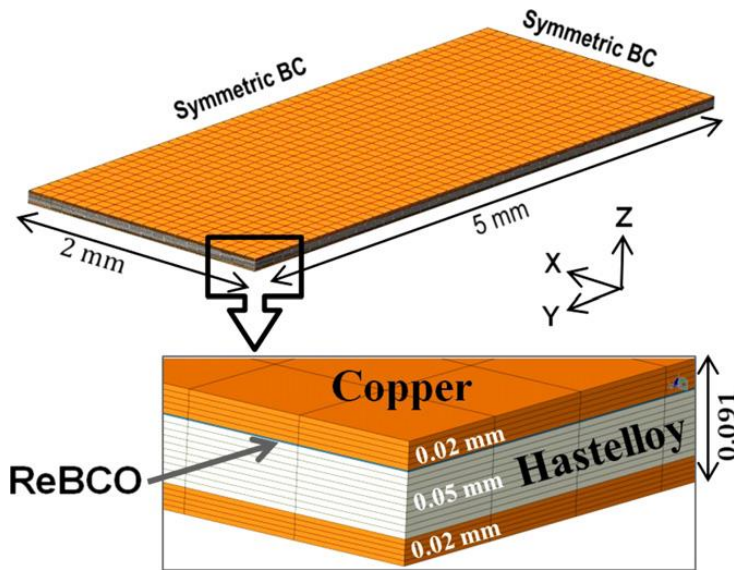
Combined controlled torsion + tensile axial stress



Transverse stress with different loading profiles

# Simulation and experiment: tensile

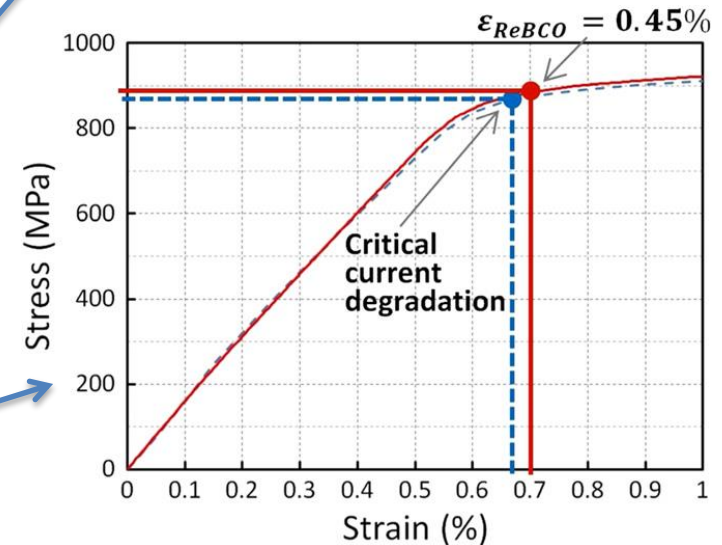
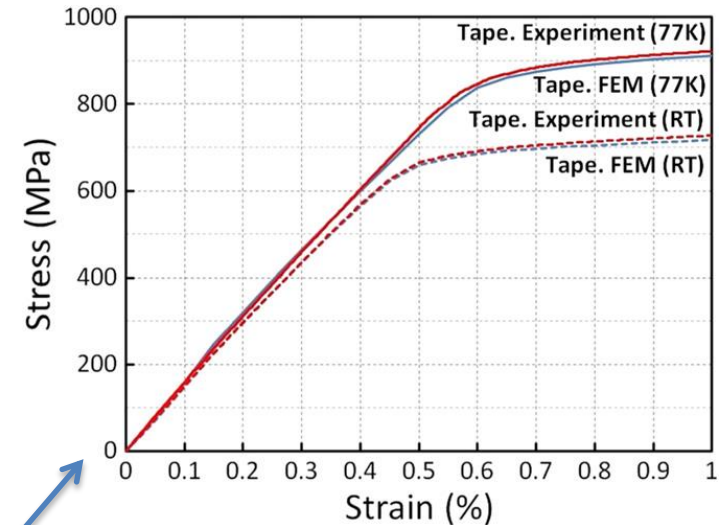
Geometry: FE mesh and boundary conditions



After determining the component properties, good agreement tensile load experiments and modeling results at RT and 77 K.

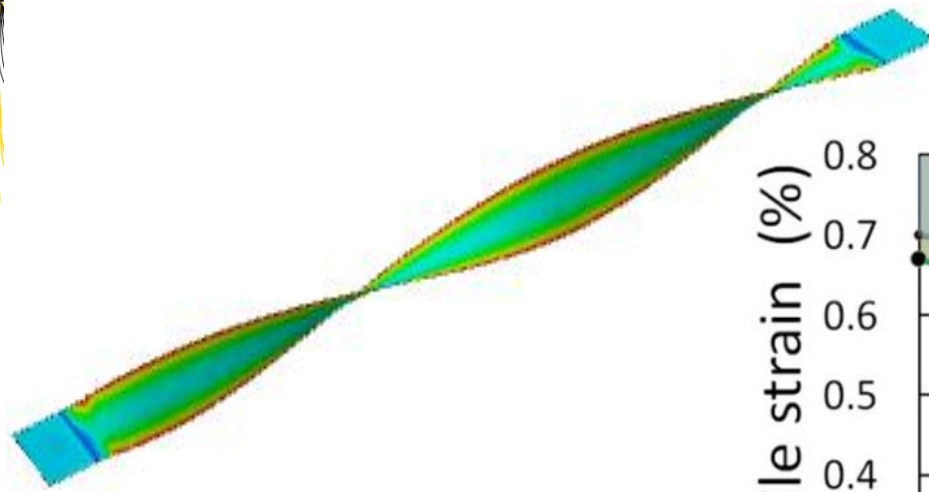
Critical intrinsic tensile strain = 0.45%. (neutron diffraction experiment K. Osamura et al.).

Results **FEM** and **experiment** at 77 K.



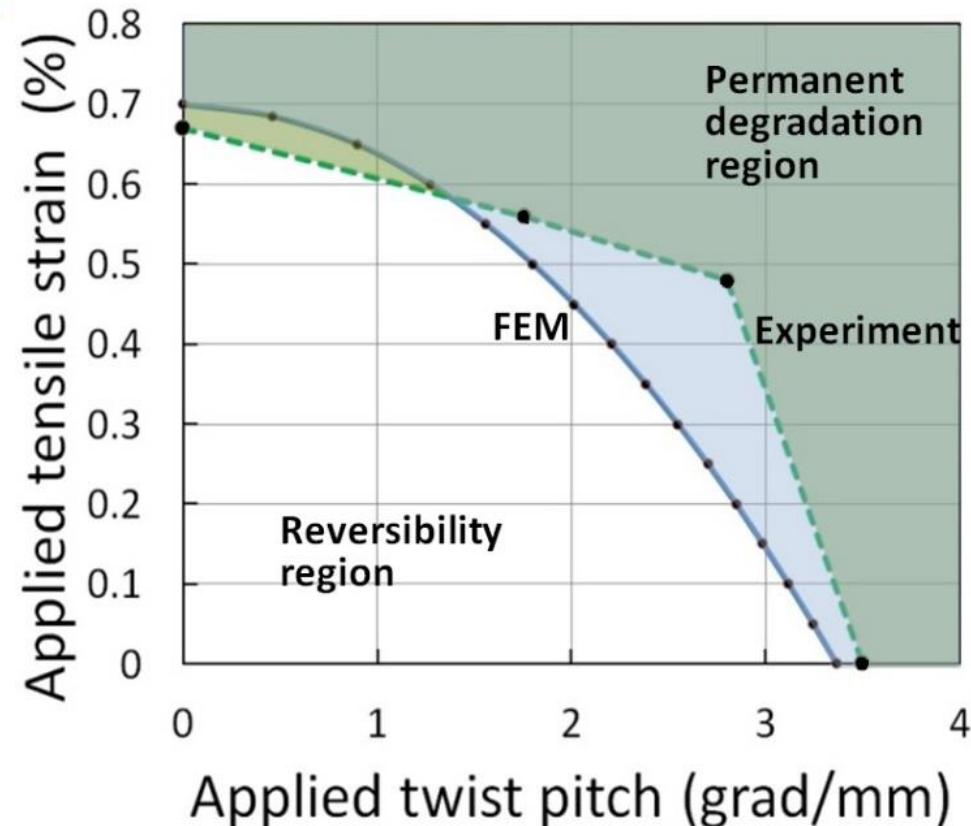
# Simulation and experiment: tensile + torsion

FEM simulation: Tensile + Torsion at 77 K, with longitudinal strain in REBCO layer

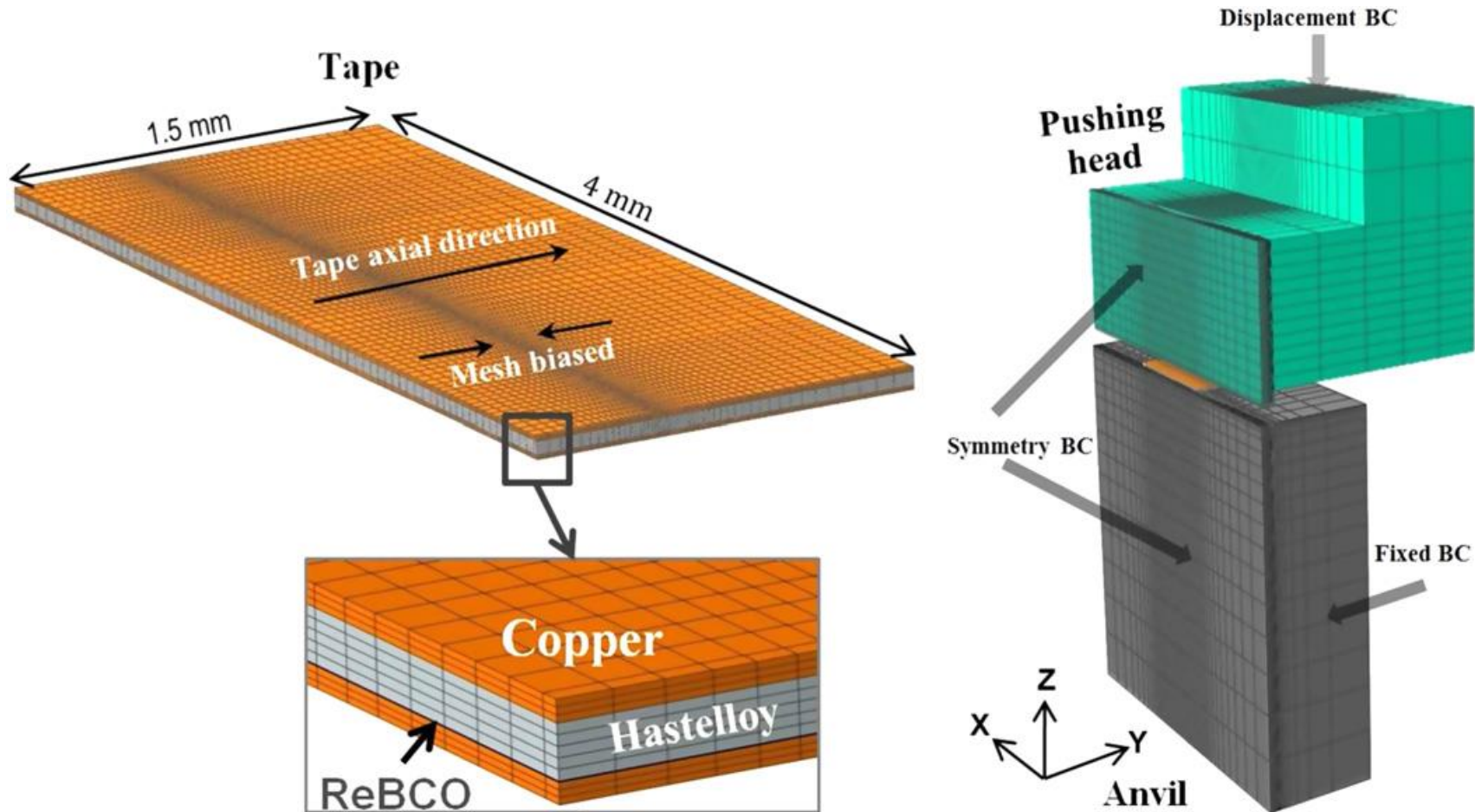


FEM computation: critical strain in REBCO layer as a function of applied external tensile strain and applied torsion strain at 77 K

Experimental:  $I_c$  measurement with 10  $\mu\text{V/m}$  criterion (less sensitive with increasing torsion)



# FEM transverse load

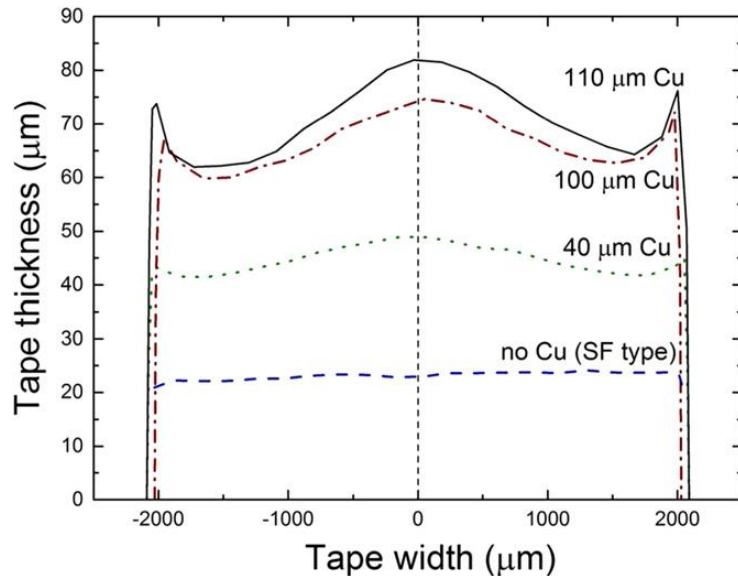


Extensive FE mesh of tape, anvil and pushing head, since deformation of all parts is important

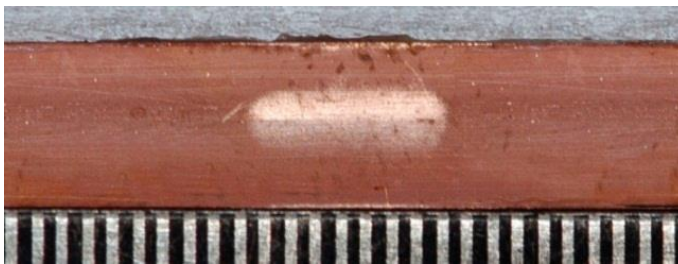
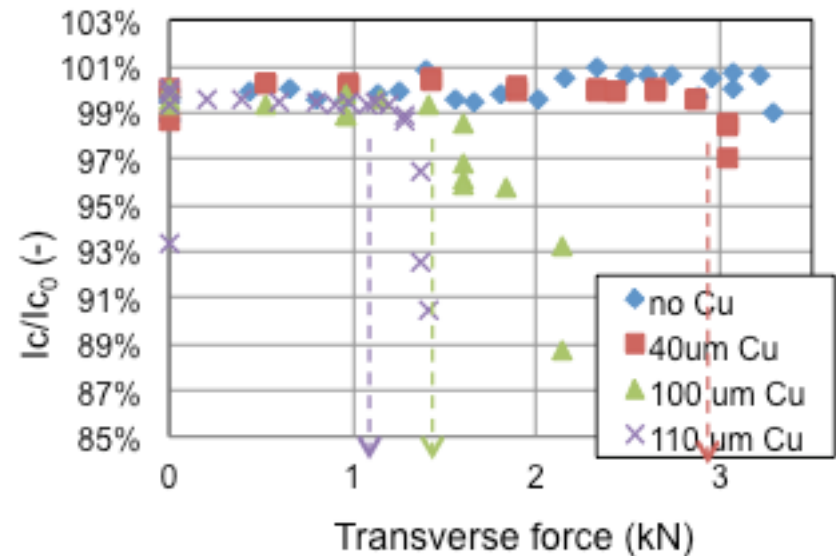
UNIVERSITY OF TWENTE.

# Tape thickness variation, transverse stress

SEM analysis of tape thickness



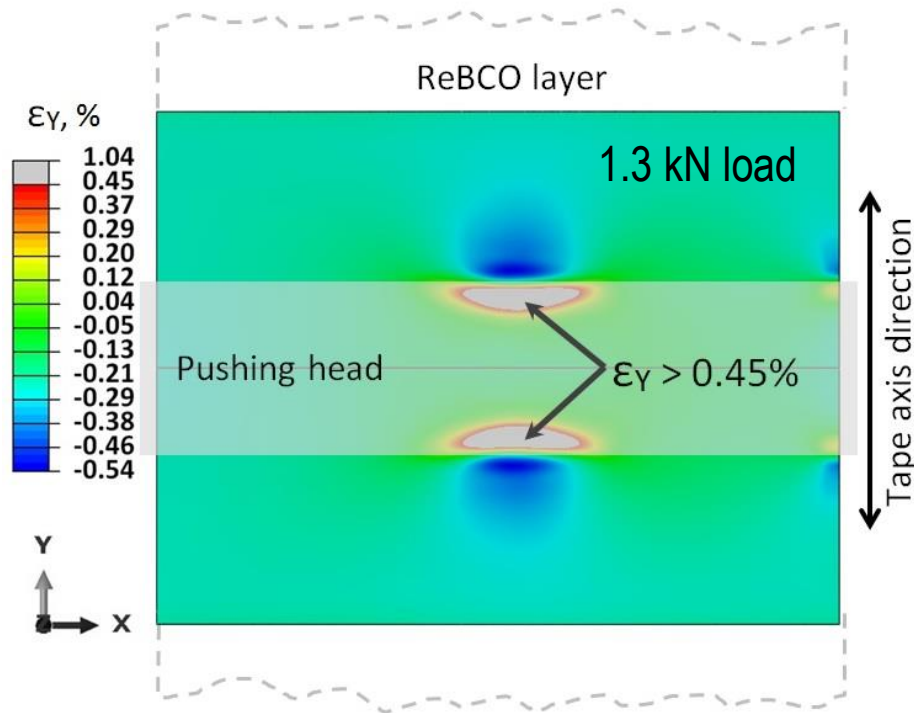
$I_c$  degradation vs tape thickness



4 mm pushing head (40 μm Cu)

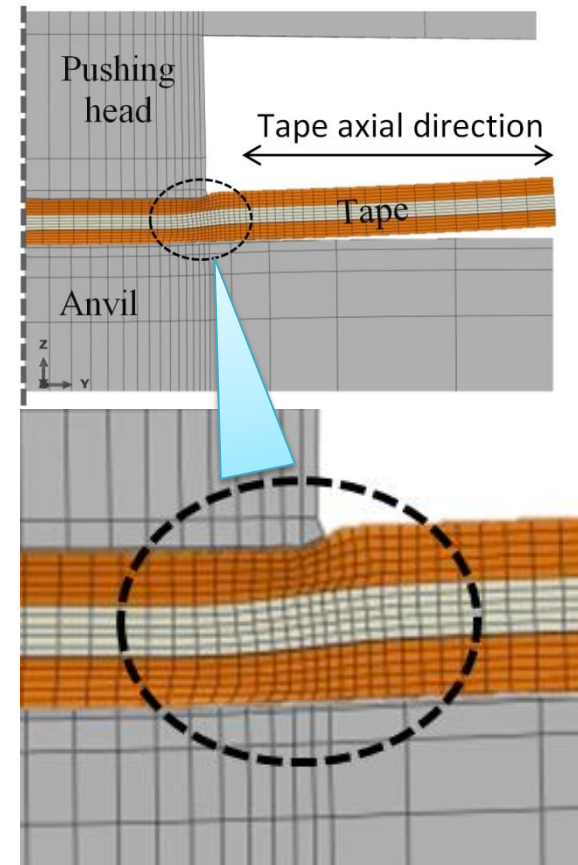
- Copper thickness not uniform over tape width.
- How much is influence of copper thickness, how much of inhomogeneity?

# FEM transverse load, thickness copper

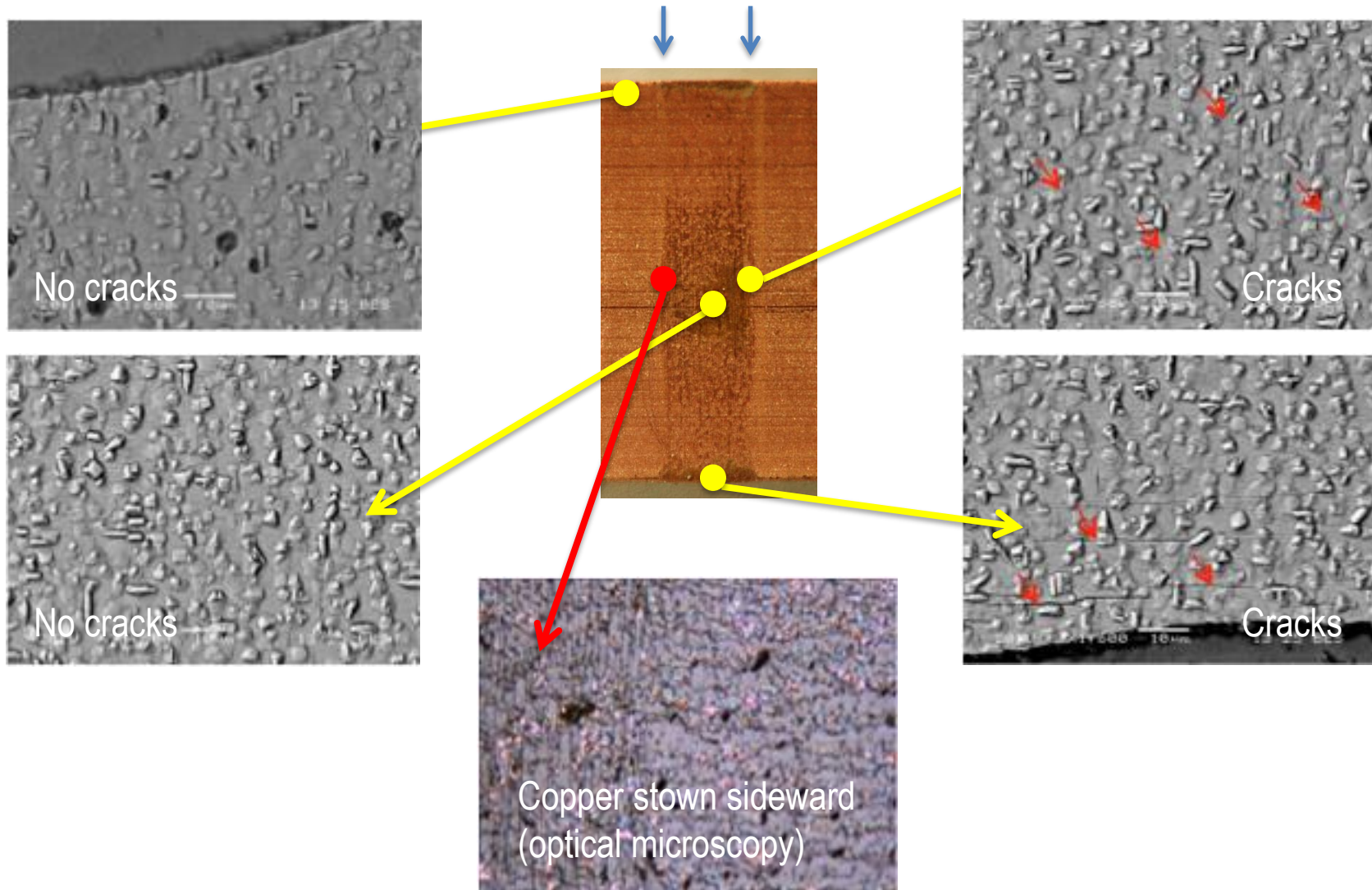


In plane strain in REBCO layer calculated using 100  $\mu\text{m}$  copper thickness.

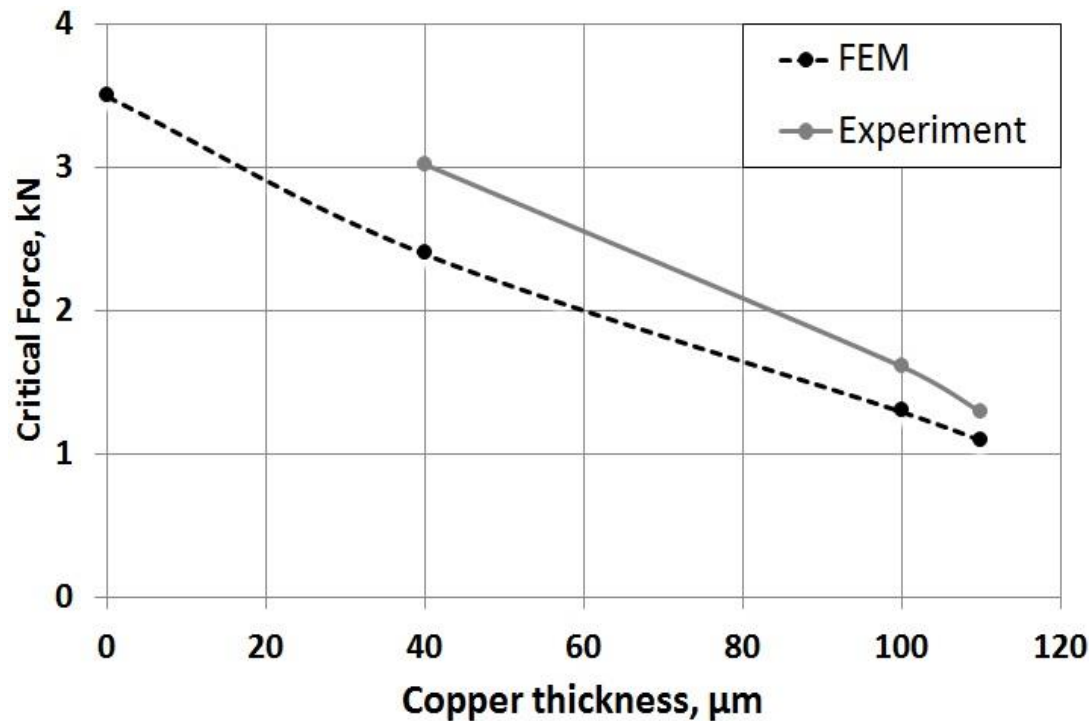
- The strain concentration areas are localized at boundaries of the pushing head
- Copper starts flowing in outward direction, increasing strain in REBCO plane



# Transverse stress SEM micrographs



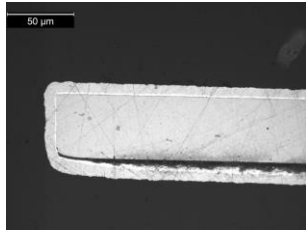
# Transverse load, FEM versus experiment



Critical force as a function of copper layer thickness at 77K. FEM model and experimental results.

Measured Cu thickness profiles are used for FEM computation

# Transverse load: Cu thickness & profiles

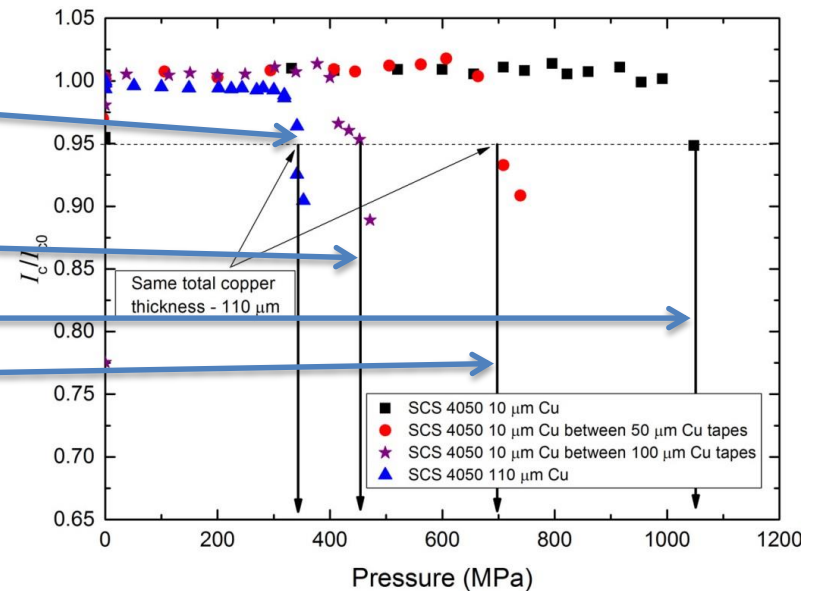
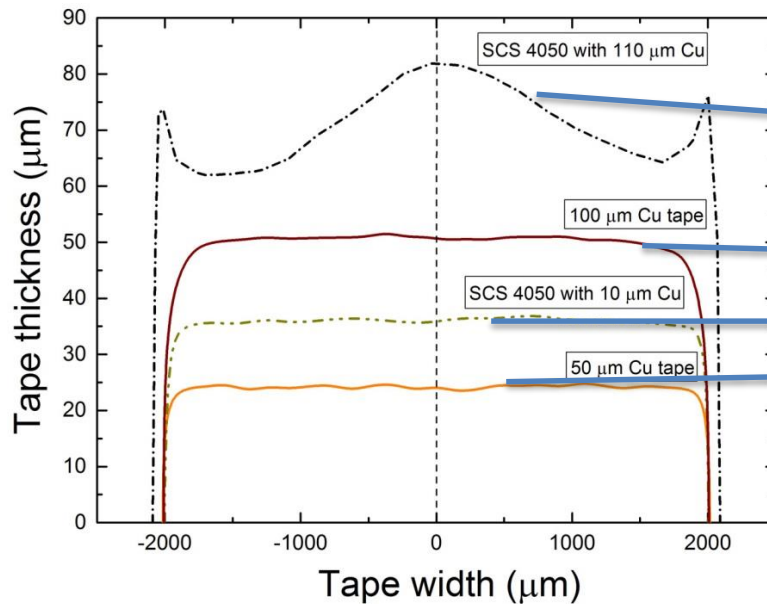


50 µm Cu tape  
100 µm Cu tape

Super power<sup>®</sup> 2G SCS4050 with 10 µm Cu layer

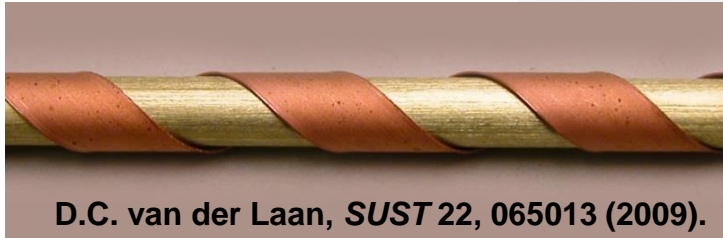


No “dog boning” effect, uniform tape thickness is over width.

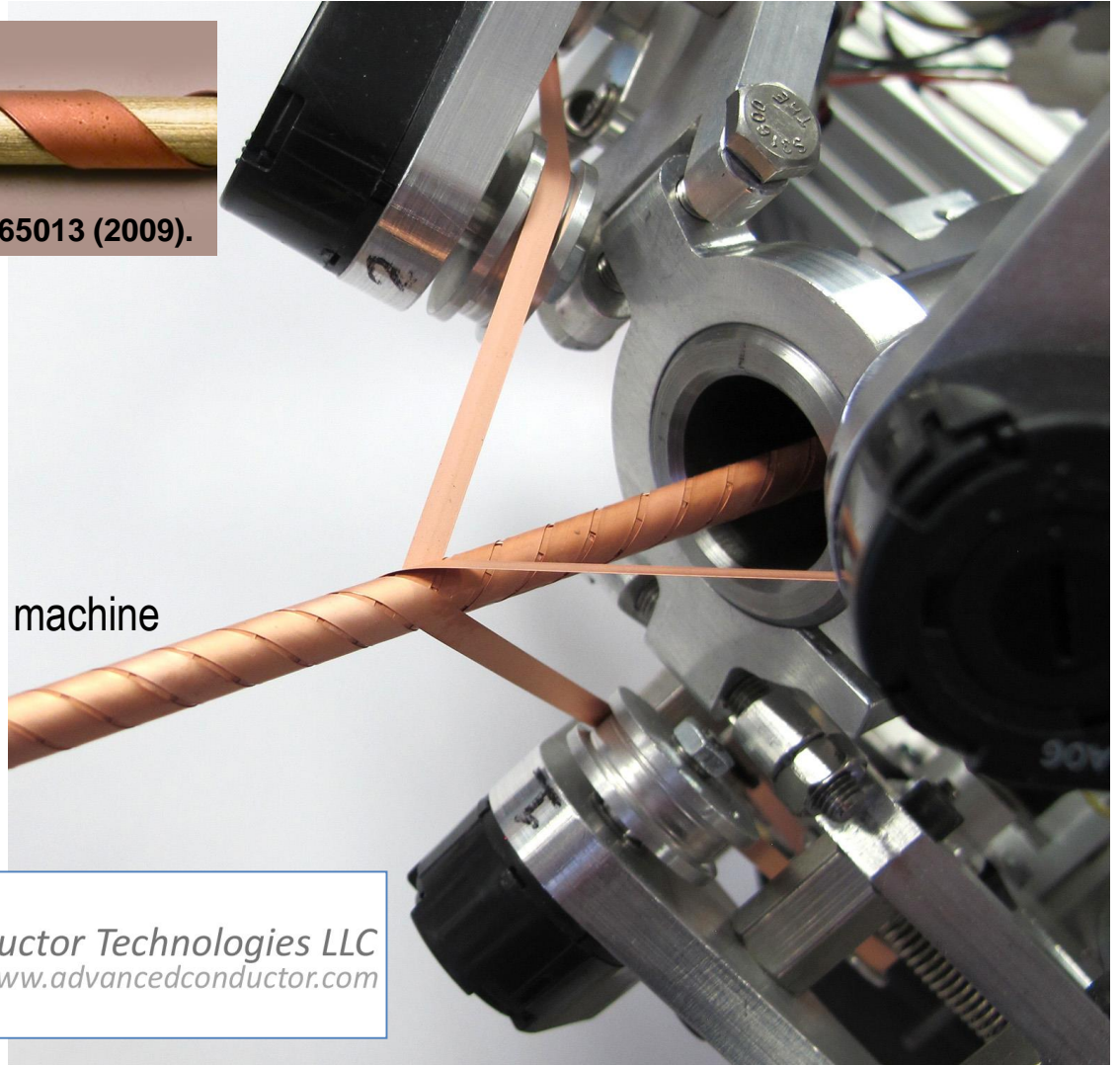


Both, copper layer thickness and surface homogeneity play a role, thickness-Cu most.

# CORC cable

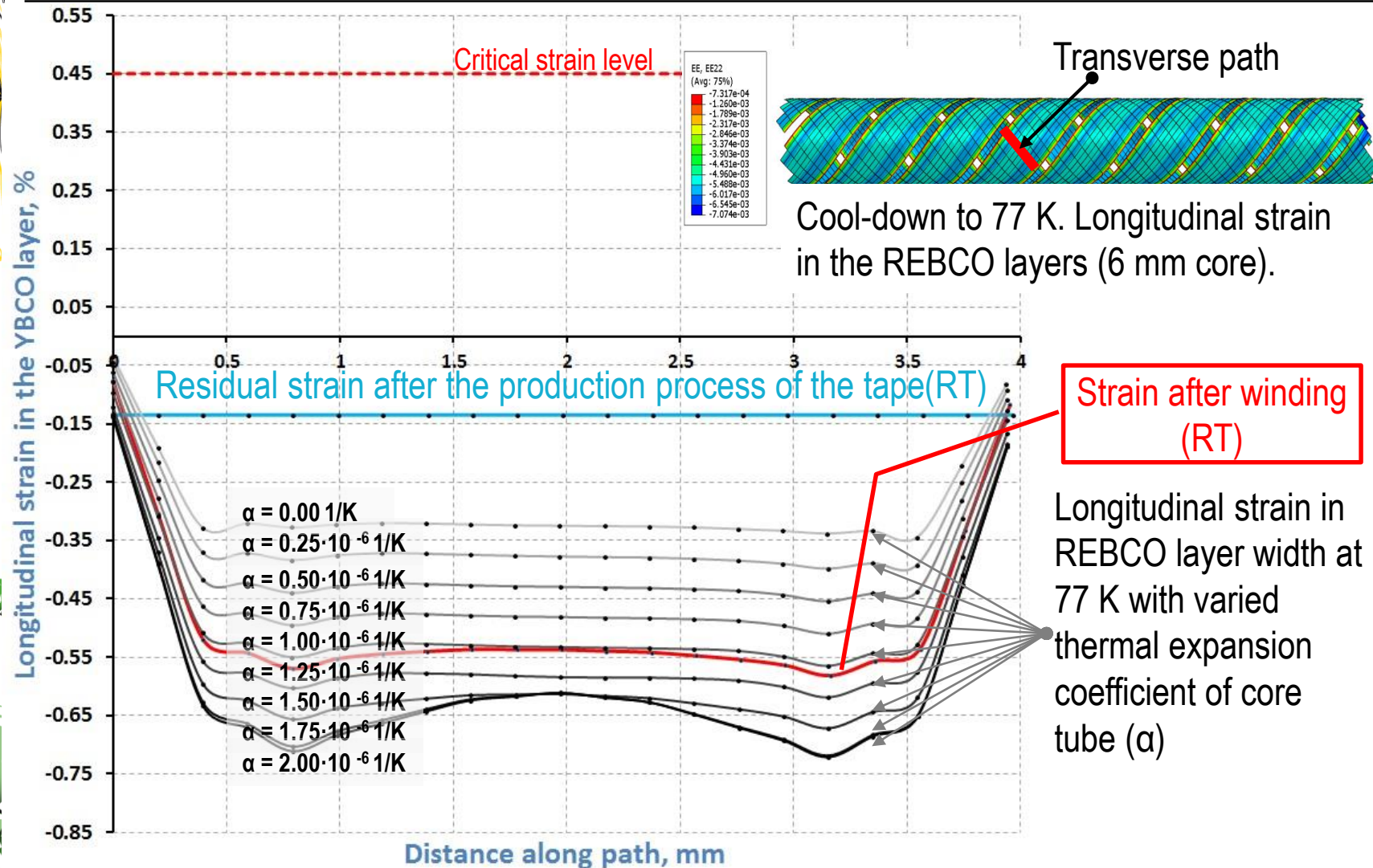


Cable winding machine



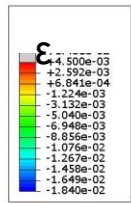
*Advanced Conductor Technologies LLC*  
[www.advancedconductor.com](http://www.advancedconductor.com)

# CORC cable FE modeling: cool down

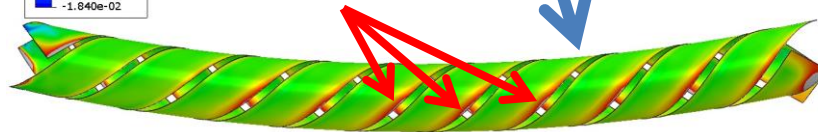


# Bending one layer CORC cable (3 tapes)

Cable bending radius  
 $R = 200$  mm



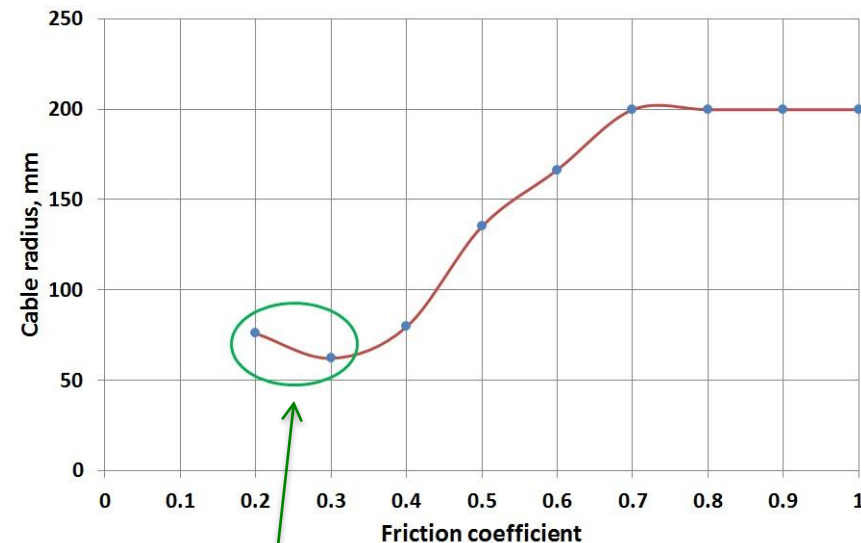
$\epsilon_{irr} = 0.45\%$



Strain along tape direction in REBCO at  
cable radius  $R = 200$  mm and  $\mu = 1$   
(cable core 6 mm)

Variable parameter:

$\mu$  – friction coefficient tape-core interface



Bending  $R$  for  $\epsilon = 0.45\%$  versus friction coefficient

For  $\mu = 0.2$  and  $0.3$  no convergence reached in computation


Work in progress .... but use of lubricant to reduce  $\mu$  seems a good idea ...



# Summary

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- Systematic studies performed on SCS4050 REBCO tape under tensile, torsion and transverse load.
- Tape FE model validated against experiments.
- Homogeneity of tape surface but mostly thickness of copper layer plays significant role in allowable transverse peak load.
- CORC modeling in progress for cable and core optimization.



K Ilin, K A Yagotintsev, C Zhou, P Gao, J Kosse, S J Otten, W A J Wessel, T J Haugan, D C van der Laan, and A Nijhuis, "Experiments and FE modeling of stress–strain state in ReBCO tape under tensile, torsional and transverse load", *Supercond. Sci. Technol.* 28 (2015) 055006 (17pp) doi:10.1088/0953-2048/28/5/055006