



Design of MW-Class Industrial Motors by AMSC

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M2Or2A-01 [Invited]



List of Published Reference

THIS PRESENTATION IS BASED ON THE FOLLOWING AMSC (A FEW OTHERS) PUBLIC INFORMATION

- Kalsi, S.S., "Applications of High Temperature Superconductors to Electric Power Equipment", IEEE/Wiley, ISBN 978-0-470-16768-7, 2011
- S.S. Kalsi, D. Madura, G. Snitchler, M. Ross, J. Voccio and M. Ingram, "Discussion of Test Results of a Superconductor Synchronous Condenser on a Utility Grid", Applied Superconductivity, IEEE Transactions on, Volume: 17, Issue: 2, Year 2007
- S. S. Kalsi, D. Madura, M. Ross, M. Ingram, R. Belhomme, P. Bousseau and J-Y. Roger, 'Operating Experience of a Superconducting Dynamic Synchronous Compensator', Paper No. A1-108, CIGRE Session 2006 in Paris
- Kalsi, S.S.; Gamble, B.B.; Snitchler, G.; Ige, S.O.; "The status of HTS ship propulsion motor developments", <u>Power Engineering Society General Meeting</u>, 2006. IEEE, 18-22 June 2006 Page(s):5 pp., Digital Object Identifier 10.1109/PES.2006.1709643
- Kalsi, S.; Madura, D.; MacDonald, T.; Ingram, M.; Grant, I.; "Operating Experience of Superconductor Dynamic Synchronous Condenser", PES TD 2005/2006, May 21-24, 2006 Page(s):899 902
- Kalsi, S.S.; Henderson, N.; Gritter, D.; Nayak, O.; Gallagher, C.; "Benefits of HTS technology to ship systems", <u>Electric Ship Technologies Symposium</u>, 2005 IEEE, 25-27 July 2005 Page(s):437 443, Digital Object Identifier 10.1109/ESTS.2005.1524712
- Snitchler, G.; Gamble, B.; Kalsi, S.S.; "The performance of a 5 MW high temperature superconductor ship propulsion motor", Applied Superconductivity, IEEE Transactions on, Volume 15, Issue 2, Part 2, June 2005 Page(s):2206 2209, Digital Object Identifier 10.1109/TASC.2005.849613
- Haran, K.; Kalsi, S.S.; Arndt, T.; Karmaker, H.; Badcock, R.; Buckley, R.; Haugan, T.; Izumi, M.; Loder, D.; Bray, J.; Masson, P.; Stautner, W.; "High Power Density Superconducting Rotating Machines – Development Status and Technology Roadmap", Supercond. Sci. Technol. 30, (2017) 123002 (41pp)
- Kalsi, S.S., Hamilton, K.A. and Badcock, R.A., "Superconducting rotating machines for aerospace applications", Presented at AIAA Conference, Cincinnati, OH, 2018



Superconducting Rotating Machines



OUTLINE

- Possible applications
- Superconductors
- SC Machine Configurations
- High Speed SC Machines
- Low Speed SC Machines
- Ultra High-Speed SC Machines
- Outlook

Conventional motor







POSSIBLE SUPERCONDUCTORS FOR APPLICATIONS





Types of Superconductors

- LTS NbTi and Nb₃Sn
- Operate at ~ 5 K
- Cooled with liquid helium
- Moderate field
- Low cost conductors



LTS are used in MRI and High Field Magnets

- HTS BSCCO and ReBCO
- Operate at ~ 20 77 K
- Cooled with LH₂, LNe, LN₂ and Refrigerators
- Very high fields
- High cost conductors

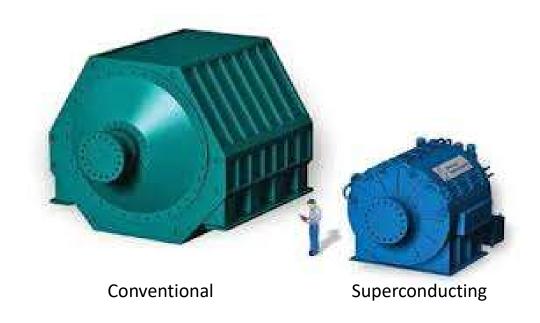


HTS have still to find a niche application



Bi₂Sr₂Ca₂Cu₃O





SC MACHINE CONFIGURATIONS







Superconducting (SC) Machine Configuration

- Majority of machines are synchronous type employing SC for the DC field winding
- Until the nineties, most machines were built with NbTi (low temperature superconductors – LTS)
- Nineties onwards, High Temperature Superconductors (HTS) became favorite
- Majority of the SC machines have DC excitation winding on the rotor
- In a few applications, DC excitation winding is on the stator and rotor carries AC armature winding
- Homopolar synchronous machines are most suited for very high-speed applications

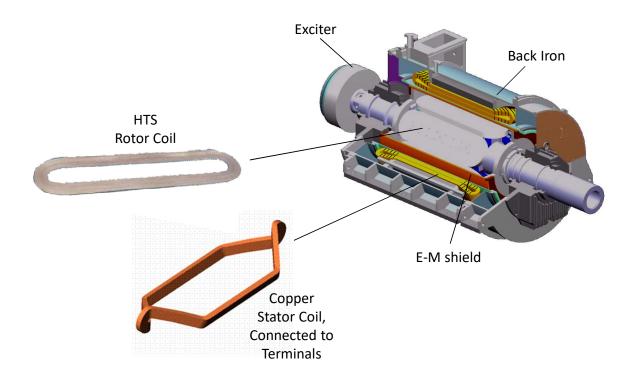
Only HTS based machines are discussed in this presentation







Key Components of HTS Rotating Machines



Most commonly used configurations: HTS field winding and Copper armature winding



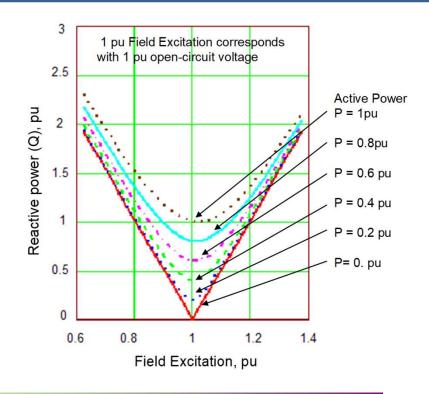
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What makes HTS Machines attractive?

Features making such machines attractive are;

- Compact size
- Light weight
- Ability to supply reactive power (MVARs) up to full MVA rating (both leading and lagging)
- Virtually no harmonics in the terminal voltage
- Improved rotor life elimination of thermal load cycling of field winding current changes
- Higher efficiency under partial and fullload operations
- Lower vibrations and noise



Ability to operate over the whole dynamic range of P and Q powers enhances dynamic stability of the machine and the system





What makes HTS Machines attractive?

Harmonics generated inside an HTS synchronous machine are extremely small as shown below;

Fraction of

Harmonic	Fraction of	Harmonic	F	undamental
Order	Fundamental	Order	Radial	Tangential
1	1	1	1	1
3	0	3	-0.057	0.116
5	5.977·10-4	5	3.869·10-4	7.097·10-3
7	7.394·10 ⁻⁶	7	4.567·10-5	-1.153·10-3
9	0	9	-7.546·10 ⁻⁵	-4.378·10-4
11	6.074 · 10 - 8	11	4.55·10-6	-4.586·10 ⁻⁵
13	1.542·10-10	13	-8.935·10 ⁻⁷	1.027·10-5
15	0	15	5.559·10-7	4.827·10-6
17	1.032·10-11	17	-1.149·10 ⁻⁸	5.882·10-7
19	-3.381·10-14	19	-2.729·10 ⁻⁹	-1.475·10 ⁻⁷
Harmonics generated by Harmonics generated by stator AC windin				

Lower harmonic content eases machine component design and simplifies external control systems



field winding in stator

on the rotor surface



Examples of High-Speed Machines Built and Tested at AMSC

- 1000 hp, 1800 rpm synchronous motor
- 5000 hp, 1800 rpm synchronous motor
- 8 MVAR, 1800 rpm synchronous condenser

HIGH SPEED SC MACHINES





AMSC INDUSTRIAL MOTORS HIGH SPEED MACHINES





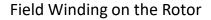


1000 HP, 1800 RPM Synchronous Motor

- First motor jointly built by AMSC and Baldor/Rockwell Automation
- 1000 HP, 1800-RPM, 4-pole
- Field Winding Employed BSCCO-2223 conductor @25 K
- Armature Winding Dimond type copper coils
- HTS Cooled with liquid neon
- Tested in the Summer 2000
- Met performance expectations









AC Winding on the Stator

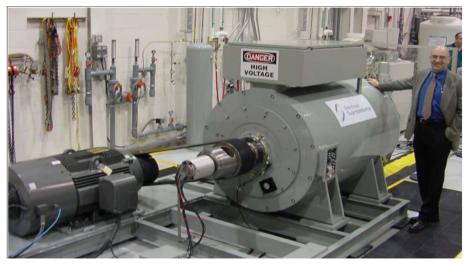
Encouraging progress on this motor motivated AMSC to built 5000 HP motor





AMSC 5000 HP Motor Features

- 5000 HP, 1800-RPM, 60 Hz motor
- Line voltage 6.6 kV
- HTS field operating at 30 K
- Field winding cooled with Gifford-McMahon (G-M) cryogenic refrigerators
- Stator winding cooled with fresh water
- Frame dimensions:
 - 1.1 m dia x 1.6 m long
- Weight 6.8 ton
- Efficiency 97.7%

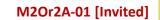




5000 HP Motor – No-load Testing June 2001

World's most powerful HTS industrial motor to date

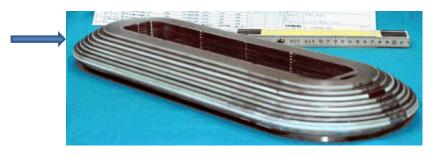




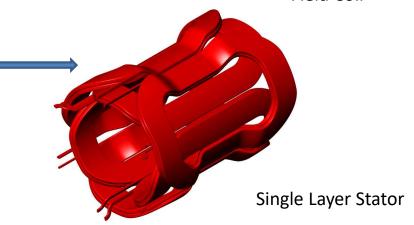


5000 HP Motor Rotor and Stator Details

- Field Winding pancake BSCCO-2223 coils
- Field Coils Conduction cooled with liquid neon
- Closed-loop cooling system used G-M cryocooler cooler
- Armature Winding Innovative Single layer copper coils
- Copper coils cooled with fresh water
- Met all performance expectations



Field Coil



Success of this project led to the US Navy Propulsion motor projects

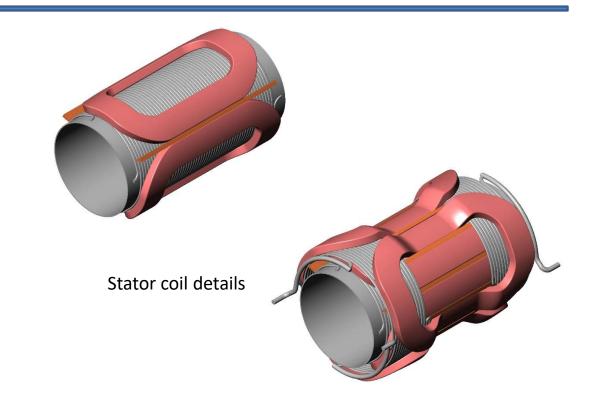


Design Features - 5,000 HP Motor



Voltage	6.6	kV L-L
Number of phases	3	
field inner radius	6.9	in
field outer radius	8.16	in
em shield thickness	1.0	in
em shield outer radius	9.60	in
armature inner radius	11.7	in
armature outer radius	13.6	in
iron yoke inner radius	14.05	in
iron yoke outer radius	18.46	in
field current density	10000	amp/cm2
armature current density	232	amp/cm2
straight length	20	in
length over end turns	39.25	in
number of poles	4	
speed	1800	rpm
power factor	0.99	
field inductance	2.78	henry
field operating current	309	amp
armature phase current	349	amp
Angle at Full Load	14.70	deg
synchronous reactance	0.25	pu
transient reactance	0.22	pu
subtransient reactance	0.15	pu
Efficiency	98	%

2019-ICMC



Showing layout of unique single layer armature coils cooled with fresh water in cooling tubes

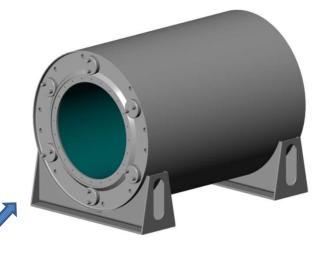




As Built Stator Components

- Conventional iron core
- Coils and cooling tubes epoxy impregnated
- Water cooled stator windings
- Litz conductor
- Single layer winding





First stator built using such coils cooled with fresh water

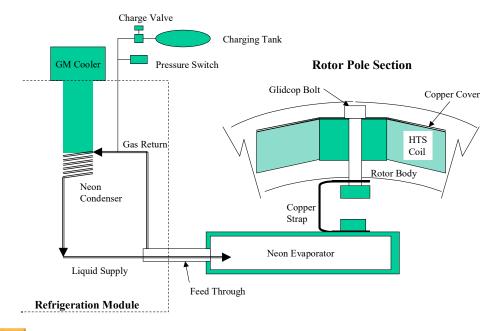
- Built by Everson Tesla – Nazareth, PA





As Built Field Coils and Cooling System

- Condensing neon heat transport
- Cryomech AL330 G-M cryocooler
- Conduction cooled HTS winding





Field coils were conduction cooled using a closed cycle neon interface medium



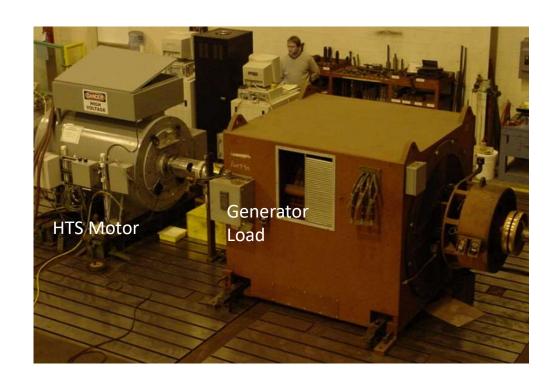




5000 HP Motor - Load Testing in June 2001

Summary of Test Results

- Factory and load testing completed per IEEE 115
- Motor efficiency: 97.7%
- 1/3 reduction in volume compared to the industry standard
- 40% reduction in losses compared to the industry standard



Achieved successful demonstration of the first powerful HTS motor in 2001







Comparison of Design and Measurements

Parameter	Design	Measured	Units
Line Voltage	6.6	6.6	kV
Phase Current	329	330	Α
Rating	5000	5000	hp
Xd	0.32	0.30	pu
Xd'	0.28	0.23	pu
Xd"	0.16	0.17	pu
Back EMF	1.043	1.035	pu
Ampere-turns	261	279	kA/pole
Power factor	Unity	Unity	

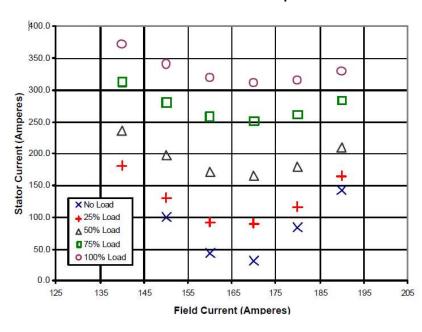
Excellent comparison between calculated and measured parameters validated design codes

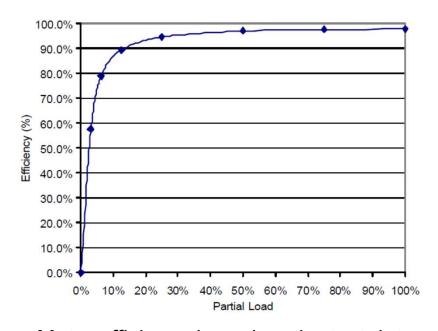




5000 HP Motor Test Results

Test measurement conducted per IEEE-115





Measured V-curves

Motor efficiency based on the test data

Excellent performance exhibited by measured V-curves and Efficiency







Lessons Learned from 5000 HP Motor

- Dominant losses are;
 - Stator Copper
 - Iron Core
 - Cryogenic power is small
- Validated machine design algorithms
- Demonstrated;
 - vacuum system over several months
 - thermal insulation system on the rotor
 - cooling systems for Rotor and Stator



Design algorithms and component validation with the 5000 HP motor were later used for designing future machines – this motor still exists at AMSC





SuperVAR®

Dynamic Synchronous Condenser

AMSC – SuperVAR

HIGH SPEED SC MACHINES



Hoeganaes, Tennessee





SuperVAR® Prototype Project Description

Similar to a conventional synchronous machine but with better performance

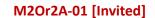
- 8 MVA prototype SuperVAR machine for testing on TVA grid
- TVA had partially supported the prototype development
- TVA had planned to order 5 production units following the successful testing of the prototype
 - rated 12 MVA at 13.8kV



Rating	8 MVAR
Voltage	13.8 kV line to line
Ambient Temp	-30° to +40°C
Losses	1.5% rating at 8MVA
	Including 30kW 480V auxiliary power

AMSC was offering 12 MVA production units for delivery in early 2006





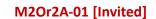


Characteristics of a SuperVAR® Condenser

- Fast reacting transient dynamic voltage support and stability (leading and lagging VARS) at a multiple of the machine rating
 - Applicable to a range of voltage regulation, power quality and voltage collapse problems
- Reduced operating costs over conventional condensers
 - Low losses even at partial load
 - No rotor rewind costs due to eliminated thermal cycling
- Generates very low levels of harmonics requiring no filters
- Simplified installation
 - Pre-packaged, self-contained units
- Operates at line voltage on low side of transmission to distribution transformer
 - Stator may be provided for distribution level voltages (up to 13.8kV)
 - No additional transformer needed in most applications

SuperVAR Condenser had very attractive features







Component Fabrication for ±8 MVAR Unit



Superconducting rotor in a conventional stator





±8 MVAR Unit at TVA Site



SuperVAR condenser and its supporting equipment mounted in a container for ease of mobility



Test Results



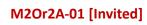
8 MVAR SuperVARTM Performance Parameters

<u>Parameters</u>	<u>Measured</u>
Synchronous reactance (x _d), pu	0.37
Transient reactance (x _d '), pu	0.21
Sub-transient reactance (x _d "), pu	0.13
Sub-transient reactance (x _q "), pu	0.13
Armature short-circuit time constant (τ_{sc}) , s	0.05
D-axis Transient open-circuit time constant (τ_{do}') , s	860
D-axis Sub-transient open-circuit time constant $(\tau_{do}")$, s	0.02
Q-axis Sub-transient open-circuit time constant $(\tau_{\alpha\alpha})$, s	0.04
Armature resistance (r _a), pu	0.007
Inertial constant, s	1.4

Machine parameters were measured – Low X_d is the key to machine's excellent performance

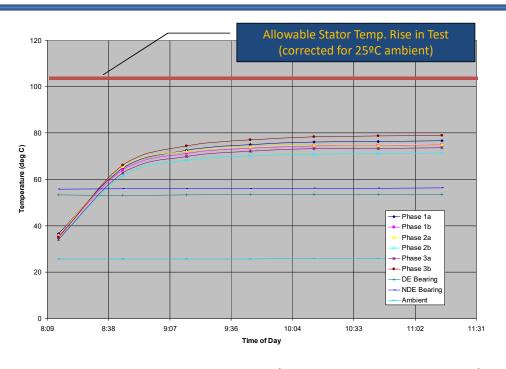


Test Results

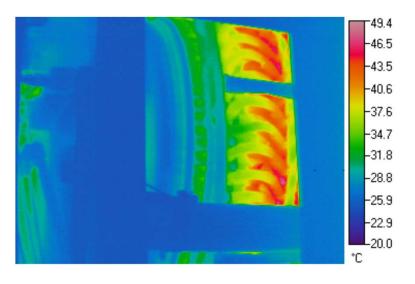




Zero Power Factor Heat Run at 8MVAR



Temperature of stator end turns after 3 hours operation at 8MVA



- Temperature rise must be ≤ 120°C at 40°C ambient temperature
- Stator end turn temperature monitored using infrared camera

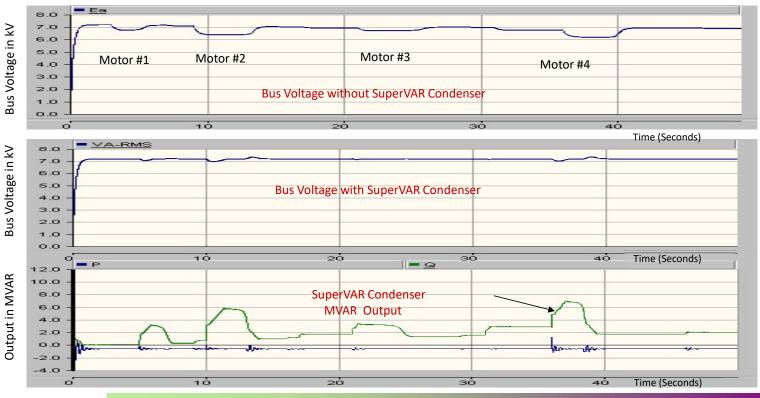
All temperatures were within design limits





Mitigating Multiple Motor Starts: Simulation

M. Ross, AMSC PES, using Power Technologies Inc. PSS/E simulation software



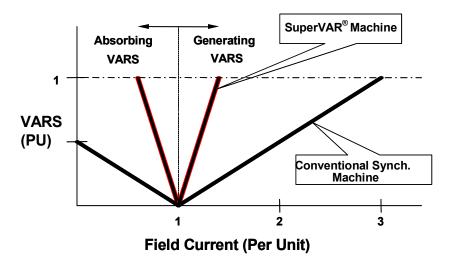
SuperVAR: an excellent solution for solving flicker problems due to switching in of large loads





Electric Utility Applications

V-Curves -- Conventional Vs. SuperVAR Condensers



SuperVAR machine leveraged proven features of Conventional stator combined with HTS rotor

SuperVAR Machine Advantages

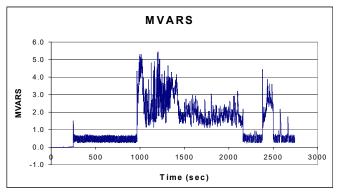
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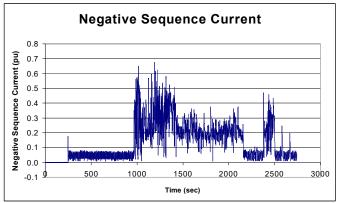


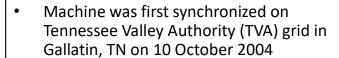




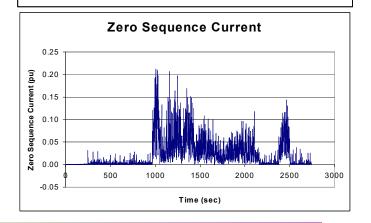
Machine Performance on TVA Grid







- Operated on regular basis between November 2004 and November 2005
- Experienced millions of transients due to the arc furnace operations
- A typical 1-hr burn cycle is shown here



SuperVAR machine operated without a single problem while experiencing high level of negative and zero sequence currents

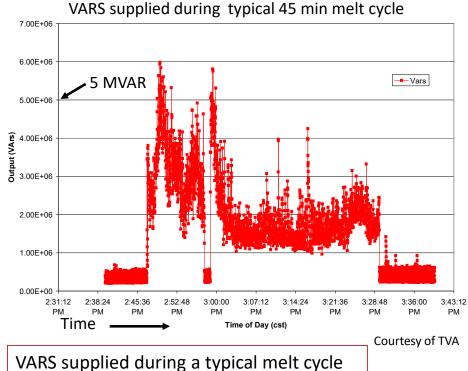






Real Life Operation on TVA Grid - I

- Machine installed on TVA grid in Gallatin, TN
- Synchronized 10 October 2004
- ±8 MVAR capability verified
- Machine reacted quasiinstantaneously to transients due to arc furnace operations



SuperVAR™ machine successfully supporting arc furnace, reducing grid disturbance





SuperVAR® Conclusions

- SuperVAR® synchronous condenser was built and tested
 - Extensive testing in the factory with > 3 hour on-grid operation
 - Operated on TVA grid in Hoeganaes, TN. -- November 2004 to
 November 2005 Regular operation lasting 1 year

SuperVAR® Condensers have applications for a wide variety of grid related problems





ULTRA HIGH-SPEED SC MACHINES





4MW, 15000-RPM AC Generator

- MW Class Power System Integration in Aircraft
- Two generator programs in progress
 - Synchronous generator utilizing HTS wire
 - Inductor (homopolar) generator with both armature and field windings stationary

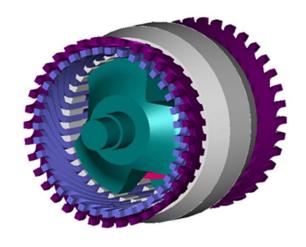
Challenge: Transferring current and coolant to the rotor at very high speed





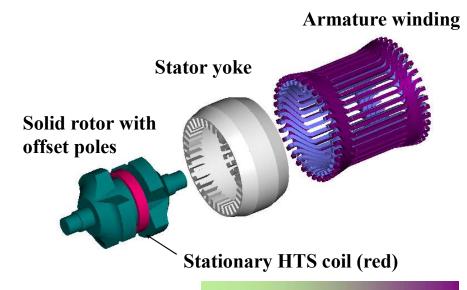
High Speed AC Inductor Generator Concept

Inductor Alternator with Stationary Superconducting Coil, Solid Rotor Forging, and Conventional Air Core Stator



2019-ICMC

Courtesy GE



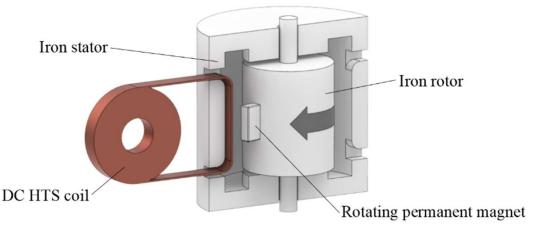
Rotor has no active components





HTS Dynamo Concept

- Field coils excited wirelessly for minimizing thermal conduction into cold environment
- Brushless exciter (Dynamo) shown here accomplishes this
- Dynamo exciter could operate at DC HTS coil/ currents > 1 kA
- Plans are to integrate it with the coolant transfer coupling



This dynamo concept has been successfully built and demonstrated by RRI-VUW





What's will make HTS Machines Attractive

- HTS technology amply demonstrated need for economic viability:
 - Low-cost HTS wire and
 - Reliable and affordable cooling system
- MUST: Improve wire performance (e.g., extended window of operation in terms of higher temperature and magnetic field and lower cost)
- Building HTS machines by leveraging synergies of off-the-shelf-components
- Designing machines by including dynamic variation of operating parameters (e.g., temperature, excitation, amount of fuel and environment)
- HTS machines may have sweet applications where other technologies are not feasible; Example: > 20 MW wind power generators and Motors/Generators for aerospace
- An affordable and reliable HTS technology may extend its applications to central power stations, wind turbine generators, ship propulsion and industrial motors

Future of the HTS technology looks very promising





Questions



