



# Laser characterization and modelling for the development of the Super LHC versatile transceiver

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## Project background

- An upgrade of the current LHC (super LHC or SLHC), planned for 2013-18, is expected to increase the luminosity by an order of magnitude to  $10^{35}$  particles/cm<sup>2</sup>/s.
- A tracking detector operating at the SLHC will require ten times more readout data bandwidth and radiation tolerance than at the current LHC detectors.
- Design a digital transceiver capable of operating at high speed (multiple GBits/s) and endure:
  - High radiation levels
  - High magnetic fields
  - Low temperatures





## Why characterize LASER devices

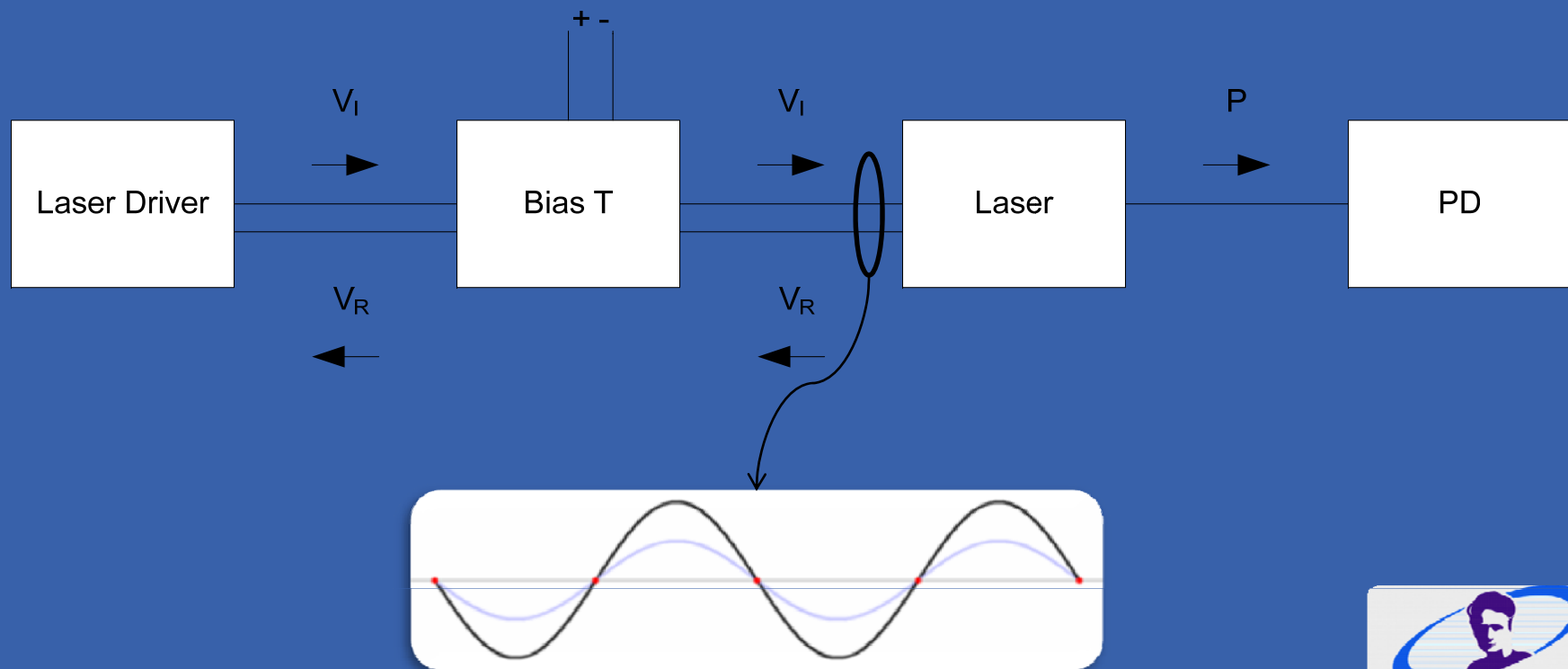
- With a device characterization one can:
  1. Evaluate the LASER device
  2. Predict interaction between LASER, driver and connection network:
    - Design matching network
    - Peaking circuit / Pre-Emphasis
    - DC electrical interface (Bias-T)
  3. Predict performance degradation with environment conditions (temperature, radiation)
  4. **Design better systems**





## Why characterize the LASER devices

- Interaction between LASER, driver and connection network:
  - Electrical impedance mismatch should be kept  $< 10\%$





## What to characterize in the LASER device

- Laser characterization
  - Power / Current / Voltage Curves
  - S-Parameters
    - Direct measurements
    - Static values obtained for a finite number of device working conditions
- Then, using input from characterization, make model
  - Predict device behaviour
    - Current threshold, BW & wavelength changes
      - Temp
      - Radiation
    - Device package modifications

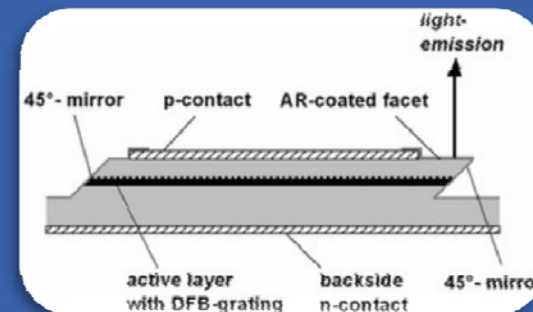
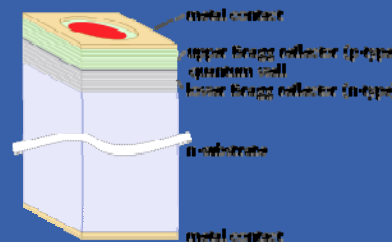
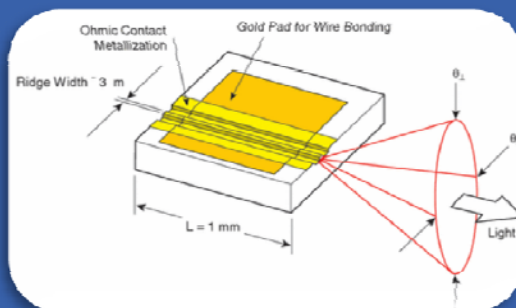




## Types of LASER devices

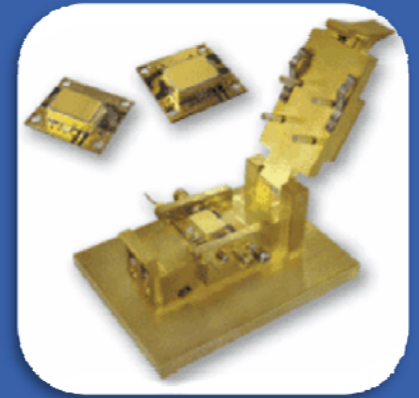


- Semiconductor LASER devices:
  - FP (Fabry-Perot LASER)
  - DFB (Distributed Feedback LASER)
  - DBR (Distributed Bragg Reflector LASER)
  - VCSEL (Vertical Cavity Surface Emitting LASER)
  - HCSEL (Horizontal Cavity Surface Emitting LASER)





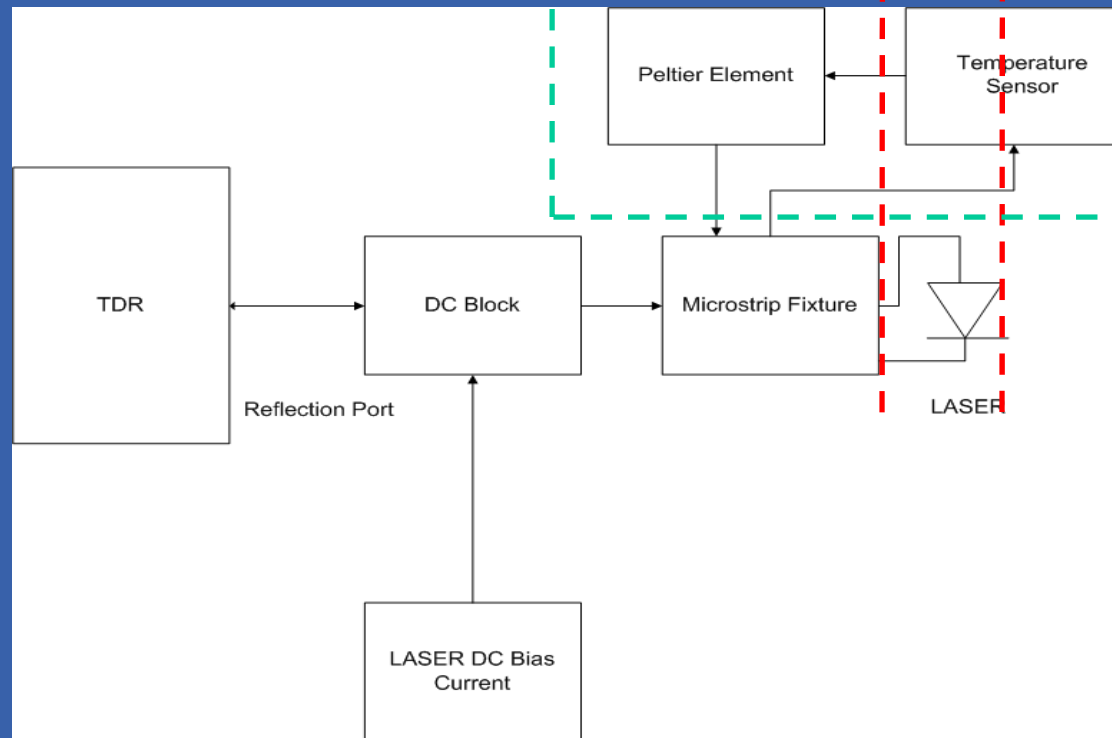
# Measurement setup



- TDR Setup

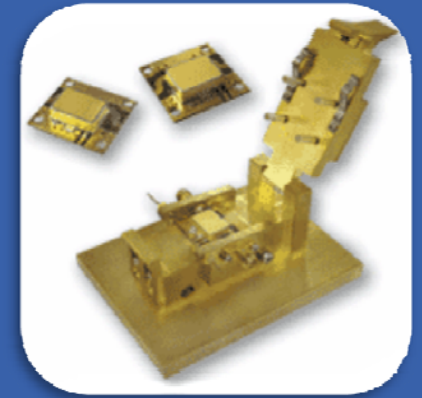
Calibrate here

Cooling system





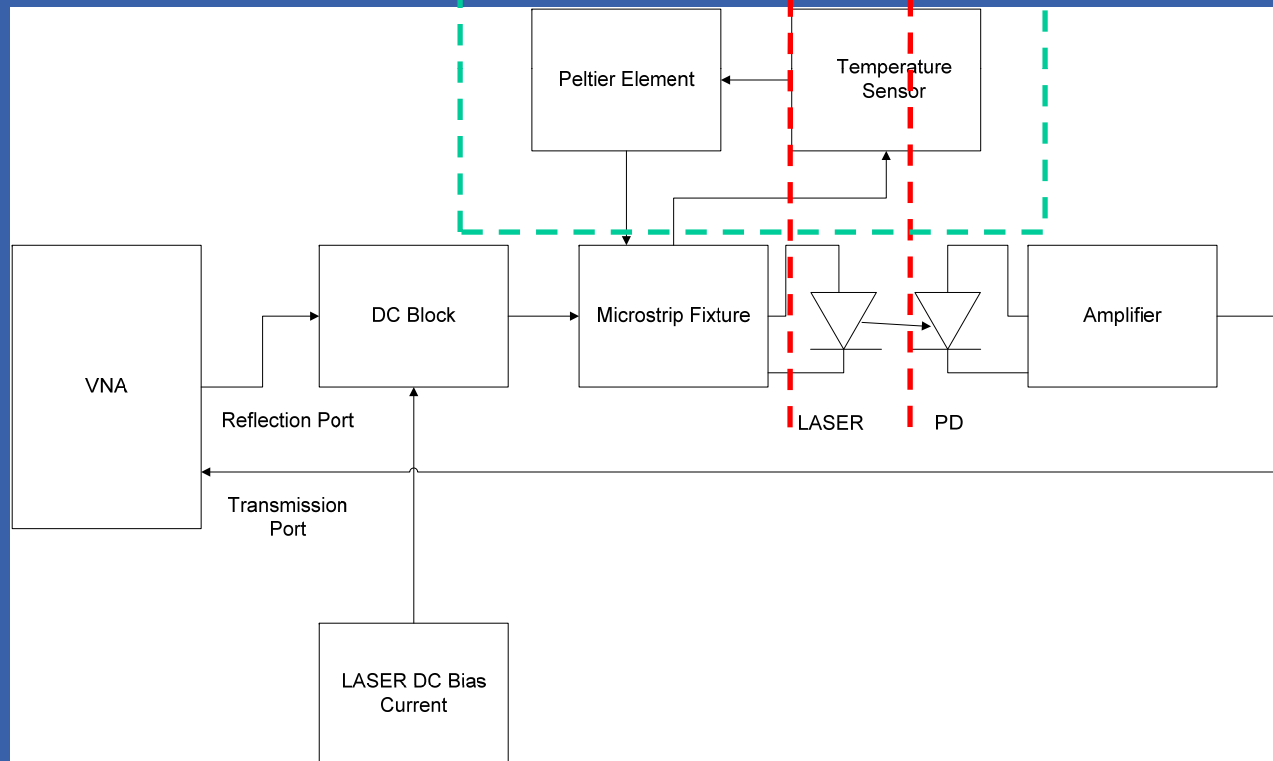
# Measurement setup



- VNA Setup

Calibrate here

Cooling system

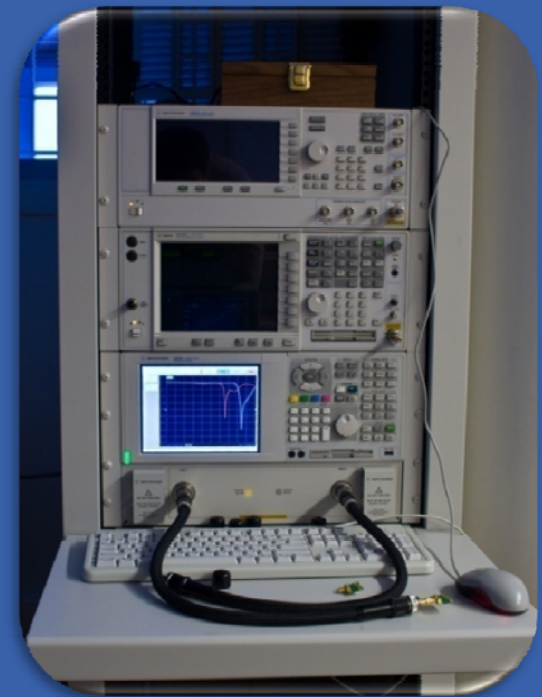
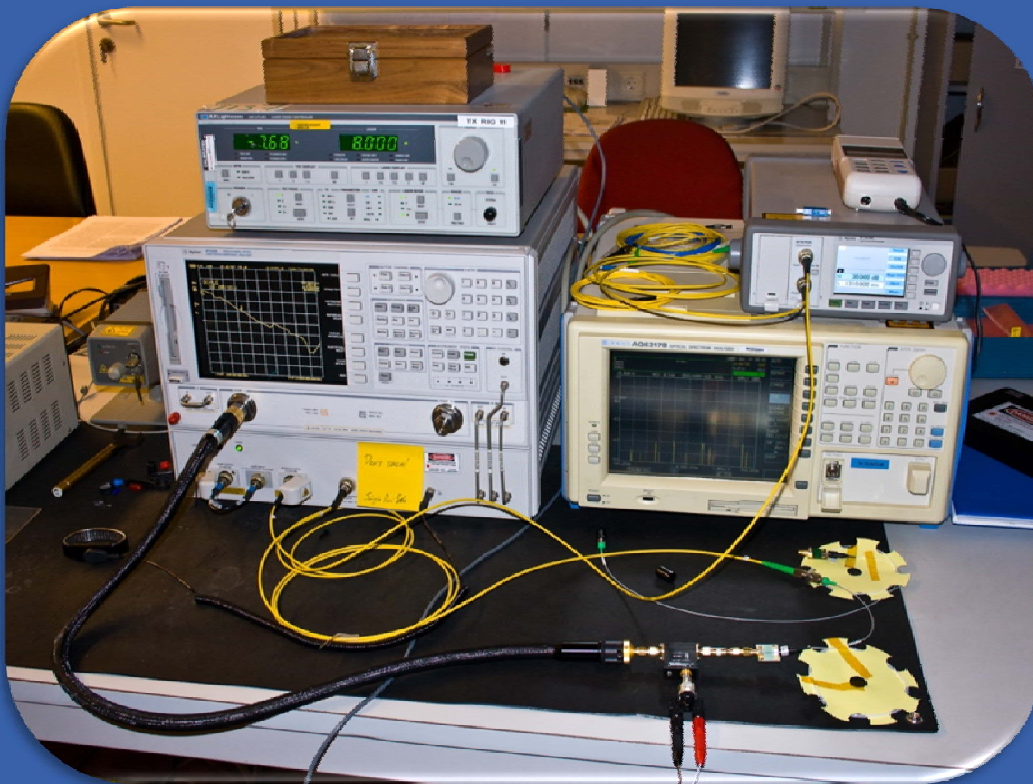
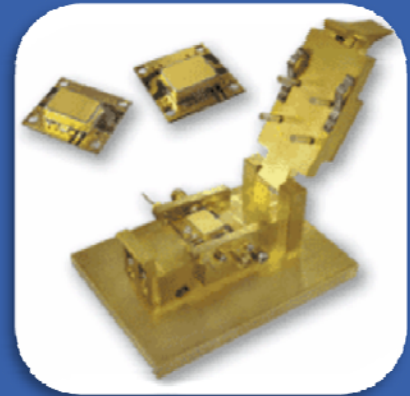






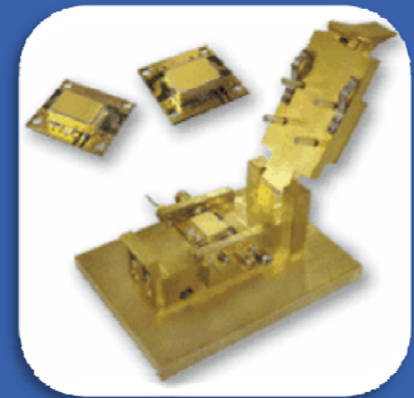
# Measurement setup

- VNA Setup

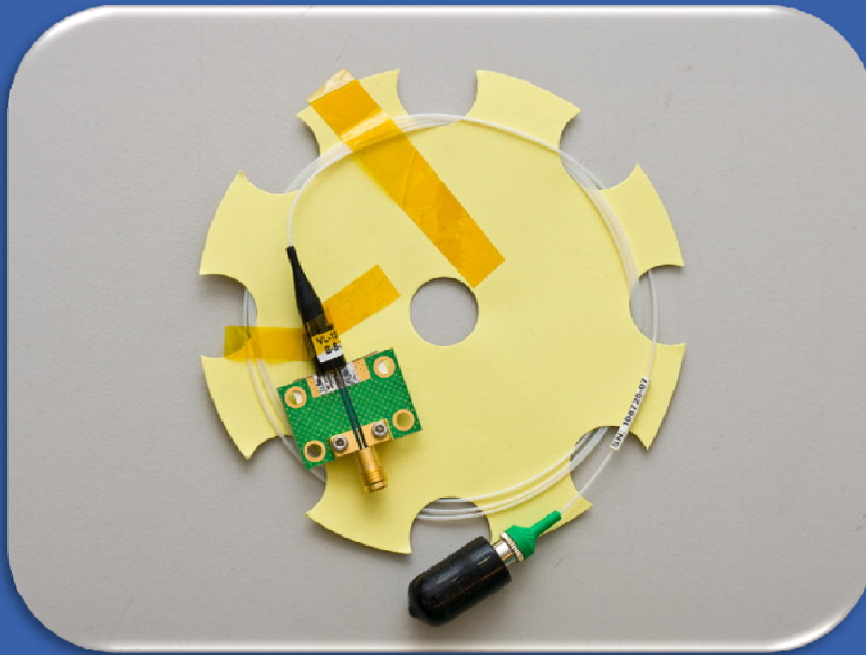




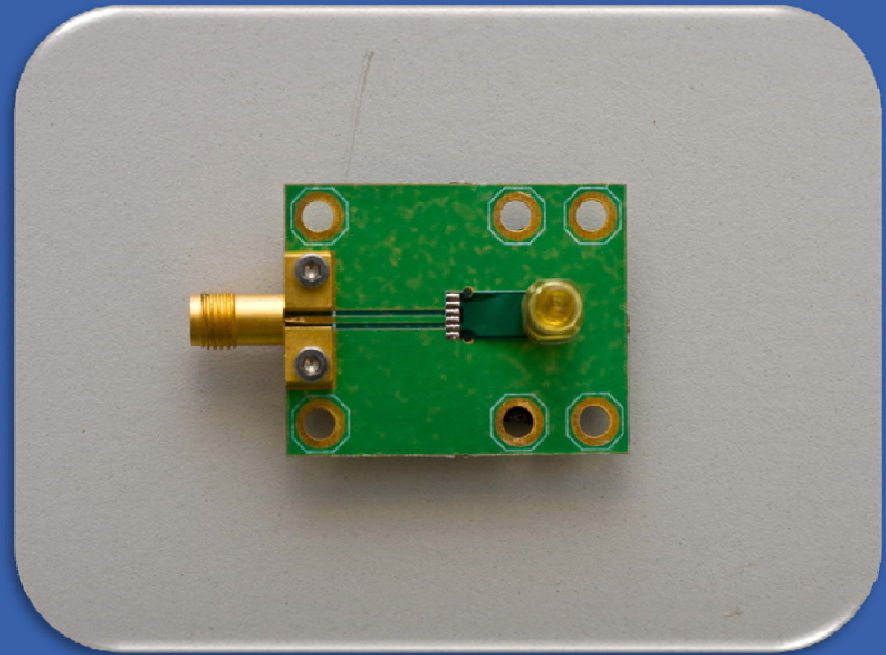
# Measurement setup



- Laser assembly



**Wired Laser**

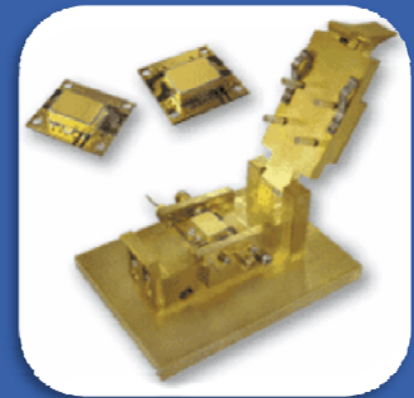


**Flex Strip Laser**





# Measurement setup

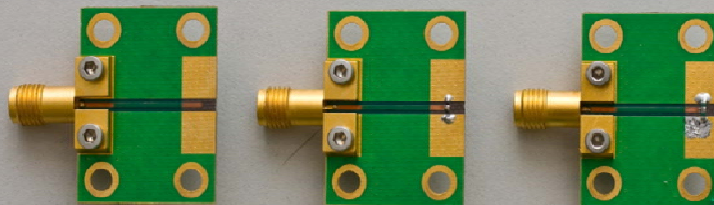


- Test fixture calibration set

Open

Short

Load

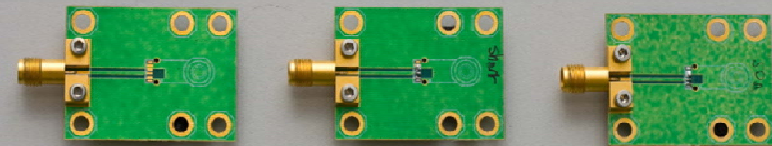


**Wired Lasers**

Open

Short

Load

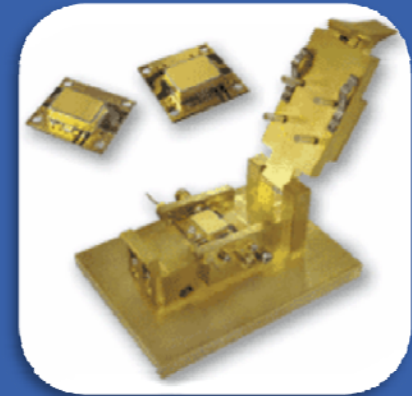


**Flex Strip Lasers**

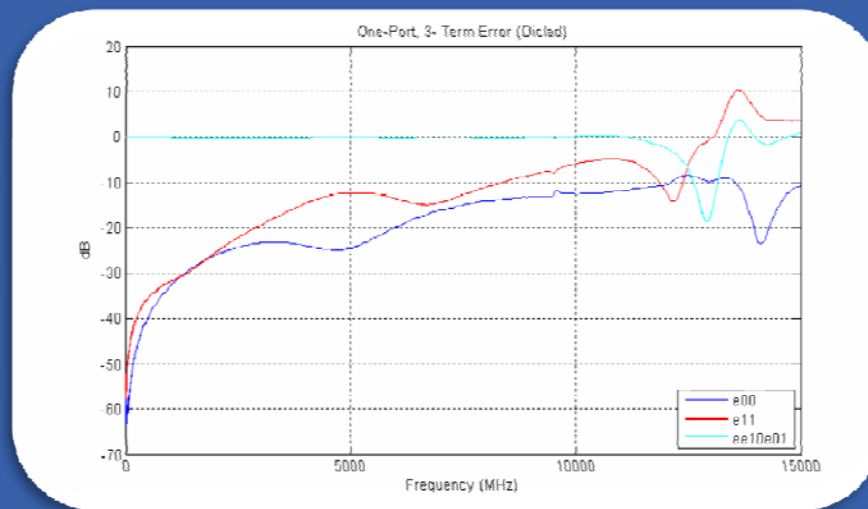
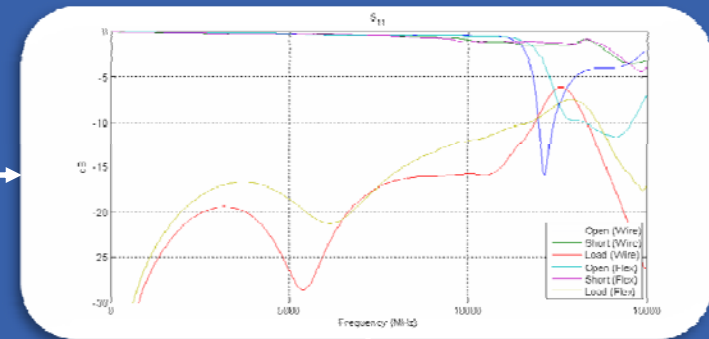
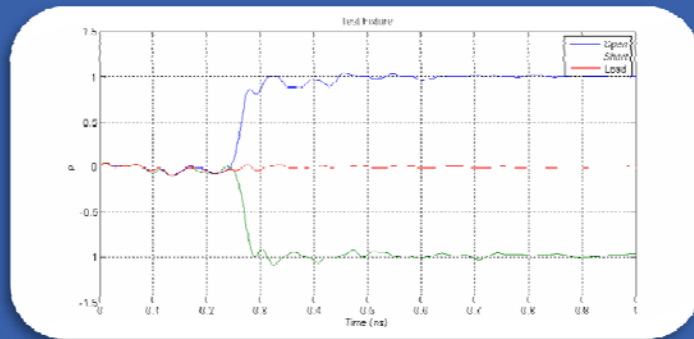




# Measurement setup



- Testing & de-embedding of the test fixture:



**3-Term Error Matrix**

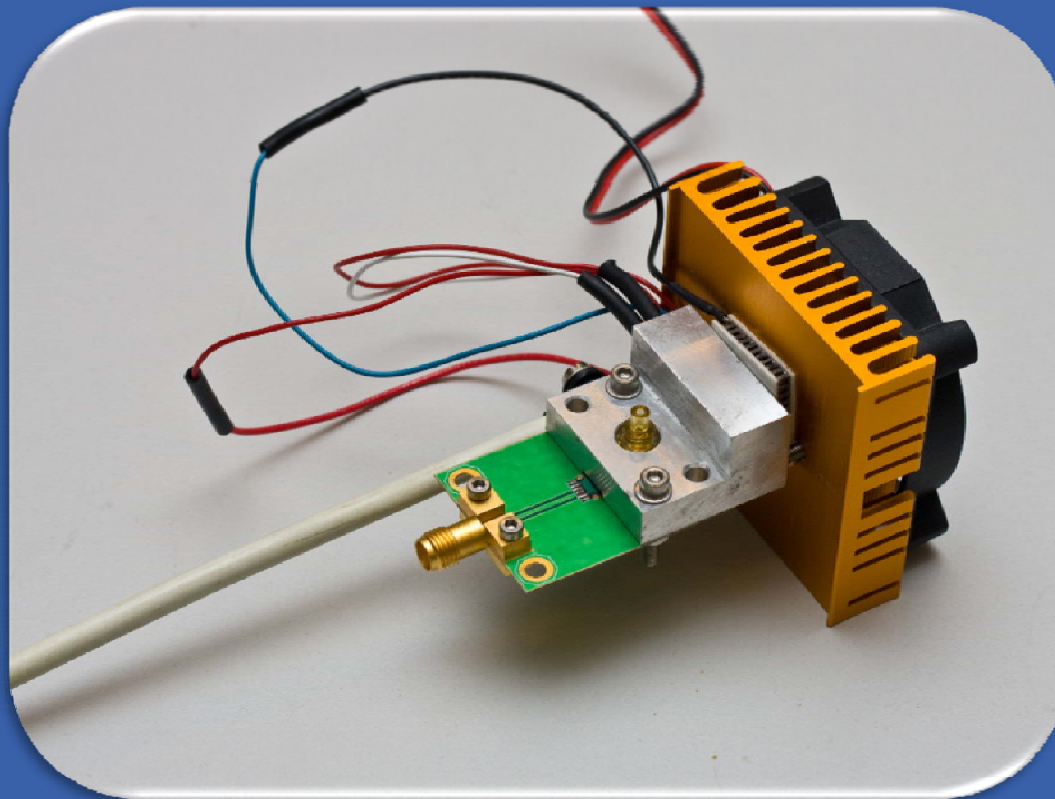
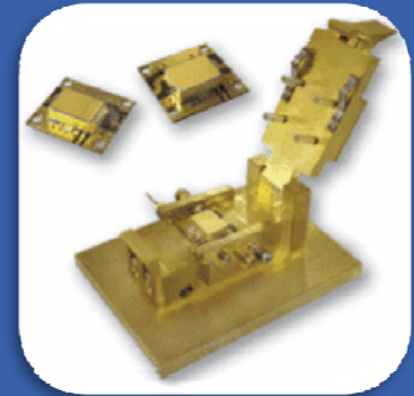


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## Measurement setup

- Temperature control system:

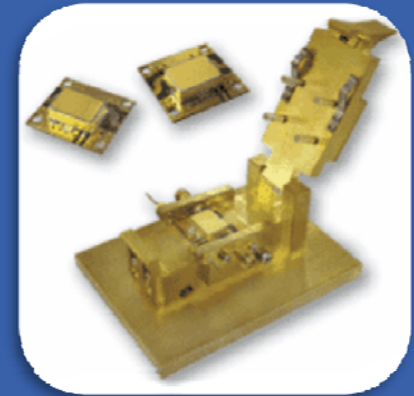


**Peltier based thermo-electric laser cooling system**

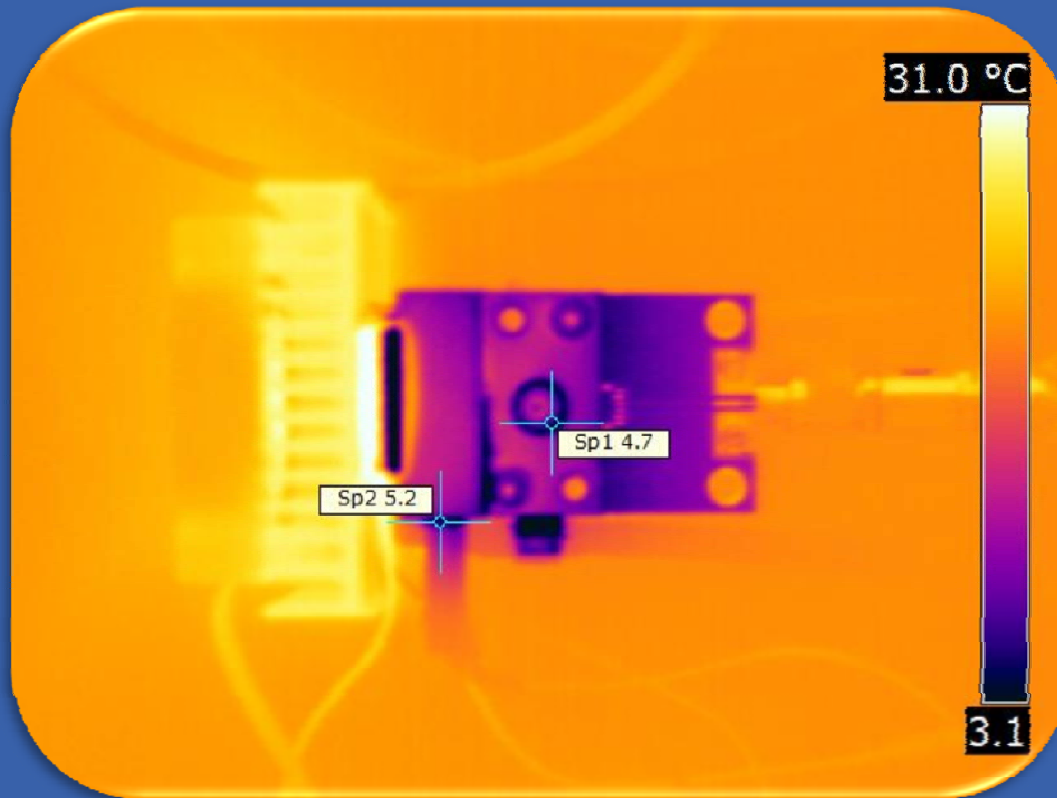




## Measurement setup



- Temperature control system:



Thermal image of the laser & cooling system set to 5°C

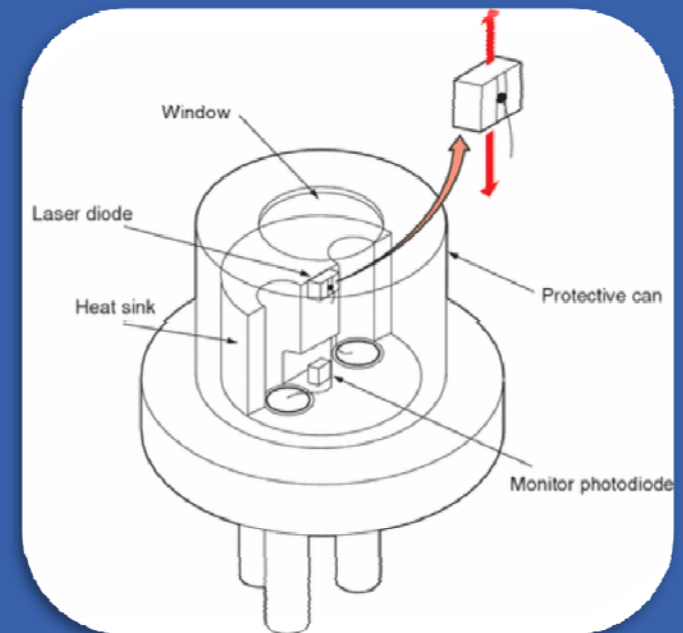




## LASER model



- Measurements lead to simplified laser model
  - Chip & Package model
  - Intrinsic Laser
    - Large signal model
      - DC model
      - Large modulation currents
    - Small signal
      - Signal model
      - Small modulation currents



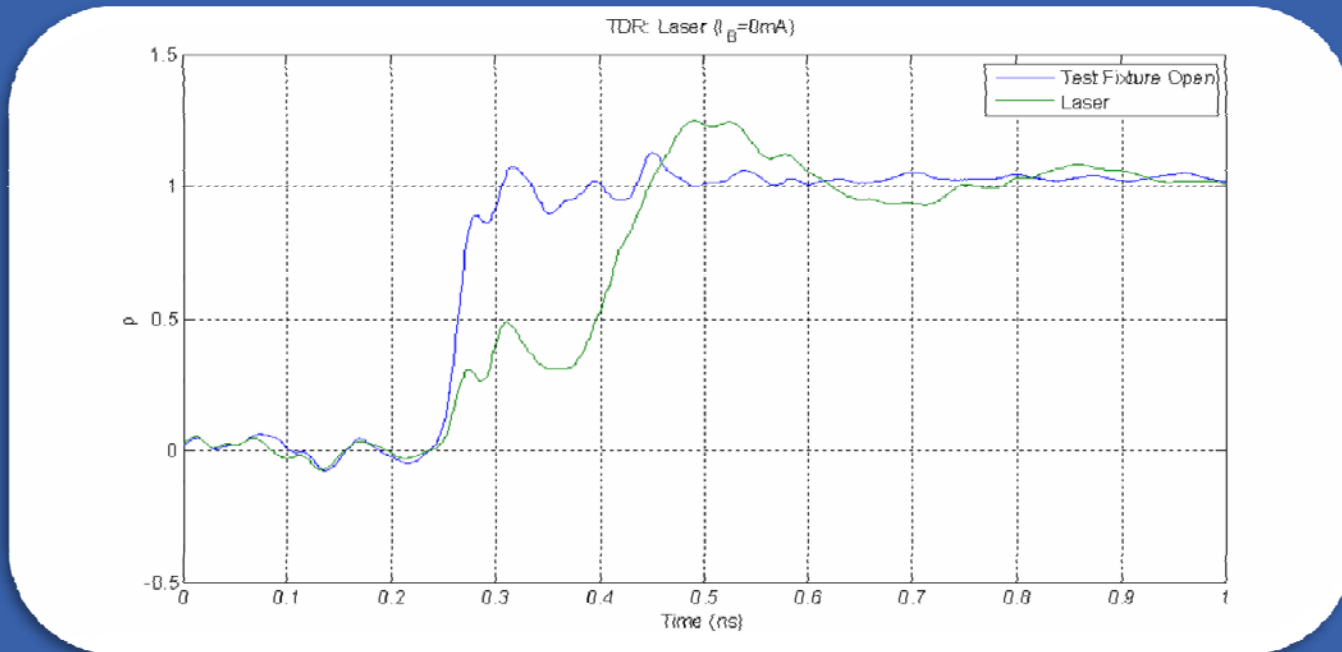
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# LASER model



- Laser TDR measurement ( $I_{bias} = 0 \text{ mA}$ )



(VL-1310-5G-P2-P4\108725-07)



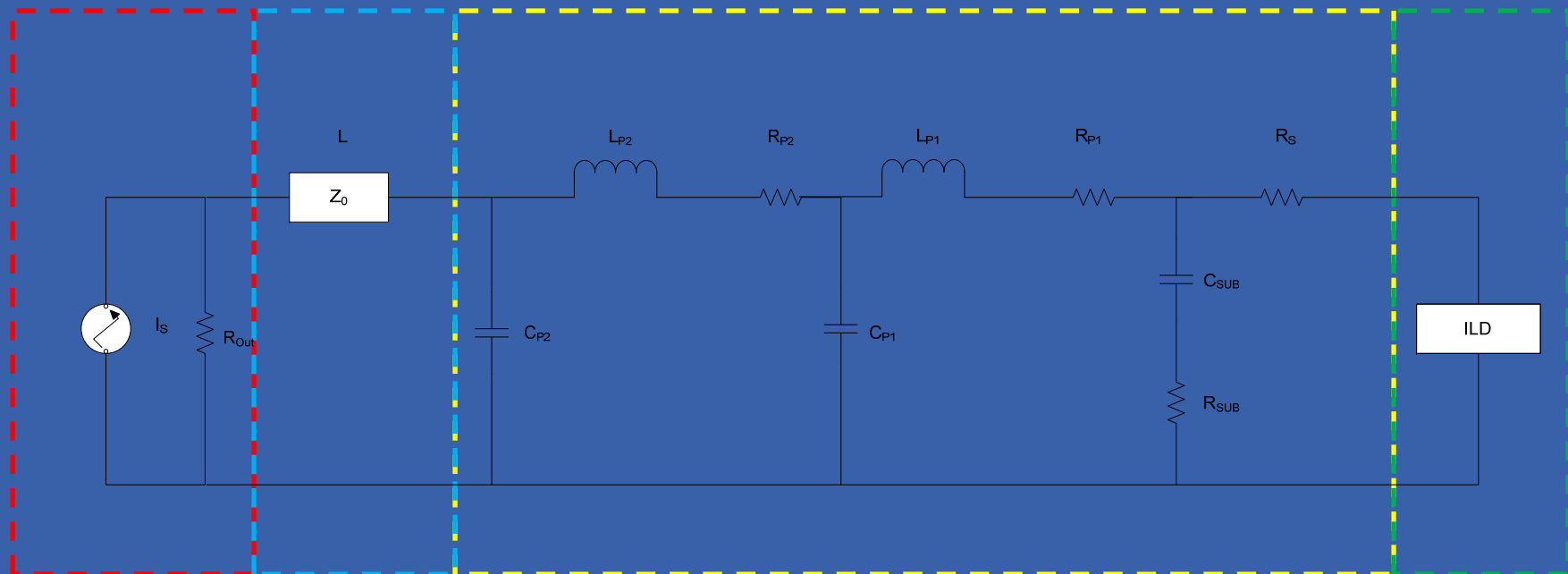




# LASER model



- Model used



Source

Test  
Fixture

Chip & Package

Intrinsic Laser



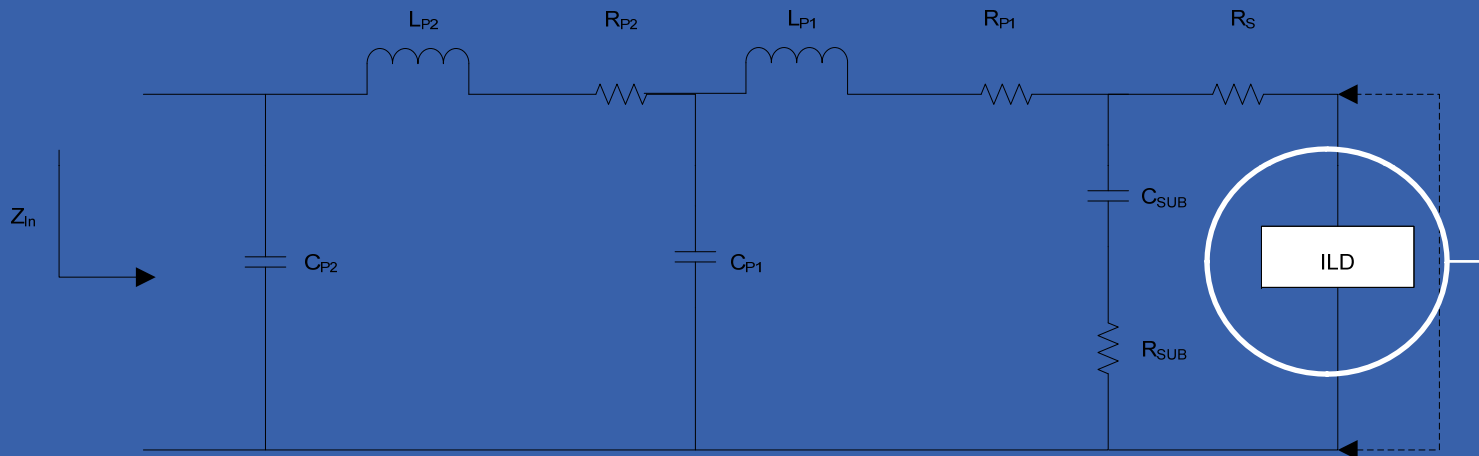
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# LASER model



- Parasitic circuit model



$$S_{11}(f) = \frac{Z_{In}(f) - R_0}{Z_{In}(f) + R_0}$$

**Bias current should have a negligible effect in  $S_{11}$ : extract the parasitic model parameters using this data**

For  $I_{Bias} > I_{th}$ ,  $|Z_{ILD}| \ll R_S$

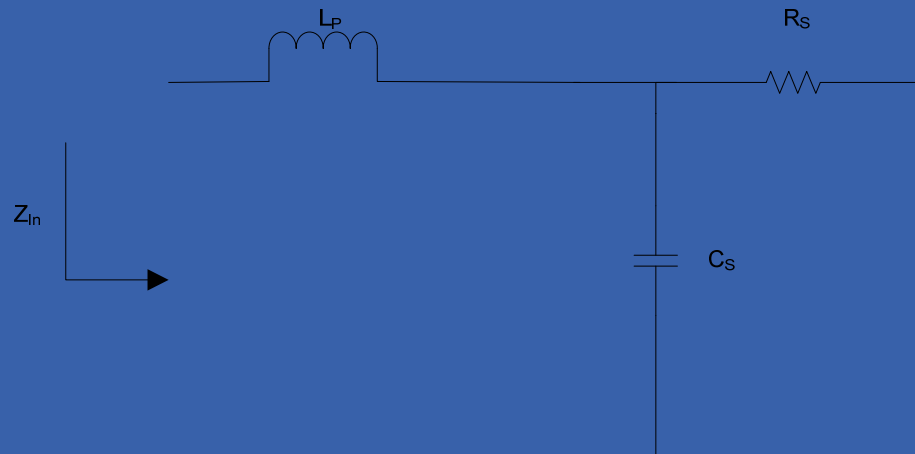




# LASER model



- Parasitic circuit simplified model



Parameters can be calculated directly from measurement data





# LASER model



- ILD model: rate equations (semiconductor LASERs):

$$\frac{dN(t)}{dt} = \frac{I(t)}{qV_a} - g_0 \frac{[N(t) - N_0]S(t)}{1 + \epsilon S(t)} - \frac{N(t)}{\tau_n}$$

$$\frac{dS(t)}{dt} = \Gamma g_0 \frac{[N(t) - N_0]S(t)}{1 + \epsilon S(t)} - \frac{S(t)}{\tau_p} + \frac{\Gamma\beta}{\tau_n} N(t)$$

$$\frac{d\phi(t)}{dt} = \frac{1}{2} \left[ \Gamma g_0 [N(t) - N_0] + \frac{1}{\tau_p} \right]$$

$$p(t) = \frac{S(t)V_a\eta_0\hbar\nu}{2\Gamma\tau_p}$$

**Carrier density**

**Photon density**

**Optical phase**

**Optical power**

- Model ILD using:
  - Explicitly through differential equations
  - Linear approximation at bias point
    - For small signal model
    - Simpler simulations



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## LASER model



- Intrinsic Laser Diode Modelling

$$\frac{H_{Global}(f, I_{Bias})}{H_{Global}(f, I_{Ref})} = \frac{H_{ILD}(f, I_{Bias})H_{PC}(f)H_{TF}(f)}{H_{ILD}(f, I_{Ref})H_{PC}(f)H_{TF}(f)} = \frac{H_{ILD}(f, I_{Bias})}{H_{ILD}(f, I_{Ref})}$$

The ILD parameters can be extracted without the influence of the package parasitic effects

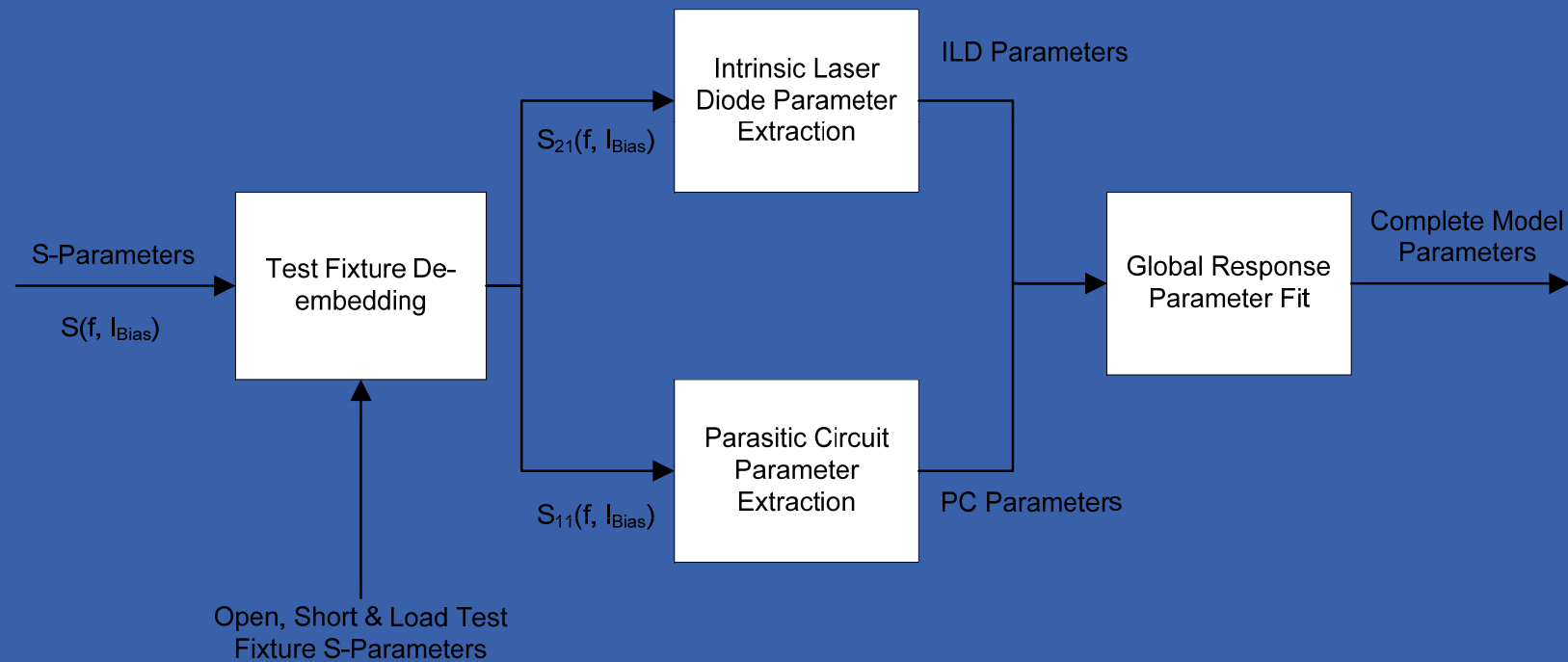




# LASER model



- Laser Model Parameter Extraction

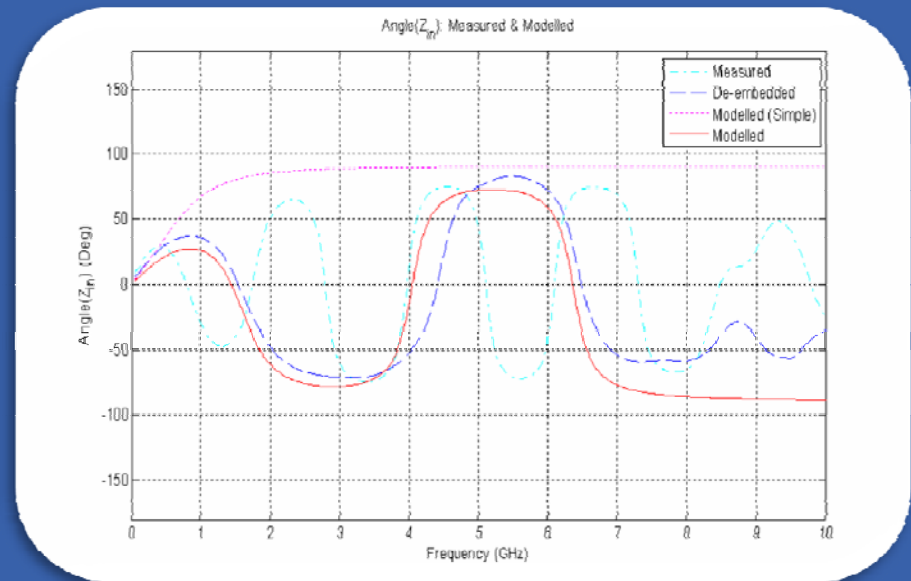
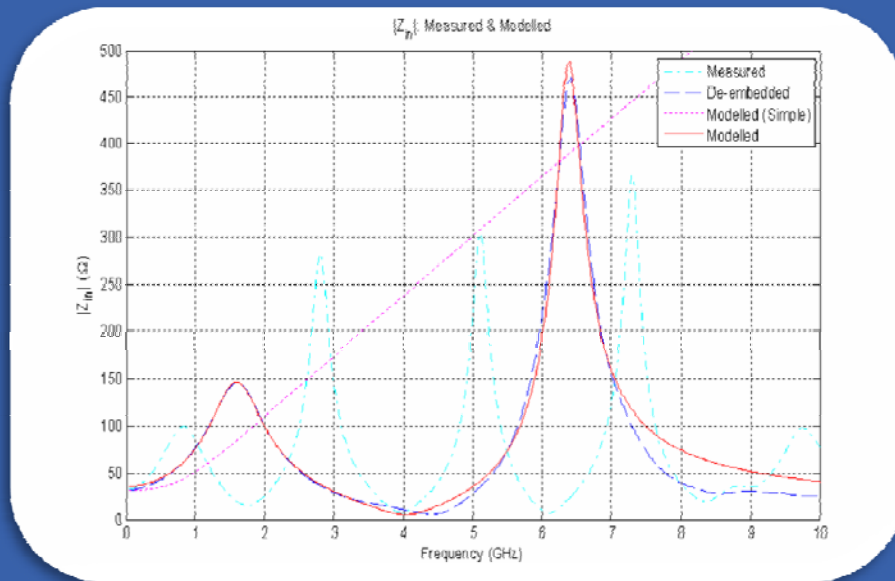




# LASER model



- Laser model : Input Impedance



**Good fit in both magnitude  
and phase over the frequency  
range of interest**

(VL-1310-5G-P2-P4\108725-07)

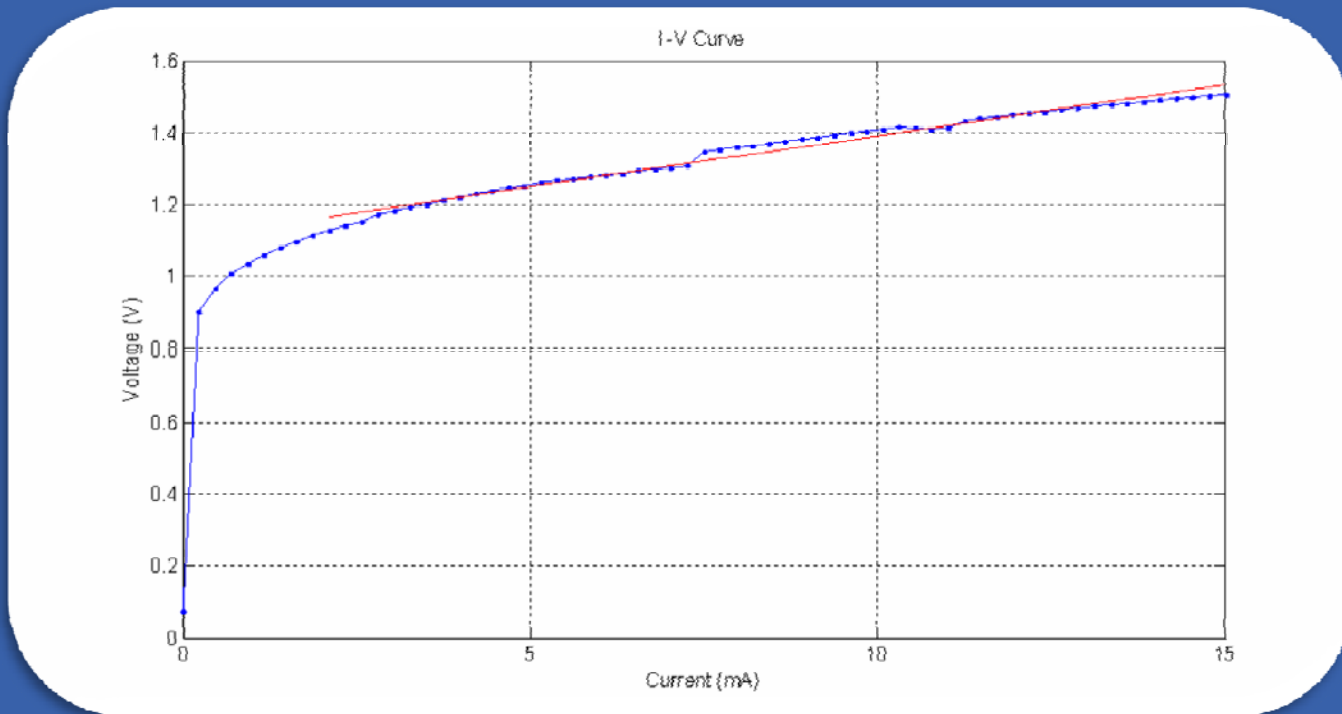




# LASER model



- Laser model : Input Impedance



**Agreement of  
DC internal  
resistance  
values  
between  
measures**

$R_S = 24 \Omega$  (extracted from  $S_{11}$ )  
 $R_S = 28 \Omega$  (extracted from I-V)

(VL-1310-5G-P2-P4\108725-07)



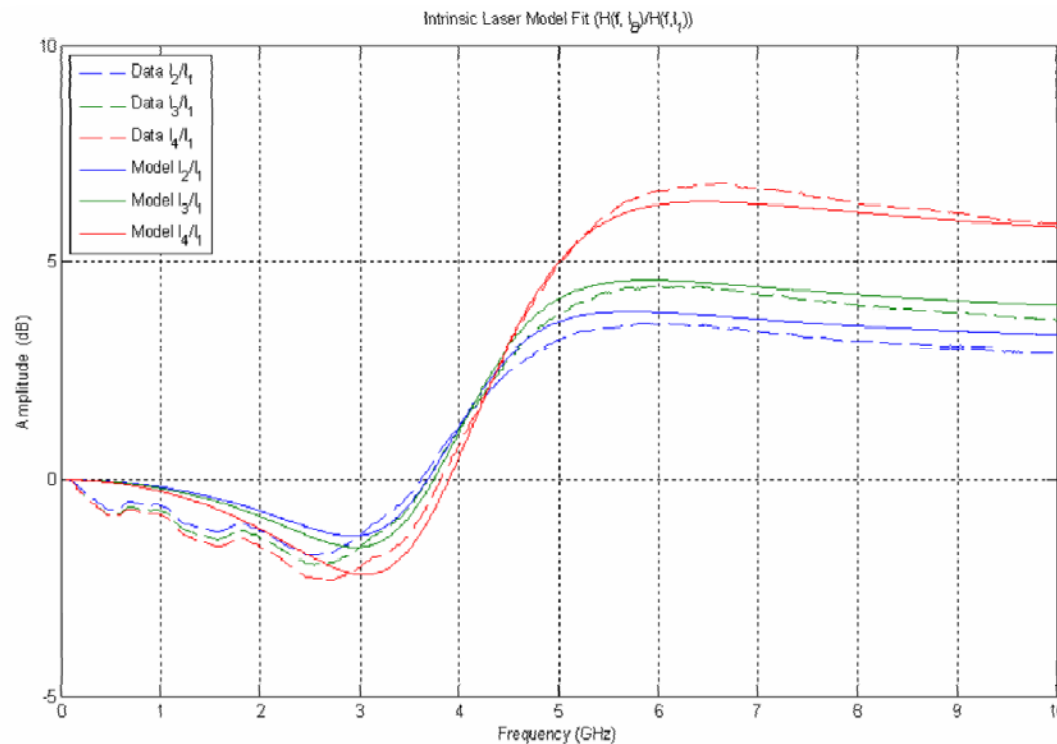




# LASER model



- Laser model : Intrinsic Laser Model



**Good agreement  
between the  
curves obtained  
with the model  
and the measured  
data**

(VL-1310-5G-P2-P4\108725-07)

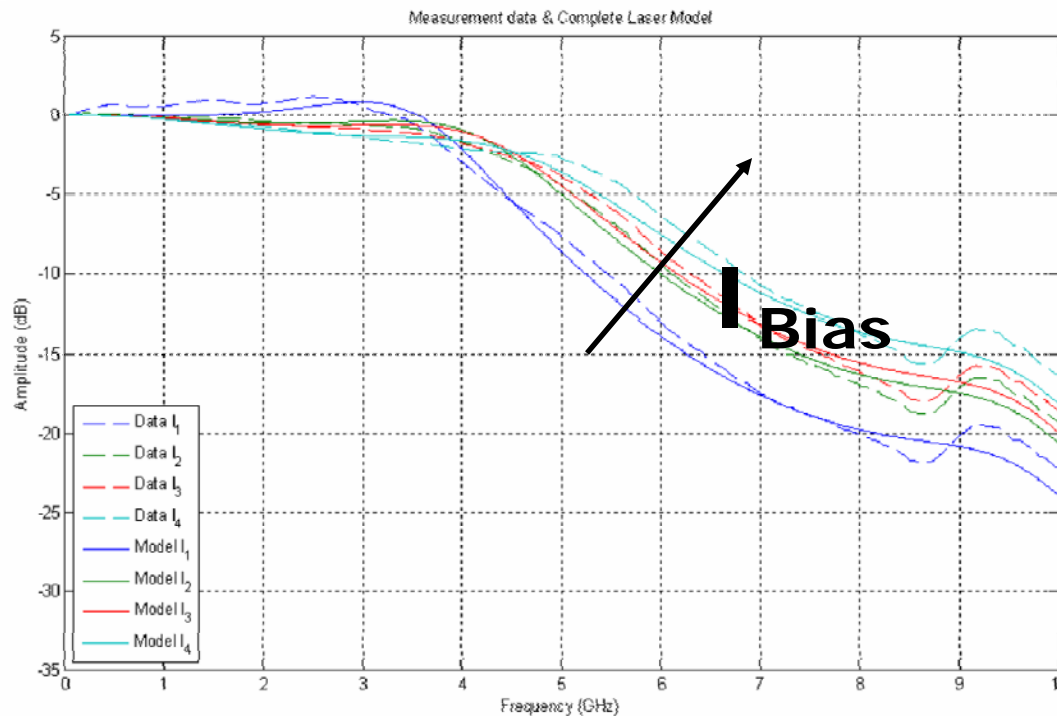




# LASER model



- Laser model : Global model (Transfer function)



**Good model fit:**

- Clear dependence on bias
- Bandwidth increases as bias increases

(VL-1310-5G-P2-P4\108725-07)

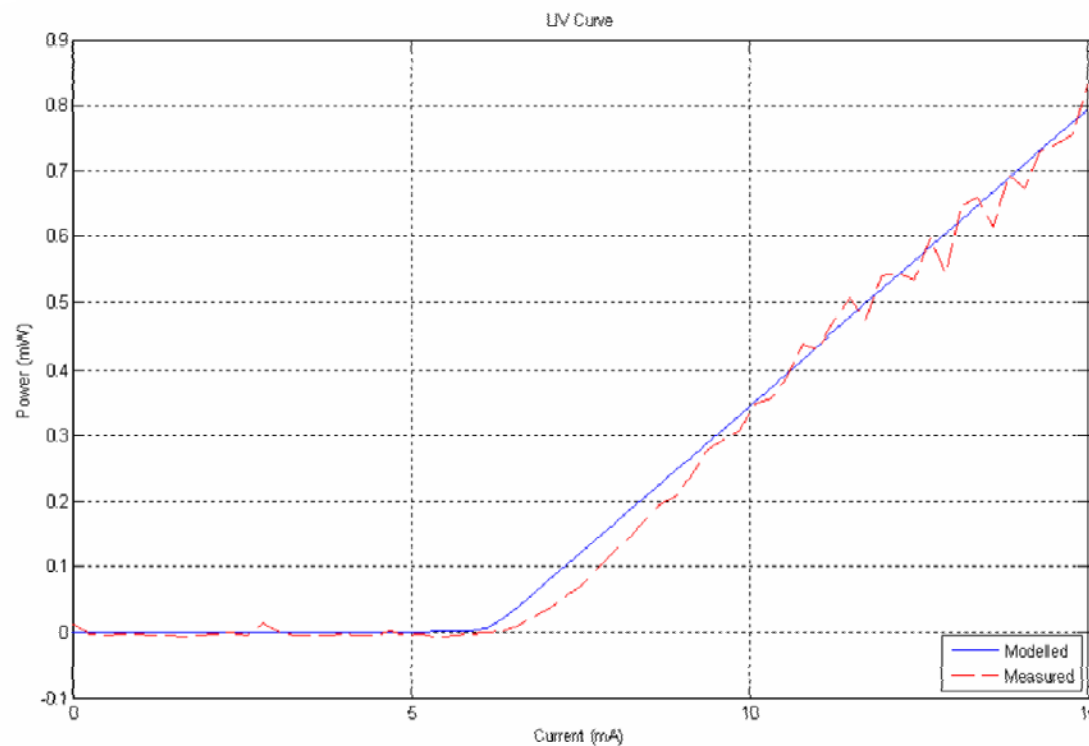




# LASER model



- Laser model : Global model (I-L Curve)



**Model is able to predict back a quantity that was not included in the model fit**

(VL-1310-5G-P2-P4\108725-07)

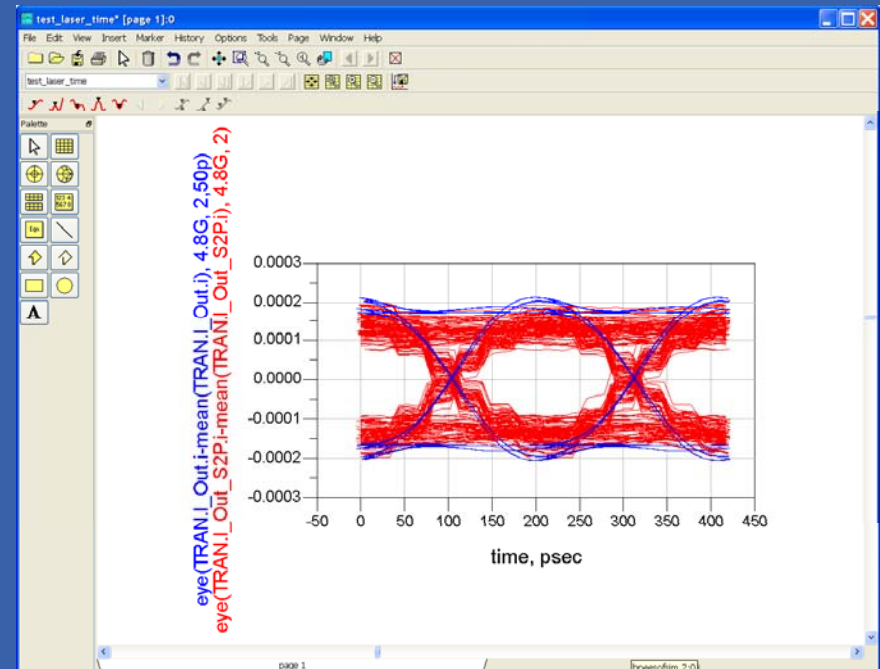
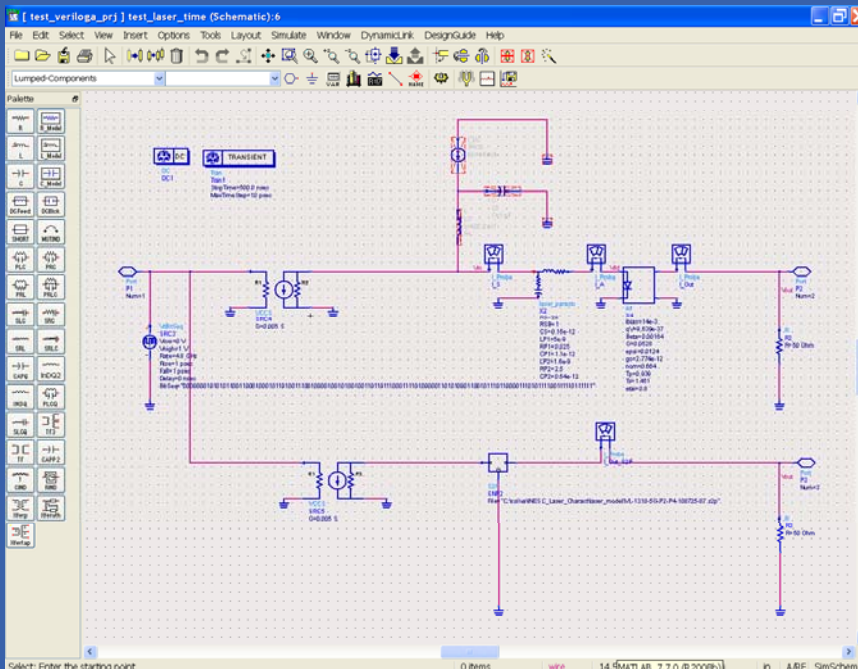




# On going work



- Model tuning (evaluate model with transceiver designer):



Simulation using the developed Verilog-A implementation of the laser model in ADS

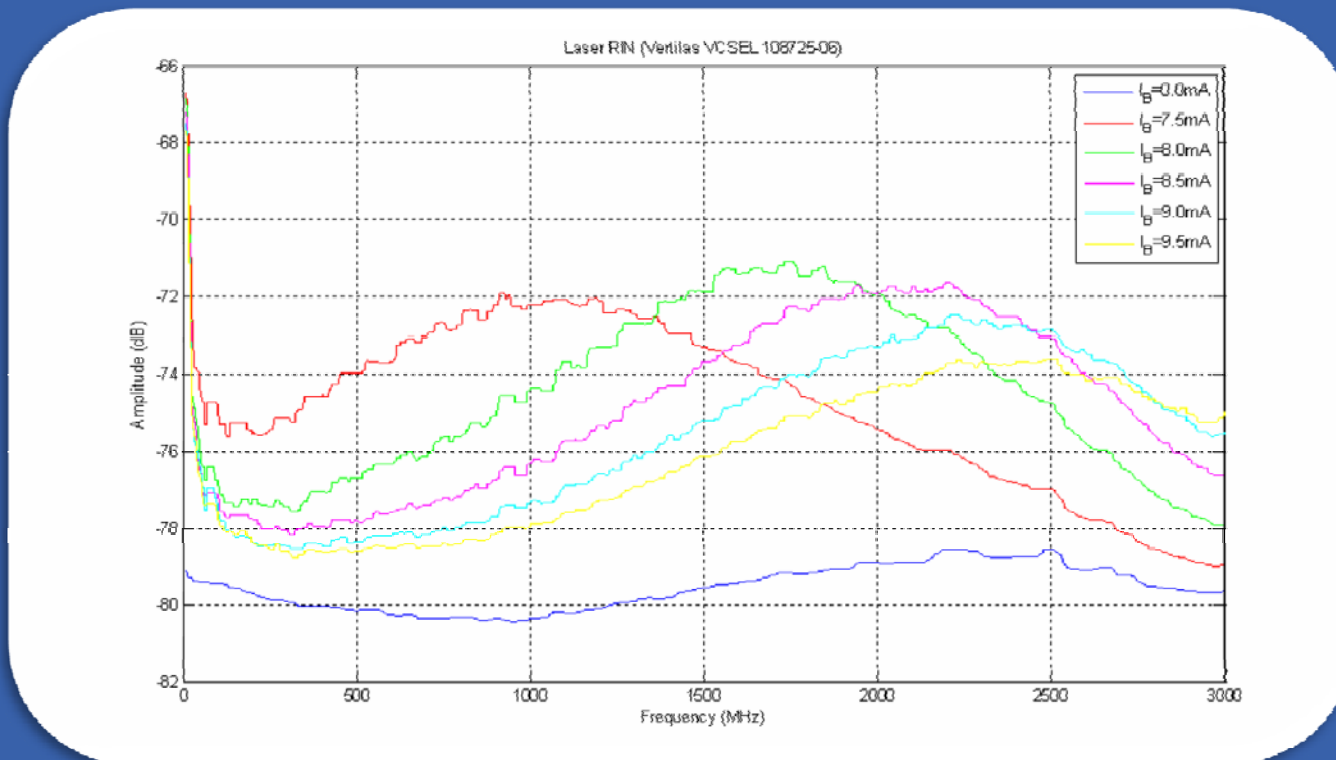




## On going work



- Laser parameter extraction using noise (RIN) measurements:



(VL-1310-5G-P2-P4\108725-07)

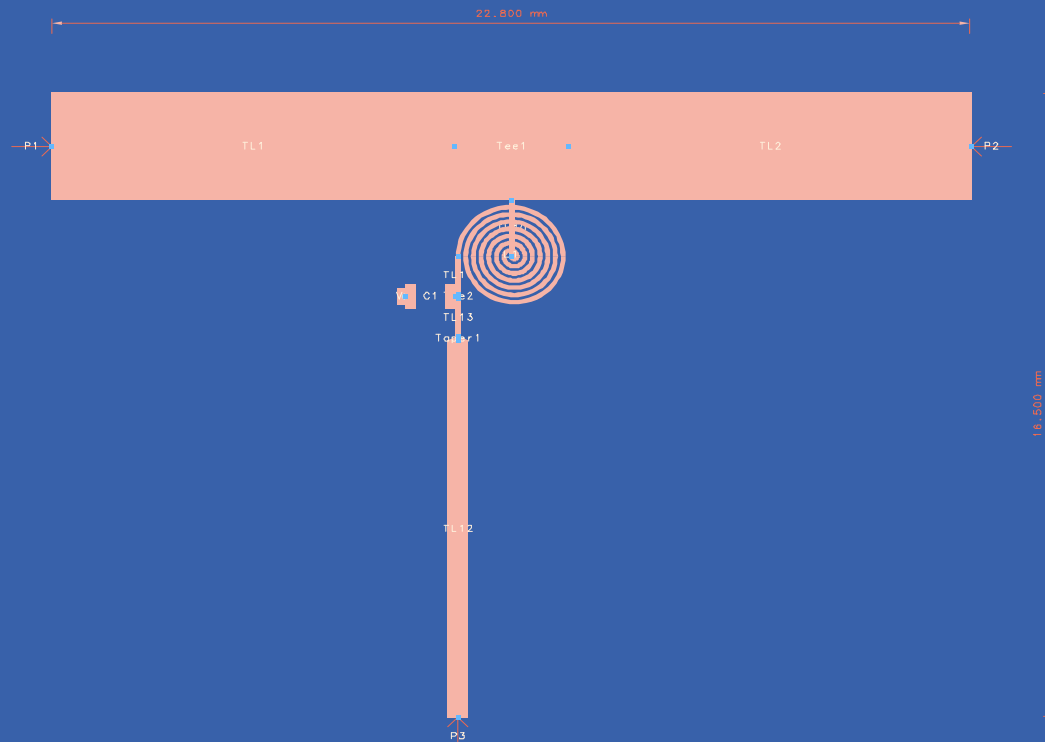




# On going work



- Microstrip Bias-T:





## Conclusion



- A laser model suitable for large variety of laser was developed.
- Accurate modelling of the input impedance was achieved:
  - Essential for designing matching network and bias-T.
- Good agreement obtained between the ILD model and the measured data:
  - Transfer-function;
  - L-I curve;
  - Eye-Diagram.
- Development of good-practices in HF PCB layout.

**Thank you for your attention!**



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