

E<sub>uro</sub> C<sub>ir</sub> C<sub>ol</sub>

## 2<sup>nd</sup> Review of the EuroCircol WP5

### Block coil: mechanics

CEA

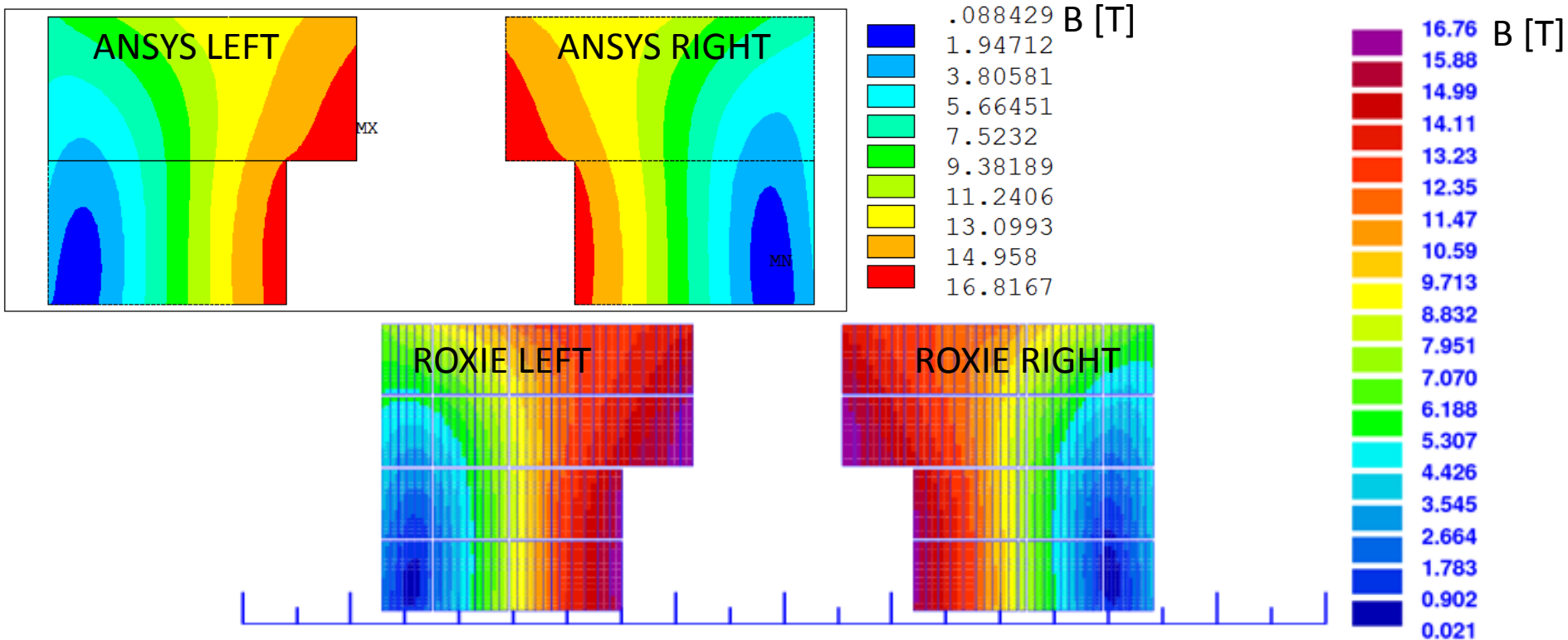
CERN, 9 oct 2017

# Mechanical investigation

- Double aperture model 194 mm interbeam
- Investigation up to **16.0 T** central field (**100%** of nominal current)
- Bladder&key structure
- 2D analysis

# Magnetism Roxie-Ansys

- Ansys:** Coefficient 1.01 on the current: 10 100 A instead of 10 000 A in Roxie



kN/m	Roxie	Roxie	Ansys	Ansys
	Left	Right	Left	Right
Fx	-8269	7636	-8259	7634
Fy	-3535	-2960	-3649	-3071

- Coil maximum stress
  - @ 4.2 K: 200 MPa
  - @ 300 K: 150 MPa

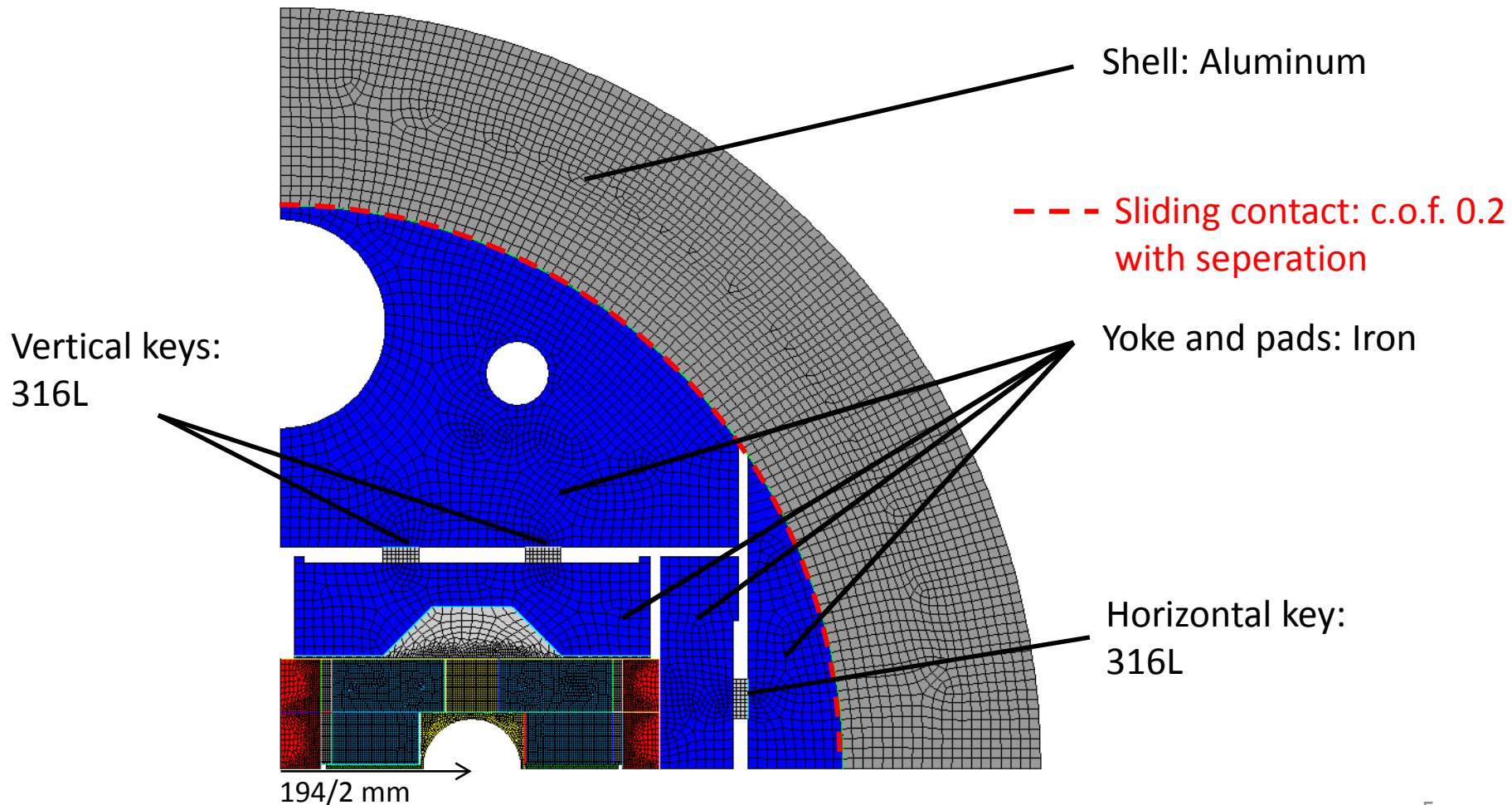
Material	R <sub>p0.2</sub> [MPa]	
	293 K	4.3 K
Al 7075	480	690
SS 316 LN	350	1050
NITRONIC 40	350	1240
Ferromagnetic iron	<del>180</del> 230	720*
Ti 6Al 4V	800	1650

Material	E [GPa]		pr	$(L_{4.3K} - L_{293K}) / L_{293K}$
	293 K	4.3 K		
Coil	EX = <del>44</del> 25 EY = <del>52</del> 30 GXY = 21	EX = <del>44</del> 27.5 EY = <del>52</del> 33 GXY = 21	0.3	X = 3.36e-3 Y = 3.08e-3
StSt	193	210	0.28	2.84e-3
Iron	213	224	0.28	1.97e-3
Aluminum	70	79	0.34	4.2e-3
Titanium	<del>130</del> 115	<del>130</del> 126.5	0.3	1.74e-3
Nitronic 40	210	225	0.28	2.6e-3

\*Ferromagnetic iron @ 4.2 K stress < ~~200~~ 380 MPa in tension (1st principal stress)

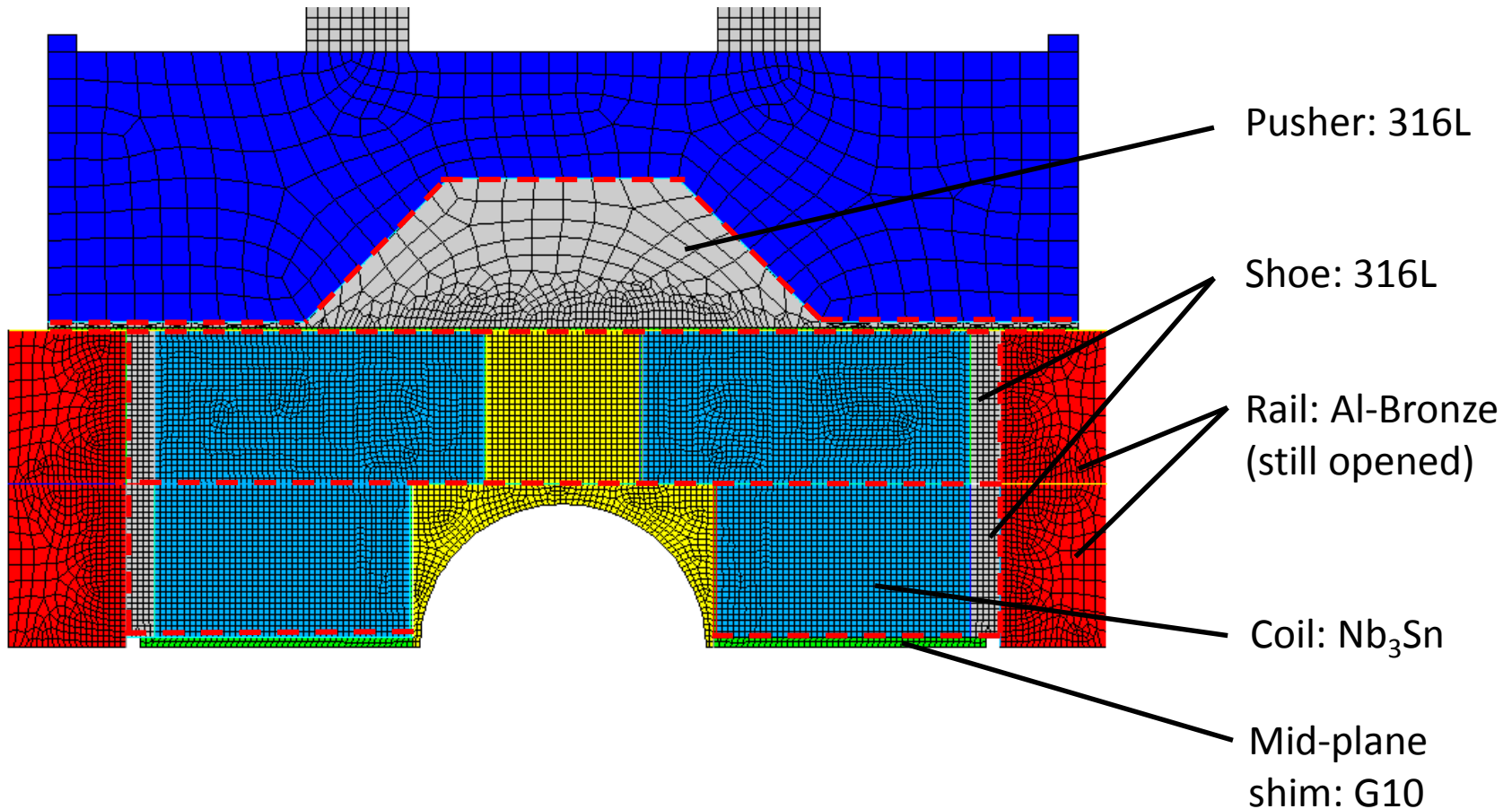
# 2D model description

- Double aperture: 194 mm interbeam



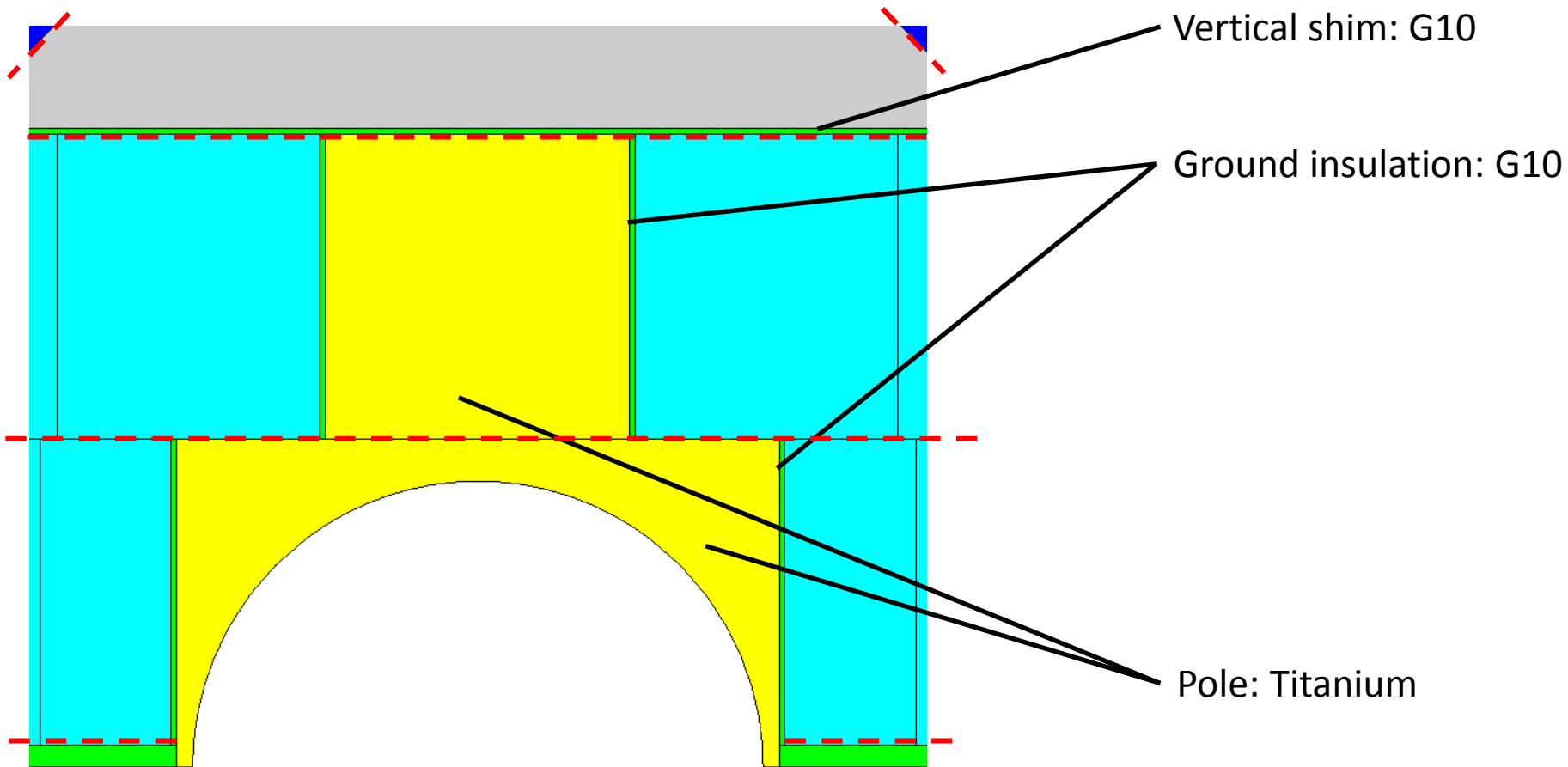
# 2D model description

--- Sliding contact: c.o.f. 0.2  
with separation



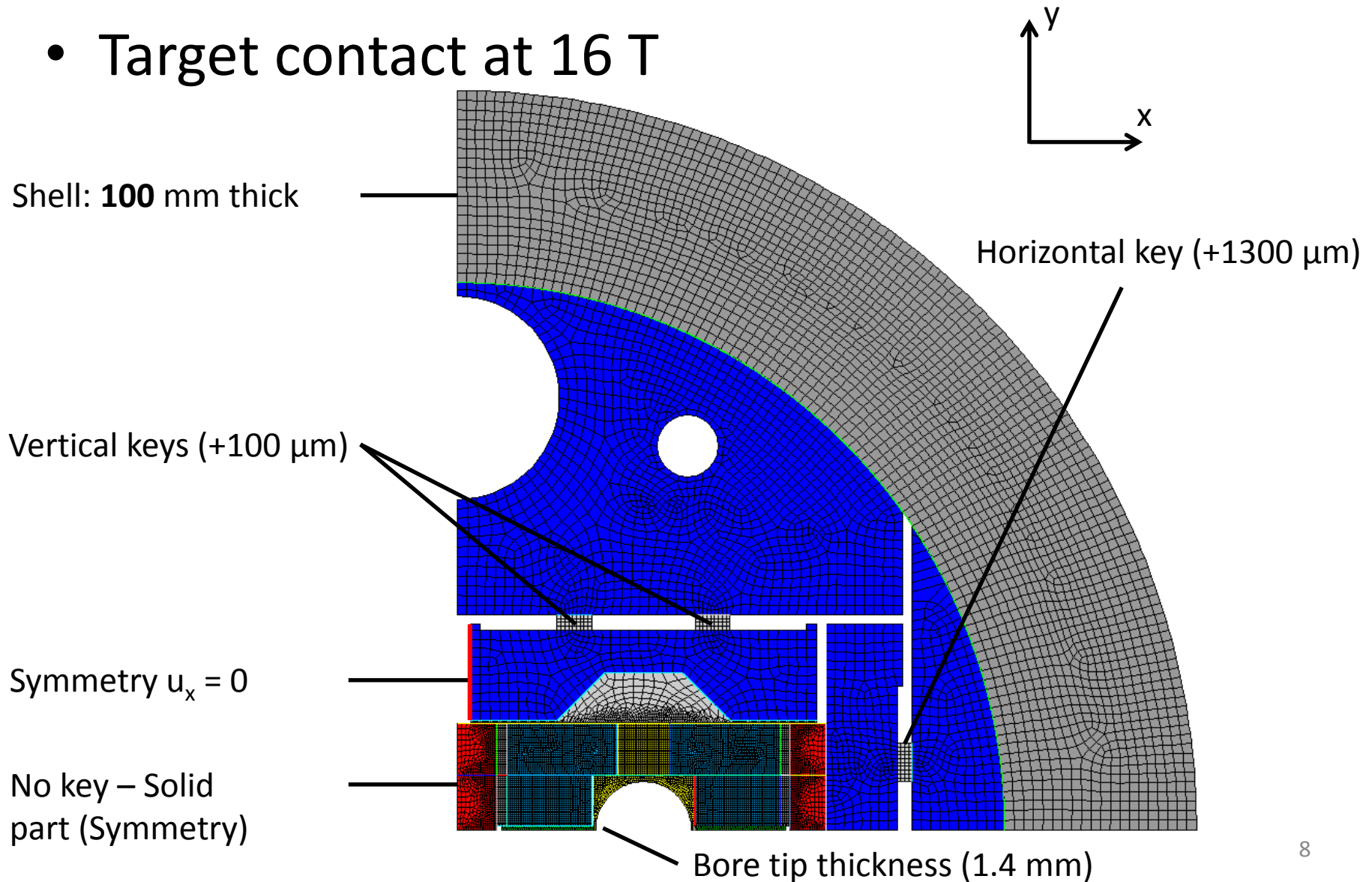
# 2D model description

--- Sliding contact: c.o.f. 0.2 with separation



# Model features

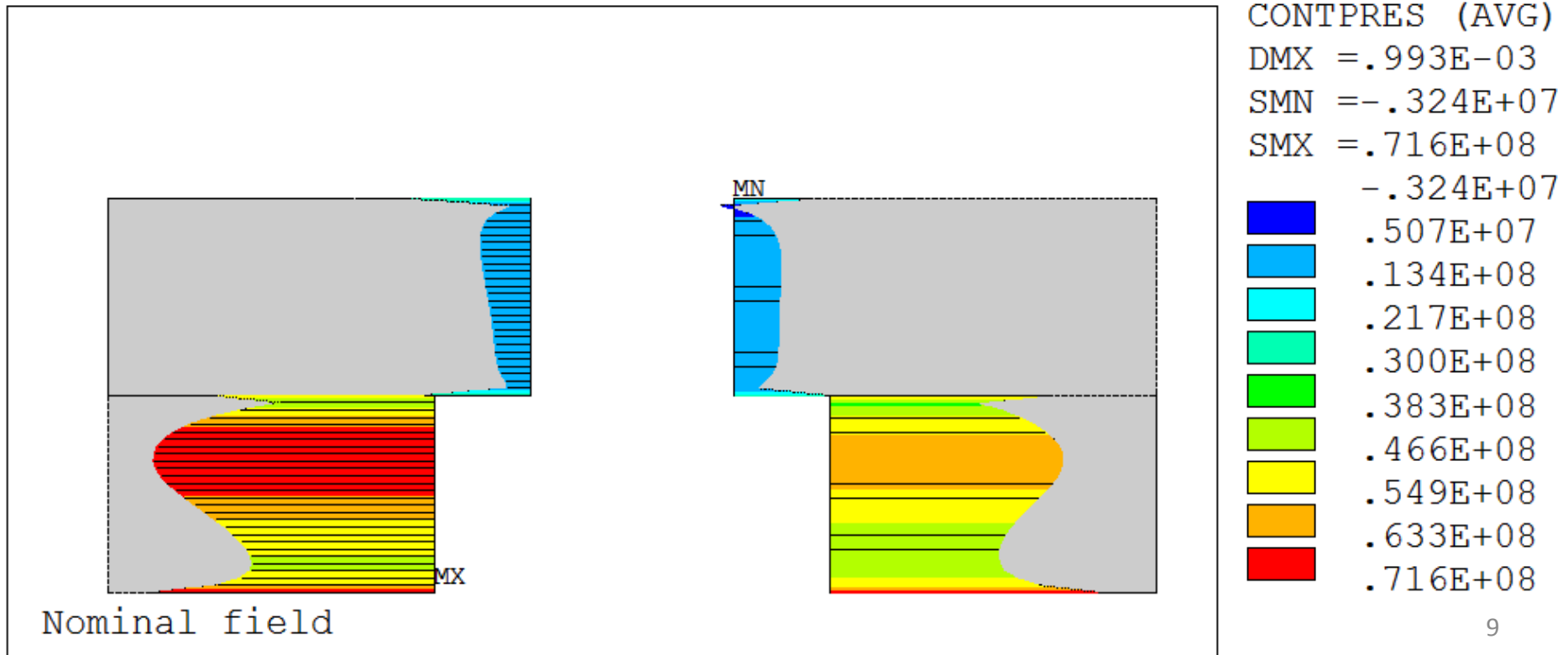
- Target contact at 16 T





# Contact at 16 T

- Distribution under nominal operation:
  - Reminder  $F_{x\_left} = 8.3 \text{ MN/m}$ ;  $F_{y\_left} = 3.5 \text{ MN/m}$
  - Contact from  $-3 \text{ MPa}$  (tension) to  $72 \text{ MPa}$  (compression)



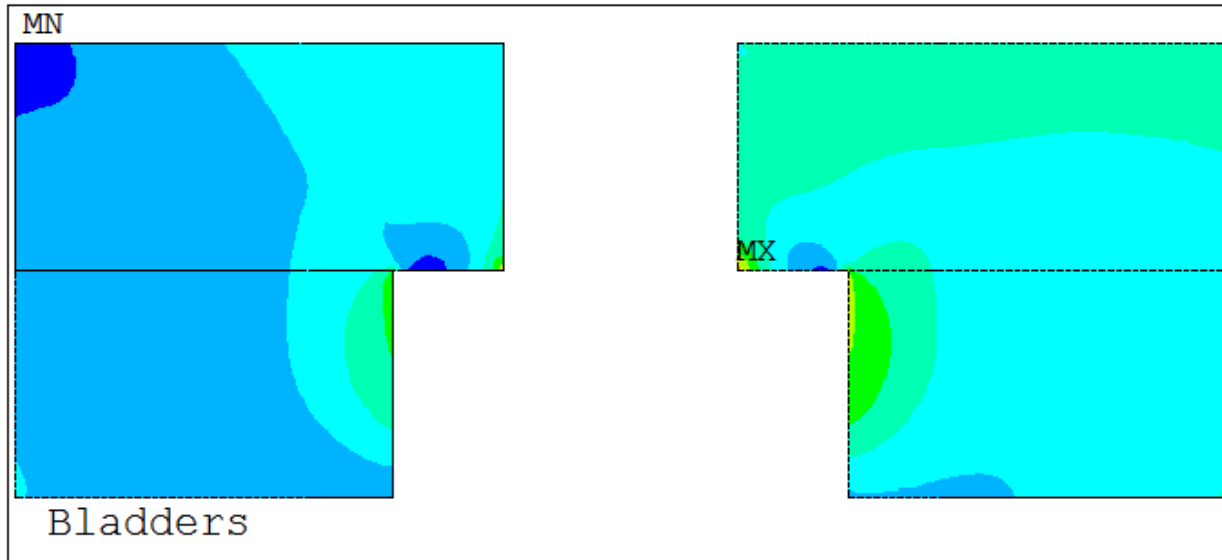
# Nb<sub>3</sub>Sn coil stress (bladders)

- Von Mises stress (bladders inflated)

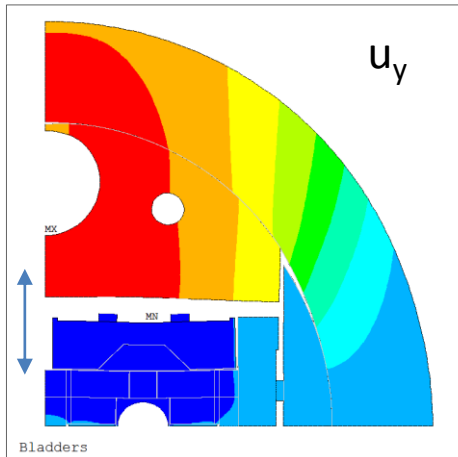
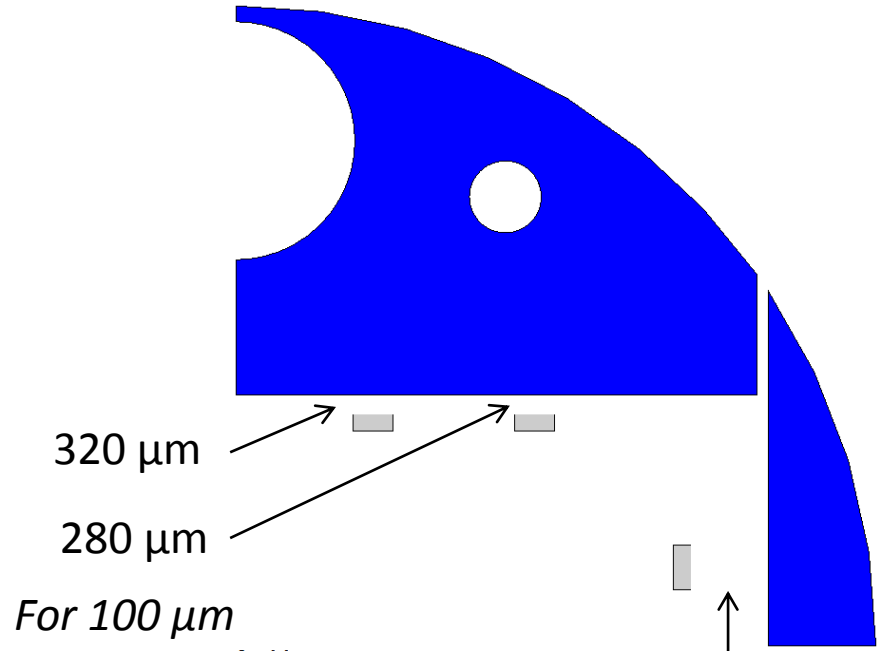
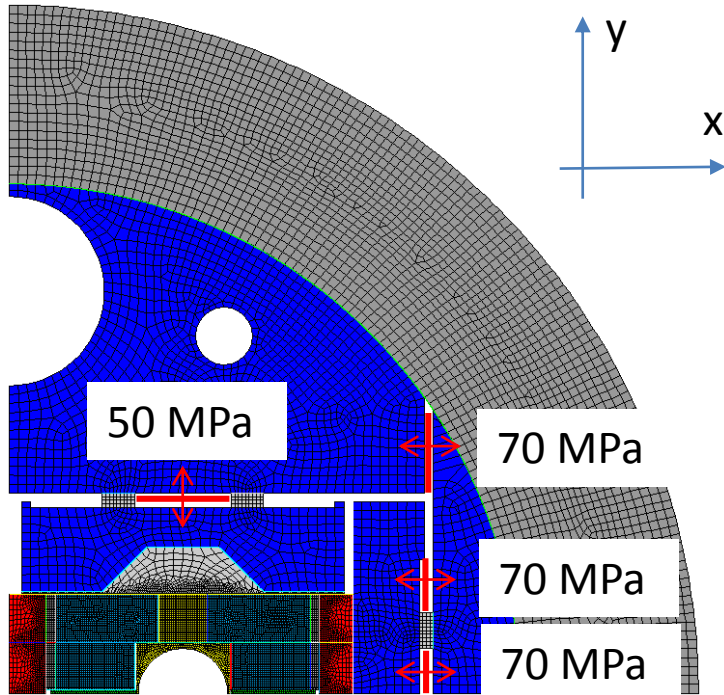
```

SEQV      (AVG)
PowerGraphics
EFACET=1
AVRES=Mat
DMX  =.296E-03
SMN  =.297E+08
SMX  =.133E+09
      .297E+08
      .412E+08
      .527E+08
      .642E+08
      .757E+08
      .872E+08
      .987E+08
      .110E+09
      .122E+09
      .133E+09
  
```

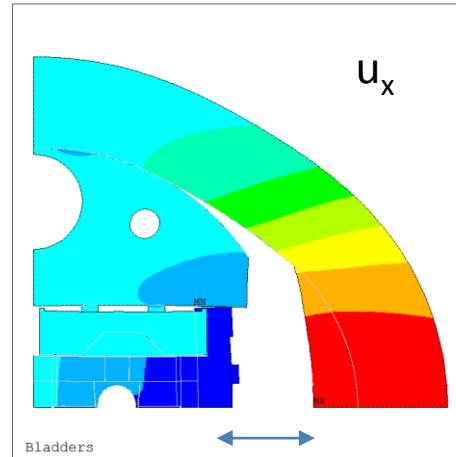
Peak von Mises stress: 133 MPa



# Bladder inflation



ANSYS Release 16.1  
 NODAL SOLUTION  
 STEP=1  
 SUB =1  
 TIME=1  
 UY (AVG)  
 RSYS=0  
 PowerGraphics  
 EFACET=1  
 AVRES=Mat  
 DMX =.312E-03  
 SMN =-.402E-04  
 SMX =.312E-03  
 -.402E-04  
 -.111E-05  
 .380E-04  
 .771E-04  
 .116E-03  
 .155E-03  
 .194E-03  
 .233E-03  
 .273E-03  
 .312E-03

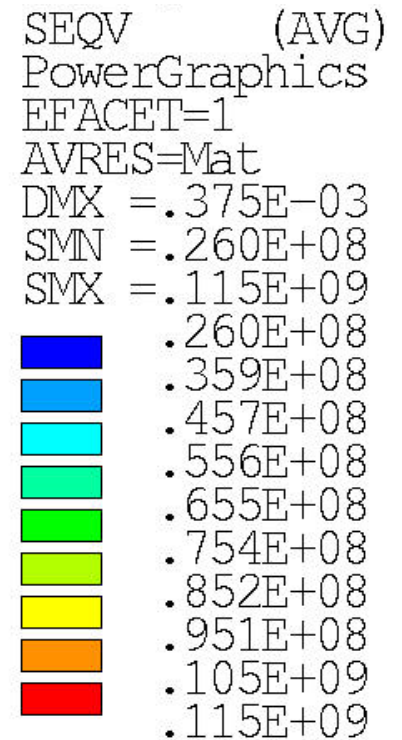
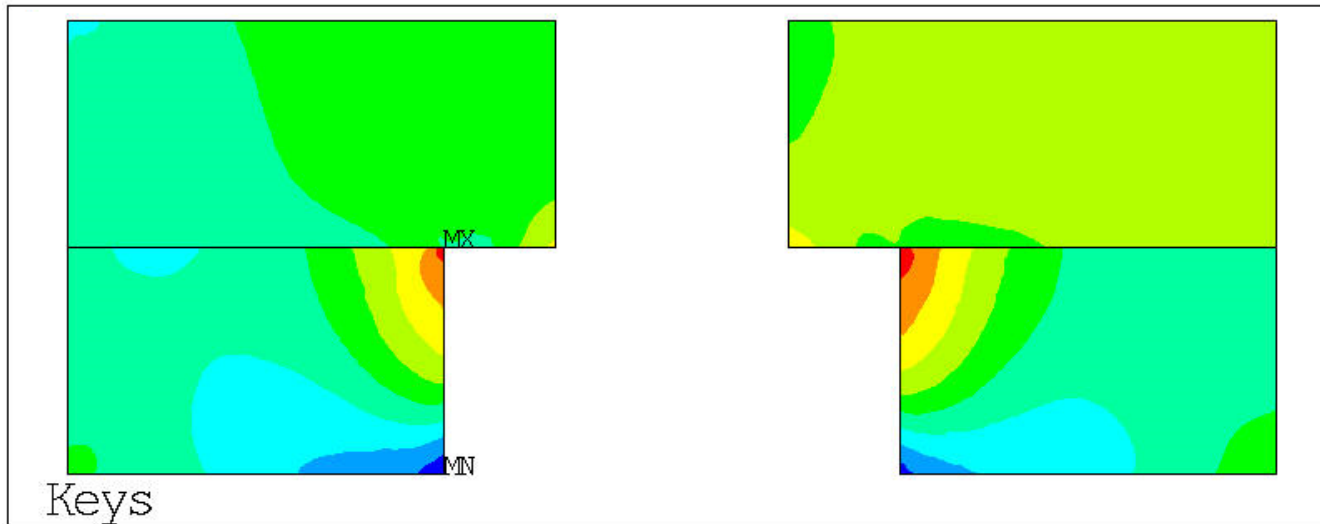


ANSYS Release 16.1  
 NODAL SOLUTION  
 STEP=1  
 SUB =1  
 TIME=1  
 UX (AVG)  
 RSYS=0  
 PowerGraphics  
 EFACET=1  
 AVRES=Mat  
 DMX =.001281  
 SMN =-.384E-03  
 SMX =.001281  
 -.384E-03  
 -.199E-03  
 -.140E-04  
 .171E-03  
 .356E-03  
 .541E-03  
 .726E-03  
 .911E-03  
 .001096  
 .001281

# Nb<sub>3</sub>Sn coil stress (keys in)

- Von Mises stress (keys in)

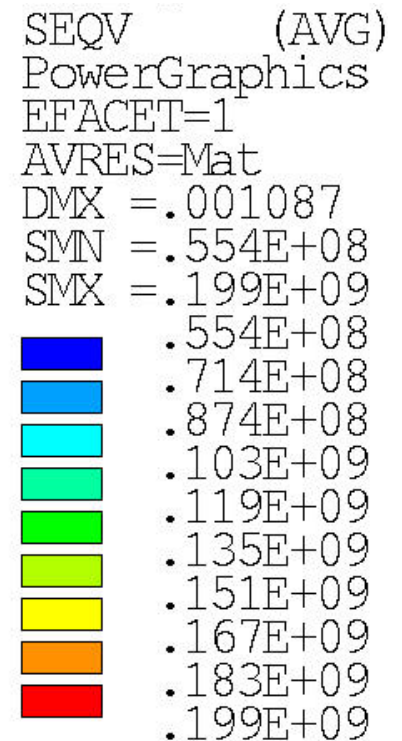
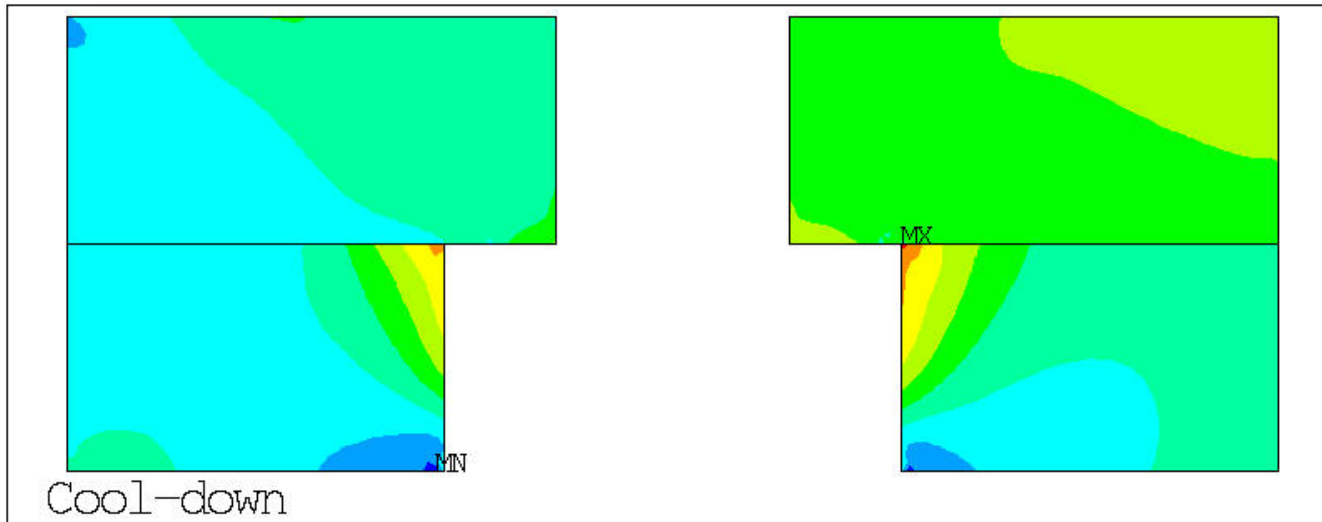
Peak von Mises stress: 115 MPa



# Nb<sub>3</sub>Sn coil stress (cool-down)

- Von Mises stress (cool-down)

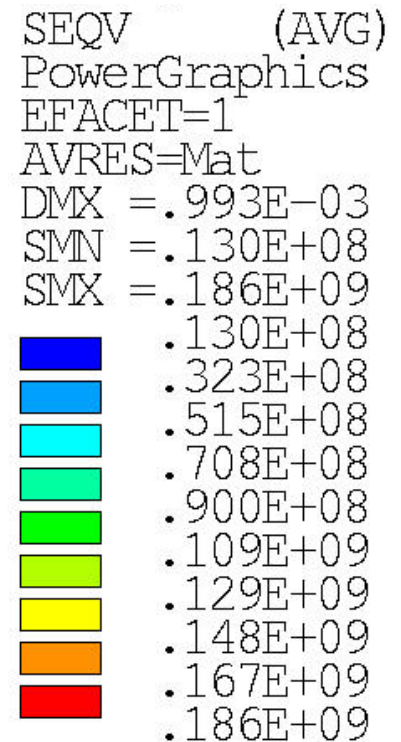
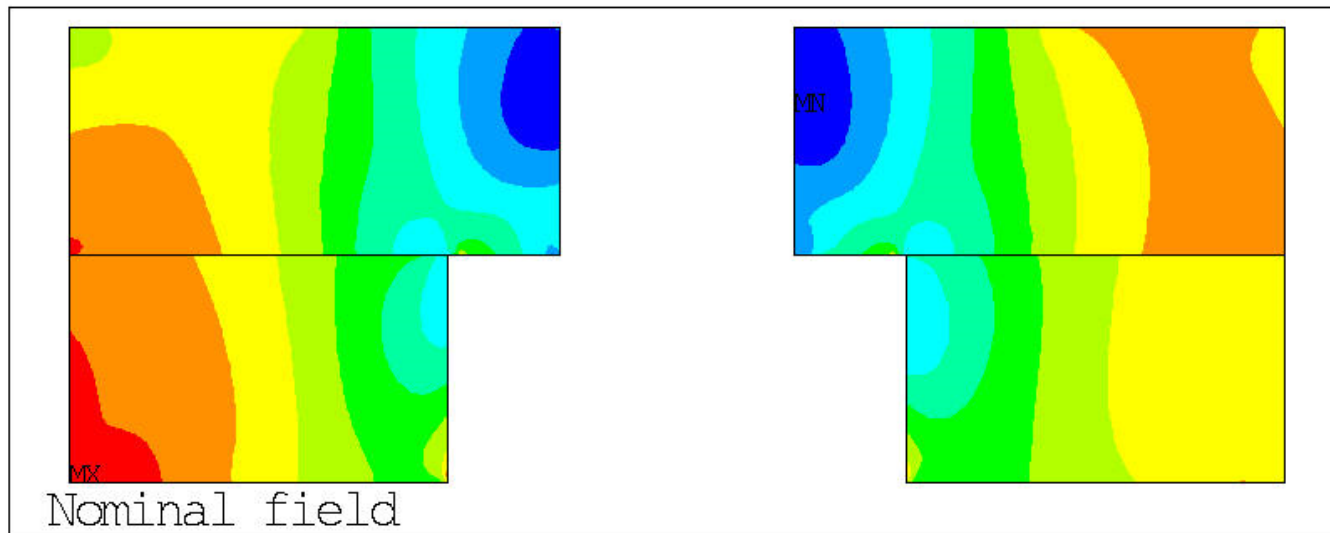
Peak von Mises stress: 199 MPa



# Nb<sub>3</sub>Sn coil stress (16 T)

- Von Mises stress (16 T)

Peak von Mises stress: 186 MPa



# Summary of peak stresses

- Summary peak stress values:

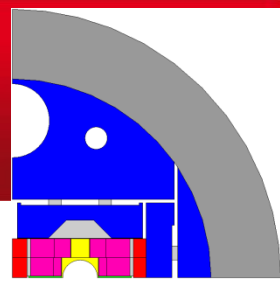
$\sigma$ von Mises [MPa]	Left	Right
Bladder	114	133
Key	115	113
Cool-down	188	199
Powering 16 T	186	160

Right: To better balance

$\sigma_x$ [MPa]	Left	Right
Bladder	-92	-102
Key	-123	-121
Cool-down	-205	-218
Powering 16 T	-205	-180

Right: To better balance

-> To better balance the right part, one can play on the positioning/width/thickness of the vertical/horizontal keys (to be done)



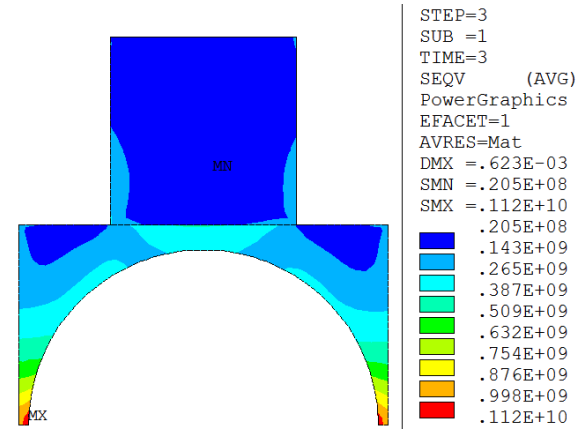
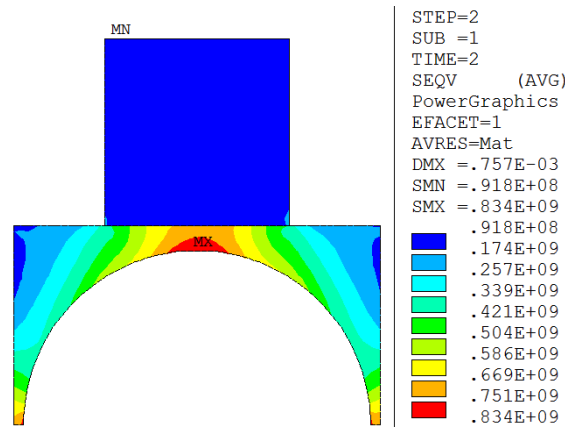
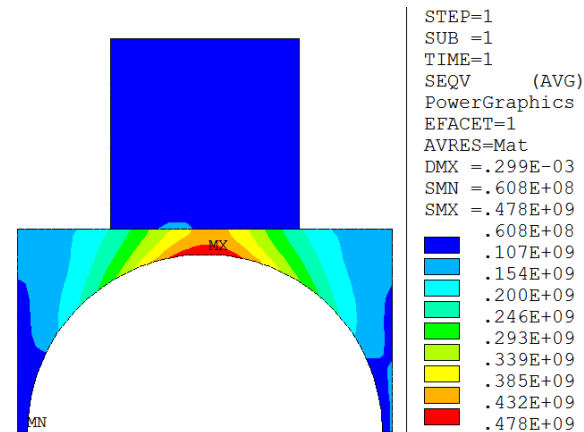
- Pole: von Mises stress

	293 K	4.3 K
Ti 6Al 4V	800	1650

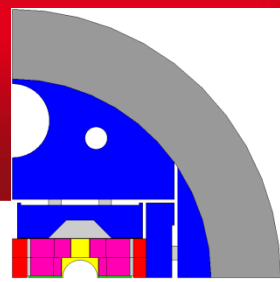
Keys in  
478 MPa ✓

Cold  
834 MPa ✓

16 T  
1120 MPa ✓

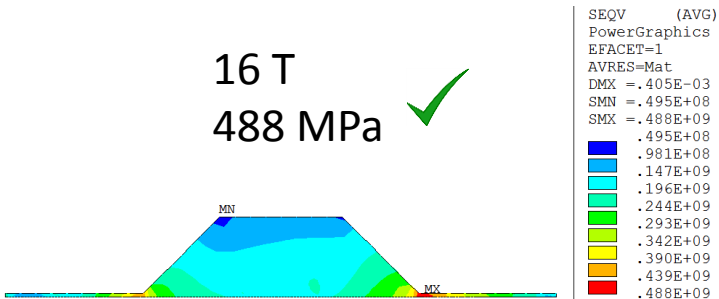
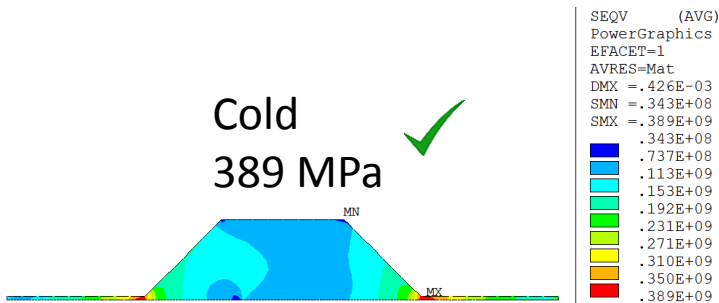
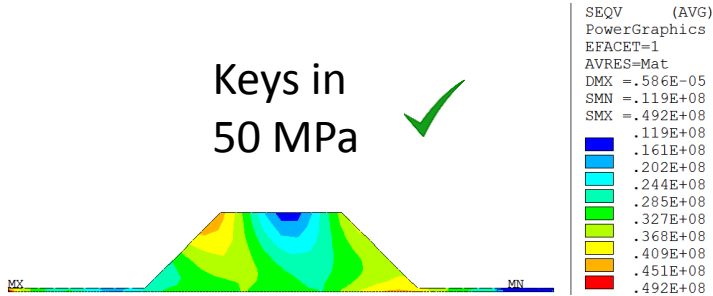






- Pusher: von Mises stress

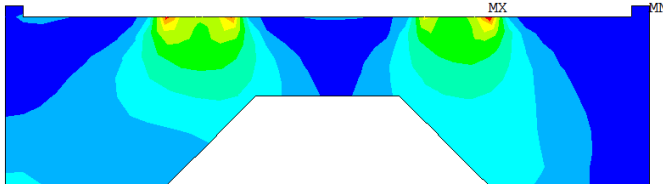
	293 K	4.3 K
SS 316 LN	350	1050



# Vertical pad

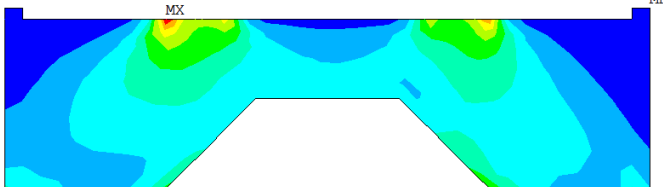
- von Mises

Keys in  
146 MPa ✓



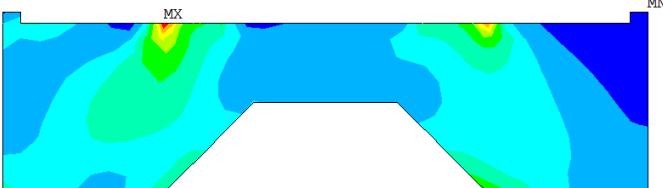
```
SEQV (AVG)
PowerGraphics
EFACET=1
AVRES=Mat
DMX =.142E-04
SMN =93548.1
SMX =.146E+09
93548.1
.163E+08
.326E+08
.488E+08
.650E+08
.812E+08
.975E+08
.114E+09
.130E+09
.146E+09
```

Cold  
416 MPa ✓



```
SEQV (AVG)
PowerGraphics
EFACET=1
AVRES=Mat
DMX =.490E-03
SMN =339743
SMX =.416E+09
339743
.466E+08
.928E+08
.139E+09
.185E+09
.231E+09
.278E+09
.324E+09
.370E+09
.416E+09
```

16 T  
535 MPa ✓



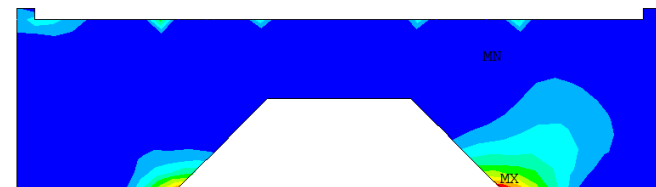
```
SEQV (AVG)
PowerGraphics
EFACET=1
AVRES=Mat
DMX =.494E-03
SMN =325458
SMX =.535E+09
325458
.597E+08
.119E+09
.178E+09
.238E+09
.297E+09
.357E+09
.416E+09
.475E+09
.535E+09
```

	293 K	4.3 K
Ferromagnetic iron	230	720*

\* $\sigma_1 < 380$  MPa

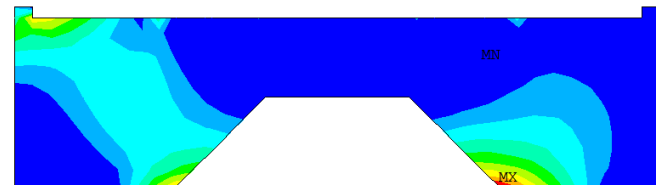
- $\sigma_1$

Cold  
146 MPa ✓



```
S1 (AVG)
PowerGraphics
EFACET=1
AVRES=Mat
DMX =.490E-03
SMX =.154E+09
0
.171E+08
.342E+08
.512E+08
.683E+08
.854E+08
.102E+09
.120E+09
.137E+09
.154E+09
```

16 T  
256 MPa ✓

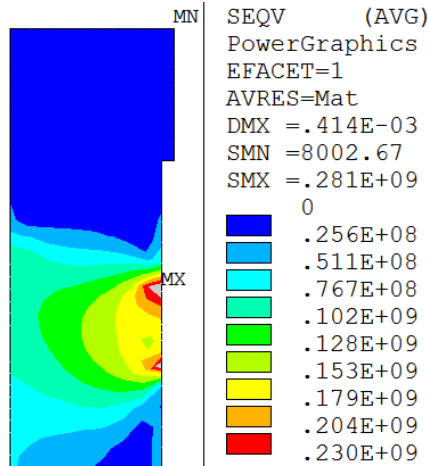


```
S1 (AVG)
PowerGraphics
EFACET=1
AVRES=Mat
DMX =.494E-03
SMX =.256E+09
0
.285E+08
.569E+08
.854E+08
.114E+09
.142E+09
.171E+09
.199E+09
.228E+09
.256E+09
```

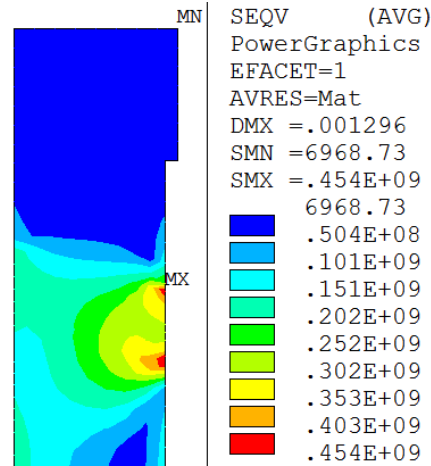
	293 K	4.3 K
Ferromagnetic iron	230	720*

## • Von Mises

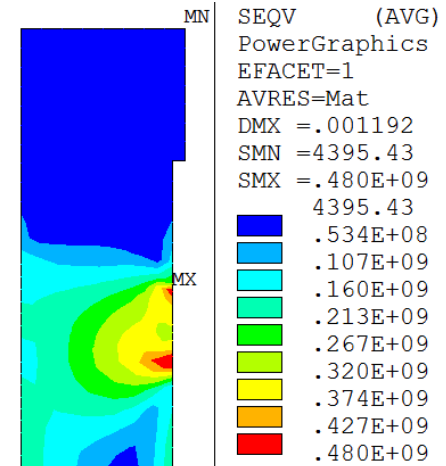
\* $\sigma_1 < 380$  MPa



Keys in: 281 MPa ✗

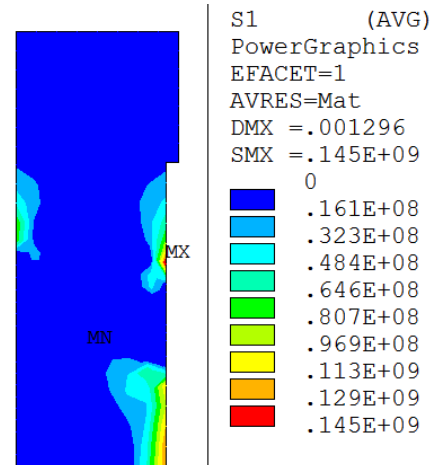


Cold: 454 MPa ✓

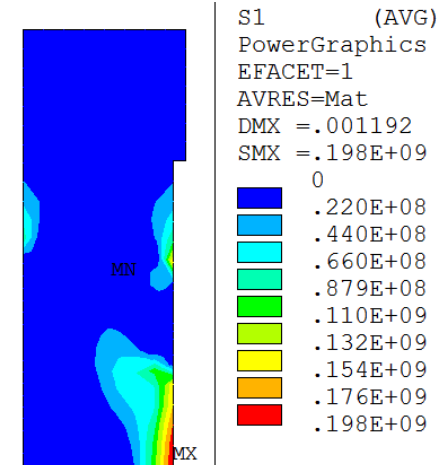


16 T: 480 MPa ✓

## • $\sigma_1$



Cold: 145 MPa ✓



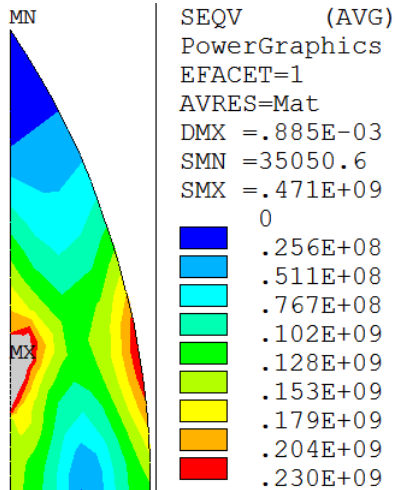
16 T: 198 MPa ✓

# Lateral Yoke

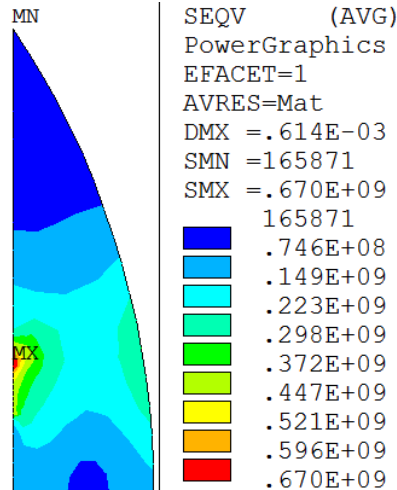
	293 K	4.3 K
Ferromagnetic iron	230	720*

## • Von Mises

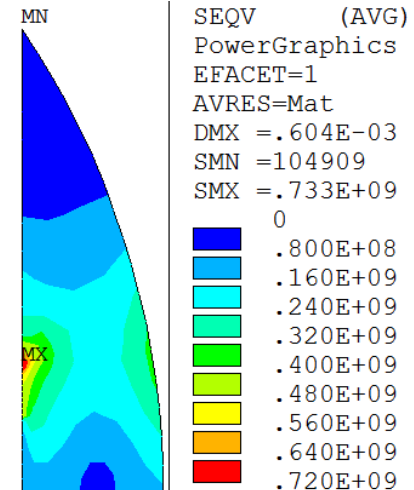
\* $\sigma_1 < 380$  MPa



Keys in: 471 MPa ✗

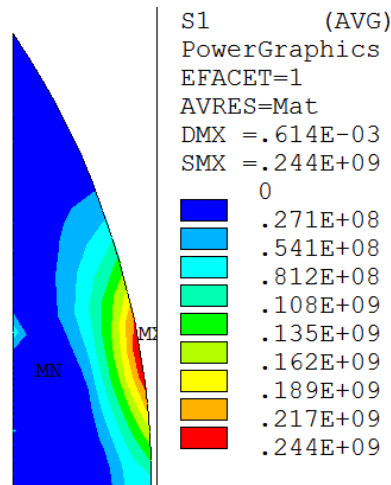
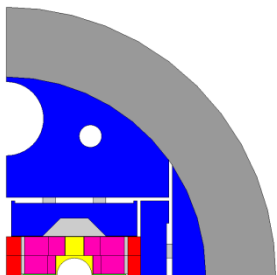


Cold: 670 MPa ✓

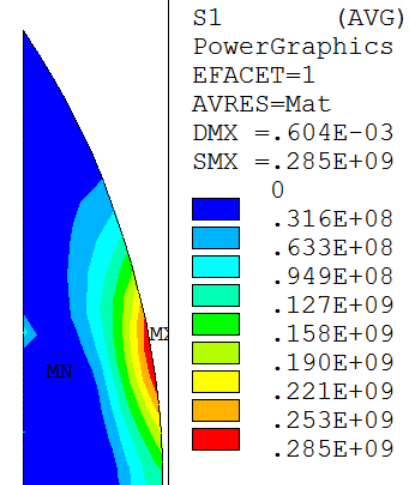


16 T: 733 MPa ✗

## • $\sigma_1$

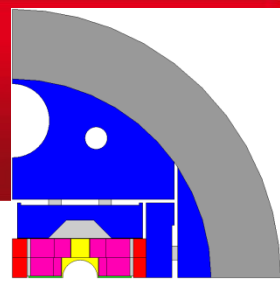


Cold: 244 MPa ✓



16 T: 285 MPa ✓

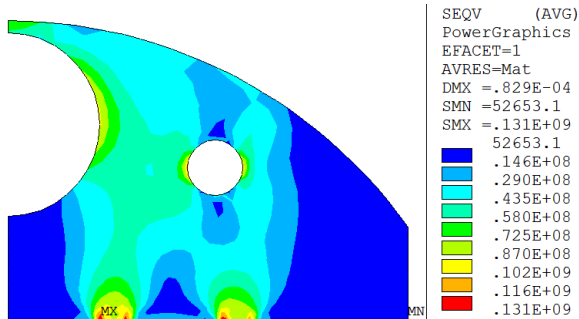
# Upper Yoke



- Von Mises

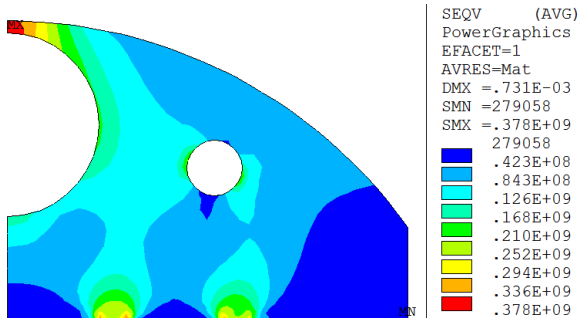
	293 K	4.3 K
Ferromagnetic iron	230	720*

\* $\sigma_1 < 380$  MPa

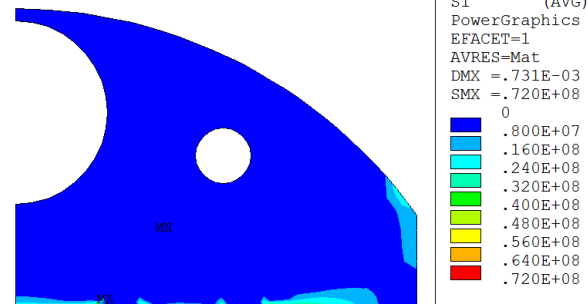


Keys in  
131 MPa ✓

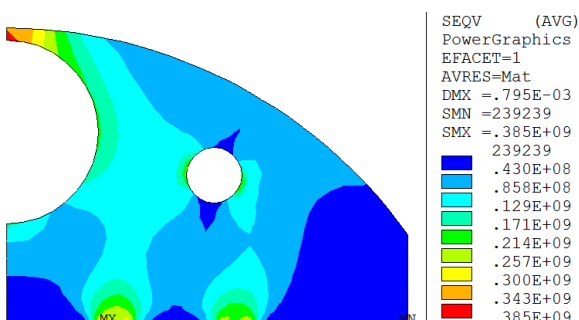
- $\sigma_1$



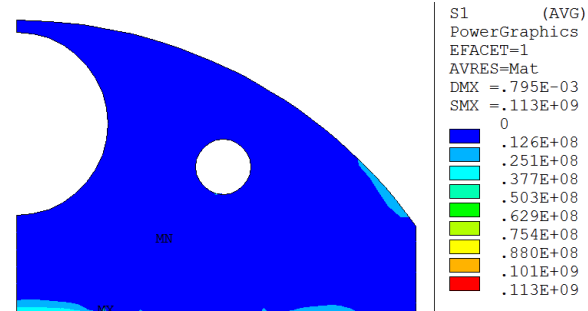
Cold  
378 MPa ✓



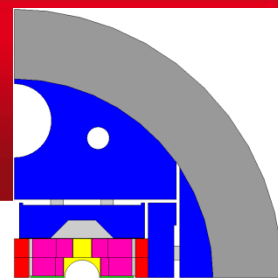
Cold  
72 MPa ✓



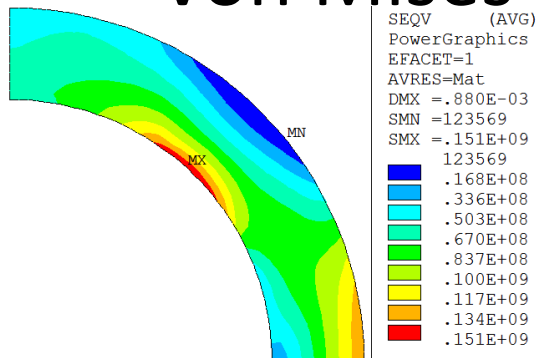
16 T  
385 MPa ✓



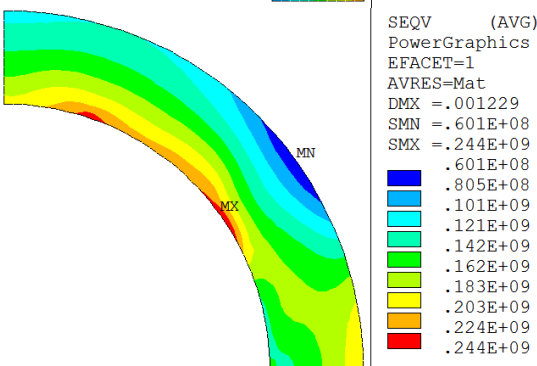
16 T  
113 MPa ✓



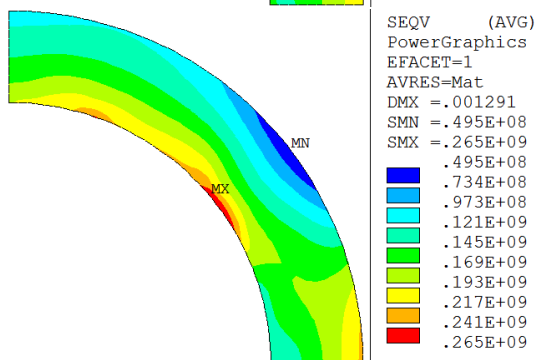
- Von Mises



Keys in  
151 MPa ✓



Cold  
244 MPa ✓



16 T  
385 MPa ✓

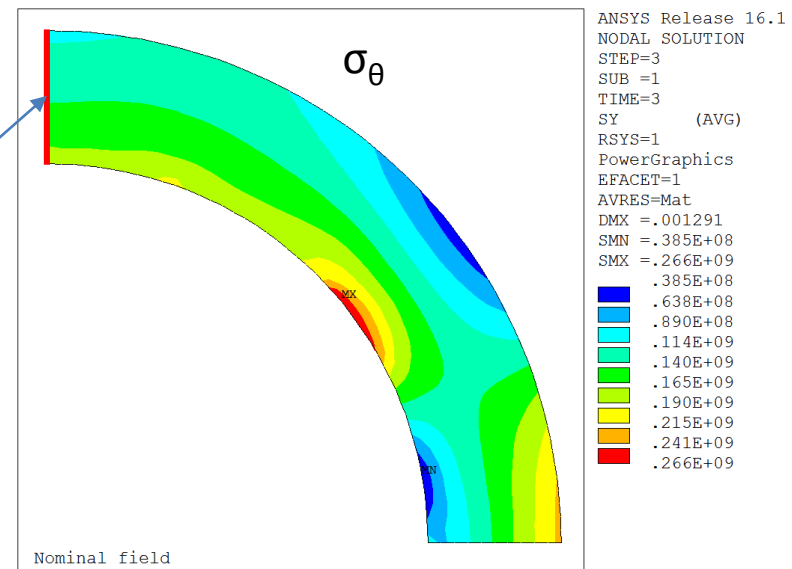
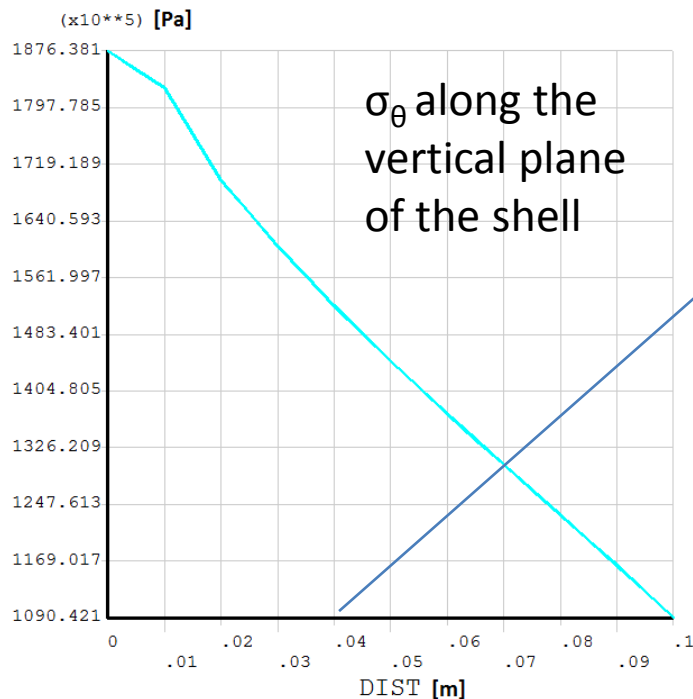
	293 K	4.3 K
Al 7075	480	690

# Conclusion

- Investigation of double aperture mechanical design with **194 mm** interbeam distance
- Investigation **@ 16 T**
- Peak stress in **Nb<sub>3</sub>Sn coil at the limit**
- Peak stress in the horizontal **iron** components **above the limit at warm** (key contact with lateral yoke and horizontal pad)
- **Bladder** pressure of **70 MPa** in operation

# EXTRA: Force in the shell

- Fx left (+8.25 MN/m) & Fx right (-7.63 MN/m)
  - > 15.88 MN/m
- Average azimuthal force in the shell
  - > 14.65 MN/m





# cea EXTRA: Block magnet comparison

Magnet	Bore	Pole tip	displacement [ $\mu\text{m}$ ]			Strain [ $\mu\text{m}/\text{m}$ ]			$\Delta\epsilon/\Delta\text{disp}$	Material properties	
	field [T]	thickness [mm]	cold	powering	pow-cold	cold	powering	pow-cold	[ $\mu\epsilon/\mu\text{m}$ ]	Nb3Sn	Ti-6Al-4V
ECC block v20ar	16.8	1.75	-198	-49	149	-5887	-1580	4307	29	ECC (E~25;30;27.5;33 GPa)	116 GPa / 126.5 GPa
ECC block v19ar	16.8	1.75	-169	-57	112	-5231	-1598	3633	32	LARP (E~44 GPa, 52 GPa)	130 GPa / 130 GPa
ECC block v18ar	16.8	1.9	-162	-50	112	-4558	-1019	3539	32	LARP (E~44 GPa, 52 GPa)	130 GPa / 130 GPa
ECC block v17ar	16.8	2	-167	-55	112	-4436	-955	3481	31	LARP (E~44 GPa, 52 GPa)	130 GPa / 130 GPa
ECC block v16ar	16.8	6.3	-179	-72	107	-4878	-1272	3606	34	LARP (E~44 GPa, 52 GPa)	130 GPa / 130 GPa
Fresca2	13	5	-304	-140	164	-5048	-2480	2568	16	LBNL (E~44 GPa, 44 GPa)	100 GPa / 120 GPa
Fresca2	13	6.5	-306	-142	164	-5051	-2481	2570	16	LBNL (E~44 GPa, 44 GPa)	100 GPa / 120 GPa
Fresca2	13	8	-307	-141	166	-5058	-2472	2586	16	LBNL (E~44 GPa, 44 GPa)	100 GPa / 120 GPa
Fresca2	15	8	-409	-190	219	-7187	-3778	3409	16	LBNL (E~44 GPa, 44 GPa)	100 GPa / 120 GPa
Fresca2	13	16	-232	-101	132	-3931	-1042	2889	22	LBNL (E~44 GPa, 44 GPa)	100 GPa / 120 GPa
RMM_graded_v21_d	16	1	-174	-56	118	-4617	-1071	3546	30	LBNL (E~44 GPa, 44 GPa)	110 GPa / 120 GPa
RMM_graded_v21_c	16	2	-173	-55	118	-4666	-1056	3610	31	LBNL (E~44 GPa, 44 GPa)	110 GPa / 120 GPa
RMM_graded_v21_b	16	4	-171	-55	116	-4757	-1115	3643	32	LBNL (E~44 GPa, 44 GPa)	110 GPa / 120 GPa
RMM_graded_v21_a	16	6	-168	-58	111	-4832	-1245	3587	32	LBNL (E~44 GPa, 44 GPa)	110 GPa / 120 GPa
HD3	14	1.65	-134	-51	83	-3690	-667	3023	36	LARP (E~44 GPa, 52 GPa)	110 GPa / 120 GPa

**ECC displacement and strain impacted by material properties** not by bore tip thickness

**RMM\_graded and ECC similar behavior** with similar properties

**Fresca2 biggest displacement – HD3 smallest displacement...**

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