



Air Force Research Laboratory



Integrity ★ Service ★ Excellence

Calorimetric Measurements of YBCO Superconductor and Metallic Cables at High dB/dt in a Cryogenic Stator Machine Environment



Michael D. Sumption, Ph.D.
Ohio State University
Timothy J. Haugan, Ph.D.
Aerospace Systems Directorate
Air Force Research Laboratory





CO-AUTHORS, ACKNOWLEDGEMENTS



- **Air Force Research Laboratory – Aerospace Systems Directorate**
 - T.J Haugan
- **Univ. of Dayton Research Institute (@ AFRL)**
 - J.P. Murphy, C. Ebbing
- **The Ohio State University**
 - M.D. Sumption
 - M. Majoros
 - E.W. Collings



Acknowledgements: Support by *Air Force Office of Scientific Research (AFOSR)* and *The Air Force Research Laboratory (AFRL/RQ)*





Overview



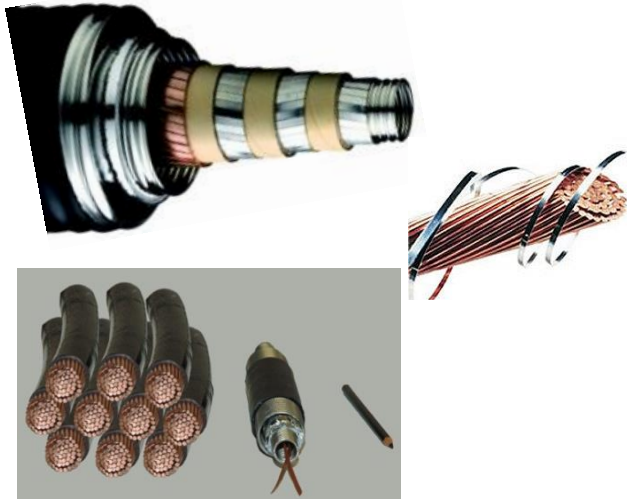
- The U.S. Air Force Research Laboratory (AFRL) facility for the measurement of AC loss in superconductors at high $B \cdot dB/dt$
- The test device has a spinning rotor consisting of permanent magnets arranged in a Halbach array; which exposes samples in a stator position with a peak radial field of 0.57 T, and with high rotation speeds up to 3600 rpm achieves a radial dB/dt is 543 T/s and tangential dB/dt is 249 T/s.
- Loss is measured by calorimetry at 77.2K using nitrogen boil-off from a double wall calorimeter feeding a gas flow meter, and the system was calibrated using power from a known resistor.
- This work describes the use of this test facility to measure and compare AC losses of a variety of YBCO coated conductors and cable styles.
- Conductors of YBCO are provided by several manufacturers with different architectures including filamented, varying width, and stabilizers



AC Loss Critical for Components of Interest to the AF



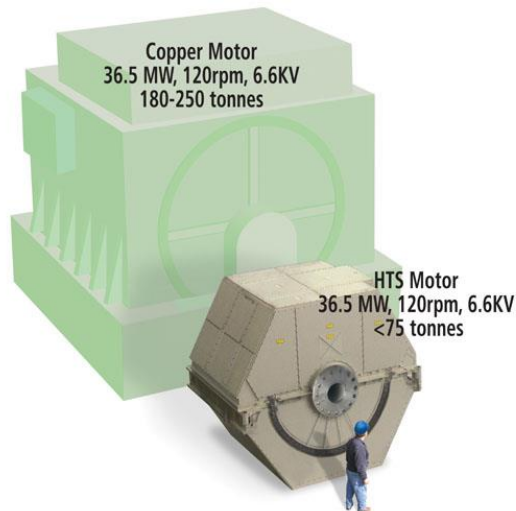
Power Transmission



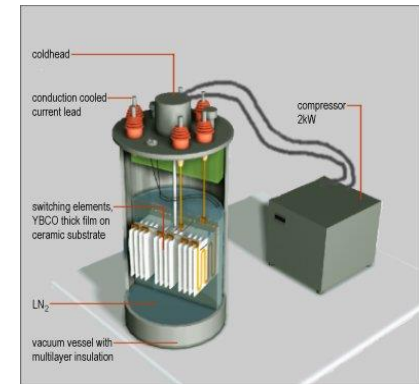
(SMES) Energy Storage



Generators/Motors



Fault Current Limiters



Transformers



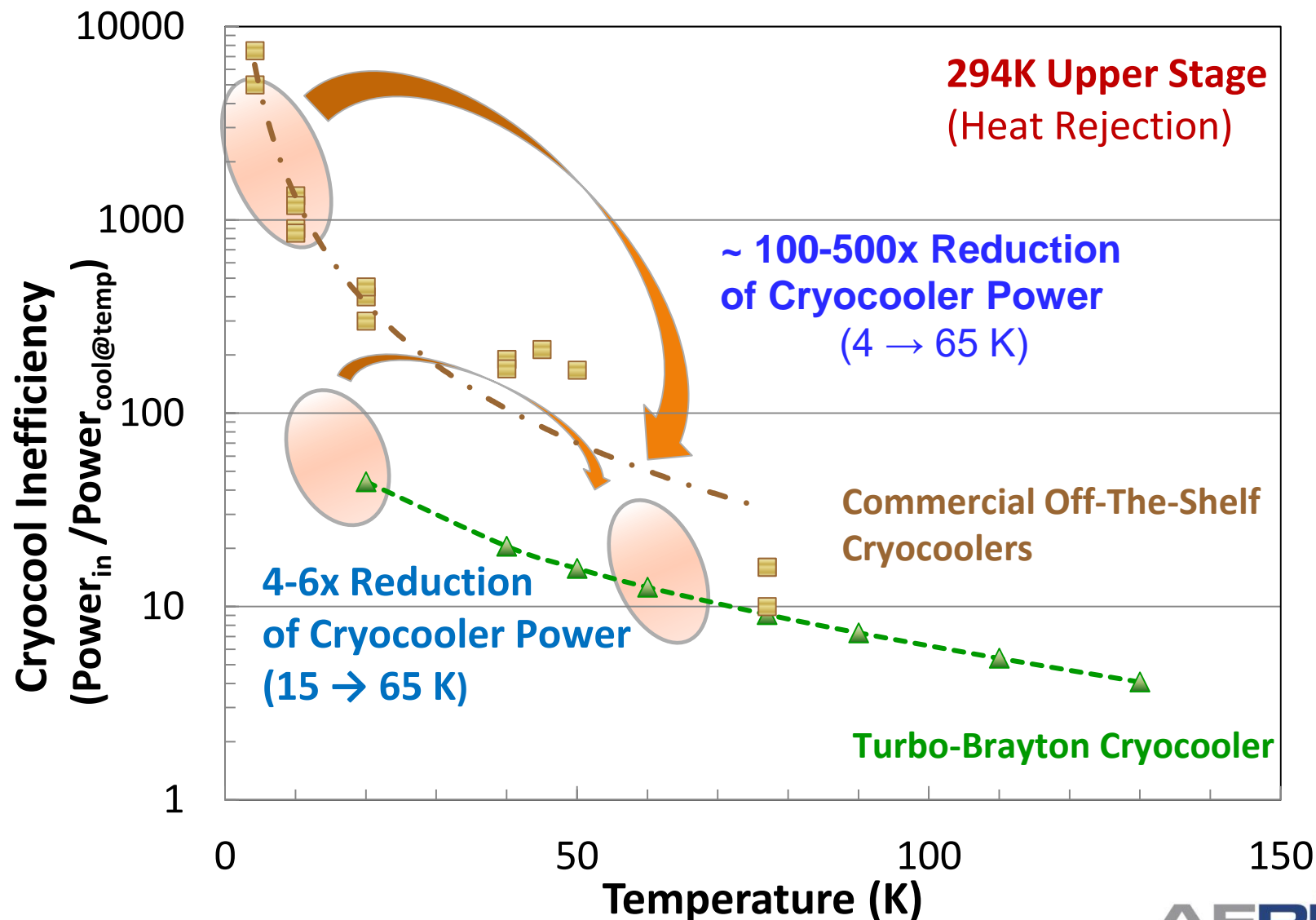
<http://www.conectus.org>

DISTRIBUTION A: Approved for public release. Distribution unlimited.





Cryocooler Efficiencies





Need for high B and dB/dt Testing

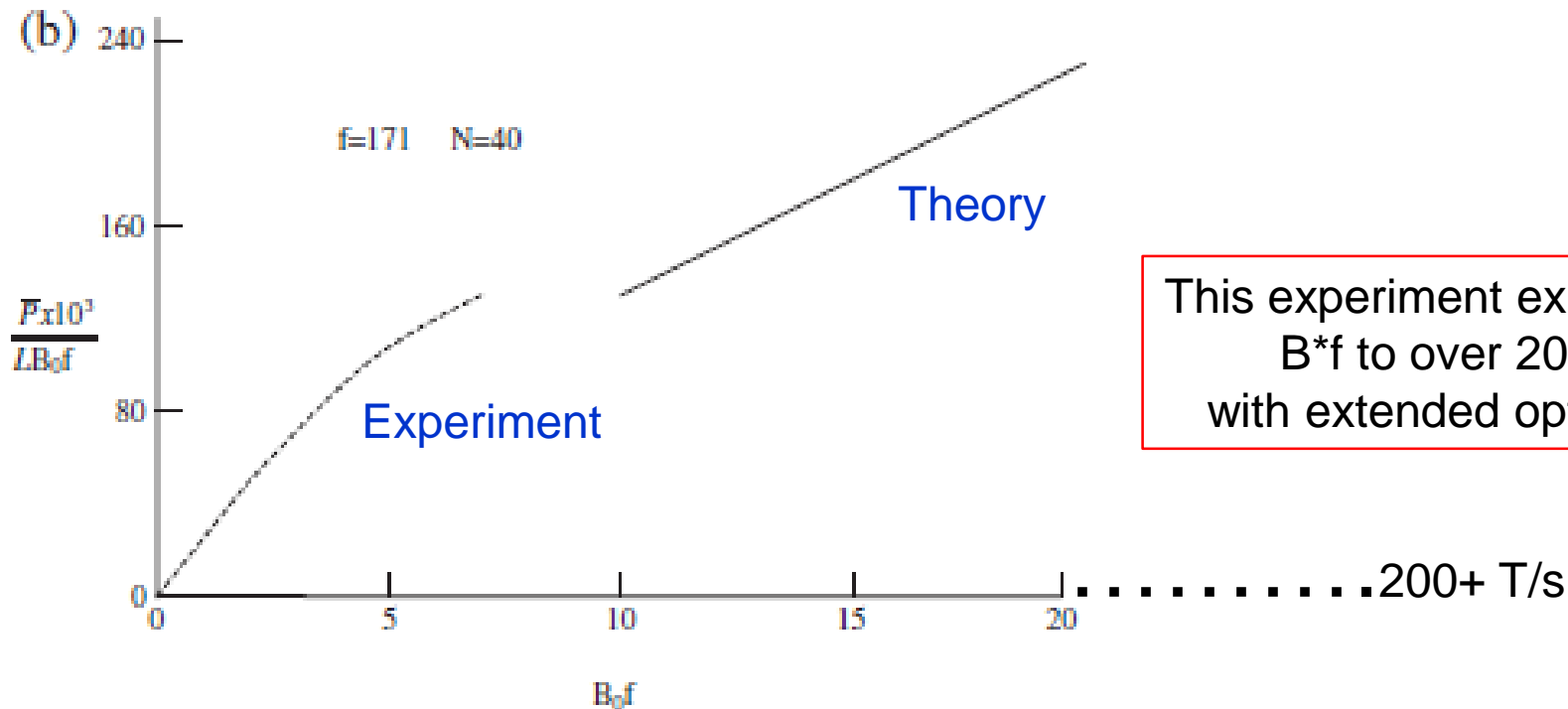


- **Windings in a motor/generator see high dB/dt like no other superconducting machine (e.g., 400 Hz and 0.5-1 T)**
- Extrapolate to high dB/dt in principle, need actual tests to make predictions reliable
- Easy to imagine a magnet which can reach these values of B and dB/dt , but
 - Such a magnet would need to be SC to reach the needed fields without Fe
 - The losses would require a SC of the kind we wish to develop
 - Would require high voltage (10s of kV).

**Alternative: Move sample and field relative to each other
Effectively - a motor simulator- “mock” motor/generator!**



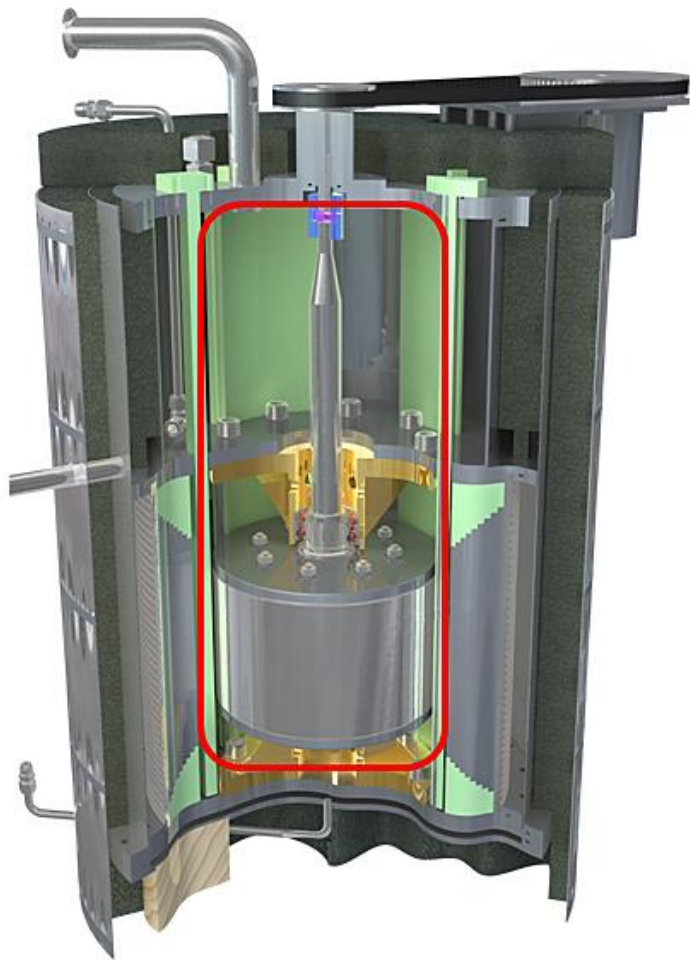
SMC AC Loss Device – Investigate New Physics at High B^*f ?



Reduced loss expression plotted against reduced magnetic field for frequency of 171 Hz for (a) ... (b) 40-filament sample. Dashed lines are approximate copies of weak field measurements published by Levin *et al*, and solid lines calculated from strong field results given here. From Carr *et al*, Supercond. Sci Technol. **20**, 168 (2007).



Phase 2-External Magnetic Field Stator Environment

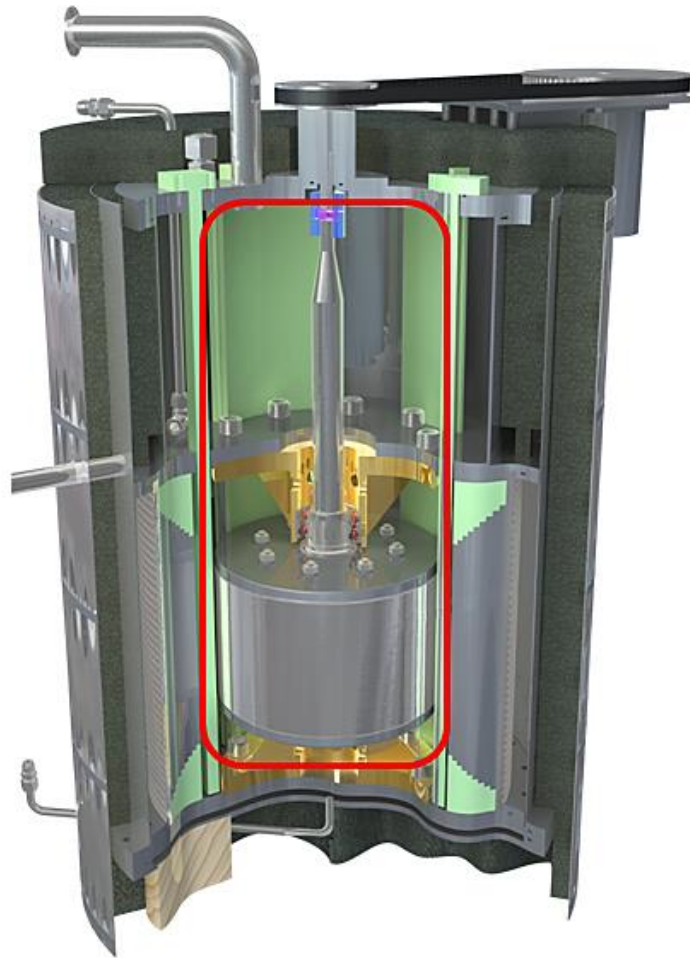


**8 Pole Permanent Magnet Rotor
Provides 0.62 Tesla
0 Hz to 400 Hz**





Spin-around-magnet (SAM) AC Loss Test Device - Time-Varying Magnetic Field in a Stator Environment



World-unique AC Loss Test Device

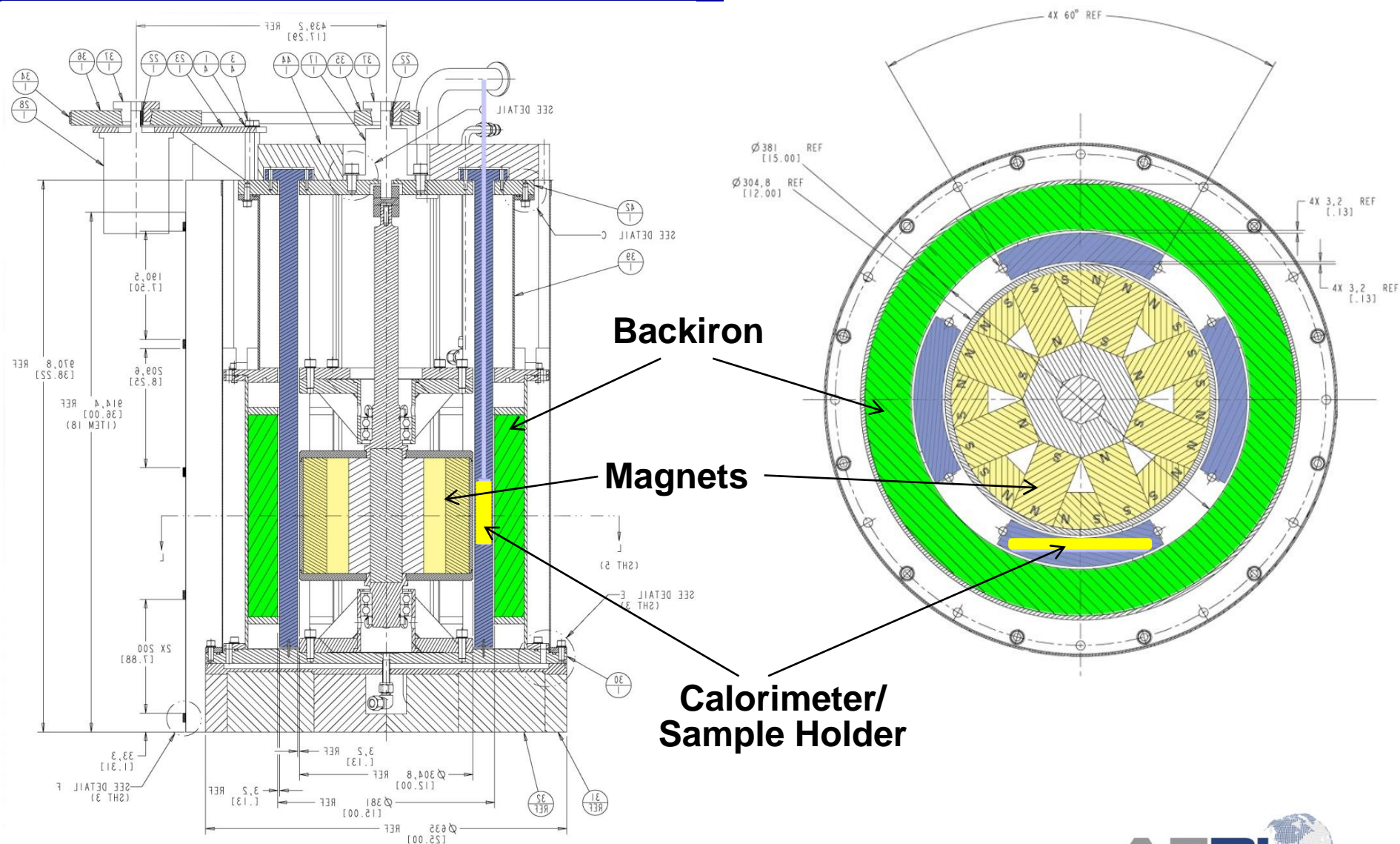
- 8-pole Hallbach Array of NdFeB Magnets
- B-field = 0.62 T
- **Frequency = 0 to 400 HZ (required for AF)**
- **Sweep Rate $B \cdot f = 240$ T/s**
(~ 15x higher than standard world-wide)
- Calorimetry Measurement – very precise
- **77K with liquid N_2**
- **4.2 K with liquid He !**
- **20 K with liquid Hydrogen (?)**
- Tapes, Cables, Coils – small or large
- AC loss in real stator environment, complex B and I varying in time and space

**8 Pole Permanent Magnet Rotor
Provides 0.62 Tesla
0 Hz to 400 Hz**

J. Murphy, et al., IEEE Trans. Appl. Supercond.
23(3), 4701505 (Jun 2013)

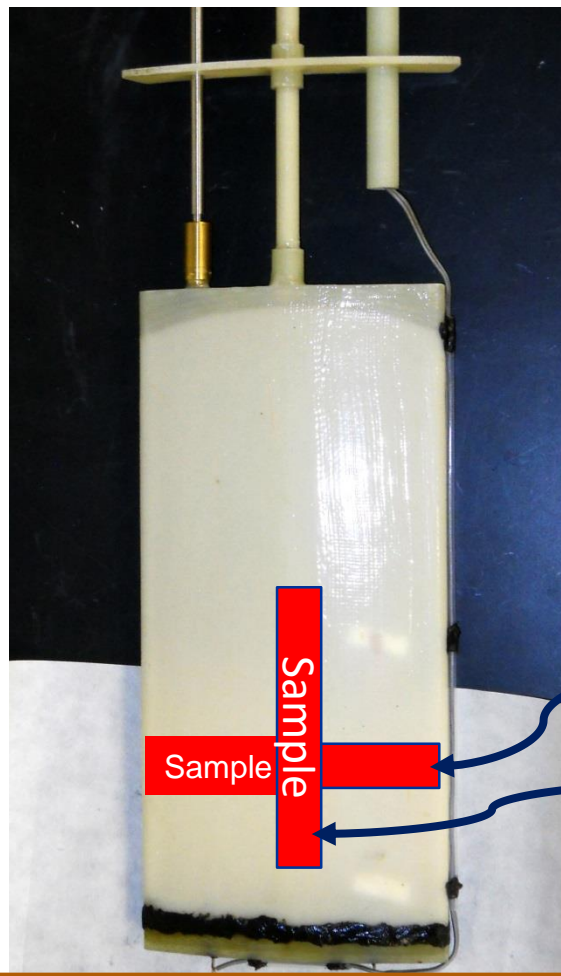
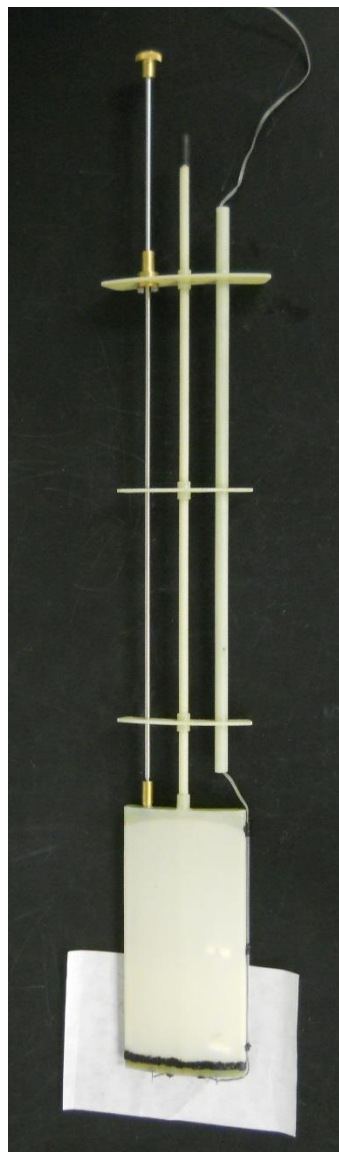


Machine Cross Sections





Sample Holder/Calorimeter



Sealed Sample holder
LN₂ Filled via remote operated
valve on top
Sample inserted through bottom
port which is sealed with a plug
Contains resistors for heating
All fiberglass except valve and
resistance heater

Sample orientation:
Horizontal is parallel to the
magnet motion
Vertical is perpendicular to the
magnet motion

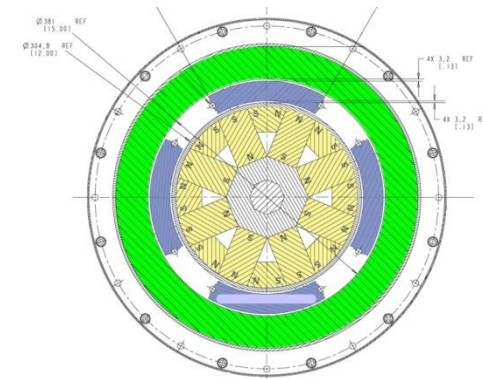
Direction of Magnetic Field Motion
Relative to Sample Holder



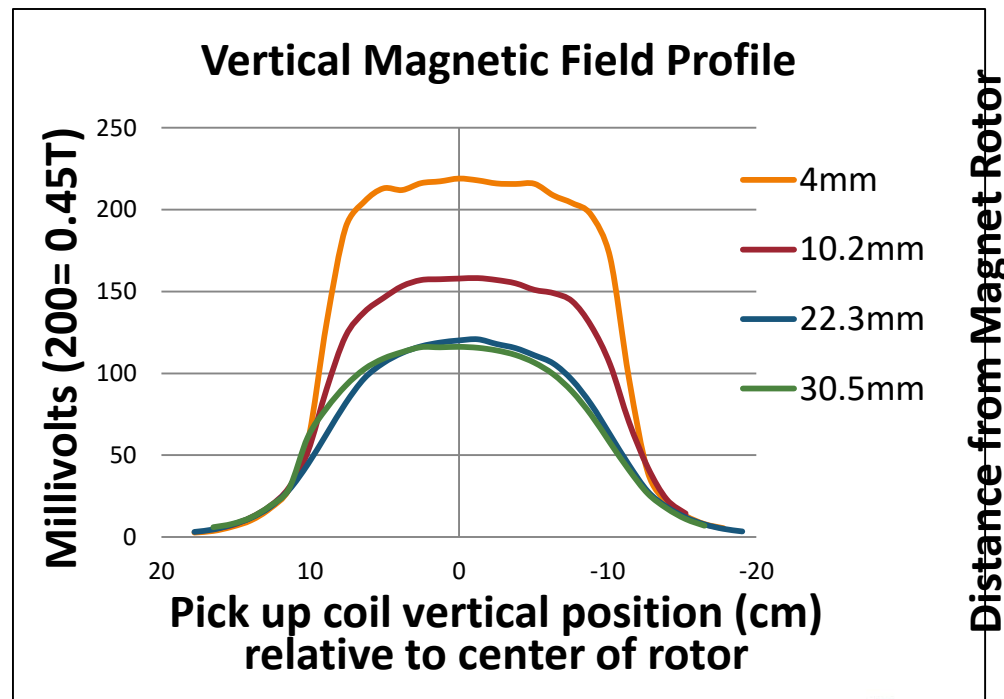
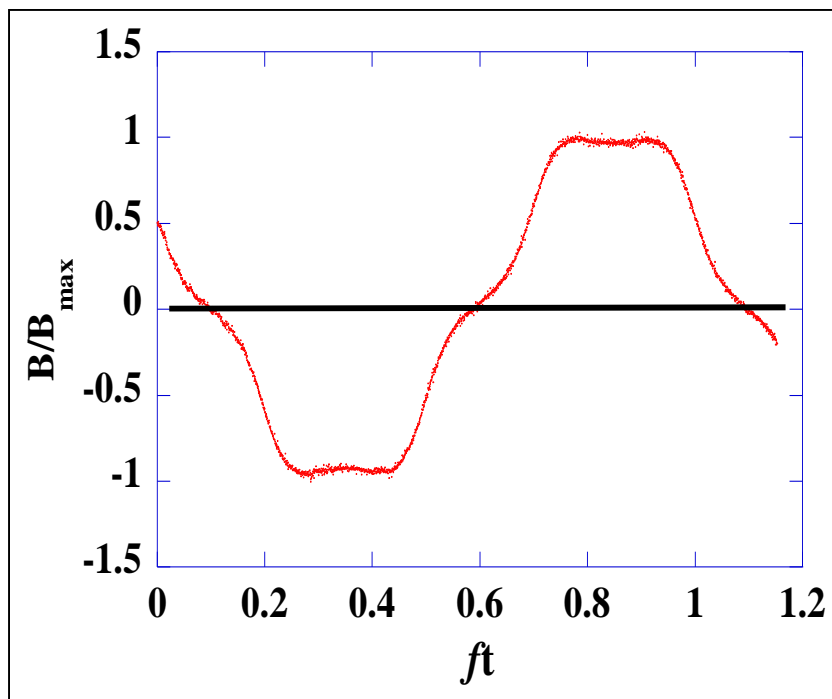
SAM Machine (dB/dt) Calibration and Properties



- In the 0.35 Tesla plane (~ 10 mm from rotor)
- At 900 RPM (60Hz) sweep rate is 12.25 T/Sec
- At 6000 RPM (400Hz) sweep rate is 140 T/Sec

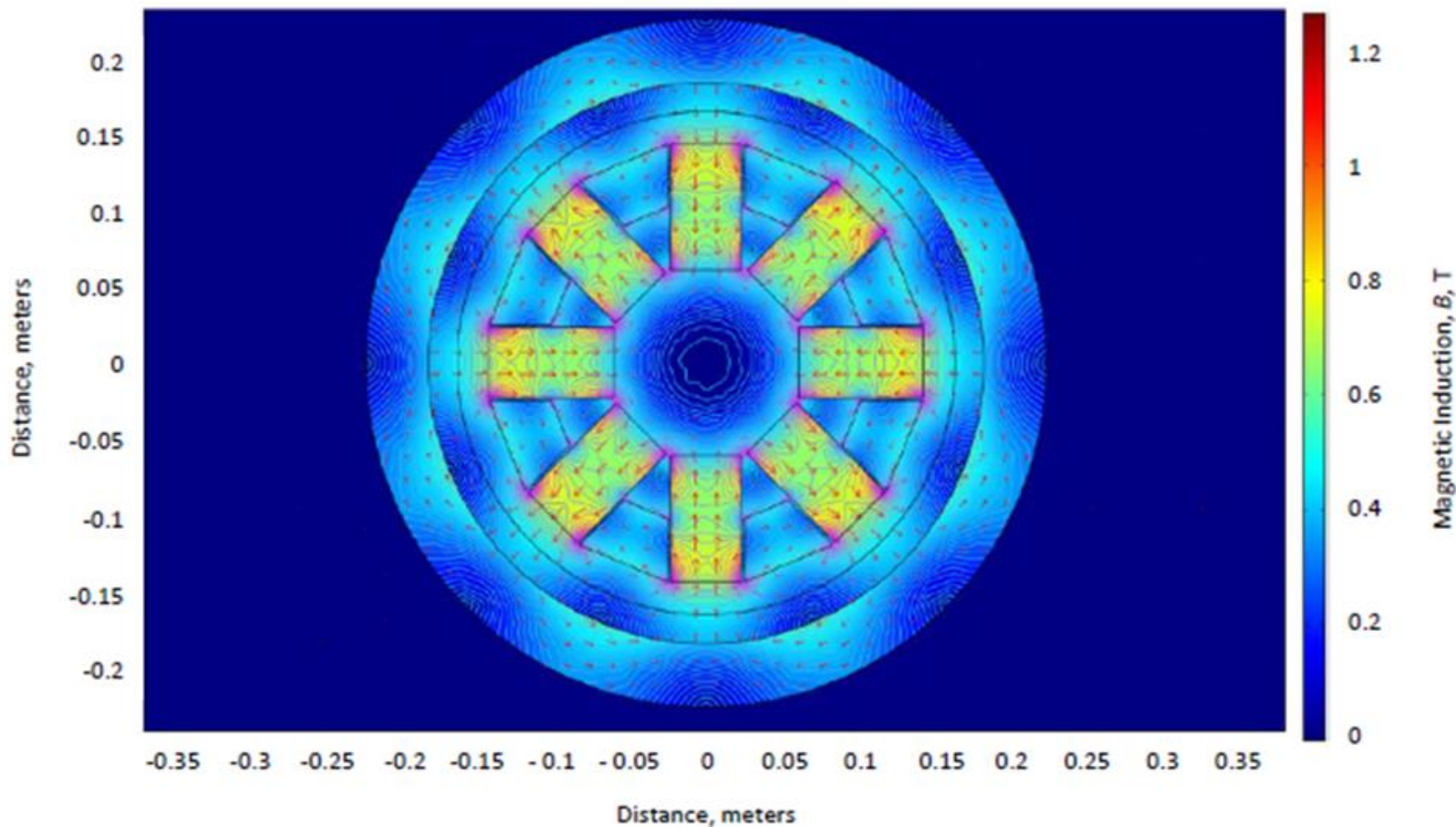


(dB/dt) at one location





Contour and color map of $|B|$ (in T) together with B vectors

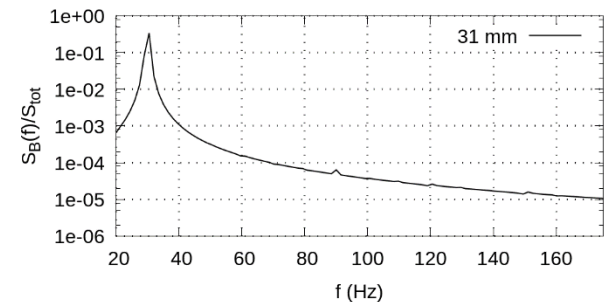
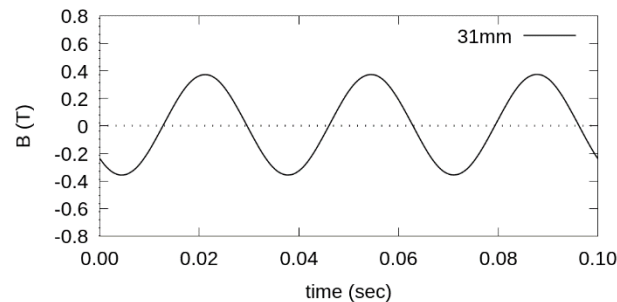
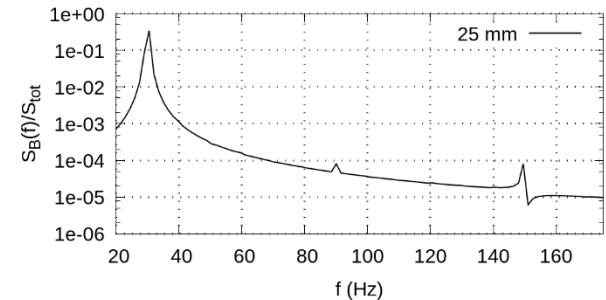
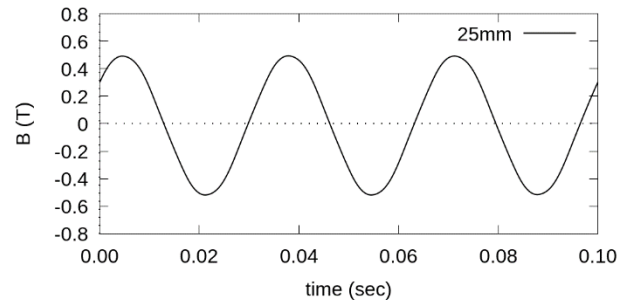
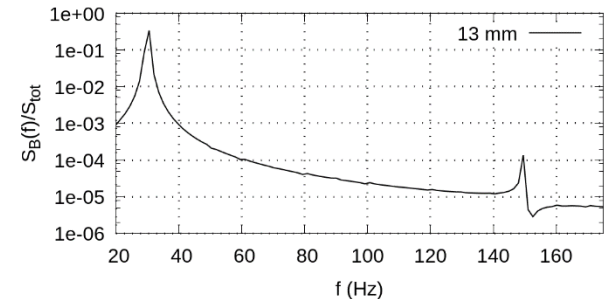
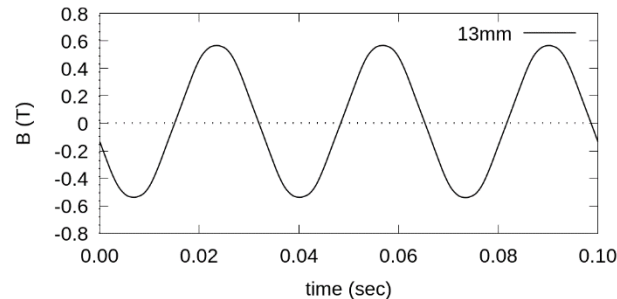


Finite Element calculations show both radial and tangential moving fields
Actual mapped fields correspond with the calculations



Radial Fields in SMC

- Radial B at three different radial distances within the gap
- The peak radial field (0.566 T) drops slightly with increasing R
- Shown at right are the fft
- The signal is very similar to a pure sine wave, with small harmonics at 3 and 5 times the fundamental

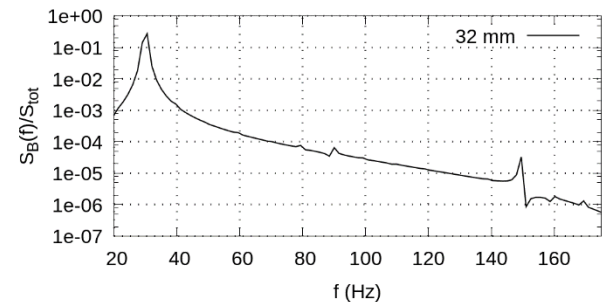
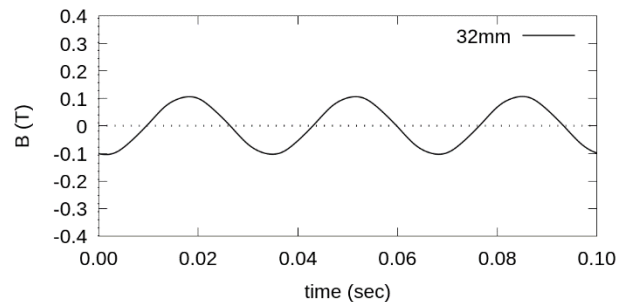
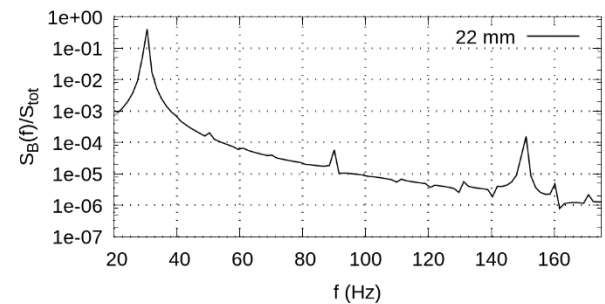
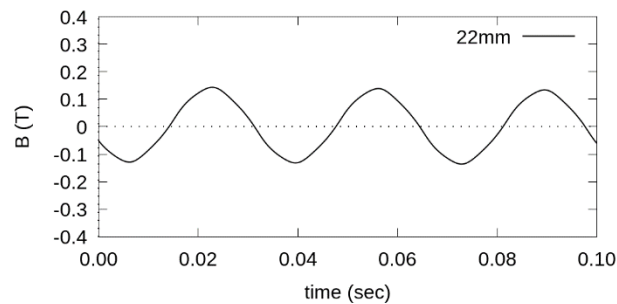
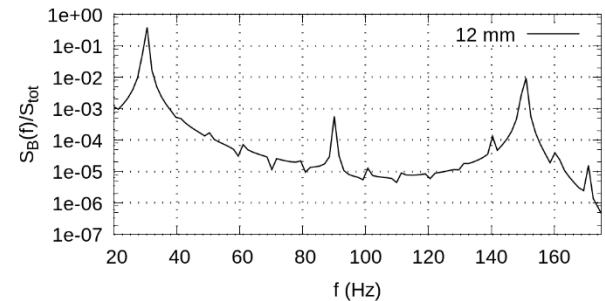
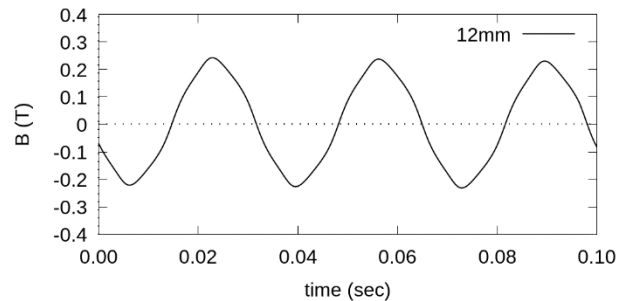




Tangential Fields in SMC

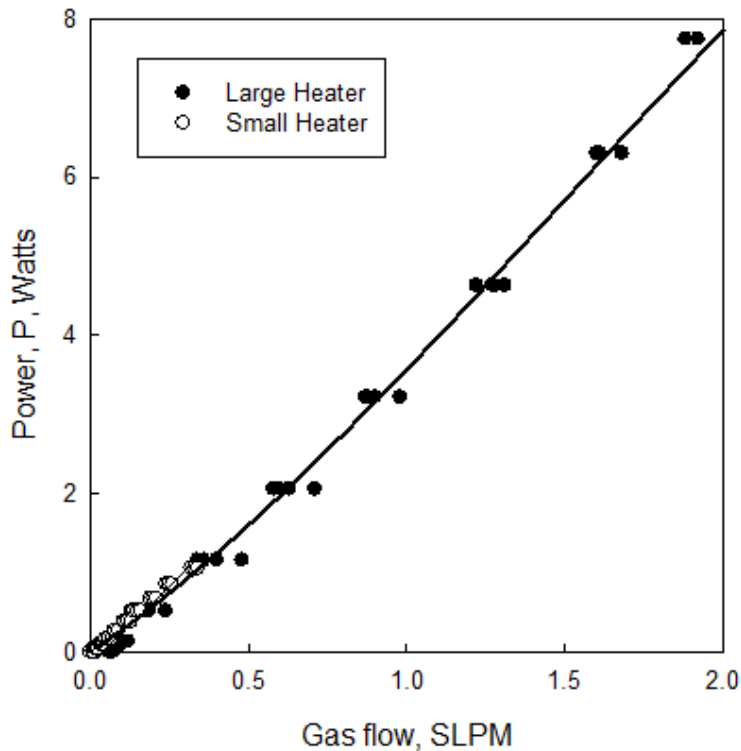


- Tangential B at three different radial distances within the gap
- The peak tangential field (0.242 T) drops with increasing R
- Shown at right are the fft
- The signal is still primarily a sine wave, but with greater deviations than for the radial case



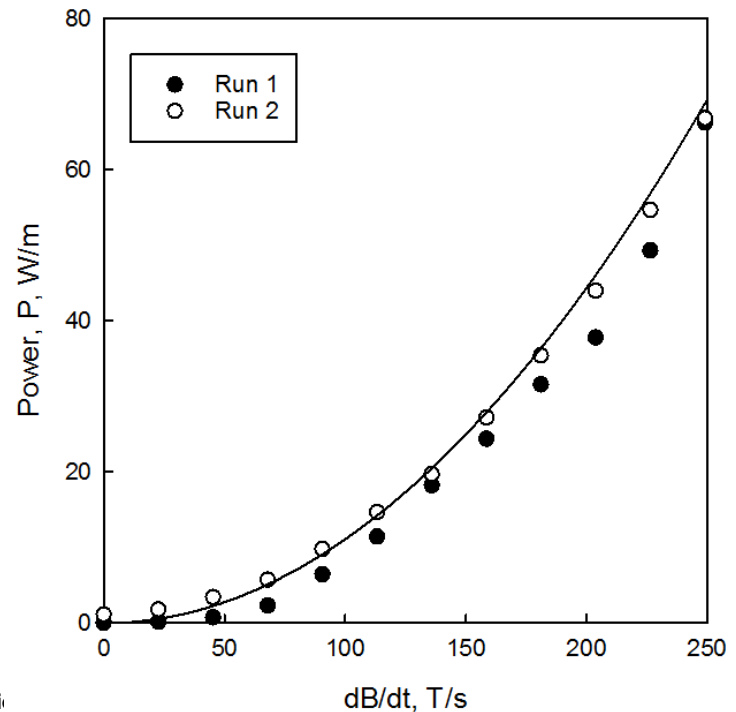


Calibration with Heater and Cu sample



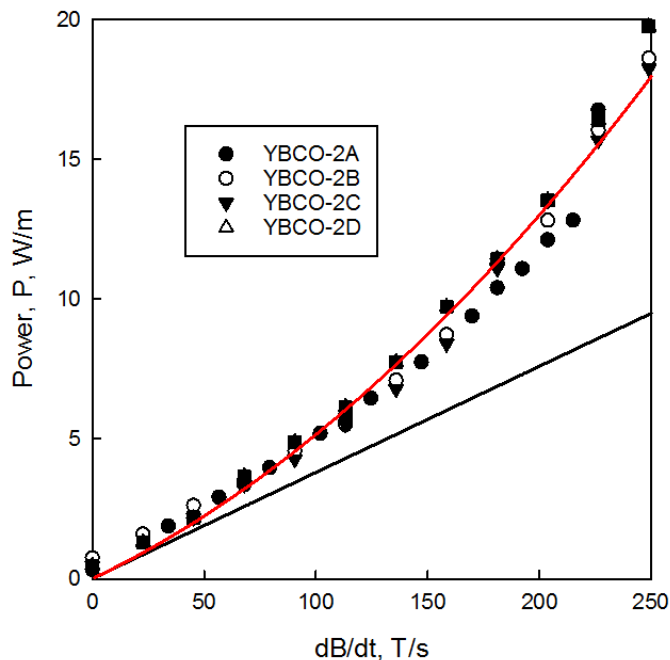
Calibration of calorimeter. $P(W) = -0.0096 + 2.7581 * GF + 1.0575 * GF^2 - 0.2346 * GF^3$

Power loss (P) vs dB/dt for the Cu strip Sample. Fit assumes $RR = 7.37$



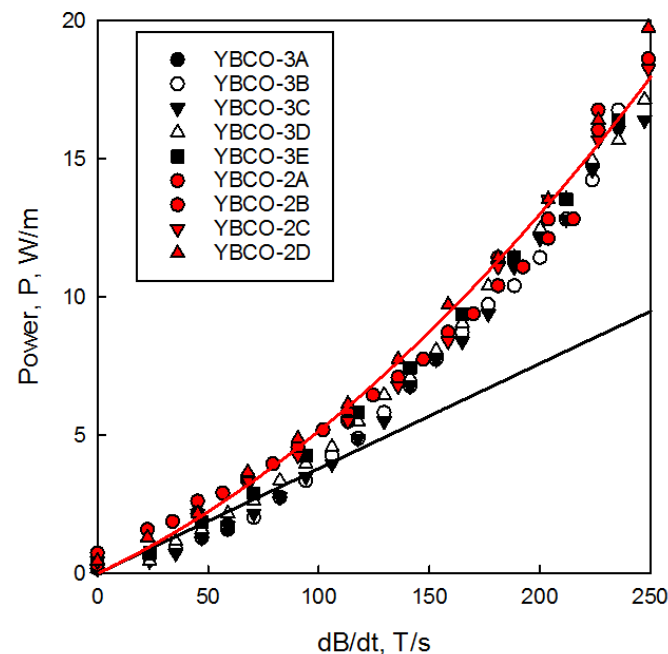


AC loss of 10 cm length YBCO tape, hysteretic and eddy current



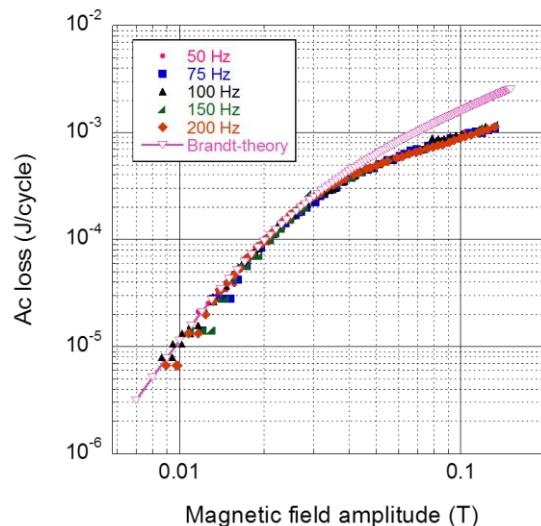
- Power Loss (P) vs dB/dt for YBCO tape samples 2 and 3
- Black line is fit for Brandt equation with $I_c = 38$ A, and red line includes eddy current contribution for RR (77 K) = 4.0

- Power Loss (P) vs dB/dt for sample YBCO tape 2
- Black line is fit for Brandt equation with $I_c = 38$ A, and red line includes eddy current contribution for RR (77 K) = 4.0



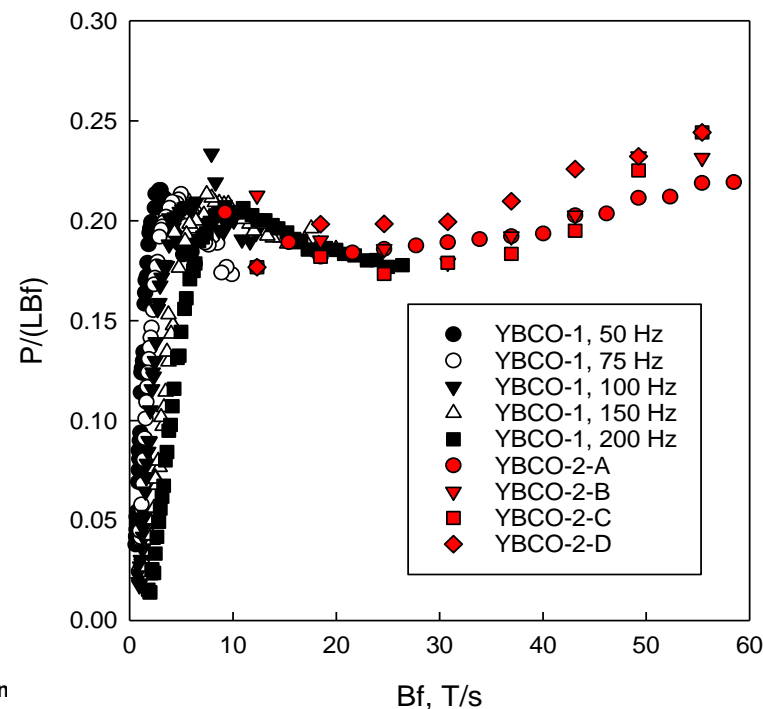


Loss measured of single tape in SMC compared to standard Inductance Measurement



- Solenoidal susceptibility rig measurements compared with Brandt theory (pink open triangles) ($I_c = 128$ A).
- In higher fields (> 0.05 T) the experimental data deviate from the theory (which uses I_c independent of magnetic field) apparently due to $I_c(B)$ dependence

- Power loss (per unit length) normalized by $B \cdot f$ vs $B \cdot f$ for SMC (shown in red) (YBCO-2) and solenoidal susceptibility rig (shown in black, for YBCO-1)

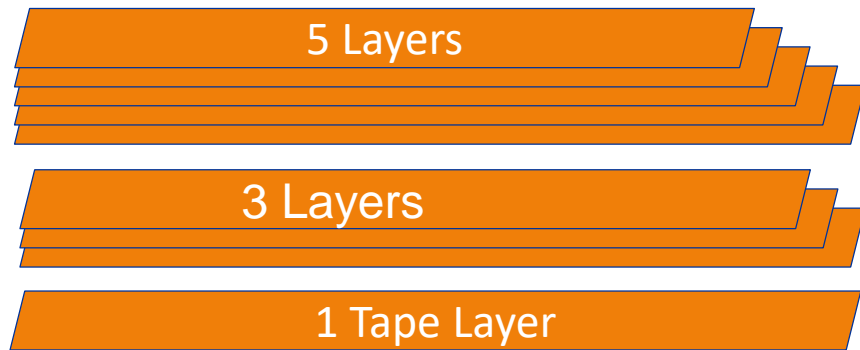




Two new Measurement Series— CORC and Carpet stacks



Carpet Stack cables



4 mm wide Superpower YBCO coated
conductor
5 layers
3 layers
1 layer
Secured with narrow strips of Kapton tape



Conductor on Round Core (CORC) cable sample from Danko



- 3.13 mm OD SS304 former
- 4.76 mm overall cable OD
- 4 mm wide Sunpower YBCO coated conductor
- 2 layers with 3 tapes each, outer layer is twisted opposite of the inner layer
- 34 mm pitch with 1 mm spacing

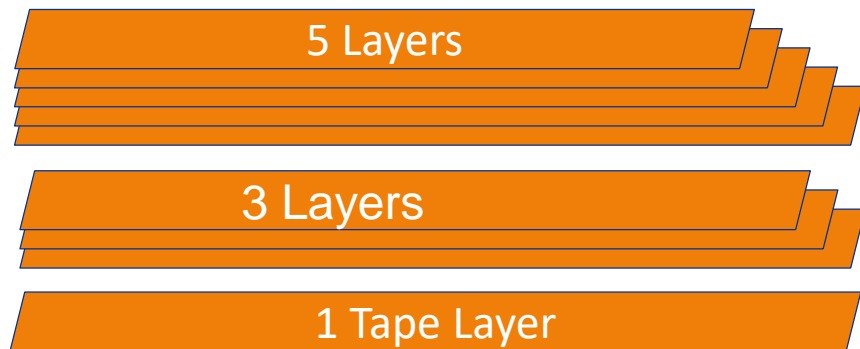
M Majoros, M D Sumption, E W Collings and
D C van der Laan, *Supercond. Sci. Technol.* 27



Influence of stacking on loss?



Carpet Stack cables with Un-Filamented tapes



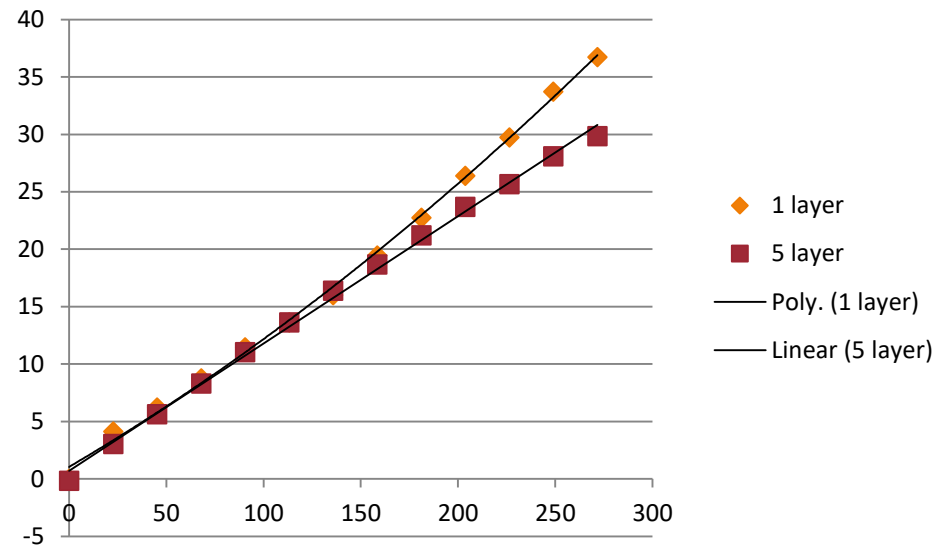
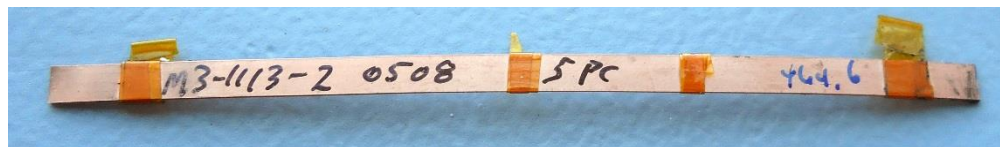
4 mm wide Sunpower YBCO coated conductor

5 layers

3 layers

1 layer

Secured with narrow strips of Kapton tape



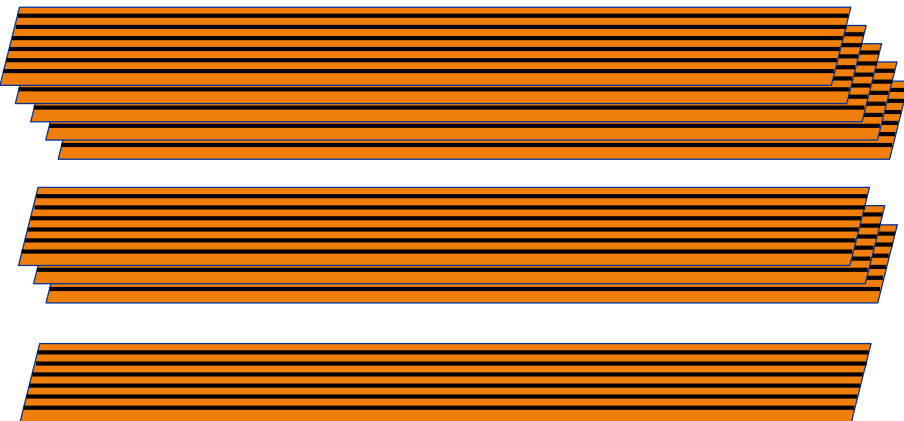
- Samples were unstriated
- $L = 10$ cm, untwisted
- $I_c = 127$ A 77 K, SF
- Loss is shown as power per meter of tape
- Here higher loss is seen for single stack, possible influence of demagnetization on loss



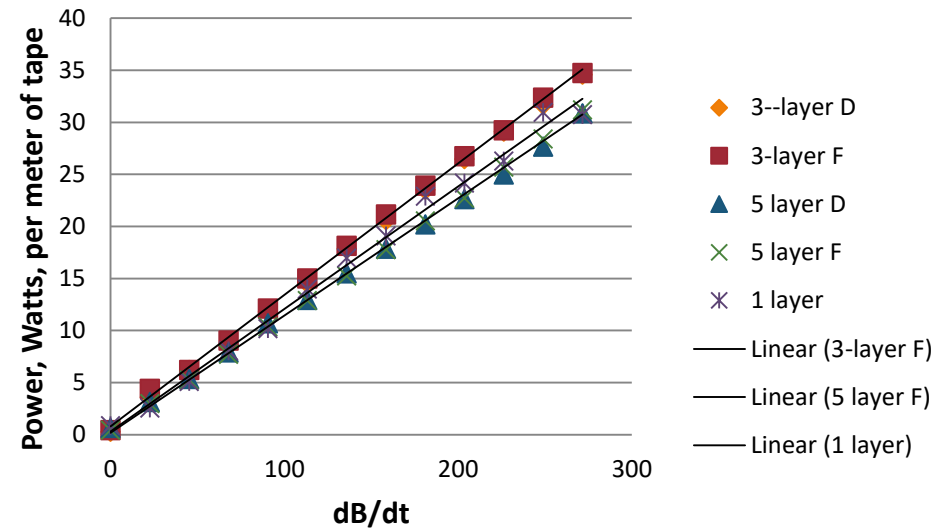
Loss in striated and Cu EP Tapes



Carpet Stack cables with Filamented tapes



4 mm wide YBCO coated conductors
Filamented and provided by Sunpower



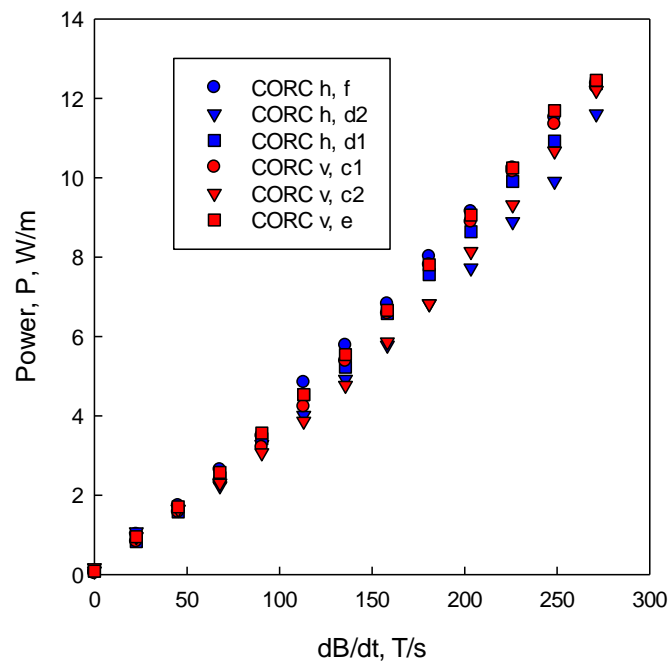
- Samples were striated
- $L = 10$ cm, untwisted
- Loss is shown as power per meter of tape
- Here no modification of loss with stacking of tapes is seen



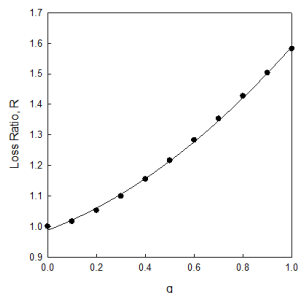
CORC AC Loss Measurements



- Two layer CORC sample
- SS304 (3.13 mm OD) former
- Cable OD of 4.76
- Superpower Coated conductor
- 4 mm wide and 0.09 mm thick.
- Two layers, each with three tapes, with a 1 mm gap between the tapes.
- Twist pitch = 34 mm, outer layer twisted in an opposite sense to the inner layer.
- Measured Vertically and Horizontally



$$H_A = \hat{x}H_{x,max} \cos(\omega t) + \hat{y}H_{y,max} \sin(\omega t)$$

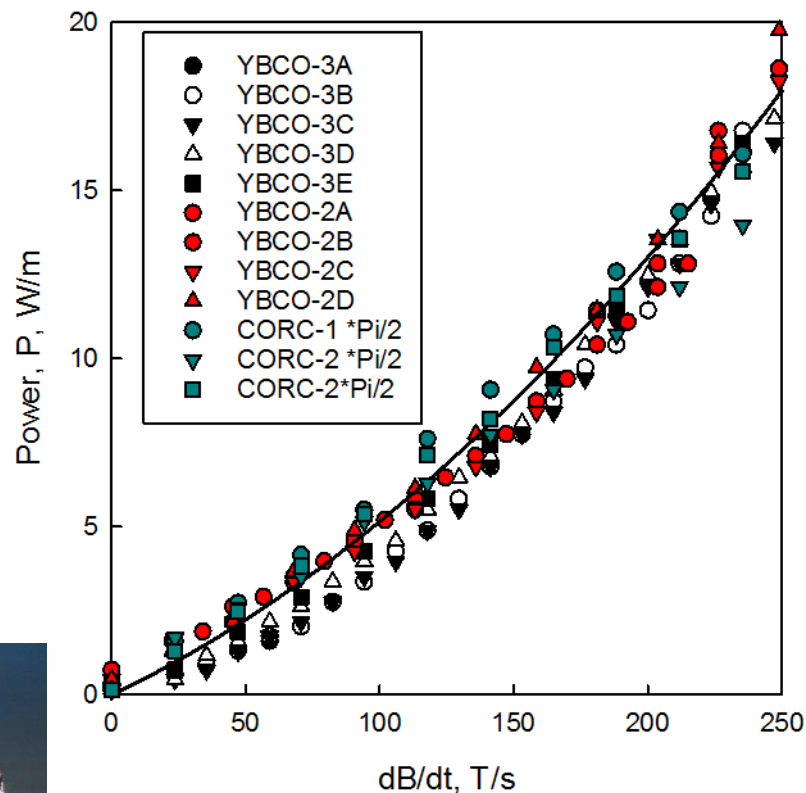




CORC compared to Tape it was wound with



- CORC cable loss per unit meter of tape multiplied by the factor $\pi/2$, as compared to tape loss per unit meter of tape. CORC cable was oriented horizontally.
- Simplistic integration of the field perpendicular to the tape appears to describe the loss for the tapes in the CORC !





Samples

Roebel Cable, IRL, NZ

TABLE I
PARAMETERS OF THE ROEBEL CABLE

Quantity	
Cable width (mm)	13
Cable thickness (mm)	1.5
Cable twist pitch (cm)	30
Cable length (cm)	30
Number of tapes in the cable	15
Tape width (mm)	5
Cable I_c (77.3K, self-field) (A)	1537.5



CORC Cable



Sample	Tapes	I_c (A)	ID (mm)	OD (mm)	Length (cm)	Striations
R1	2 x 3 = 6	608	4.96	6.17	11.7	none
S1	2 x 3 = 6	349	4.95	6.07	12.2	5
R2	3 x 3 = 9	904	4.93	6.37	11.7	none
S2	3 x 3 = 9	535	4.94	6.38	11.8	5
R3	4 x 3 = 12	1228	5.02	6.85	11.7	none
S3	4 x 3 = 12	750	4.97	6.78	11.9	5

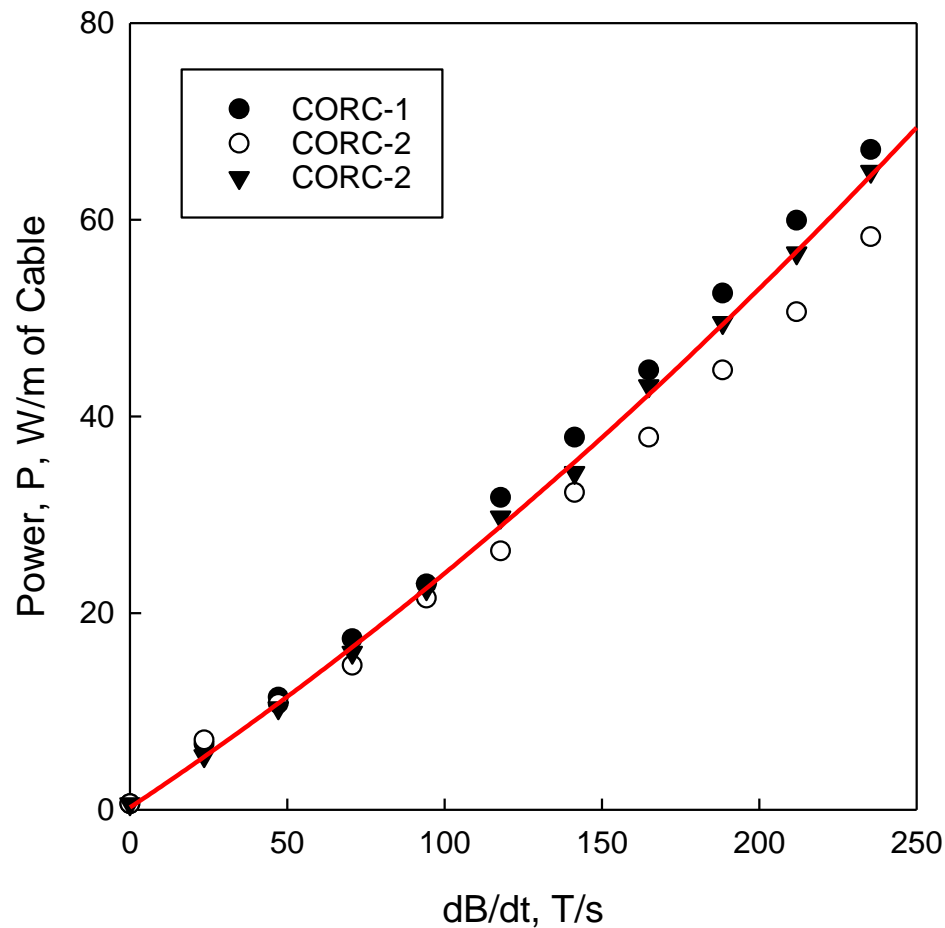
CORC Cable with layers and striations



CORC Loss per meter of Cable



- 4 mm wide tape
- Cable: 2 layers, 3 tapes per layer, 1 mm gap
- $L_p = 34$ mm, outer layer twisted in an opposite sense to the inner layer.
- Each meter of cable has 6.552 m of strand





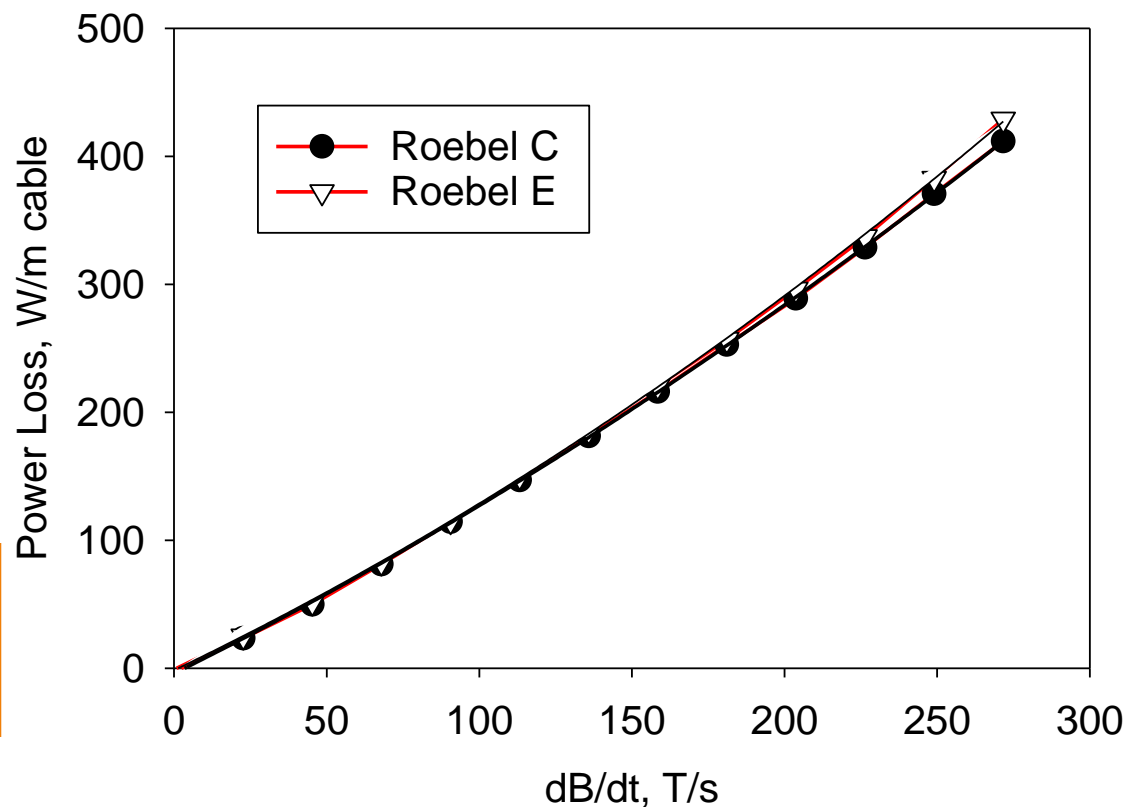
Loss in Roebel Cable

The cable was from IRL

TABLE I
PARAMETERS OF THE ROEBEL CABLE

Quantity	
Cable width (mm)	13
Cable thickness (mm)	1.5
Cable twist pitch (cm)	30
Cable length (cm)	30
Number of tapes in the cable	15
Tape width (mm)	5
Cable I_c (77.3K, self-field) (A)	1537.5

Losses per meter Cable
At 77 K, I_c per tape = 100 A,
SF

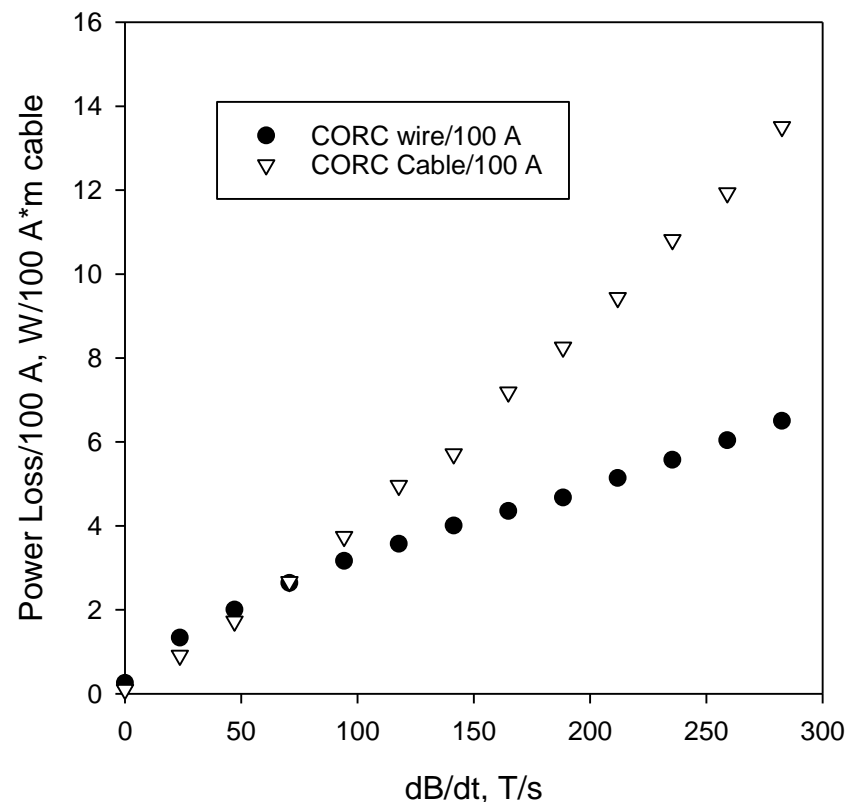
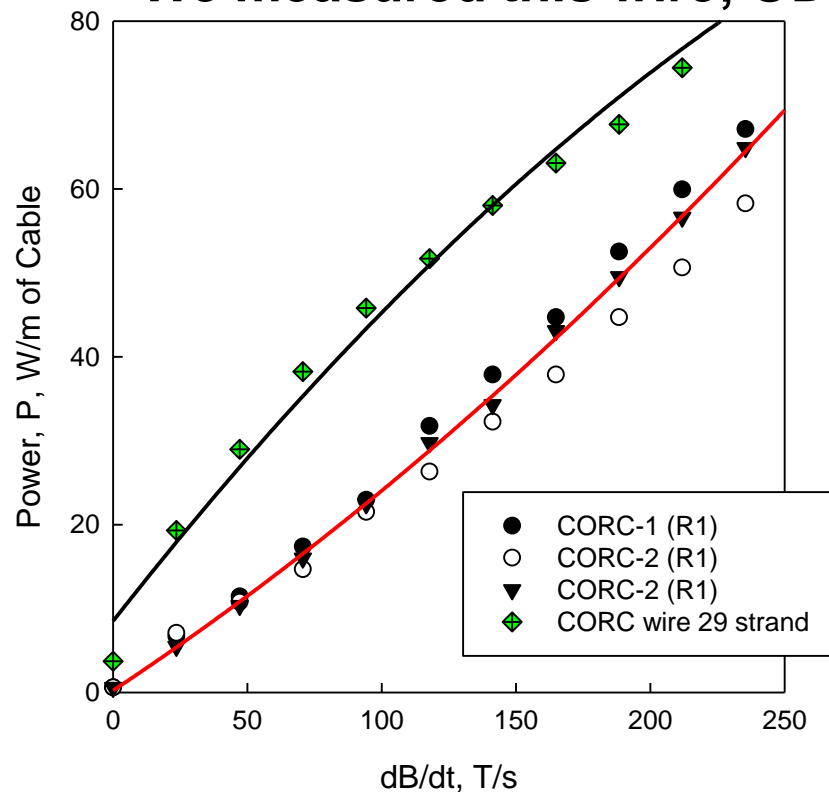




CORC Wire Loss



- New CORC Wire is available which promises lower loss and higher flexibility for making very high amperage cable
- We measured this wire; OD 3.65 mm, 29 strands





Loss Measurements of 4 filament Al Hyperconductor wire



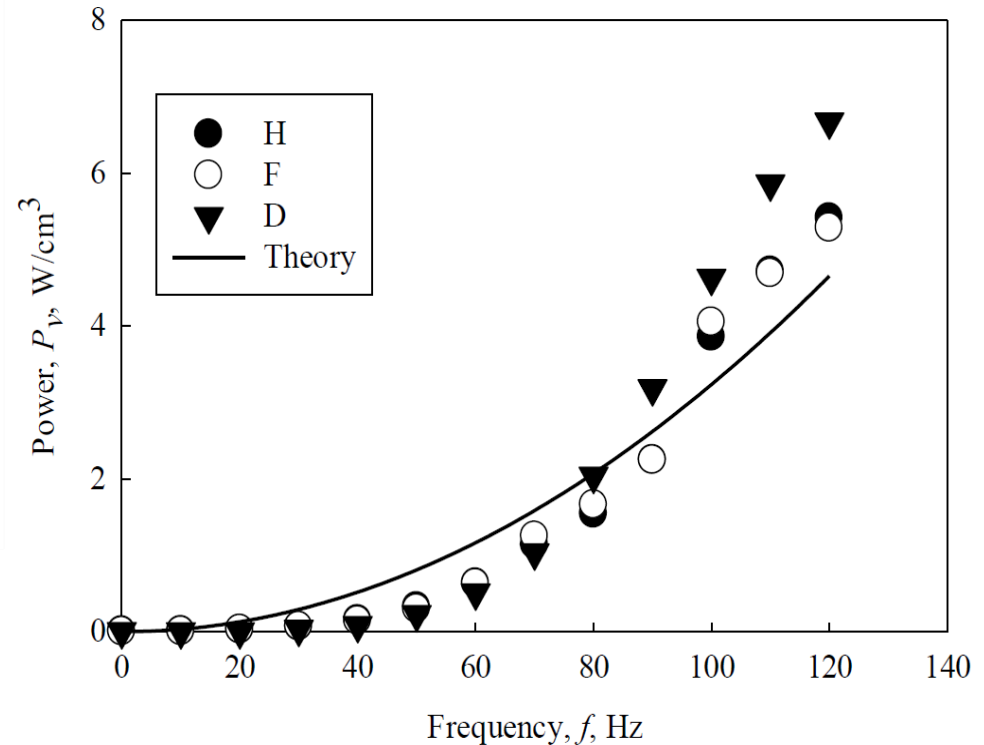
$$P_{tot} = \left\{ \begin{array}{ll} P_{e,matrix}\{d_s, \rho_m\} + P_{e,fil}\{d_f, \rho_{fil}\} + P_{coup}\{L_p, \rho_m\} & \text{if } L < L_c \\ \approx \frac{1}{2\rho_m} [fL_p B_m]^2 & \\ P_e\{d_s, \rho_{fil}\} = \frac{\pi^2}{4\rho_{fil}} [(\mu_0 H_0) d_s f]^2 & \text{if } L > L_c \end{array} \right\}$$

Where

$$L_c = \pi d \sqrt{\left(\frac{\rho_m}{\rho_{fil}}\right)}$$

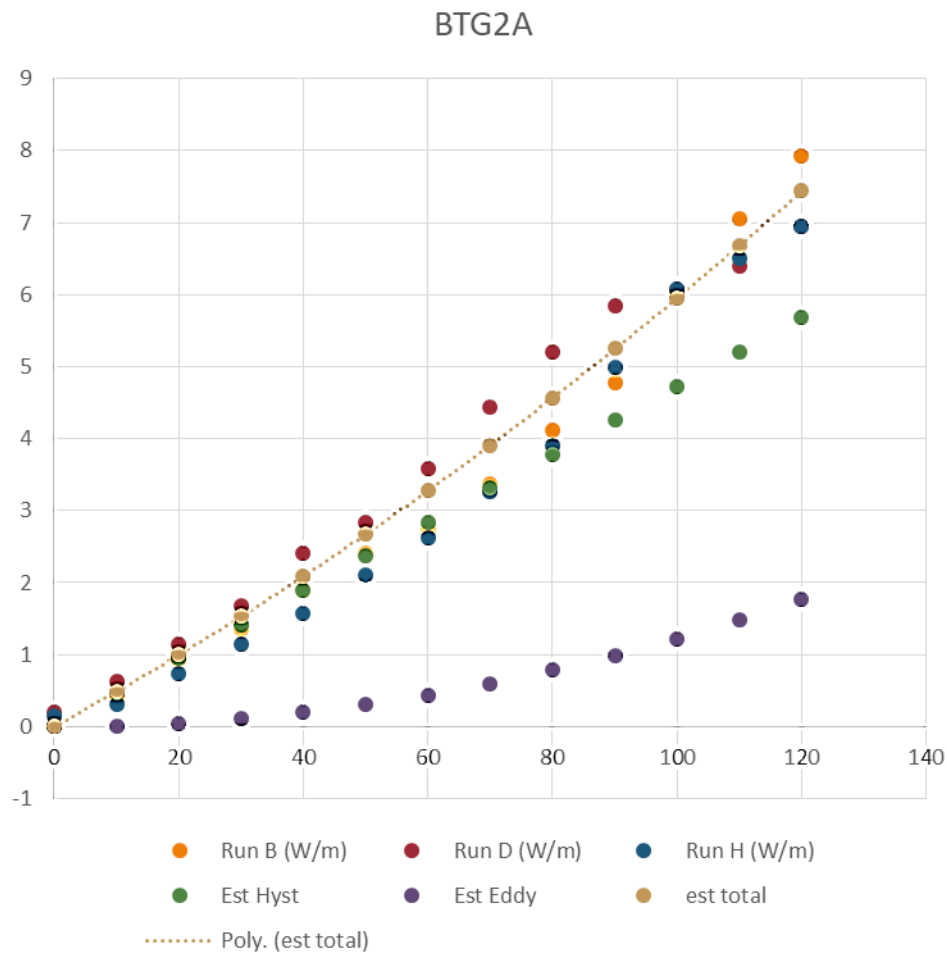
We can generate a frequency limit expression for hyperconductors

$$f = \sqrt{2} \frac{J_{cc} \rho_m}{L_p B} = \sqrt{2} \frac{J_{Cu,RT} \rho_m}{L_p B} \sqrt{\frac{\rho_{Cu,RT}}{\rho_{fil}}}$$





Recent Results on BNL Samples (exfoliated filament Cables)





Conclusions

- A new, High field, High ramp rate AC loss device operational which can reach 480 T/s!
- AC loss calibrations performed using (i) Standard resistor, (ii) Cu strip of known RR
- Explore high dB/dt characteristics of cables made of YBCO coated conductors
- Samples: striated tapes, CORC cables, Roebel cables, CORC Wires, Al Hyperconductors, Exfoliated filament samples,
- Comparison to theory and analysis

