



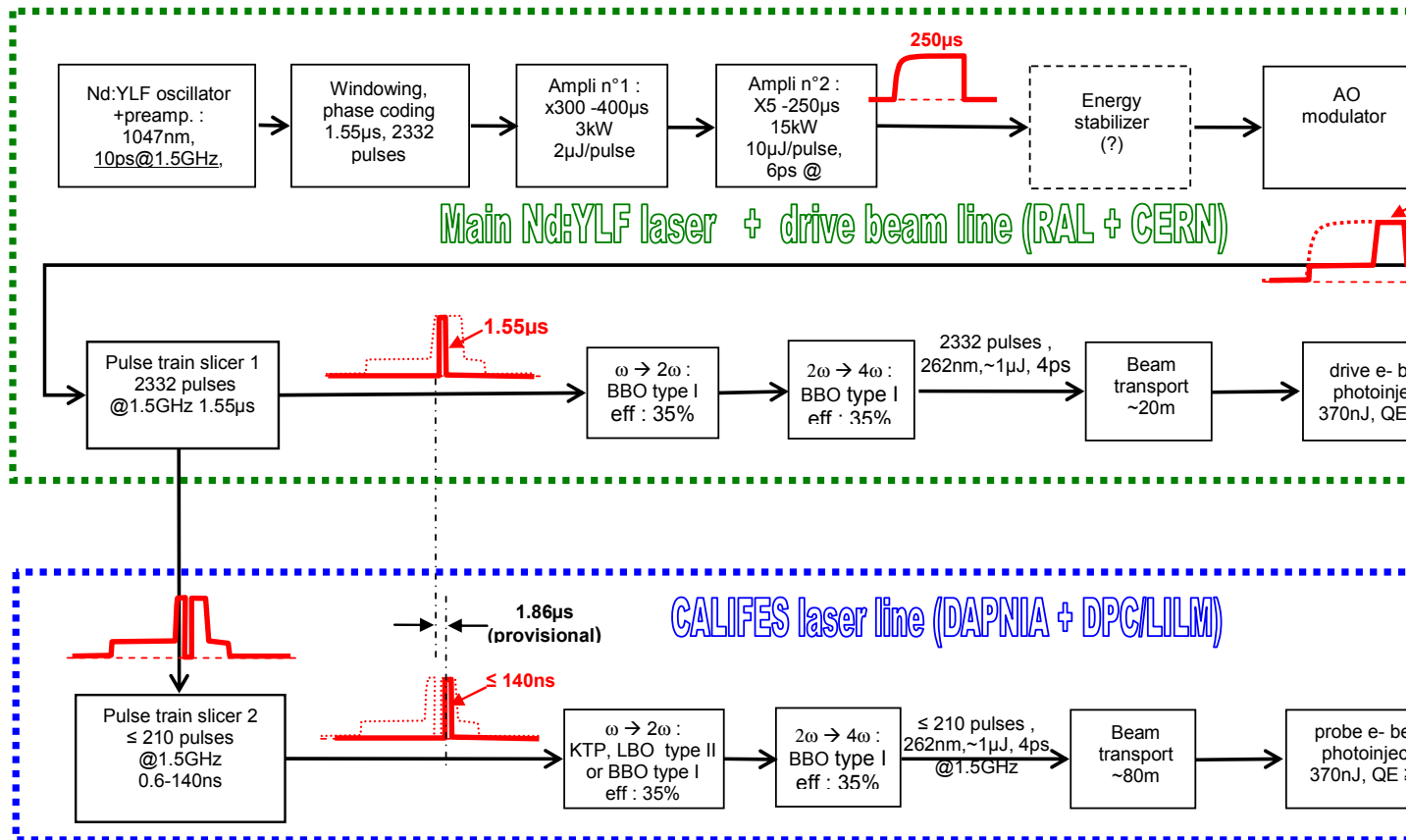
Laser beam for Califes

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CERN

P Girardot and all
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Global Scheme





- 1) Pulse picker
- 2) Frequency conversion
- 3) Transport
- 4) Conclusion

Pulse picker: scheme



The pulse picker is made with:

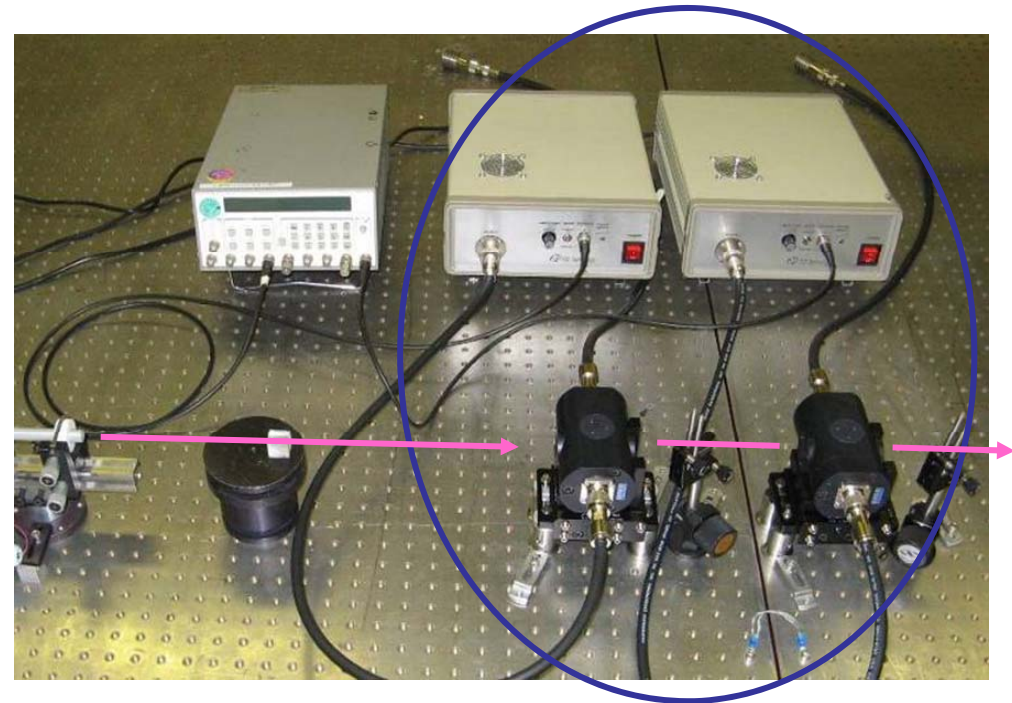
- 2 pockels cells (PC)
- 3 polarisers

One PC sets the rising edge, the other sets the falling edge

Each pockels cell is triggered by a HV pulser

Both HV pulsers are triggered by a generator

Independant triggering allows to change the duration of the pulse selected



Pulse picker

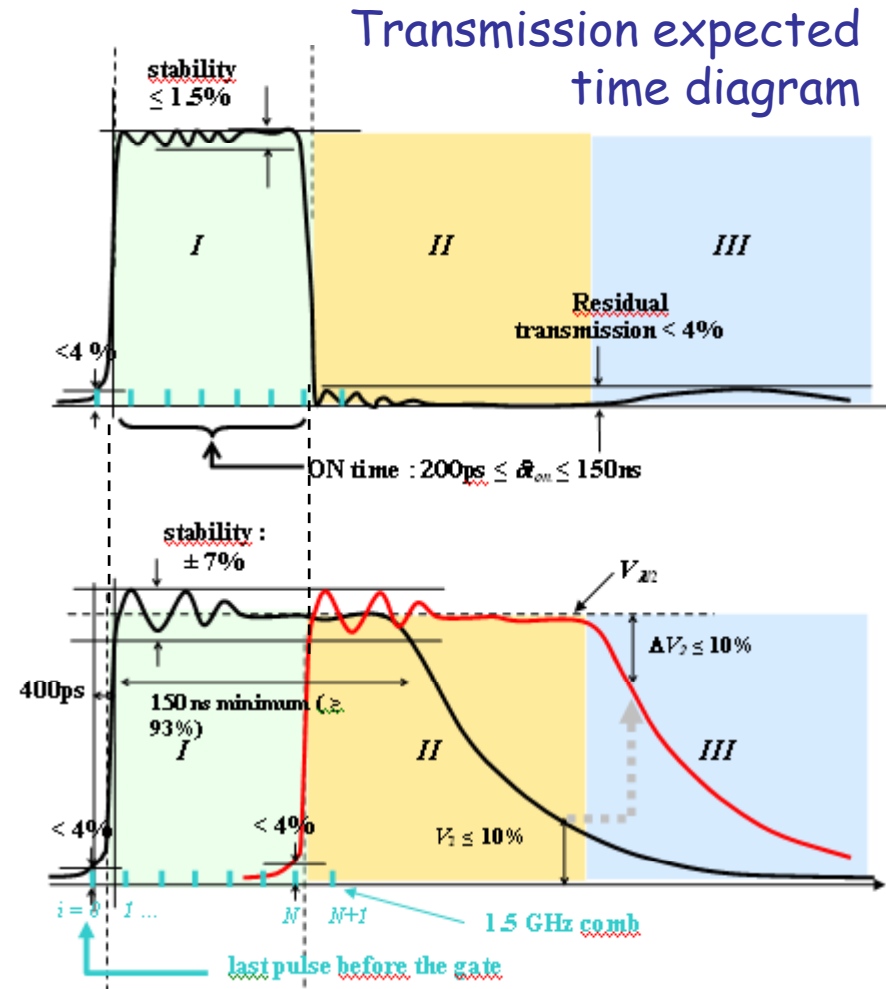
in test in Saclay

Pulse picker ordered to Leysop Ldt : specifications



Mains specifications for the pulse picker:

- sharp rise time and fall time: less than 666ps \rightarrow \sim 400 ps
- duration \sim 0.5 ns to 140 ns
- with stability better than \pm 1.5%
- low transmission ($<$ 4%) out of the pulse selected
- need for high transmission during the pulse



Related specifications HV pulse

Pulse picker: choose dry cell /fluid - transmission



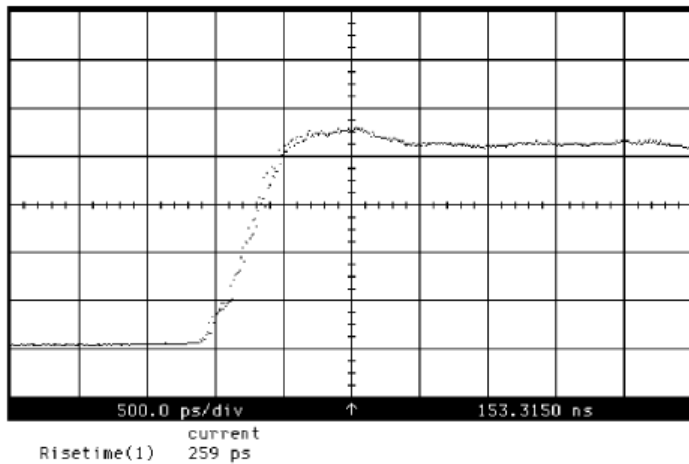
Dry cell was finally preferred:

- to avoid degradation of the fluid with peak irradiance, (especially for a long running time).
- in spite of:
 - theoretically less impedance adaptation
 - less transmission (around 1% less per cell)

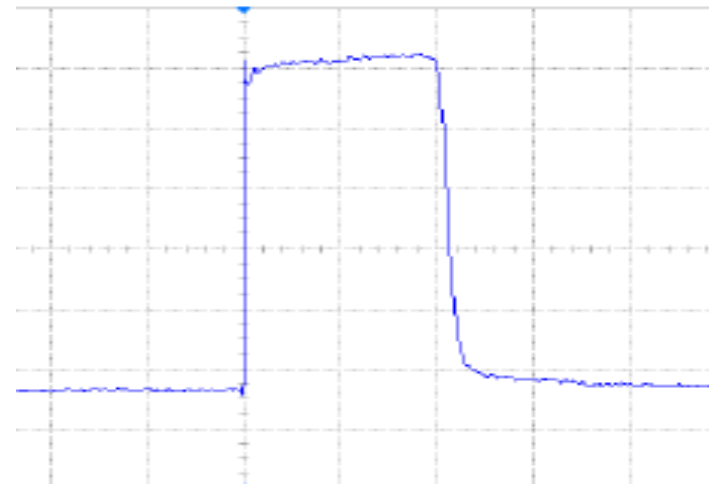
Finally, the measured transmission was about 92% per cell (a bit less than expected).

For entire pulse picker, at CERN: $T \sim 80\%$.

Pulse picker: Test Report-Temporal rise time

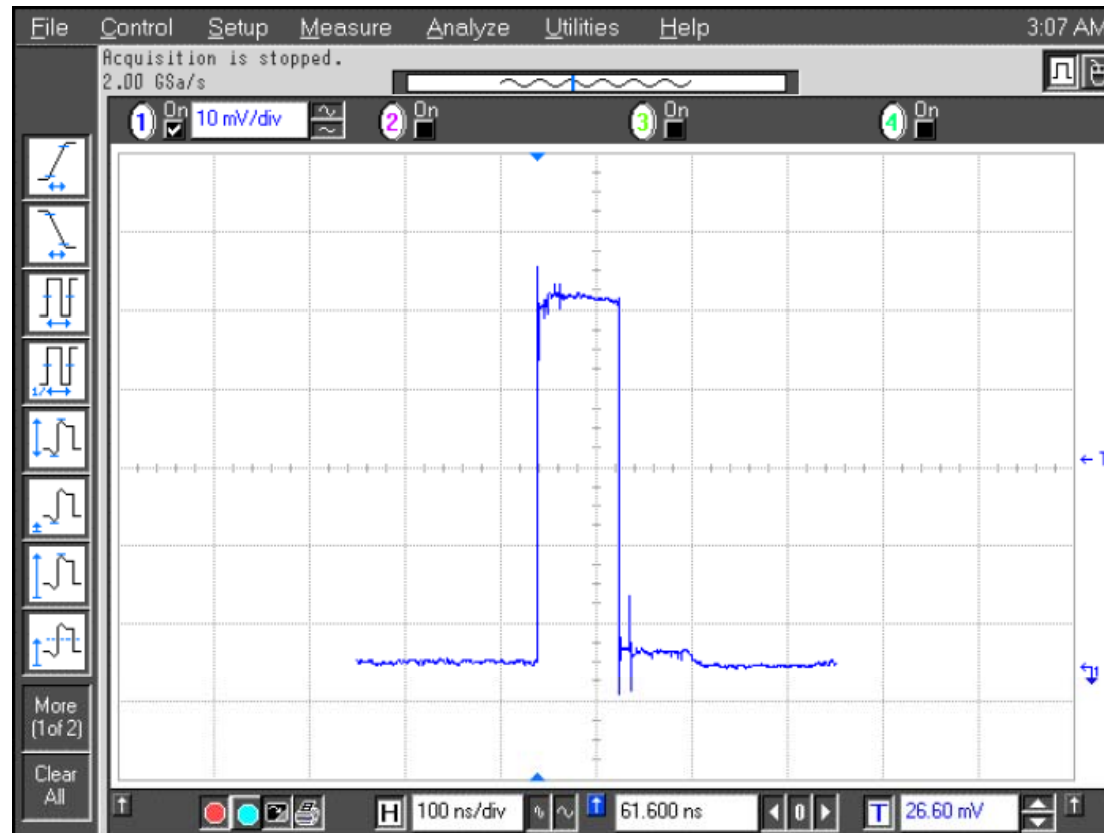


Out of the pulser
(trigerring)
measured rise time
~260ps



Out of one pockel cell
(optical):
measured rise time:
less than ~ 350ps

Pulse picker: Test Report- Chopped pulse

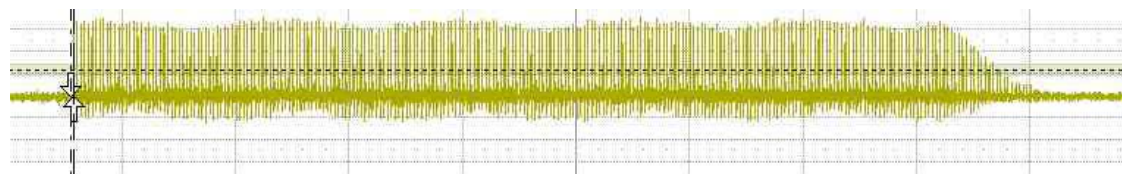


100ns Duration Chopped Pulse

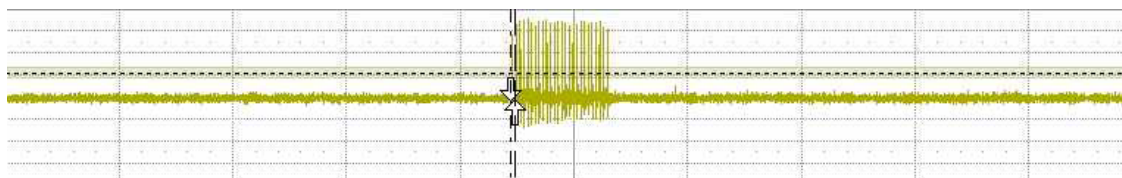
Chopped pulse - at CERN with a 60 GSamples/s oscilloscope



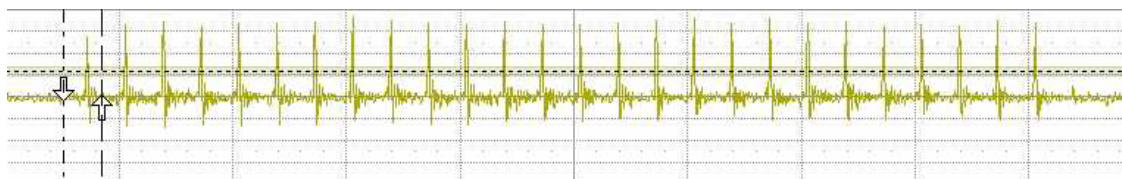
Cell 1 alone
(Cell 2 off)
20ns/div



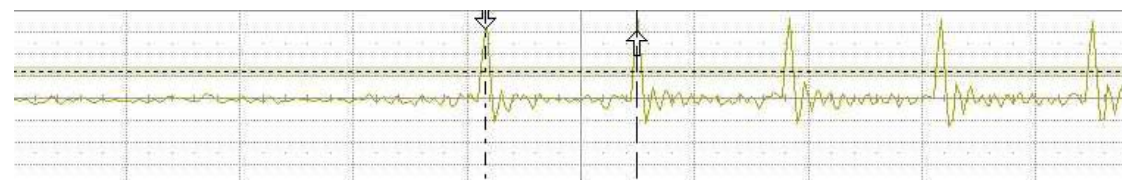
Gate 20 ns
20 ns/div



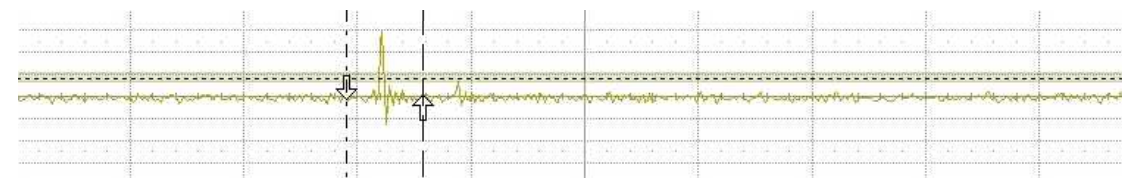
Gate 20 ns
2ns/div



Check of rising edge
500ps/div



1 pulse selected
1ns/div



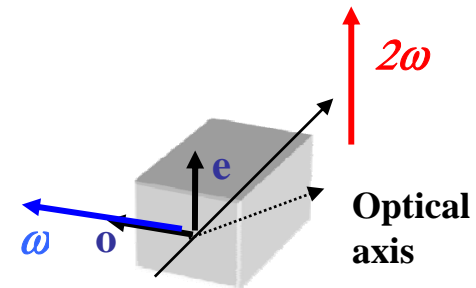
Frequency conversion - crystals considered



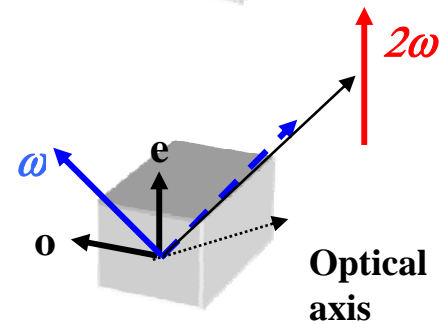
IR \rightarrow Green type II: KTP, LBO ; type I: BBO, LBO

Green \rightarrow UV type I: BBO, CLBO, KDP

TYPE I :



TYPE II :



Frequency conversion - 1047nm → 523 nm - calculations



Nominal parameters for optimisation:

- entering beam parameters: 10μJ, 6ps, 1047 nm, M^2 (beam quality factor) = 1
- CE (conversion efficiency) = 35% (→ 12% for $\omega \rightarrow 4\omega$)



	KTP (II)	LBO (I)	BBO (I)
λ_ω incident (nm)	1047	1047	1047
d_{eff} : non linearity coeff (pm.V)	3.0	0.83	2
L : length of crystal (cm)	0.6	1.5	0.8
Φ_{1/e^2} : diameter (mm)	1.8	1.5	1.8
Tolerance: <i>Critical if tolerance parameter approach 1.</i>			
Angular acceptance: $\xi_\theta = 2\theta / \Delta\theta_{acc}$	0.028	0.106	0.36
Walk-off : $\xi_\alpha = 2\alpha_{max} \cdot L / \Phi$	0.038	0.17	0.5
GVM: $\xi_{GVM} = GVM \cdot L / Dt_{1/2}$	0.44	0.267	0.79

Frequency conversion - 523 nm → 262 nm - calculations



Typical parameters and tolerances

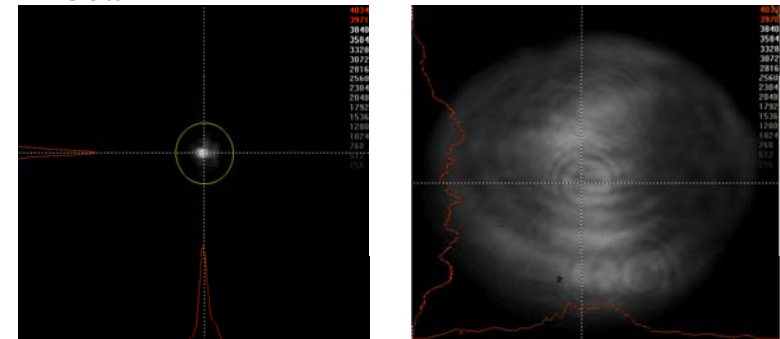
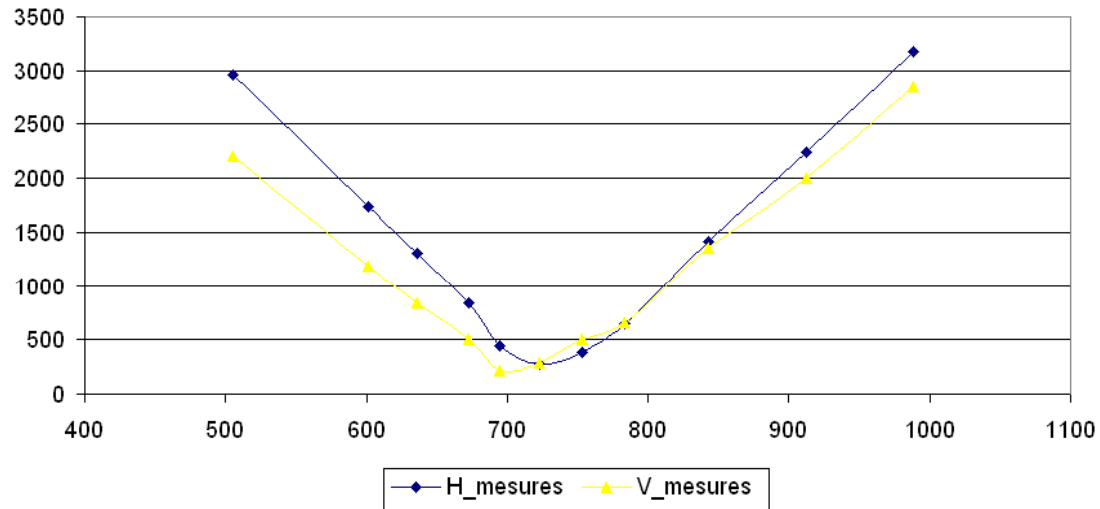
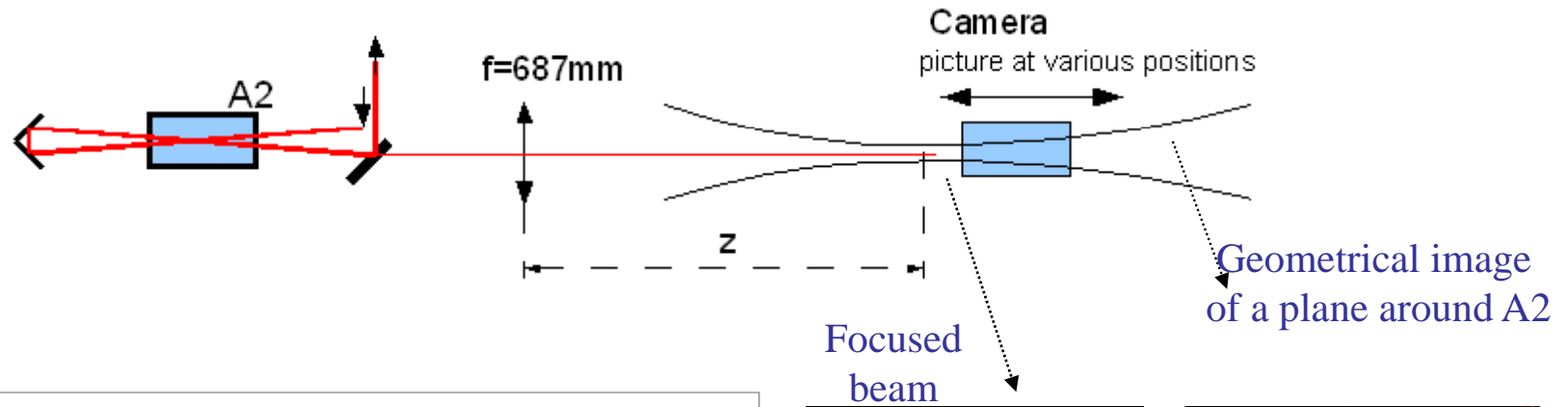
calculations for entering beam parameters: 3.5 μJ, 4.9 ps, 523 nm, M^2 (beam quality factor) = 1

and for CE (conversion efficiency) = 35% (→ 12% for $\omega \rightarrow 4\omega$)



	BBO (I)	CLBO (I)	KDP
λ_ω incident (nm)	523	523	523
d_{eff} : non linearity coeff (pm.V)	1.74	0.8	0.47
L : length of crystal (cm)	0.8	1.5	2
Φ_{1/e^2} : diameter (mm)	2.04	2.1	0.94
Tolerance: <i>Critical if tolerance parameter approach 1</i>			
Angular acceptance: $\xi_\theta = 2\theta / \Delta\theta_{acc}$	0.48	0.32	0.2
Walk-off : $\xi_\alpha = 2 \cdot \alpha_{max} \cdot L / \Phi$	0.67	0.44	0.285
GVM : $\xi_{GVM} = GVM \cdot L / Dt_{1/2}$	0.97	1.04	1.24

M² measured out of A2 amplifier

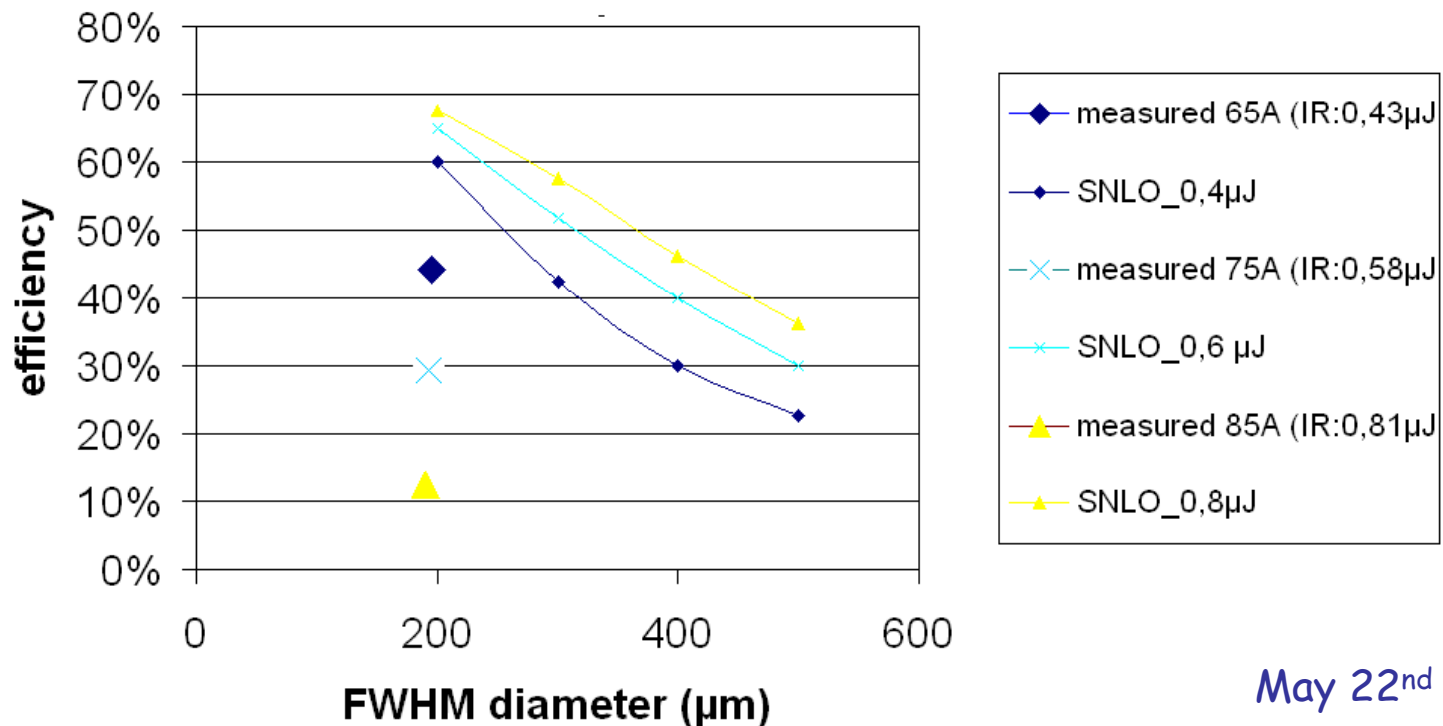


M² ~ 2 (1.5 to 2.6)
for the beam out of A2

Frequency conversion - 1047→523- simulation/measurements



On KTP, with large margin on angular acceptance, we expect:
conversion efficiency measured ~ conversion efficiency given by simulation.



May 22nd 2008

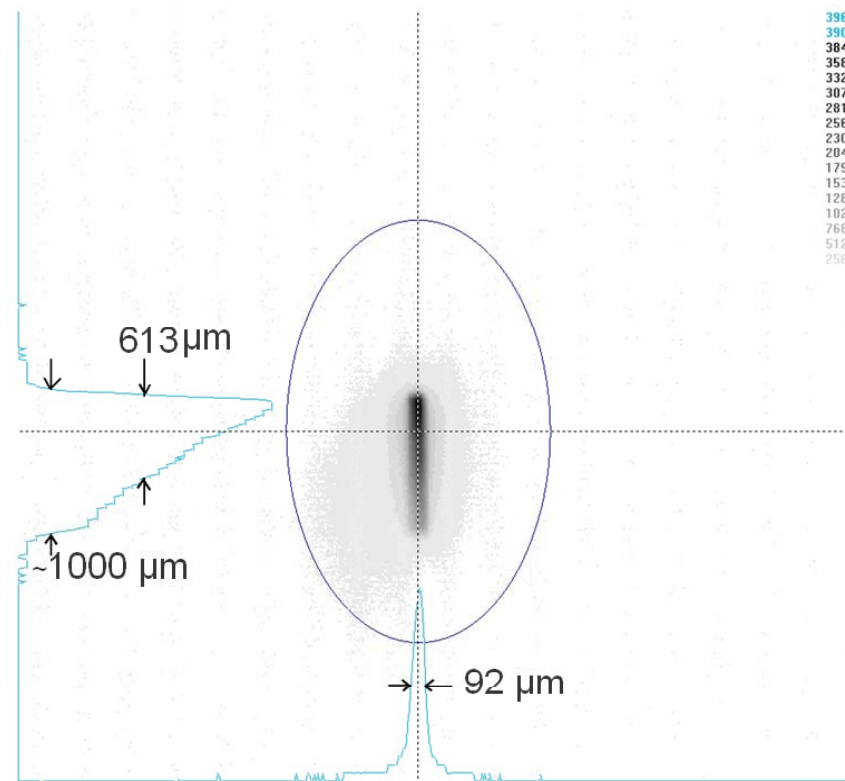
→ ASE of the laser in between the micropulses

Frequency conversion - 523→262 - large walk-off



With low IR energy, the beam has to be focused a lot.

- > walk off and angular acceptance limitations become very critical
- > lack off conversion efficiency
- > high distortion in the UV_{near} field profile.



Oct 8th 2008

Conversion efficiency (green to UV) ~ 38%

Energy (micropulse): IR:0.82μJ ; Gr:0.32μJ; UV: 0.12μJ

Amp 1 alone

(Dimension of the input green beam: 42μm x 112μm)

Frequency conversion - conclusion



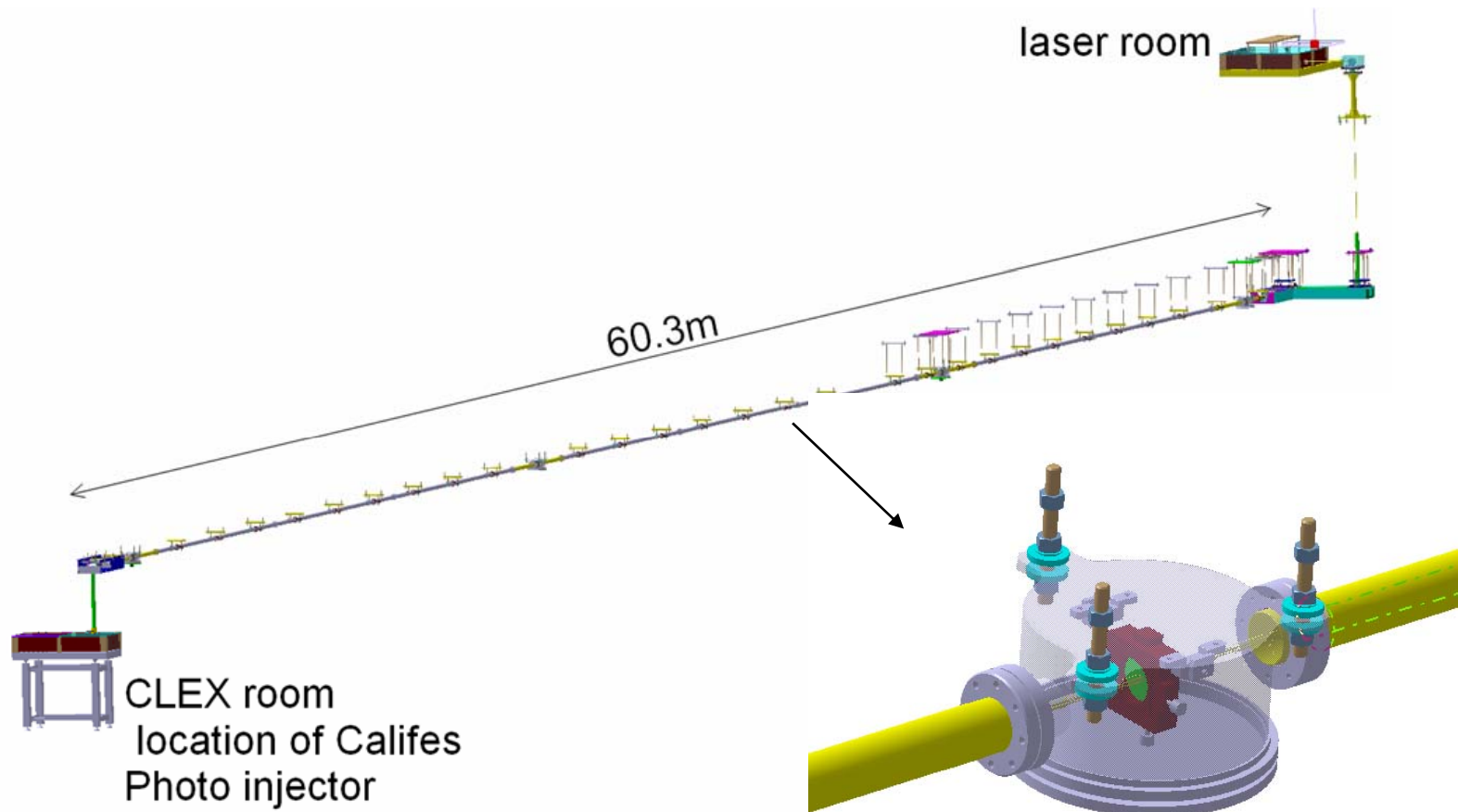
The focusing diameter on the crystal should be increased when the power increase.

A stabilized IR beam should allow to optimise a "final" configuration.

Optimized cylindrical focusing could be tested.

Other crystal (KDP) could be tested

Transport- tables and mechanical supports



under air / under vacuum beam delivery

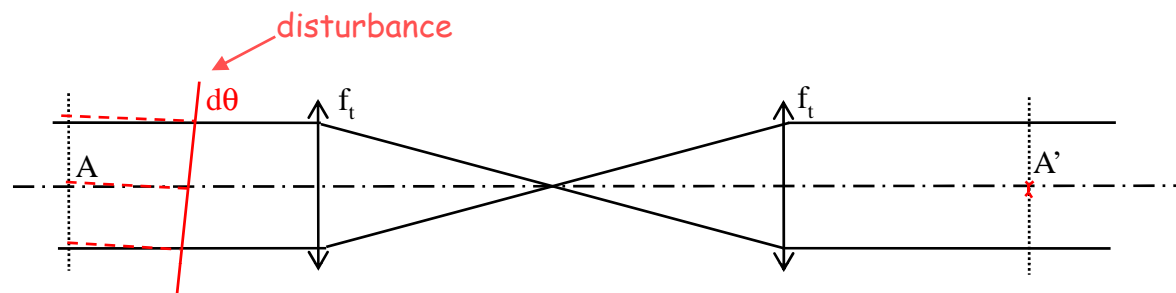


- **Consequence of Temperature and Pressure variations:**
 - $n-1$ ($\sim 3 \cdot 10^{-4}$) proportional to P et T . n : air optical index
 - $l = 80\text{m}$ and ΔT or $\Delta P = 1\%$ $\rightarrow \Delta(n \cdot l) \sim 0.3\text{mm} \rightarrow \Delta t \sim 1 \text{ ps}$.
- **Attenuation (@ 262 nm):**
 - Rayleigh Diffusion \rightarrow Transmission = 98%.
 - Ozone absorption:
 - $\alpha = \sim 10^{-17} \text{ cm}^{-2}$ (max at 255 nm). α : absorption cross section
 - 40 ppb ozone, $l = 80\text{m} \rightarrow T = 92\%$.

\rightarrow Transport under vacuum to be preferred

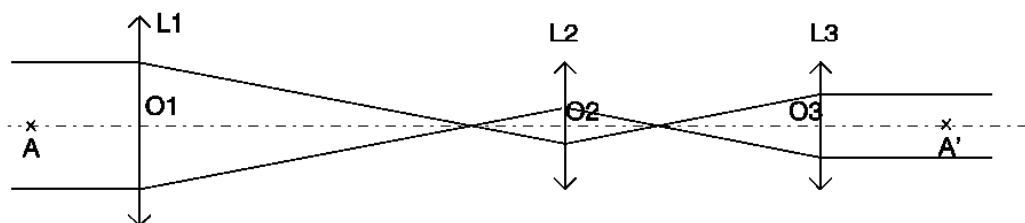
Only the straight line under the roof in CTF2 + CLEX is put under vacuum.

Optical relay /telescope



Optical relay reduce consequences of mirror vibration, air turbulence in plane A'

(A' geometrical image of A)



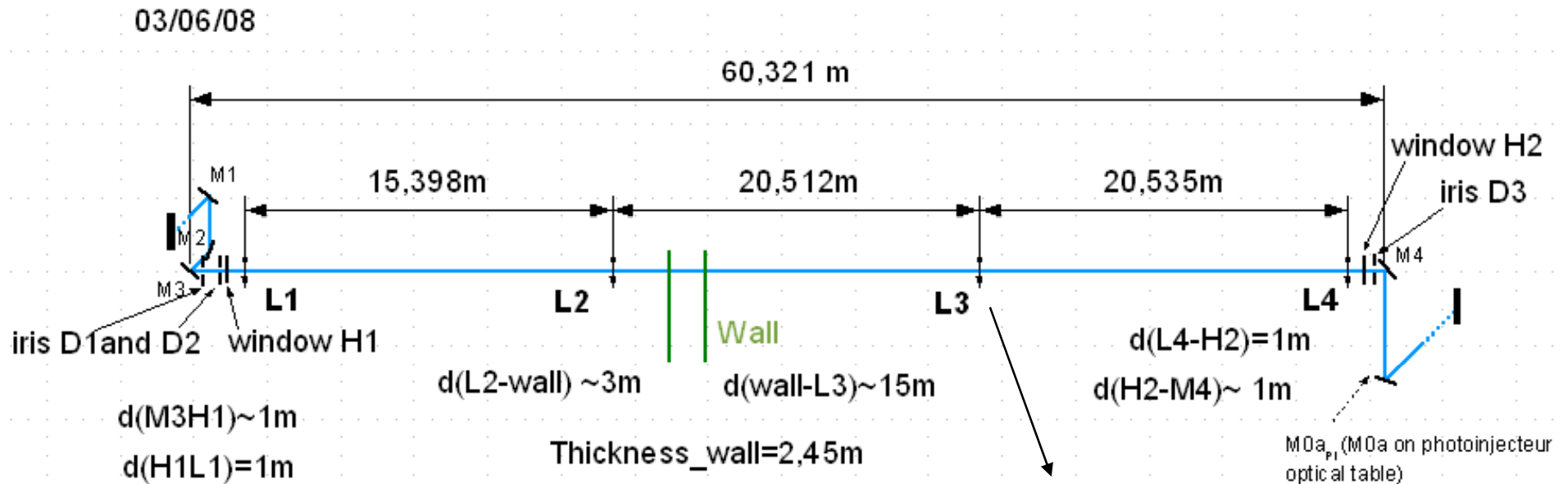
3 lenses telescope allows to:

- decrease the footprint of the optical system for a given relay distance.
- change zoom factor and relay distance (to some extent)

Long distance transport



« under the roof », 2 telescopes (2 lenses) transport the beam from the laser room to the photocathode



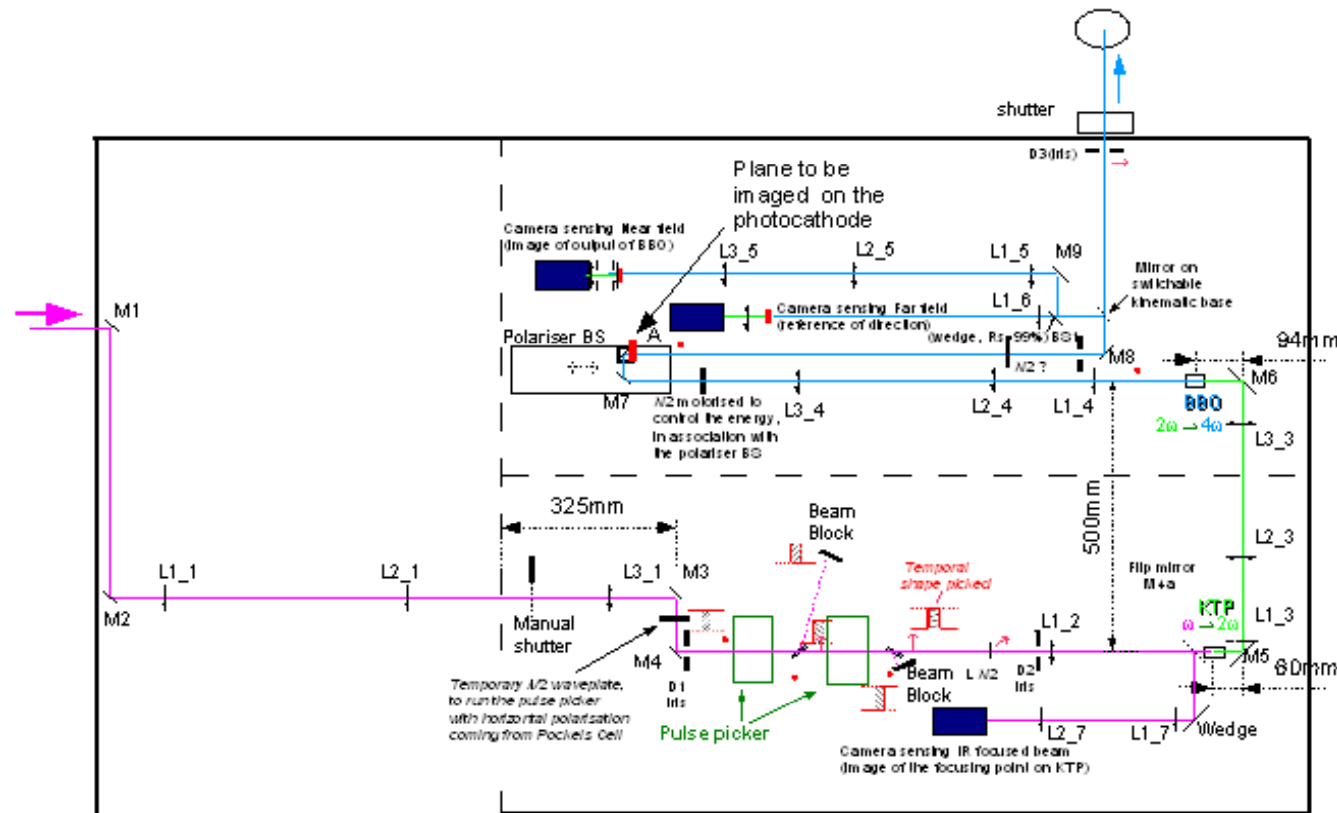
2 telescopes (2 lenses) :
 L1-L2 with $f \sim 10$ m
 L3-L4 with $f \sim 7.5$ m



Optical path on the Califes laser table



Optical path on the Califes laser table

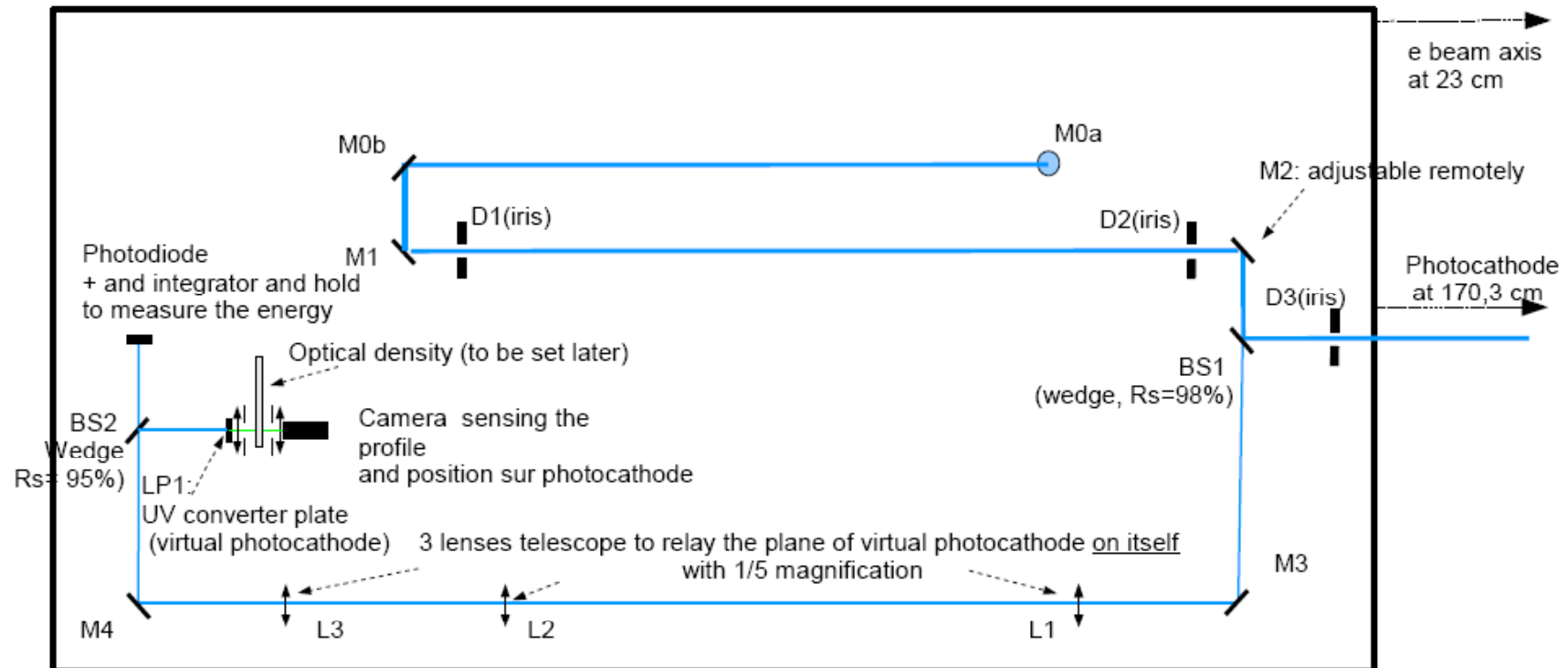


Setup of Laser table

14/10/08:

- telescope 1 to image PC on PP (Magnification = 0.8)
 - combination 2 for focusing on KTP (replaced by only one focusing lens: $f = 200\text{mm}$)
 - telescope 3 to image KTP on BBO: Mag. adjustable (0,7 on that date)
 - telescope 4 to image BBO on objet plane for transport and to adapt the size (Mag= 3,4)
 - telescope 5 to image the objet plane for transport on the camera sensing output the output plane of BBO (Mag=0.2).
 - L1_6 for sensing direction of the beam before transport/reference of direction
 - telescope 7 for imaging the focusing point (on KTP) of IR beam on the camera (Mag= 1)
- red arrows (or red points) indicate the polarisation of the beam

« photoinjector » optical table



Photoinjector

« photoinjector » optical table



Transport and sensing/ conclusion



- Some lack of quality on UV components ordered. Many components tested and returned.
- about 25 lenses, mirrors or windows between BBO and photocathode. Transmission should be 75 to 80% (85% measured between laser room and photoinjector table).
- image transport perform well, but with great walk off on BBO, the image on the photocathode is distorted.
- procedures for adjusting all systems have been provided.



- Pulse picker, transport and various sensing perform quite well
- Frequency conversion has still to be optimised with the IR laser beam working better.



Thank you for your attention

Pulse picker: how it works?



In red: the different temporal shapes of the pulse

