

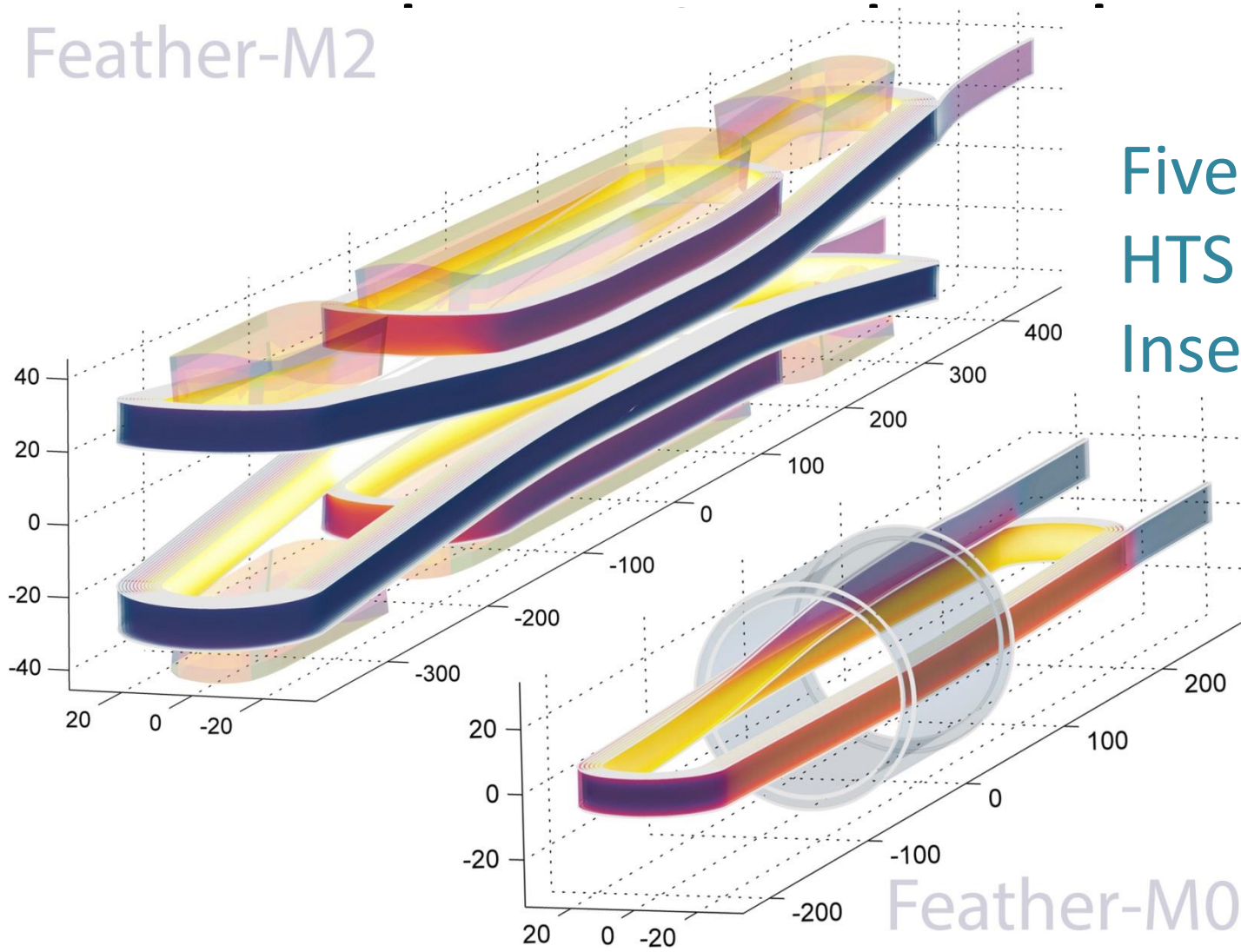
HTS Magnet Testing



Over view

- Feather Zero & Two reminder
- High temperature margin
- Testing at high temperature 60K in gas.
- Magnetic field Harmonics.
- Magnet Quench calculations.
- Test requirements

Feather-M2

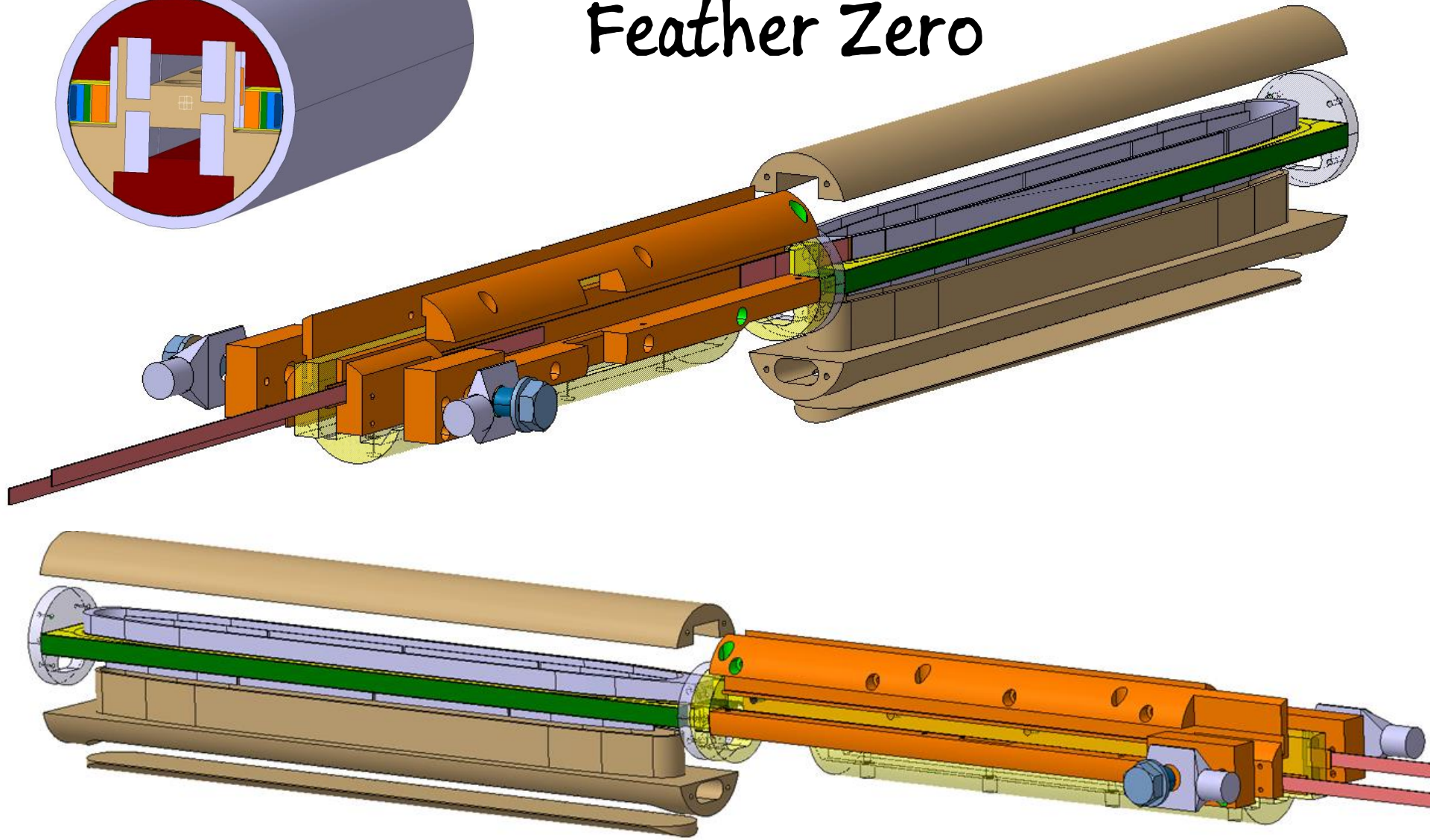
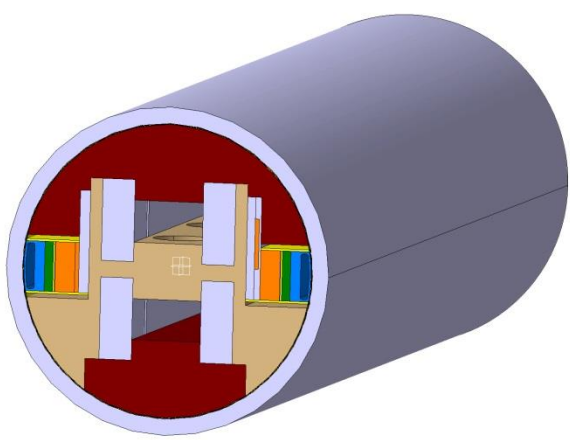


M2

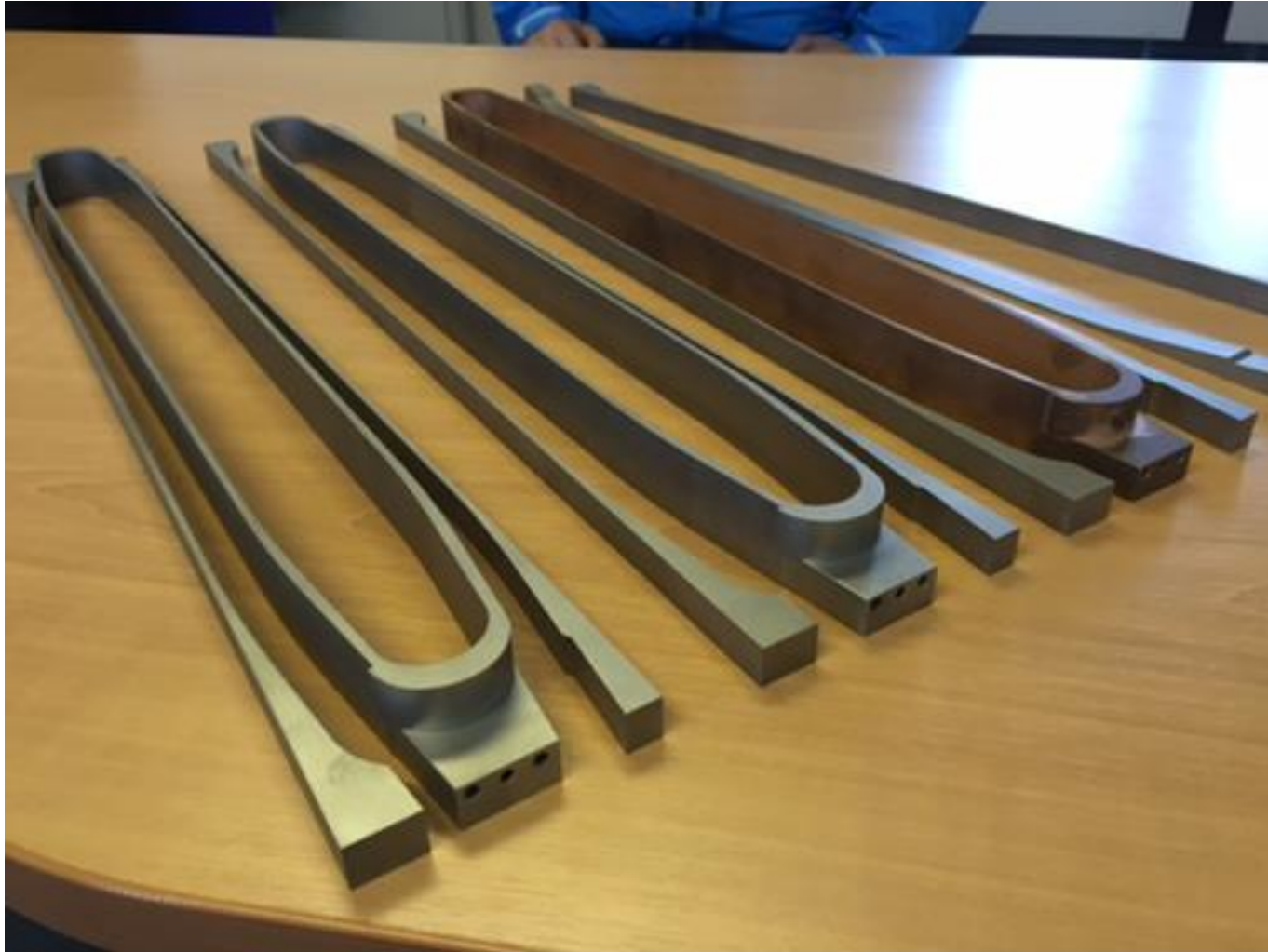
Five Tesla
HTS Research
Insert-Magnet

Feather-M0

Feather Zero

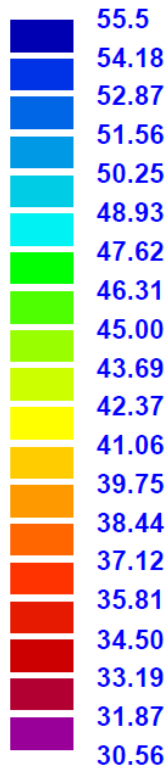


Feather Zero parts

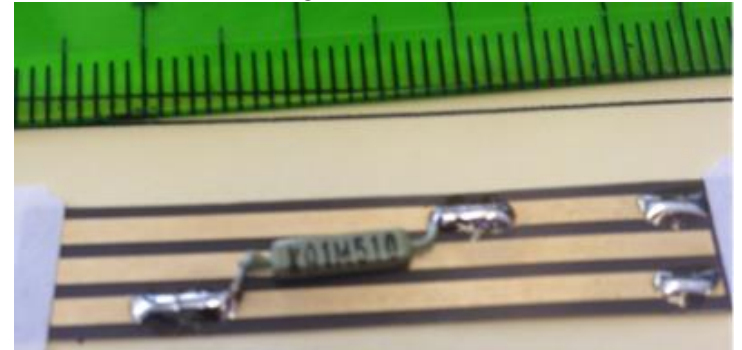
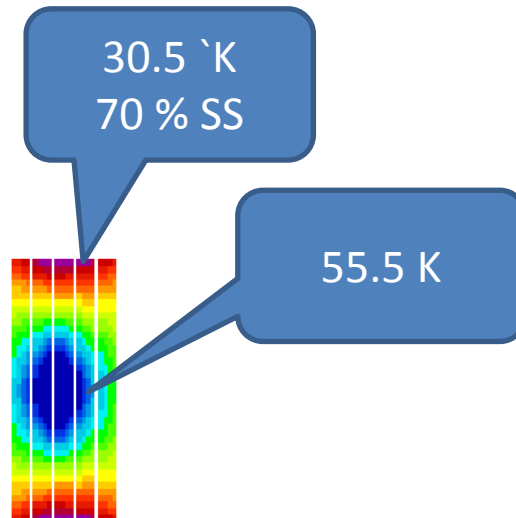


10 kA Temperature margin

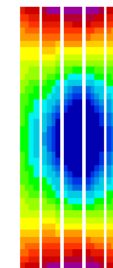
Temperature margin (at Jop,Bop,Top)(K)



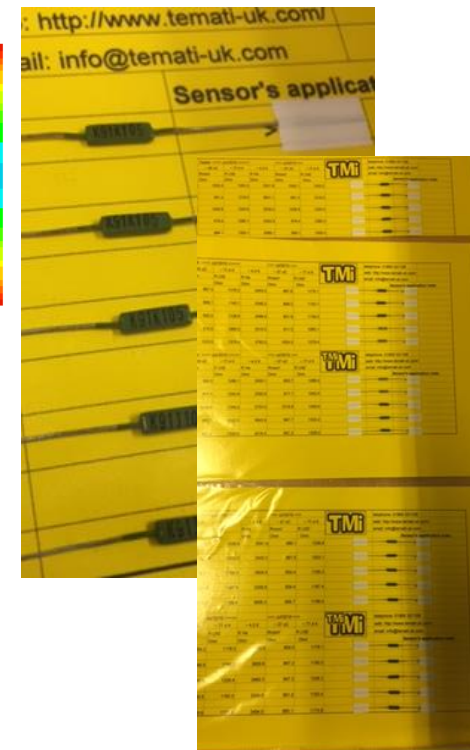
ROXIE_{10.2}



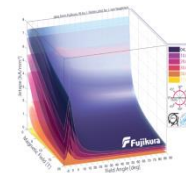
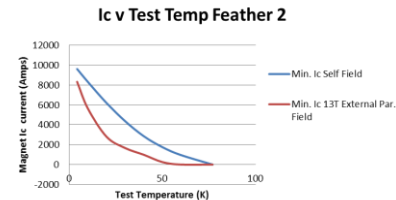
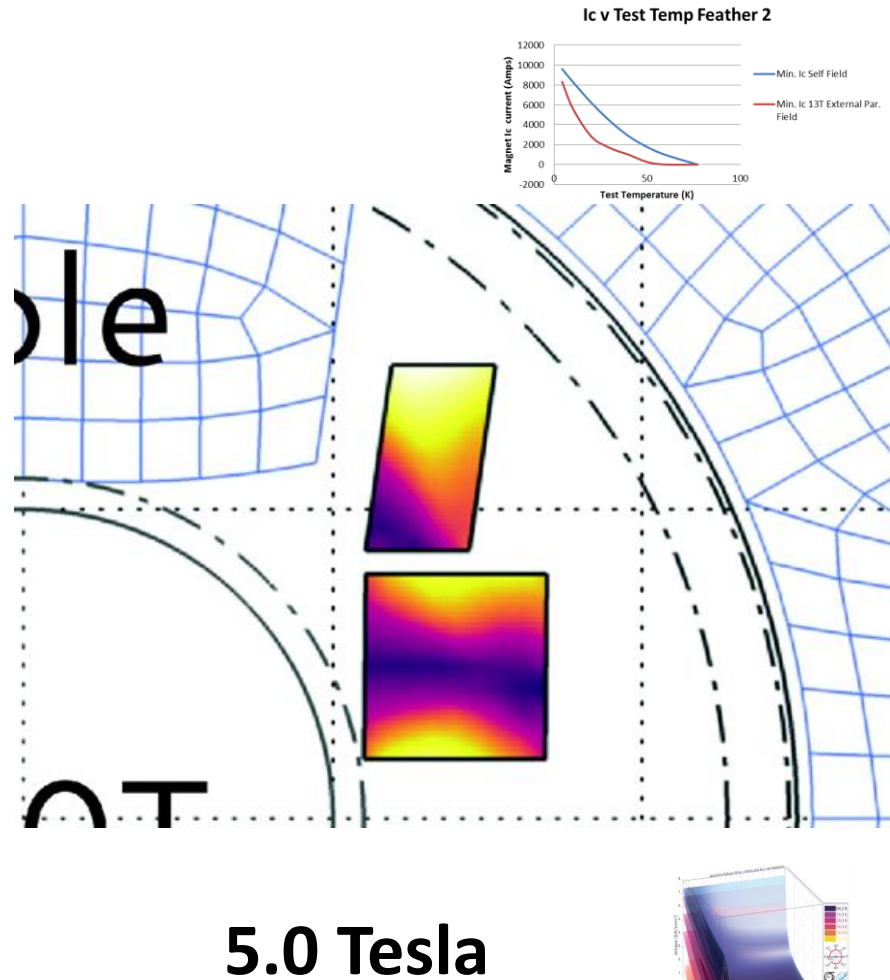
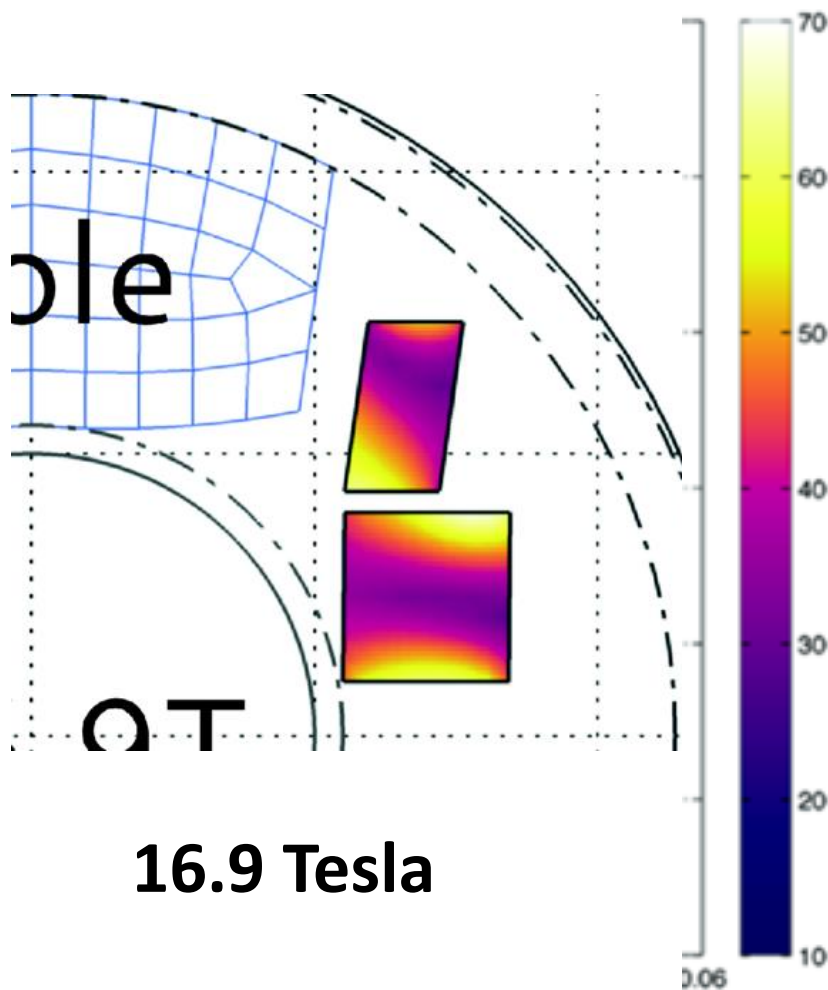
Temp. sensor CCS



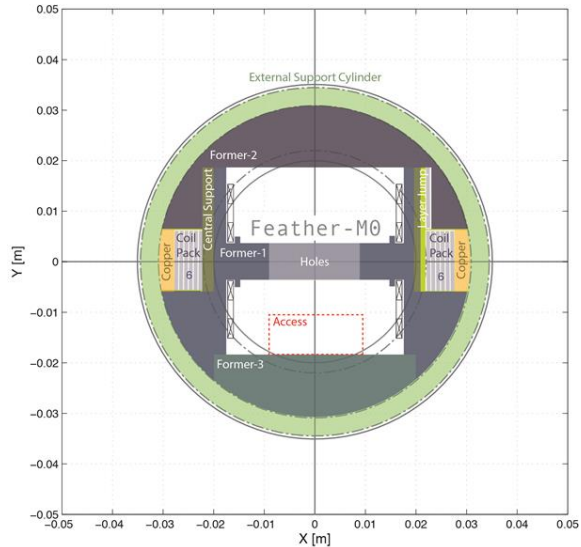
Large temperature margin can we use this for quench detection?



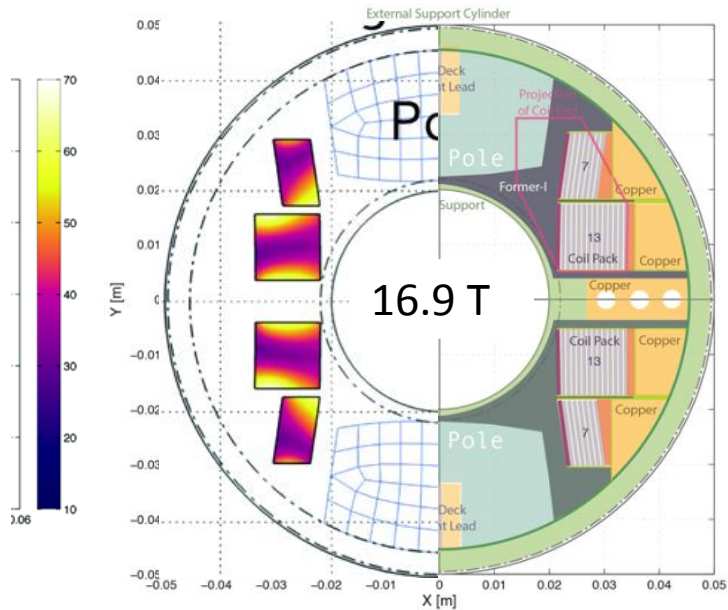
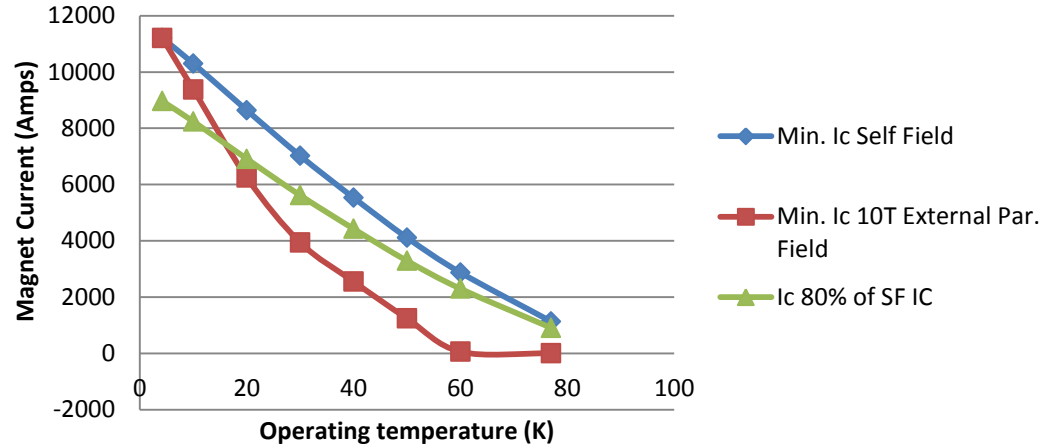
Position of short sample in coil



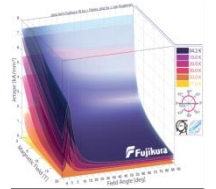
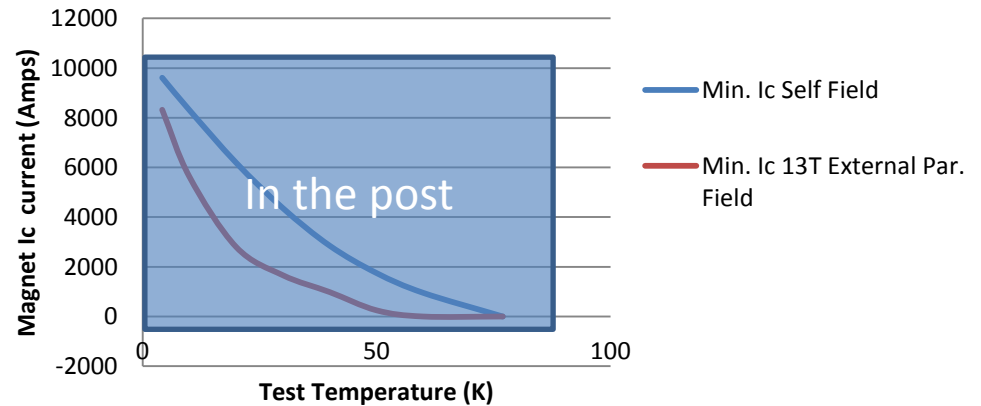
Ic v Test temperature



Feather Zero Ic. f(temp)

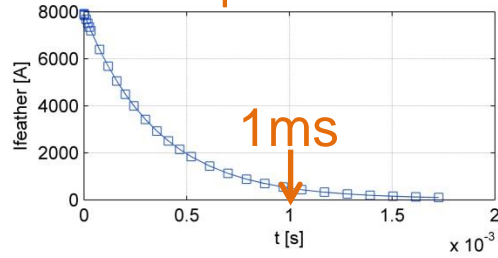


Ic v Test Temp Feather 2

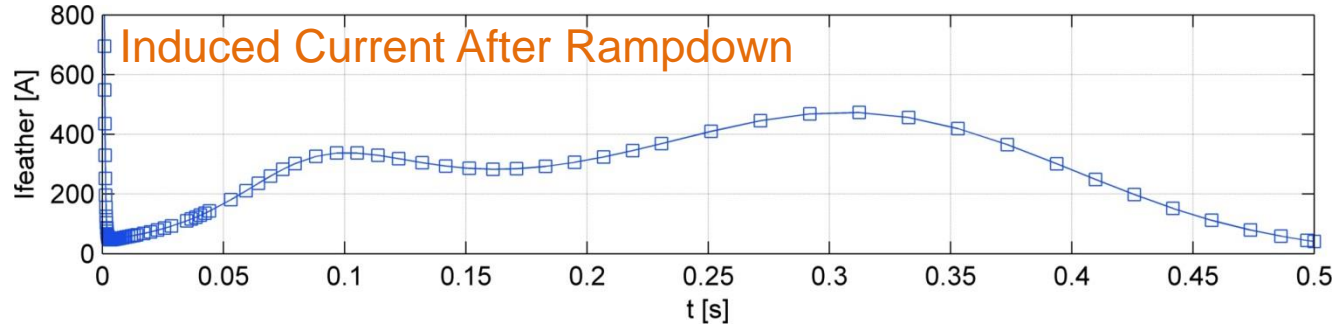
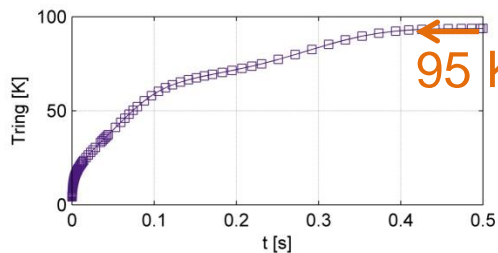
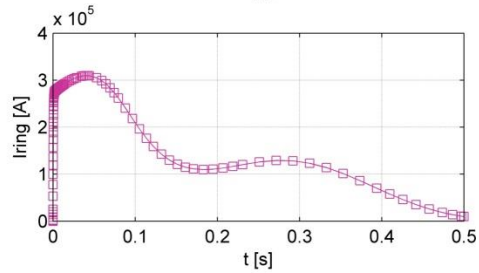
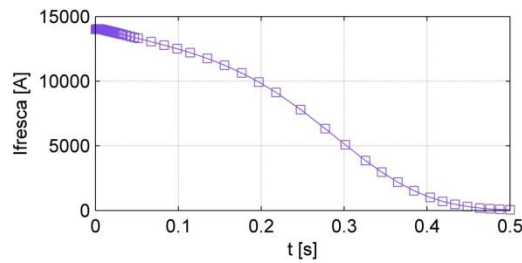
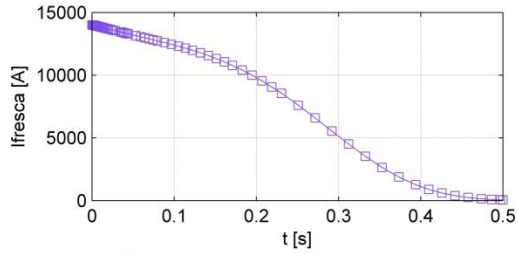
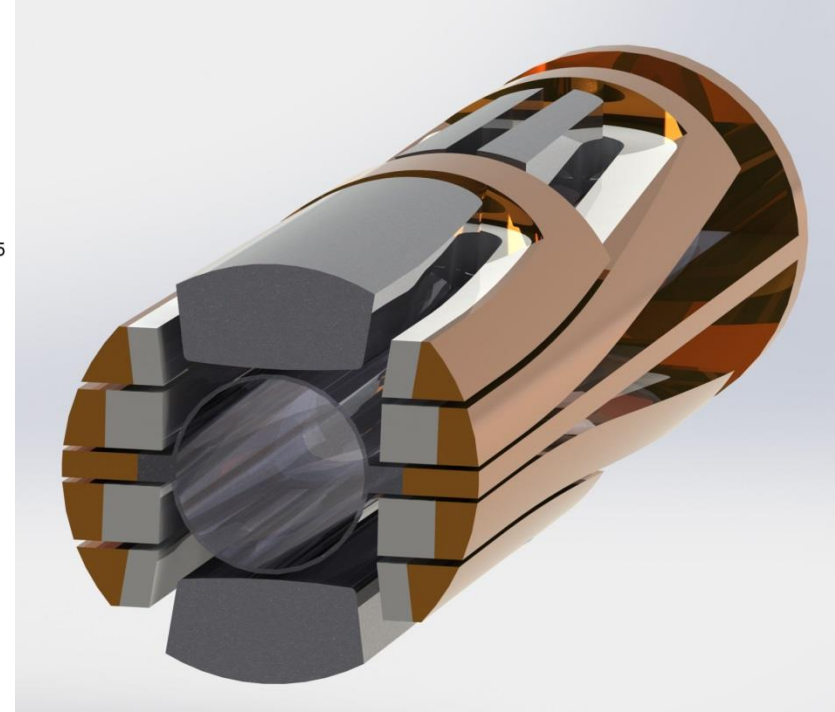
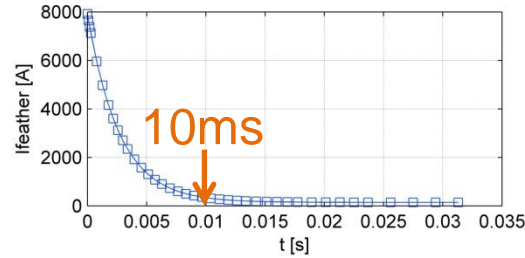


Quench Protection with Copper ICEE Loops

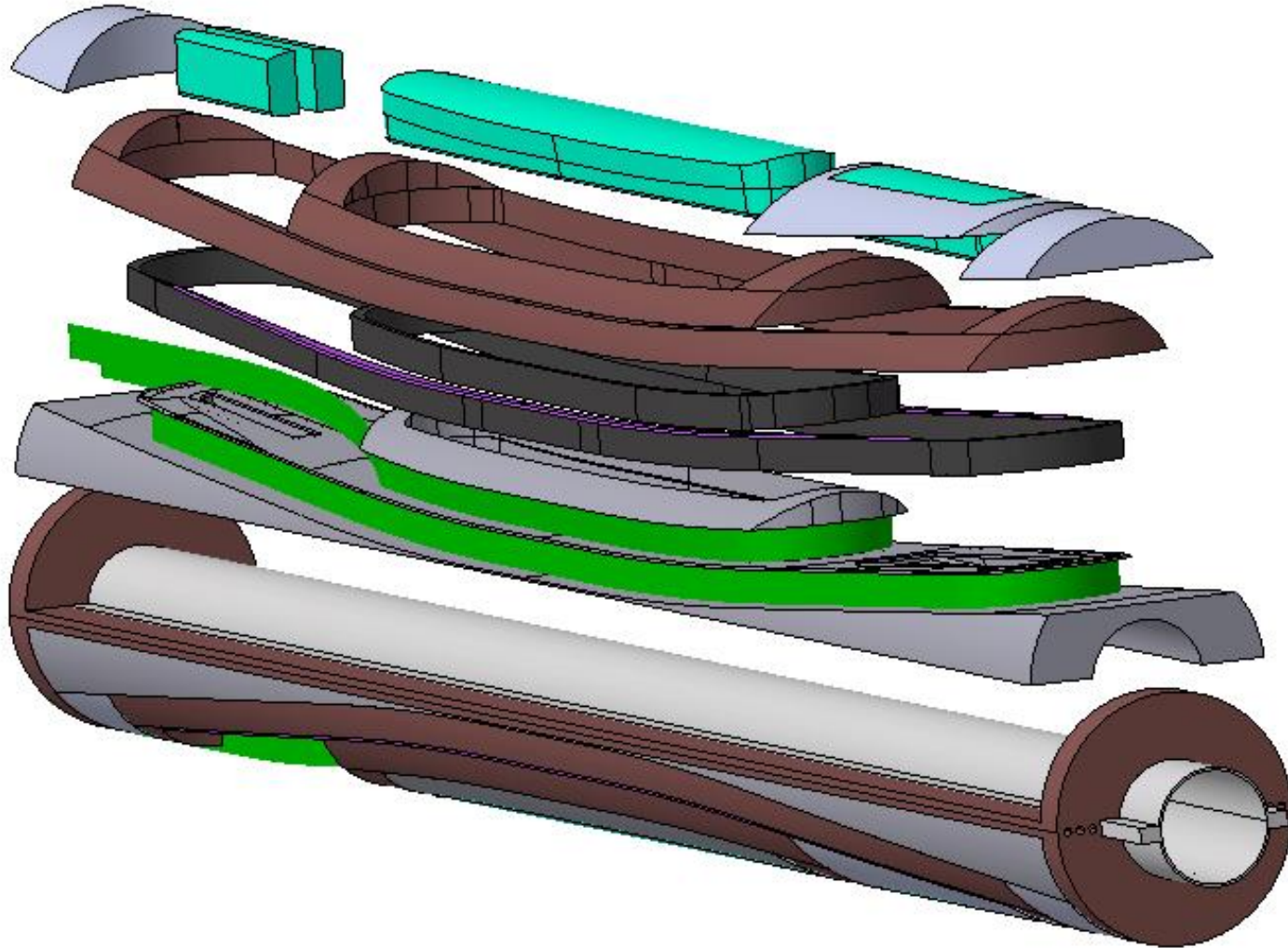
With Loops



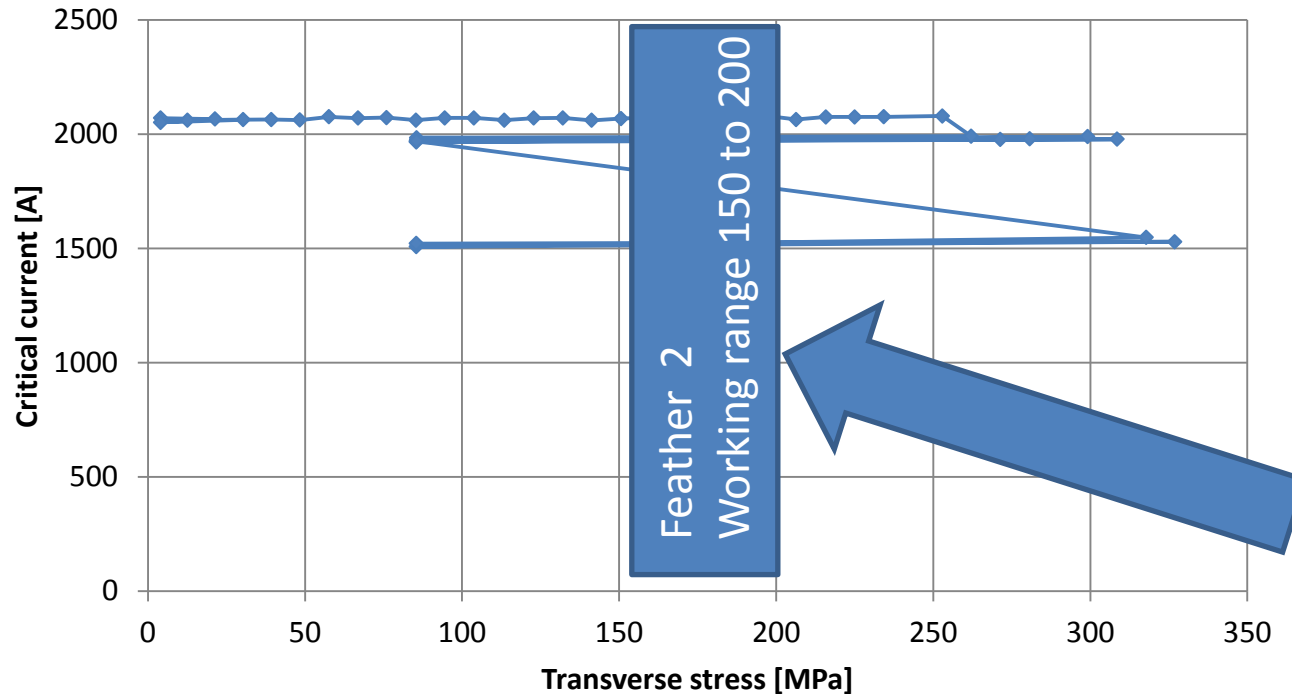
Without Loops



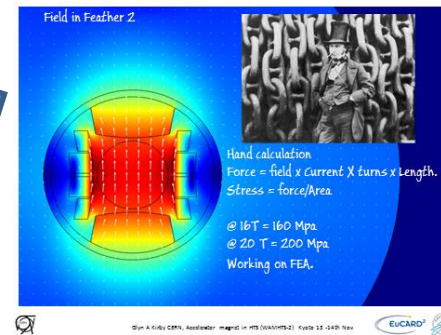
Review of Feather 2 components



I_c versus transverse stress



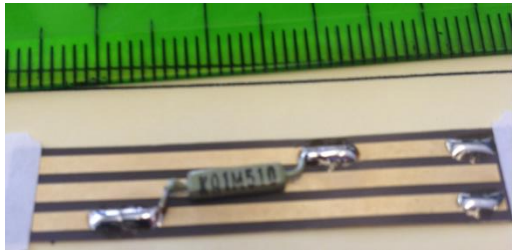
$T = 4.2 \text{ K}$
 $B = 10.5 \text{ T}$



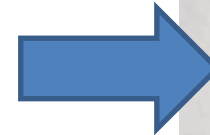
- No degradation up to 253 MPa
- Degradation at higher pressures is irreversible

Quench detection

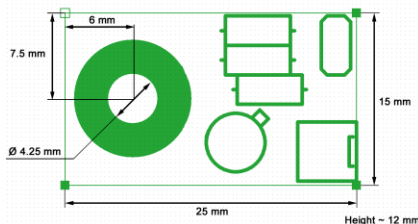
- Voltage taps (**low current**)
- Temperature sensors (high current)



- Pickup coils high current (Feather zero trial)

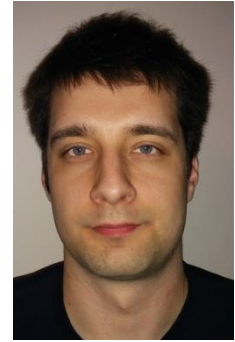


- Acoustics

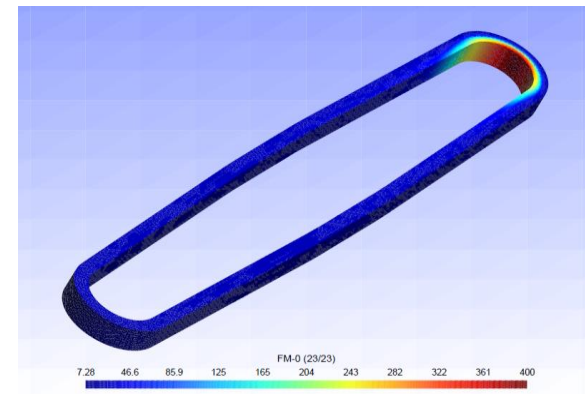
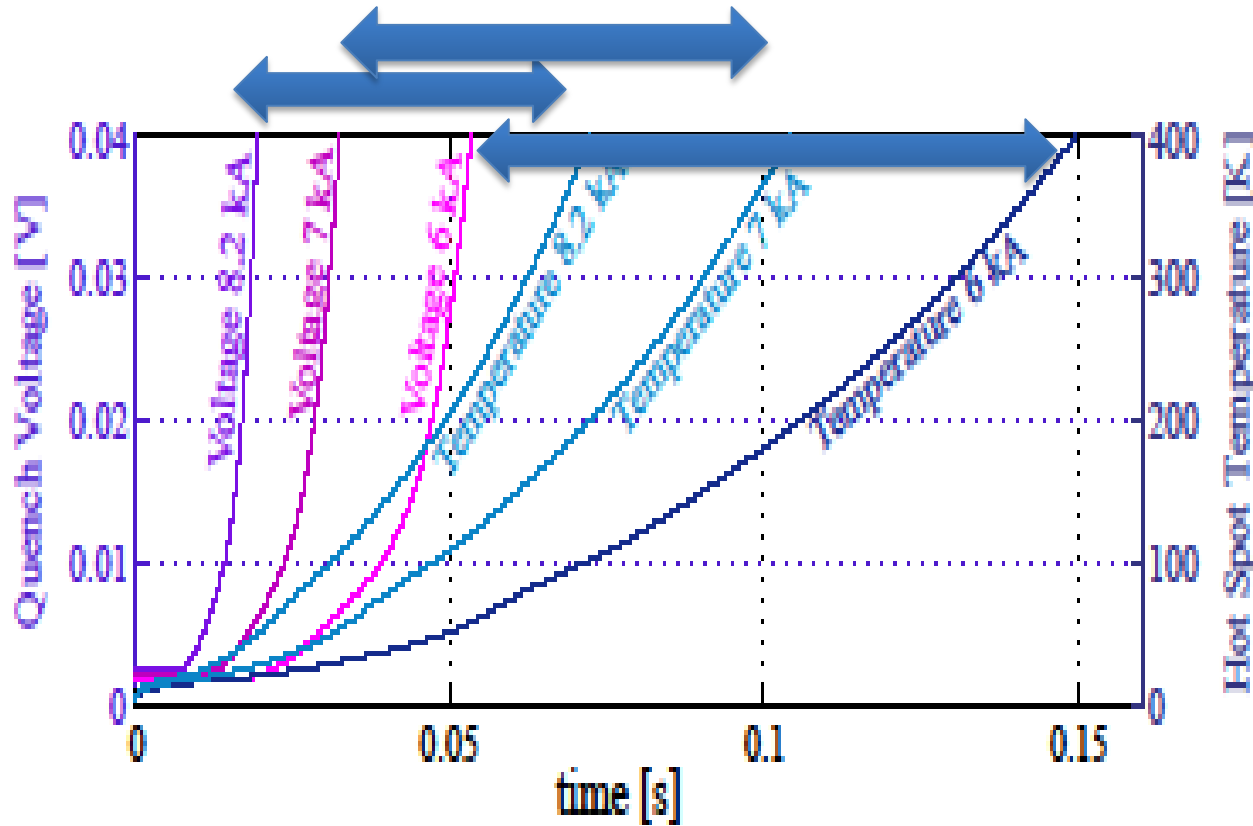


Thanks to Maxim Marchevsky at LBL

Feather-MO Quench Behaviour 4.5K f(current)

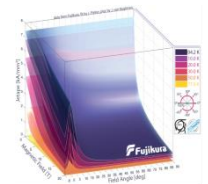


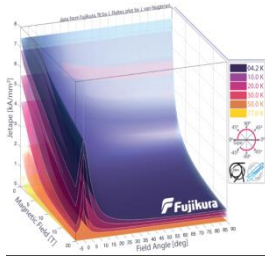
Erkki Härö



Finite Element Model using anisotropic thermal conductivities

Will we be able to see this in the cable ?



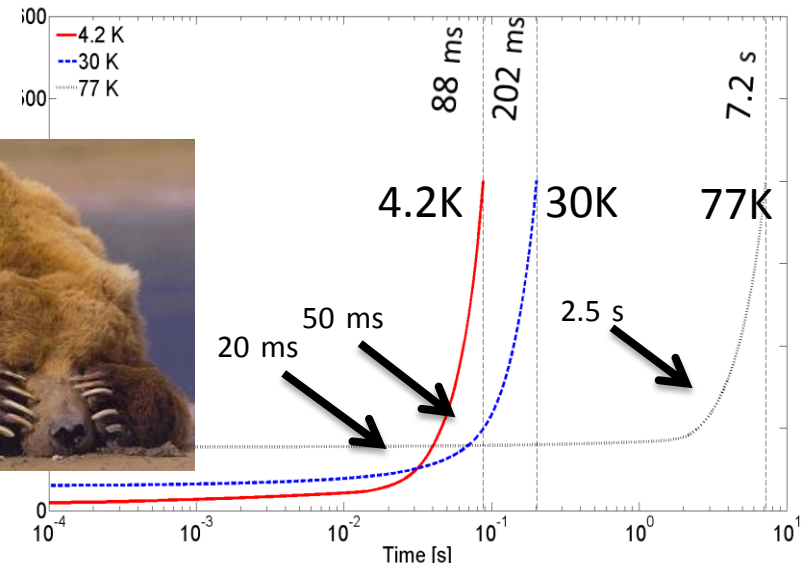
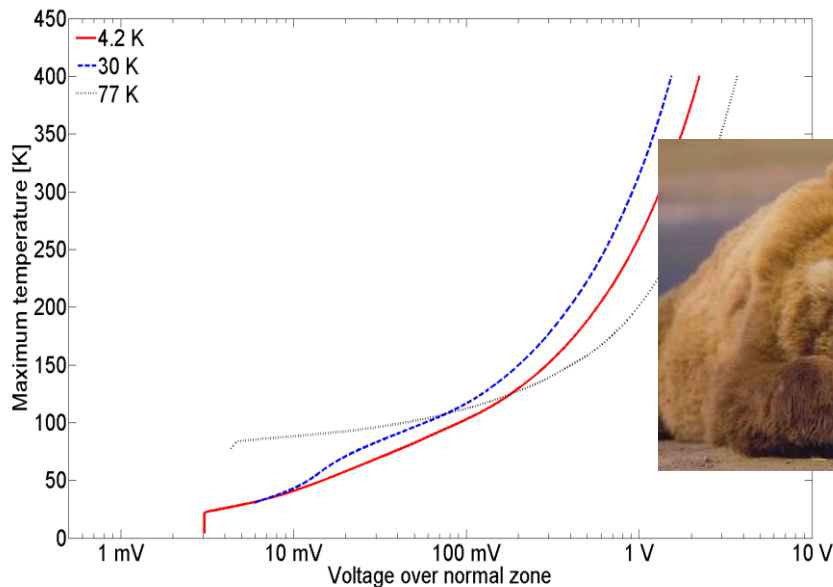


Feather MO Quench Behaviour $f(\text{test temp})$

Quench simulation results for Feather-MO with different operation temperatures: 4.2 K, 30 K and 77 K.

Operation currents with 4.2 K, 30 K and 77 K were 8960 A, 5616 A and 904 A, respectively.

Operation current was chosen to be 80 % of the short sample I_c value.



If we can see it in the Roebel cable and coil

- Current sharing refers to the current distribution between the matrix material and the superconductor provides $VnI(I)$
- In the model three options are available:
 - Pure power law (not useable for quench analysis because only valid below or just above T_{cs})
 - Linear transition between T_{cs} and T_c

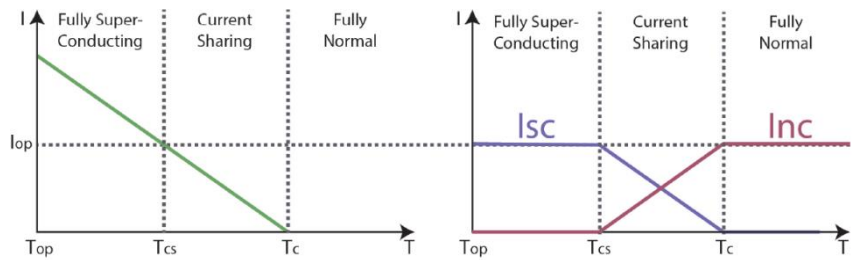
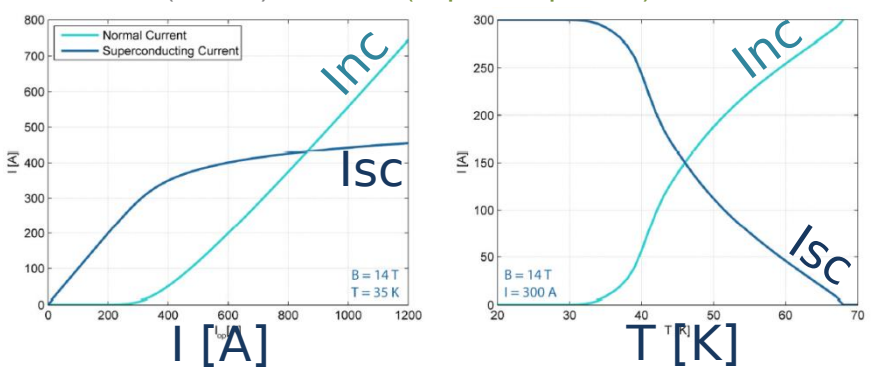
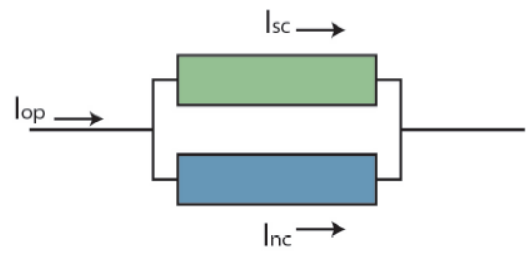


Figure 4.1: Schematic representation of current sharing in a practical superconductor (adapted from Bellis [35]).

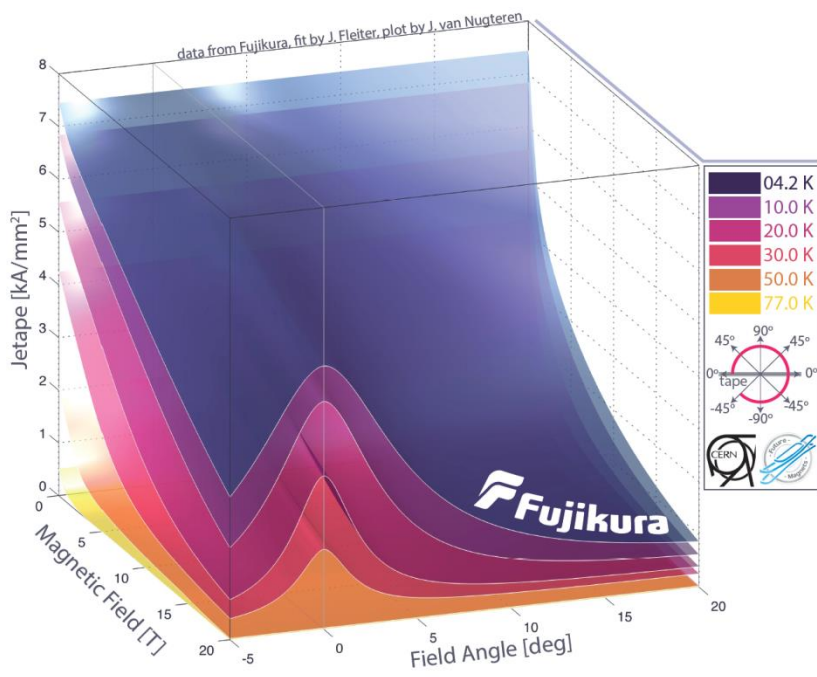
- Superconducting power law element in parallel with resistive (matrix) element (implicit equation)

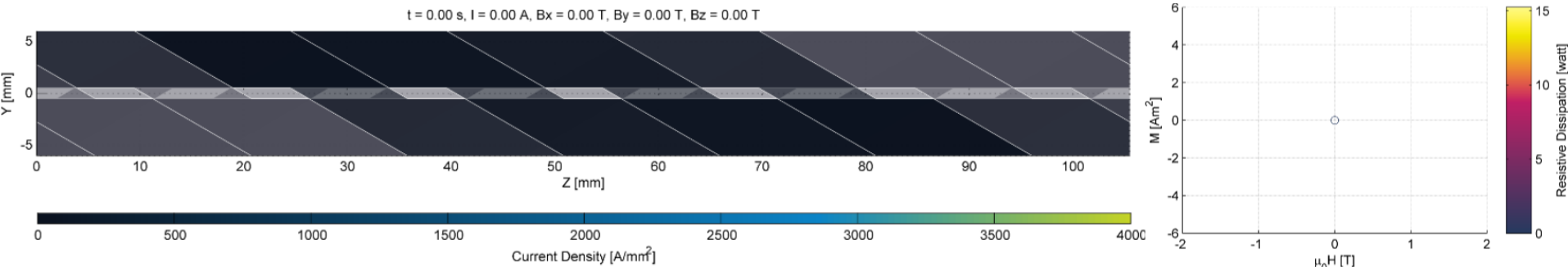


Current Sharing

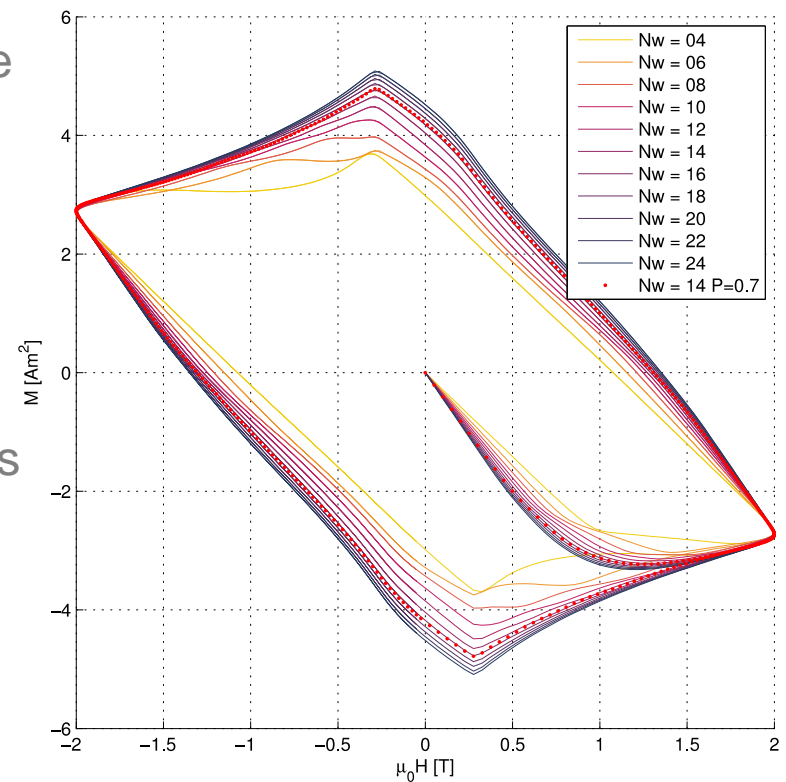


Angular Dependent Critical Current

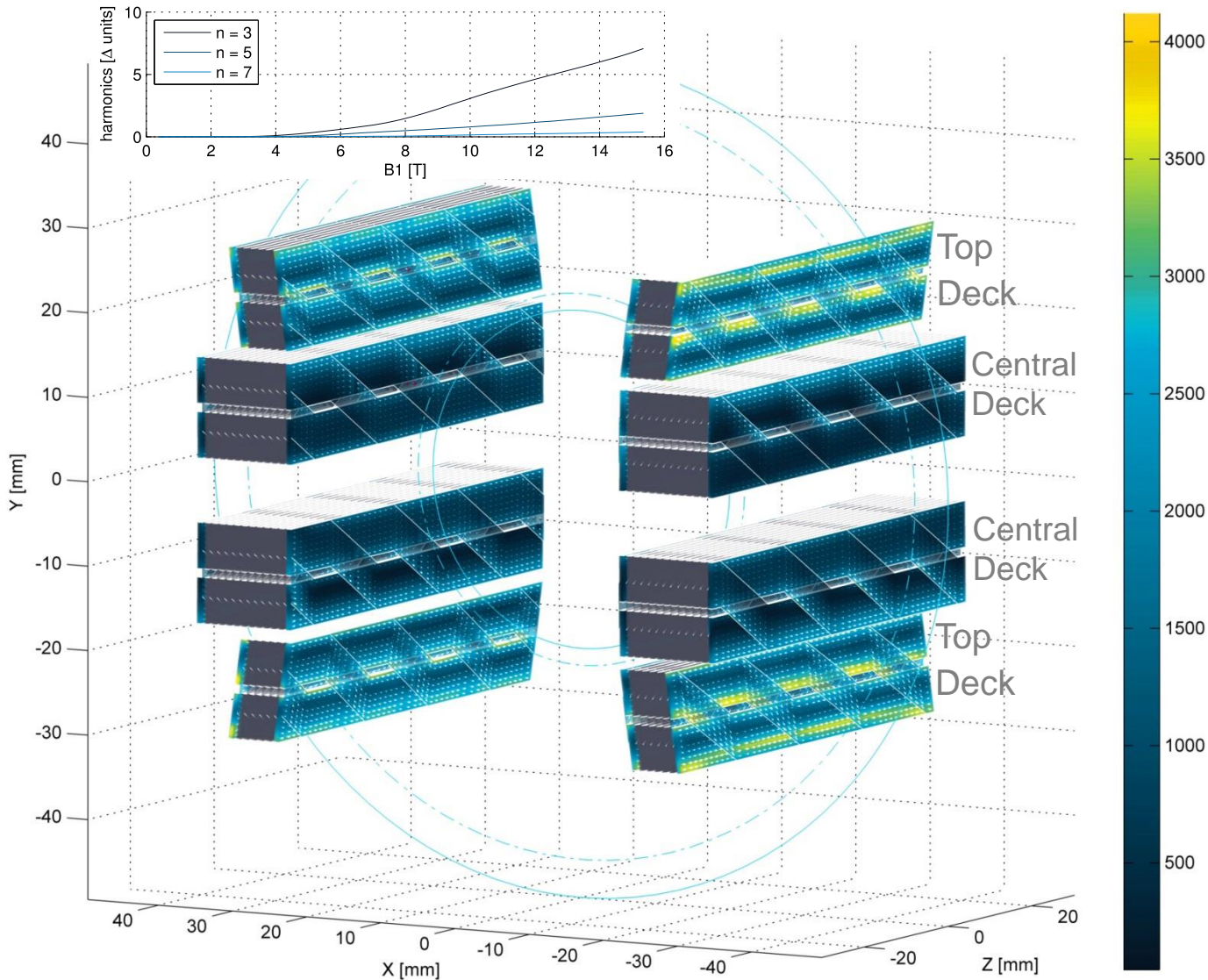




- The calculated magnetisation of a Roebel cable in -2 to 2 T sinusoidal applied field in the perpendicular direction
- Only hysteresis, almost no coupling currents observed
- Hysteresis curve as function of number of elements along width of tapes
- Studied the influence of the number of elements across the width of the tape (decided to use 14 or more)
- Measurement of hysteresis and AC-losses is on-going at the University of Twente

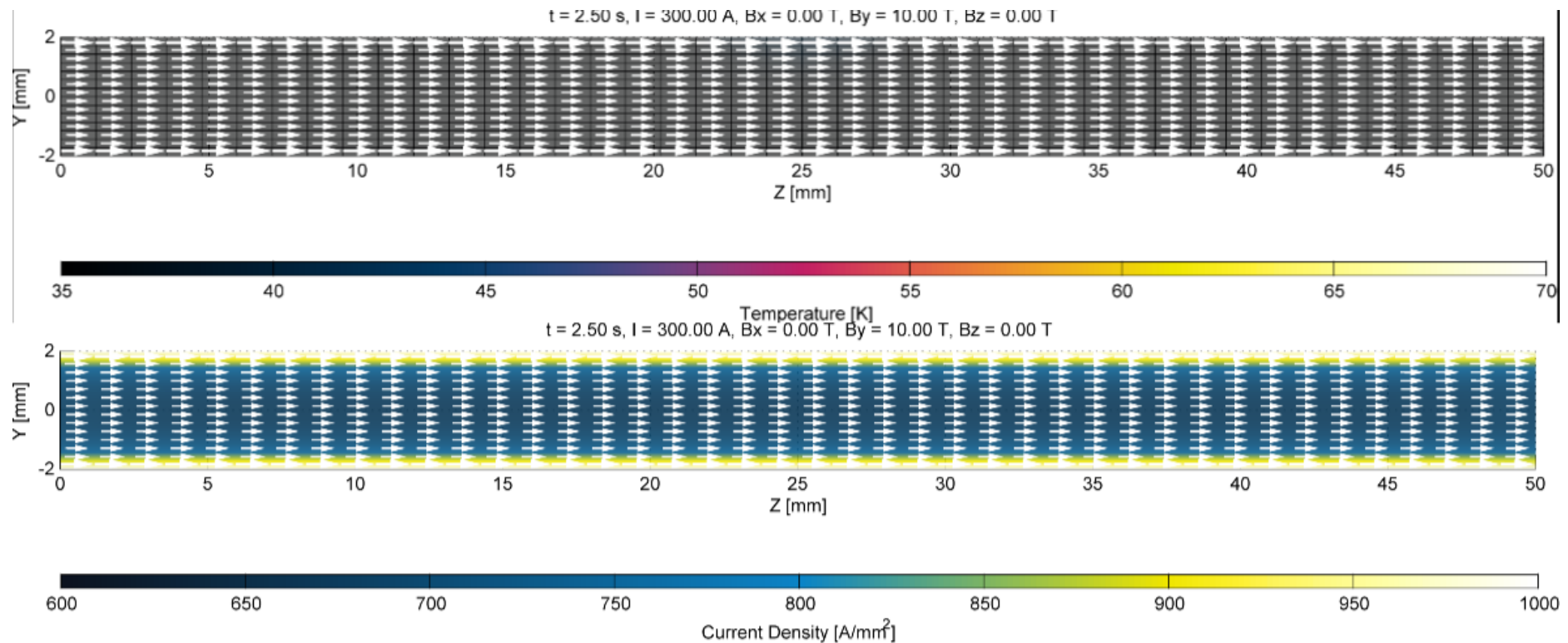


$t = 1200.00$ s, $I = 7993.33$ A, $B_x = 0.00$ T, $B_y = -12.99$ T, $B_z = 0.00$ T



- Due to limitations of the BemFem no Iron pole (yet)
- Simultaneous ramp of Fresca2 and insert over 20 minutes (1200 s)
- Top deck generates more shielding currents due to field angle
- Harmonics at $2/3$ aperture less than **10 units**
- Keeping alignment during ramping could reduce the field error by a great deal

- Comparison University of Twente normal zone propagation measurement data (master assignment JvN).
- As an example a quench at 35 K, 10 T parallel, 300 A in a 4 mm wide tape
- Quench was purposely initiated at edge of tape to show redistribution of current
- Propagation is, due to the redistribution of the current, much faster in width direction than longitudinal direction!





Pick up Coils

Voltage Taps

Acoustics

FIELD SENSORS



FPGA -DAQ



Temp sensors

Test station spec.

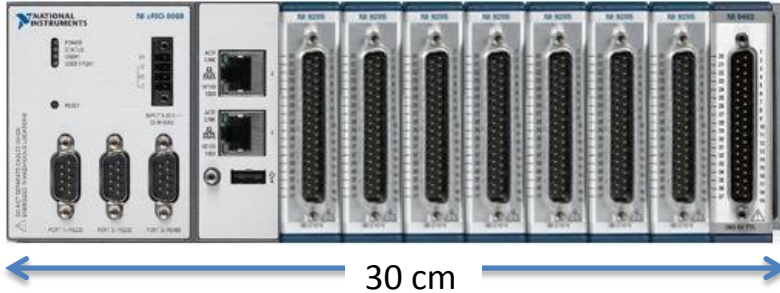
- Feather's Current ~ 10 kA
- Dump resistor.
- 10 kA semiconductor Fast switch 1 or 2 mS
- Variable test temperature ~ 80 to 4K in steps! (temp stability, current leads opp.,
- Instrumentation. (224 channel FBGA DAQ)
- Temp sensors, voltage taps, pick up coils.
- Feather 2 dynamic field measurements. 40mm
- Feather 2 in Iron yoke od ~ 240 mm
- Feather 0 in Iron yoke od ~ 120 mm

HTS Quench DAQ

NI-CompactRIO

224 total

Received at CERN 14 March



7 modules: 16 differential analog inputs each
+/- 200 mV till +/- 10 V input range
16 bits
7.8 kS/s per channel

Processor:

667 MHz dual-core ARM
512 MB RAM
1 GB storage
NI Linux Real-Time OS

FPGA:

Xilinx Artix-7
2 M cells

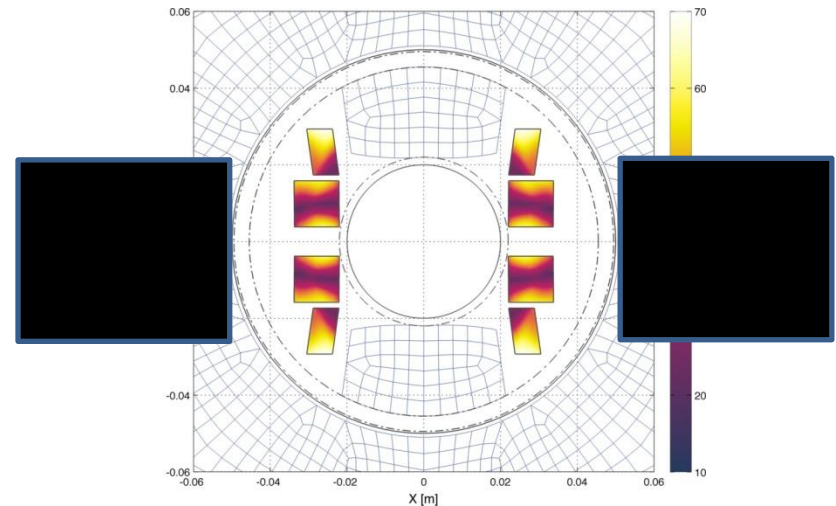
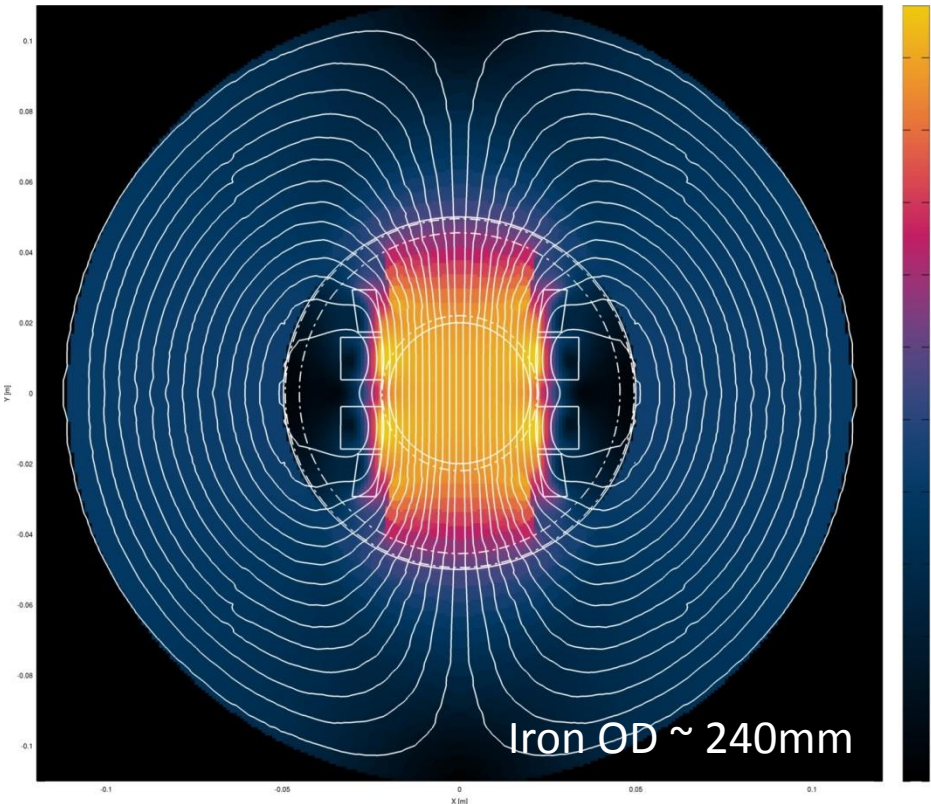
1 module: 32 digital outputs
5 V TTL
7 μ s response time

Also available: **high speed module**
4 differential analog inputs
16 bits
1 MS/s, simultaneous sampling

A similar system is used by the EL group to capture voltage transients on the electrical network caused by EDF switching, thunderstorms and internal load changes.

Cross section 5 T Stand alone

98 mm outer diameter, to be able to fit inside Fresca-2 without touching.
Standalone we may fit a simple magnetic yoke



This is one of the many possible designs we are Thinking about: Placing IRON yoke to Exaggerate the change in field angle to assess angular dependence

Possible test ideas after stand alone

