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# Update on CCT



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- CCT for FCC
  - Electromagnetic design
  - Mechanical design
- The PSI CCT model program
  - Roadmap
  - Status







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#### CCT joined the fold in Nov. 2016





#### CCT Design for FCC



- Keys to an efficient CCT design:
  - 1. Thin spars
  - 2. Wide cable, large strands  $\vdash$  Increase  $J_{e}$ .
  - 3. Thin ribs.





### PSI's CCT Design for FCC



#### • Current: 18055 A

| Layer # | n <sub>s</sub> | cuNc | loadline<br>marg. [%] | current<br>marg. [%] | T <sub>peak</sub><br>[K] | V <sub>grnd</sub><br>[V] | J <sub>cu</sub><br>[A/mm²] |
|---------|----------------|------|-----------------------|----------------------|--------------------------|--------------------------|----------------------------|
| 1       | 29             | 0.8  | 14.2                  | 111                  | 292                      | 1133                     | 1237                       |
| 2       | 25             | 1.1  | 14.4                  | 95                   | 342                      | 1264                     | 1217                       |
| 3       | 22             | 1.95 | 14.4                  | 74                   | 310                      | 1156                     | 1096                       |
| 4       | 20             | 2.6  | 15.7                  | 70                   | 338                      | 1144                     | 1103                       |

## Homogeneous coil temperature after quench.

#### Temperature [K]



- FCC-wide conductor use:
  - Total: 9.77 kt (+30% wrt. cosine theta/block)
  - NonCu: 3.75 kt
  - Cu: 6.02 kt
- Total inductance: 19.2 mH/m
- Total energy: 3.2 MJ/m



Geometric/nl. iron harmonics: b2 <= 6 units b3,4,5, .. <= 1 unit



#### 3-D Magnetic Design



#### 3-D modeling results:

- Yoke cut-back not needed (20 mT peak-field enhancement in ends).
- Magnetic length with yoke equal to that of bare coil.
- **Physical length** minus magn. length = 53 cm; equal to 11 T magnet.
- **Peak field** minus main field at 16-T bore field: 0.14 T excluding self field.
  - comparable or lower than cos-theta due to continuous current distribution.





Courtesy M. Negrazus



**Mechanical Structure** 



- CCT does not require azimuthal prestress.
- Radial prestress on the midplane provided by "scissor" laminations







NODAL SOLUTION

EMX =,539E=03 SMN =-,962E+08 SMX =,176E+09

K X

STEP=3

SUB =1 TIME=3

ANSYS R17.2 Academic

MAY 26 2017 14:31:11

511865

.346E+08

.688E+08

.103E+09

.137E+09 .171E+09

.205E+09

.239E+09

.274E+09

.308E+09

SY RSYS-101 (AVG)

#### 2D Mechanical Design





Nominal (16 T, 1.9 K)



#### **3-D** Periodic Simulation



- Generalized plane stress condition applied (following D. Arbelaez, L. Brouwer, LBNL)
- Initial 3-D results confirm 2D, but show distinct imprint of scissors lams
  - $\rightarrow$  increase protective shell thickness, change its material to iron



 $\rightarrow$  decrease lamination thickness.



#### Courtesy G. Rolando







- Improve windability through inclined channels.
- Winding tests at LBNL and PSI.
- Successful tests with LD1 cable (@LBNL), LBNL CCT cable, and 11-T cable (@PSI).



radial channel: de-cabeling











Machinability



 Successful test machining of 16-mm-deep 2-mm-wide 15-degree-inclined channels.



Courtesy Heinz Baumgartner AG

• FNAL gives some meters of cable for winding test.



#### Double-Helix CCT for FCC



Winding two Rutherford-cables into one groove, connected in series:

- Conductor weight from 9.77 kt to 9.22 kt (fewer ribs).
- Operating current from 18 kA to 16 kA.
- Inductance from 19 mH to 24 mH.
- <sup>1</sup>/<sub>2</sub> Cable unit length.
- <sup>1</sup>/<sub>2</sub> Machining path with increased speed.







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### PSI Goals towards FCC Requirements

- BERKELEY LAB
- Thin spars
- Exterior Bladder and Key structure
- Impregnation system (NHMFL resin, etc.).
- Fast quench detection and CLIQ protection.
- Wide Rutherford cable.
- Inclined channels manufacturing.









#### **Mechanical Structure**



Bladder and Key technology chosen for tuneability and relative simplicity.

- Closed and pre-loaded pad gap for maximum-rigidity cage around coils.
- Steel pads to better match coil differential contraction.
- Designed with S. Caspi, LBNL.



International conceptual design review of CD1 on June 26 at CERN (<u>http://indico.cern.ch/e/cd1cdr</u>).



### Machining and Reaction Tests.









• Reaction-trial at CERN successful, channel-geometry validated.

Test formers delivered.

• First machining-, and winding-tests.

Test winding completed.



Preparation for heat treatment.



Before heat treatment



After heat treatment



### High-Voltage and Impregnation Tests



- Mica-reinforced glass-sleeve insulation, impregnated with CTD 101-K at CERN.
- Tested so far up to 5 kV without breakdown.
- Next steps: test up to 10 kV.
- Cut the sample for microscopic control of impregnation.





Technical Coil Design

procurement of CD1 winding former and splice box.





• With essential LBNL input from drawings and discussions, we are launching



**Procurement of Reaction Furnace** 







#### **Impregnation Trials**



- Vacuum-bag impregnation training @CERN.
- First vacuum-bag impregnation at PSI in refurbished curing oven.
- Vacuum-vessel and heating-system procurement started.







Courtesy G. Montenero



### Mechanical-Model Preparation



- Shell- and pads shipped.
- All other components delivered.











#### Strain-Gauge Measurement Setup



- Strain-gauges mounted, tested, and validated at PSI.
- Dedicated training @CERN in the near future?







#### Courtesy G. Montenero





- The CCT option was established as a valid contender in the FCC design study.
- The PSI program has been designed to be complementary to and closely coordinated with the LBNL program, pushing towards specific features needed in an FCC magnet.
- PSI benefits from generous support by LBNL, integrating deeply with their program, as well as from regular exchanges and training with CERN staff who share freely and are most helpful – THANK YOU!









#### Lessons from CCT4 Test:



- 1. the magnet was not performance limited it only had subpar training.
- 2. three issues must be addressed to improve (and eventually eliminate) the training:
  - a) epoxy cracking (strong evidence in acoustic data),
    - alternatives to CTD-101-K will be tested.
    - alternative filling-schemes will be tested.
  - b) epoxy de-lamination from the metal former,
    - chemical etching to increase surface roughness will be tested.
  - c) friction due to intra-layer movement (strong evidence in acoustic data),
    - a slip-plane will be introduced.





#### **Protection Studies**



- Co-wound copper secondary windings significantly accelerate the current decay.
- Relevant only if detection and active-protection can be made more efficient.
- Cowound wire and/or interrogated optical fibers have potential to bring detection time to the order several milliseconds.
- CLIQ on CCTs promises to be effective.
- Numerical studies under way.
- About to join LBNL (L. Brouwer) effort to create user-defined ANSYS "quench elements" for consistent and efficient CLIQ modeling in ANSYS.





### Manufacturability and Cost



- Deep channels, aspect-ratio ~10.
- Inclined channels  $\rightarrow$  5-axis machining on long rotating cyl., machining tests under way.
- Selective Laser Melting (3-D printing) not successful.
- **Collaboration with IWS Fraunhofer** on fabrication of **thin-lamination formers**.
  - Laser cutting, spot welding + diffusion welding.
  - Goal: improve scalability and cost.







