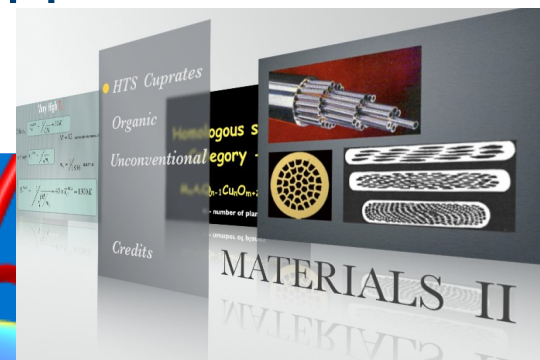


# High temperature superconducting hybrid tape stacks - an enabling technology: challenges for DC and AC applications

26<sup>th</sup> International Conference on Magnet Technology 2019  
Vancouver, Canada



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**1** Department of Materials Science and Metallurgy, University of Cambridge, 27 Charles Babbage Road, Cambridge CB3 0FS, UK

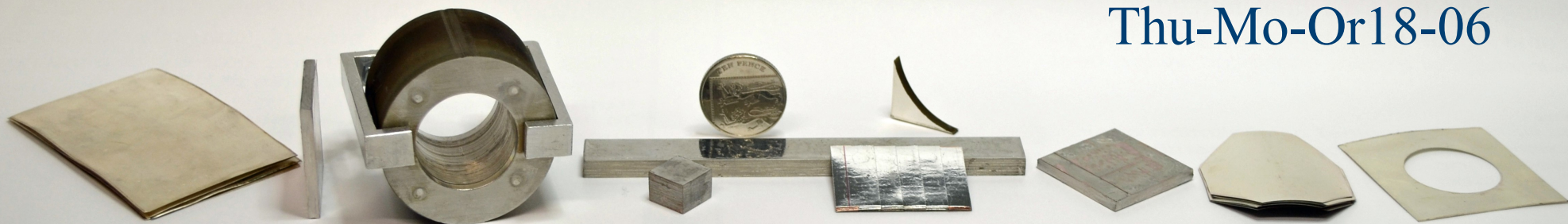
**2** Department of Physics and Energy and Bernal Institute, University of Limerick, Castletroy, Limerick, Ireland

**3** Institute of Power Engineering, Mory 8, 01-330 Warsaw, Poland

**4** Epoch Wires Ltd, Foxton, Cambridge, UK

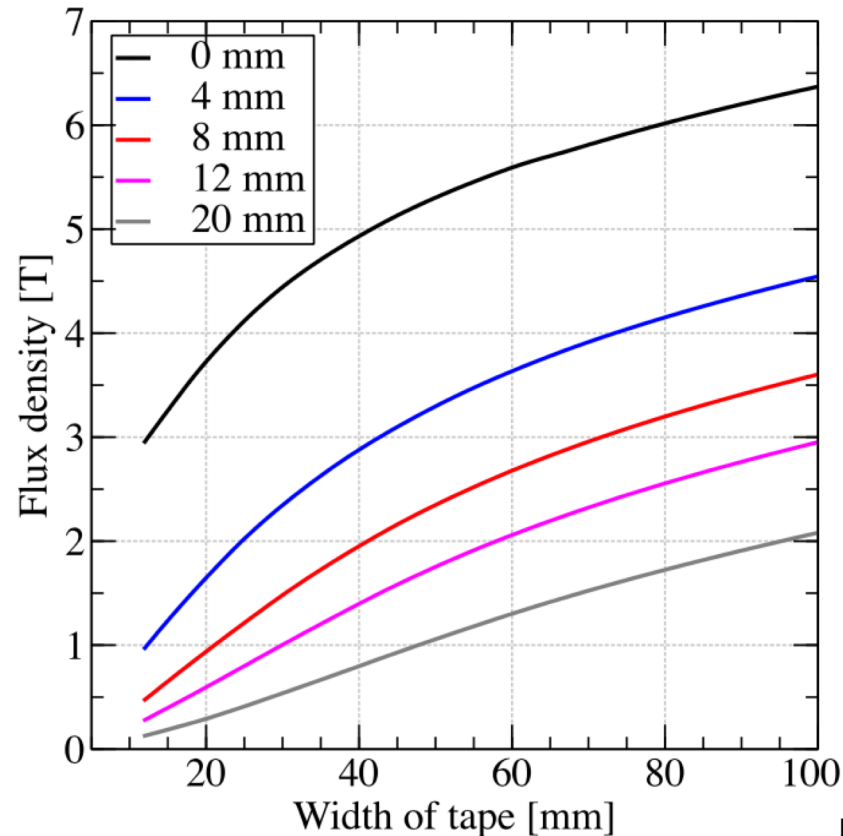
**5** Bruker BioSpin AG, Industriestrasse 26, 8117 Faellanden, Switzerland

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# Role of the YBCO tape width on stack trapped flux value

## “DC case”

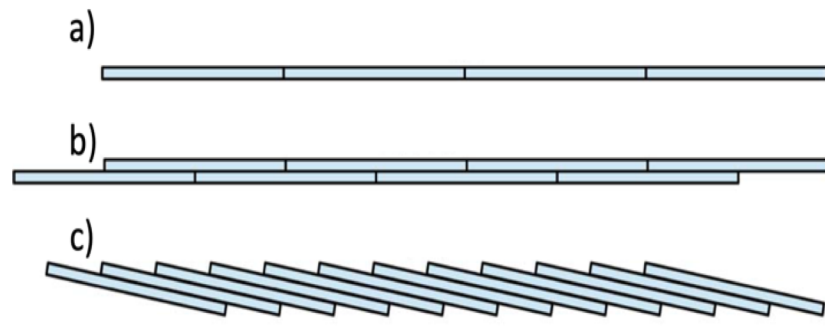


The main conclusion emerging from Fig. is that due to strong decay of magnetic field away from the superconducting stack, **narrow tape or arrays of narrow tape produce lower trapped flux.**

Field produced by HTS stack  
( $T=25\text{K}$ )

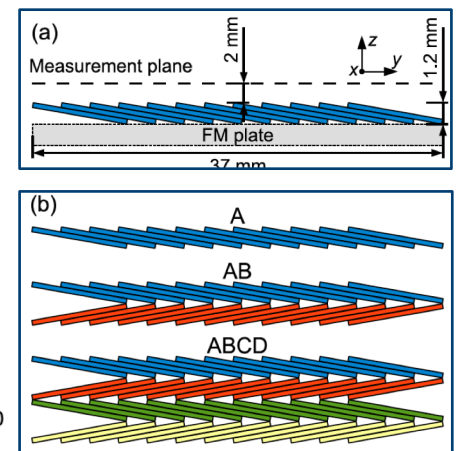
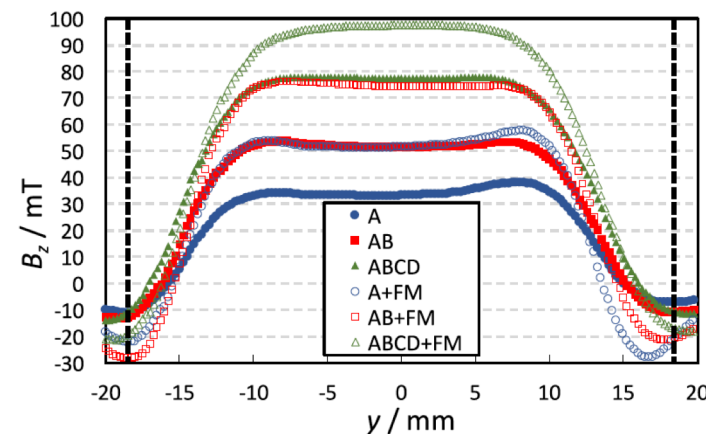
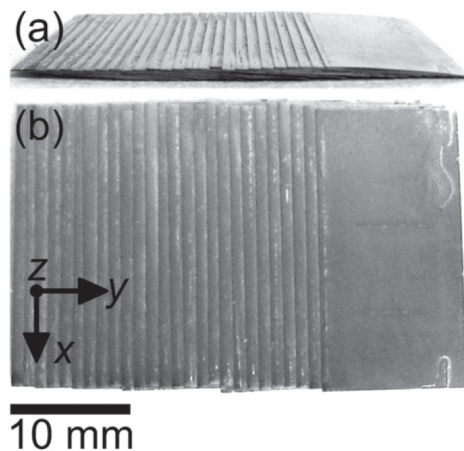
Calculation of magnetic flux density versus width of the model tape stack for different vertical distance perpendicular to the stack center (calculated curves are for distance 0, 4, 8, 12 and 20 mm away from the surface of the stack) temperature 25K.

# Angled stacking arrangement effect, using standard tapes



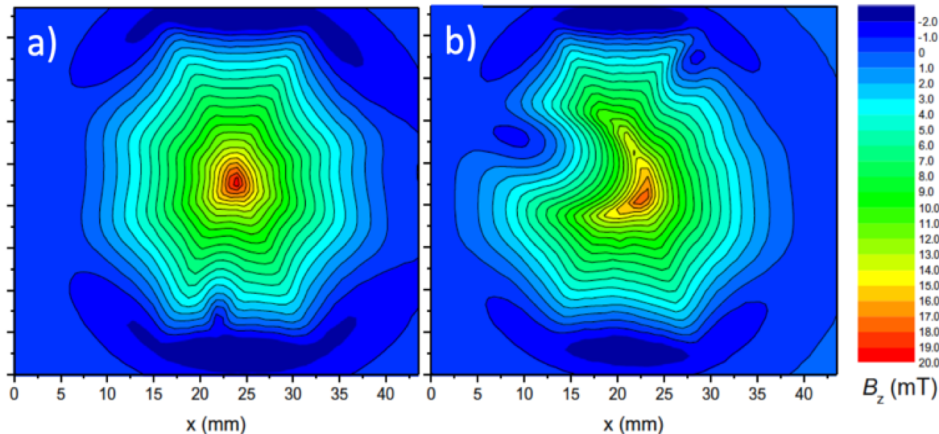
Comparison of the mean trapped flux,  $B^*$ , for configurations presented in Fig shows that **configuration b)** can trap 2.2 times higher value then configuration a)  
**configuration c)** can trap 5 times higher value then configuration a)

Schematic of the transversal cross sections of the *flat* and *angled* stacks.

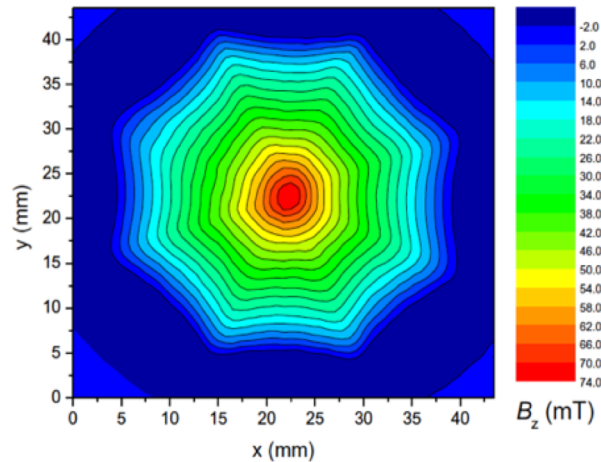


# Wide tape stack - trapped flux imperfections smoothing effect

40 mm wide YBCO tapes - off cuts !!!



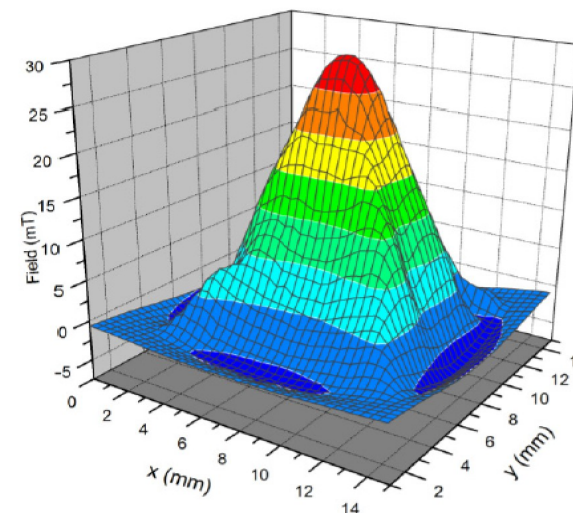
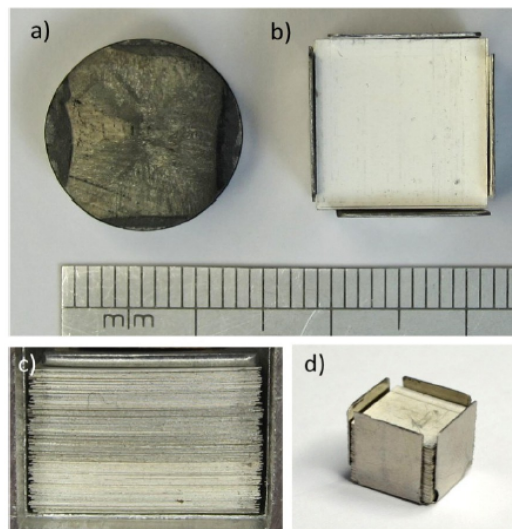
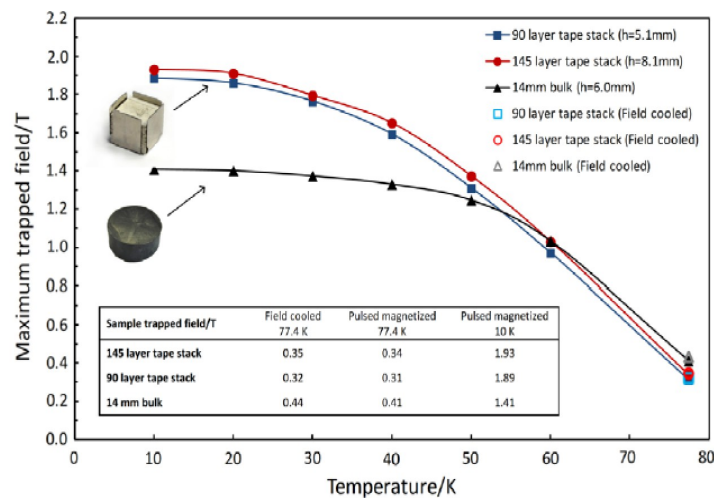
Trapped field profiles measured 0.6 mm above tape.  $B_z$  for various octagonal samples cut from 40-mm wide tape, where  $x$  is the transport axis.  
**a)** Common trapped field for a layer showing a small defect on the sample edge.  
**b)** Uncommon larger scale defect leading to an asymmetric trapped field profile.



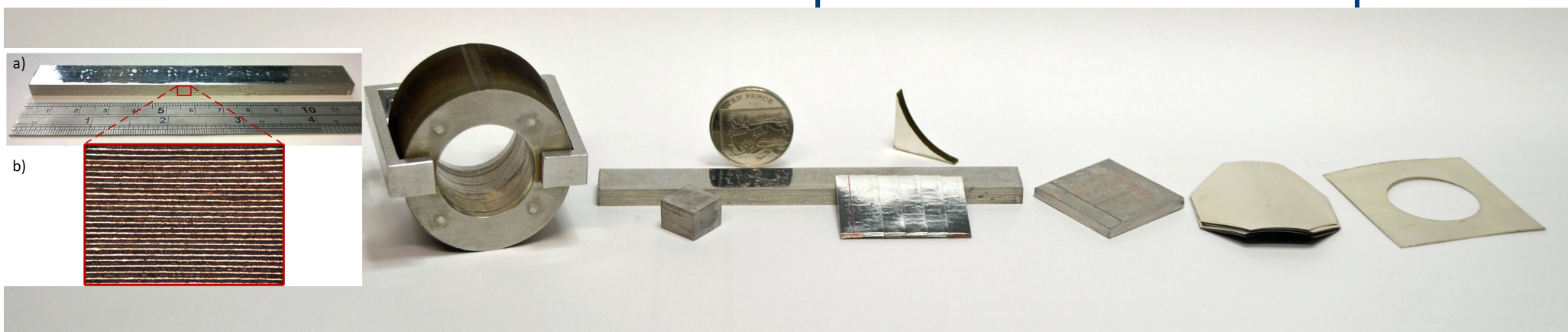
Trapped field profile measured at 0.8 mm above sample for a **stack of eight octagonal layers** cut from Tape B. Field cooling magnetization of the stack at 77 K results in a highly symmetric profile with a peak of 74 mT.



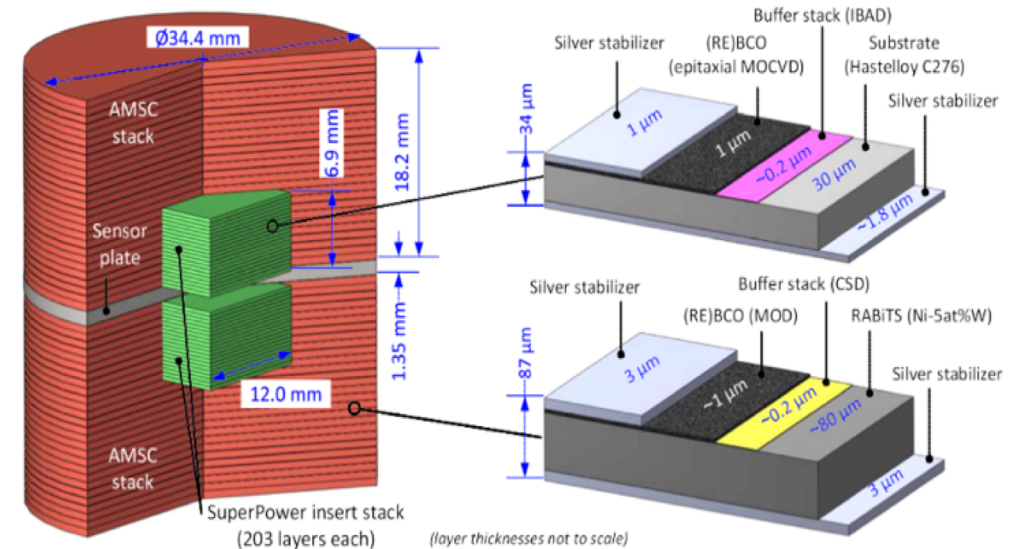
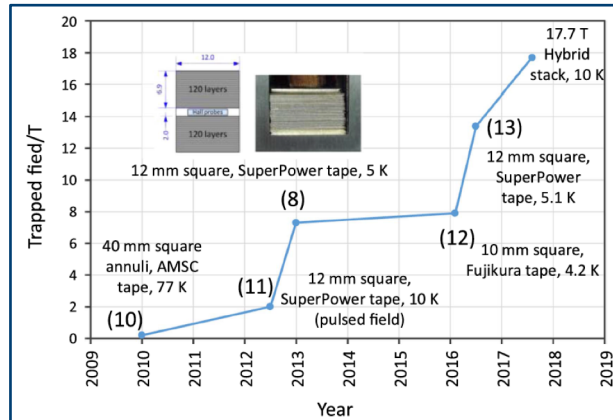
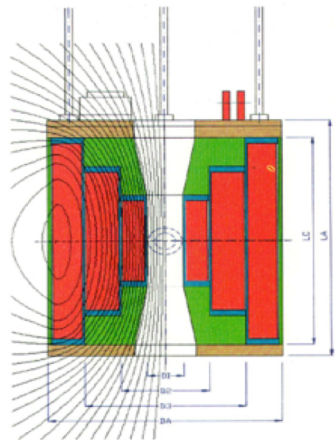
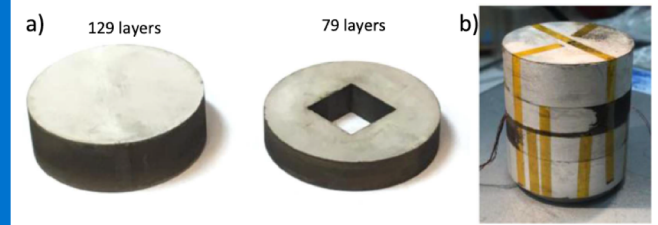
# Replacing YBCO bulks with consolidated stack of YBCO tapes



## American Superconductor 46 mm tape



# Hybrid stack as a 'composite magnet'. 17.7 T



Schematic of the hybrid magnet made from LTS superconducting conductors: The external coil was made from NbTi, the middle one was made from Nb<sub>3</sub>Sn and the central one was made from NbTi<sub>3</sub>(Sn,Ta) enabling generation of 22.59T.

Composition and geometry of the hybrid stack consisting of a 12 mm square stack made from SuperPower tape inside a 34.4 mm cylindrical stack made from AMSC tape. This hybrid structure in the analogue to composite hybrid NbTi and Nb<sub>3</sub>Sn magnets was capable of trapping world record 17.7 Tesla.



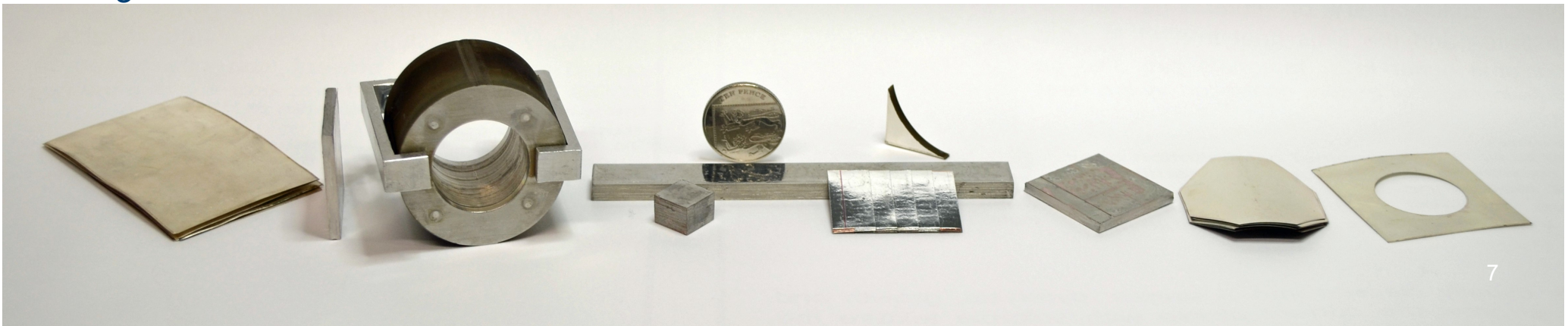
# Introduction of new wider tapes from D-nano

## RABiT substrates NiW

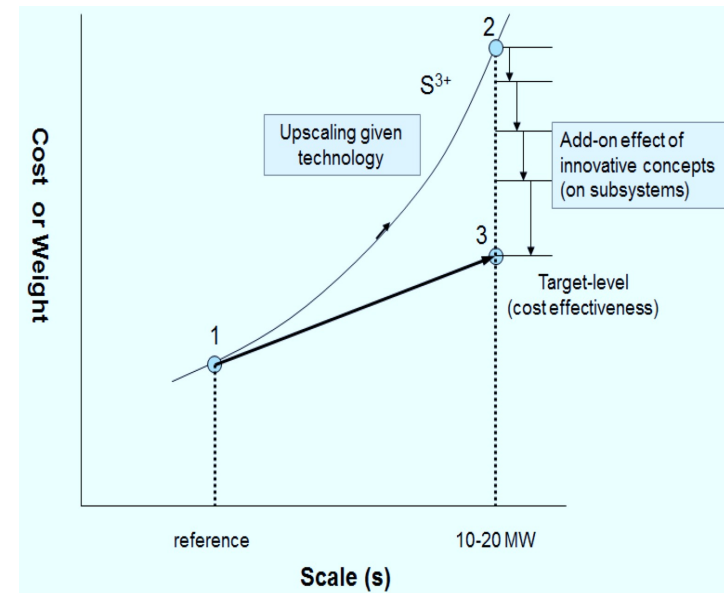
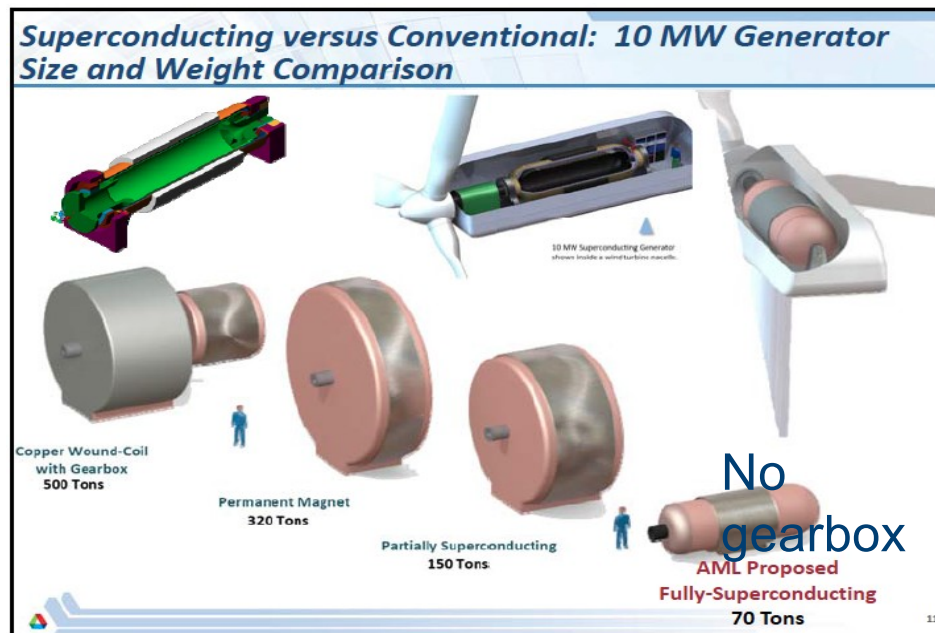
POSSIBILITY of replacement of the bulk YBCO round pellet like elements with superconducting fully stabilized almost 2D wide composite tape stacks opens up a new era of superconducting elements manufacture for levitation, energy generation and use applications.

These novel tape-stack structures which can be currently made using industrial scale manufacture of **40 mm width tapes** with the best price/performance ratio. **D-Nano Company**, is implementing plans to deposit on **100 mm wide and hundreds of meters long tapes** which will become a template for large elements characterized with high in *a-b* plane persistent paramagnetic current without that eliminate current along the *c*-axis as it is in case of bulk YBCO materials.

The benefit of conducting R&D on such stacks of tapes is it relevance to application to the high-power cables for energy physics and energy transmission application as well magnetic screens and functional NMR.



# 10 → 20 MW superconducting wind generators cooled indirectly by stored LH<sub>2</sub>



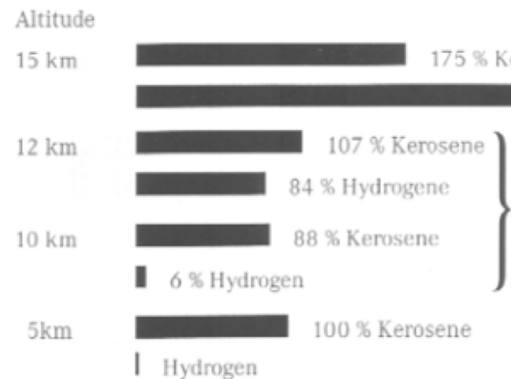
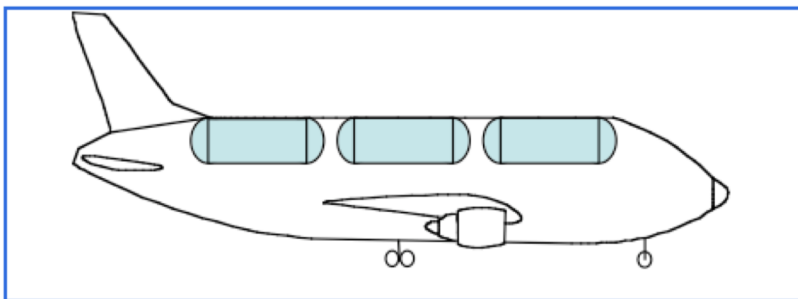
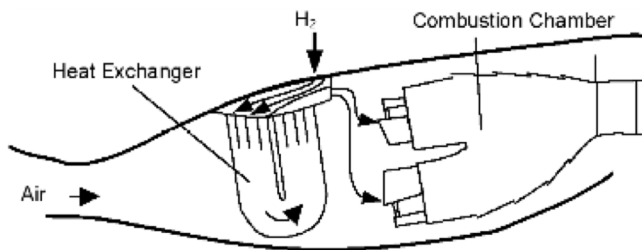
Depiction of the impact of technology innovations in reducing the cost of wind energy

One of the key targets for the design of these large multi megawatt wind turbines is to beat the cubic law of weight (and cost) of classical up scaling, which renders a **10-20 MW offshore design cost-effective**

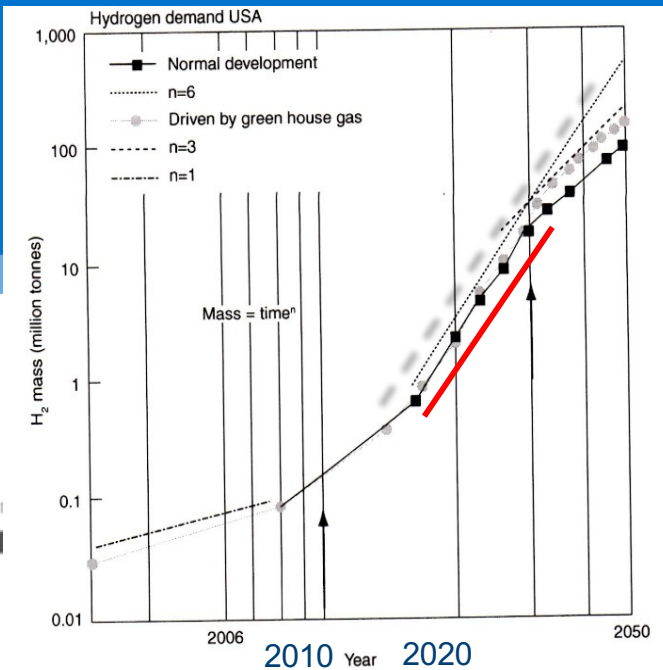
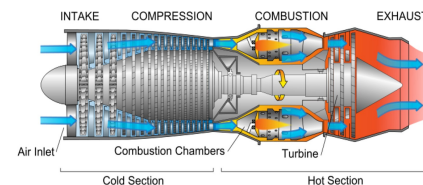


# Cryoplane: decentralised production and storage of $\text{LH}_2$ (designed in 1998)

## Hydrogen as a “fuel”



| Altitude | kerosene | hydrogen |
|----------|----------|----------|
| 15km     | 175%     | 275%     |
| 12km     | 107%     | 84%      |
| 10km     | 88%      | 6%       |
| 5km      | 100%     | 1%       |

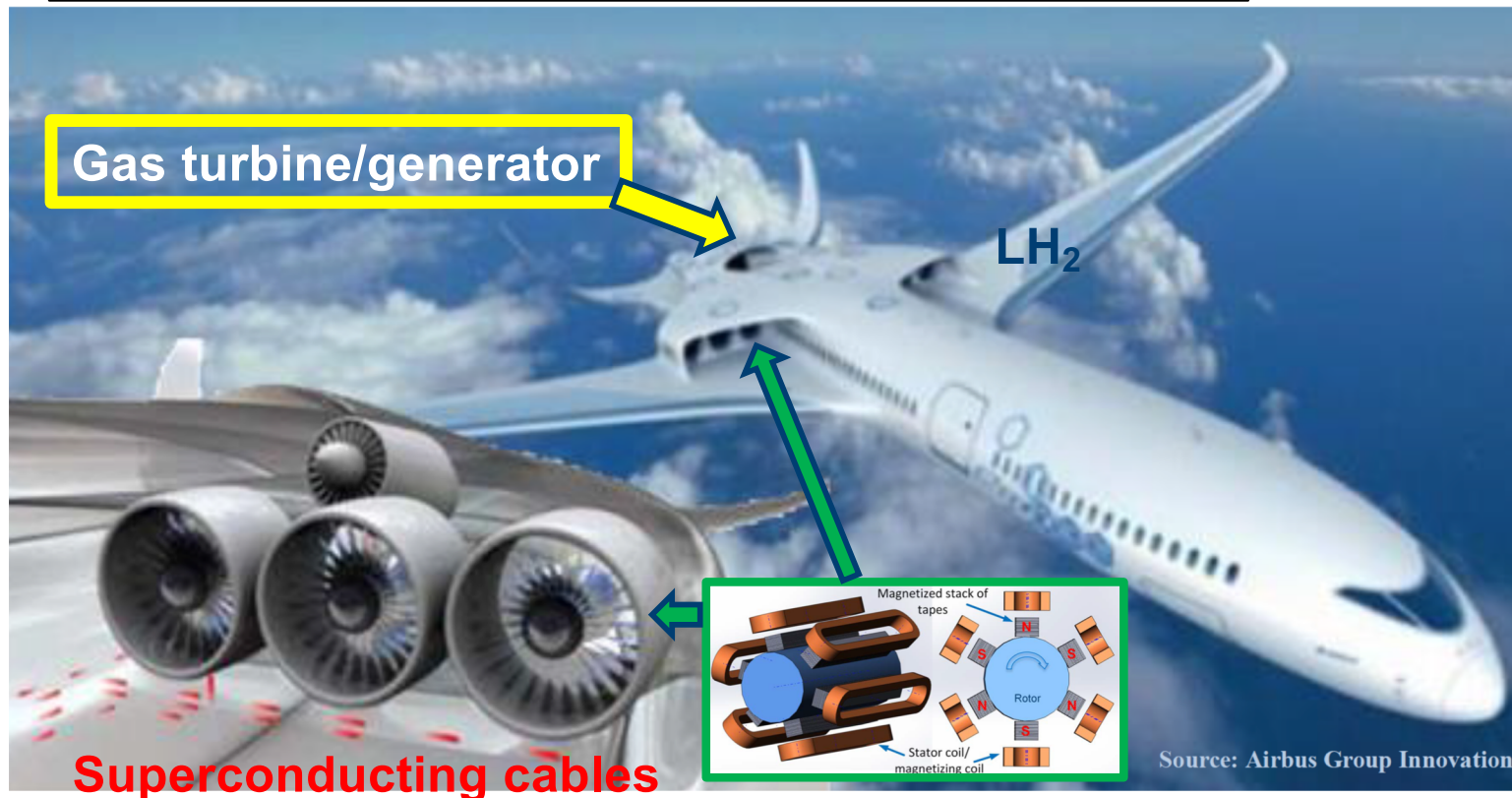


# Distributed Electrical Aerospace Propulsion project



Funded by the  
European Commission  
Grant No 723119

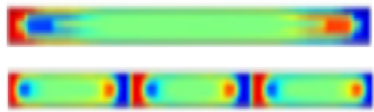
## Hydrogen as a coolant and as a “fuel”



Fully superconducting motors

IEEE TRANSACTIONS ON APPLIED SUPERCONDUCTIVITY,  
VOL. 25, NO. 3, JUNE 2015

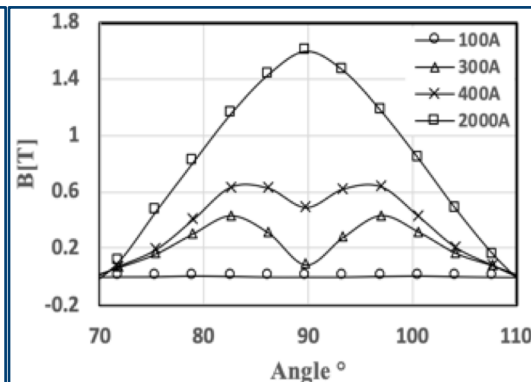
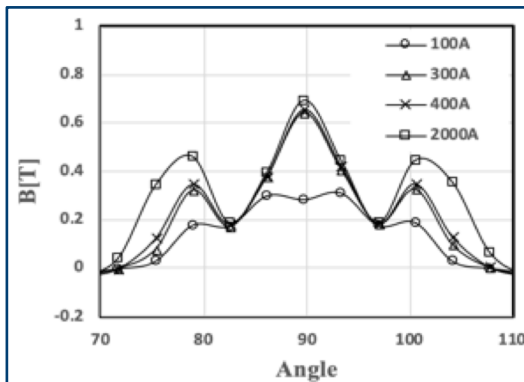
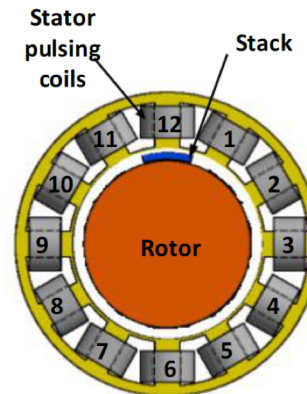
# Effect of the width of the tape on the pulse field trapped magnetic flux value



Current density distribution of straight wide and sectioned superconductor in the air with a normal field varying with a triangular shape in time: a) undersaturated case for the wide stack, b) case of undersaturated sectioned stack.

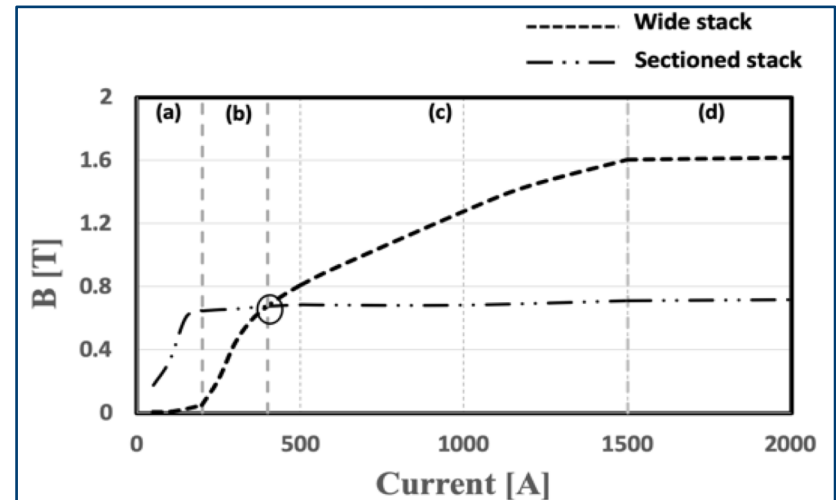
**sectioned stack**

**wide stack**



The flux density and current density distribution at different amplitudes of pulses for wide and sectioned stack.

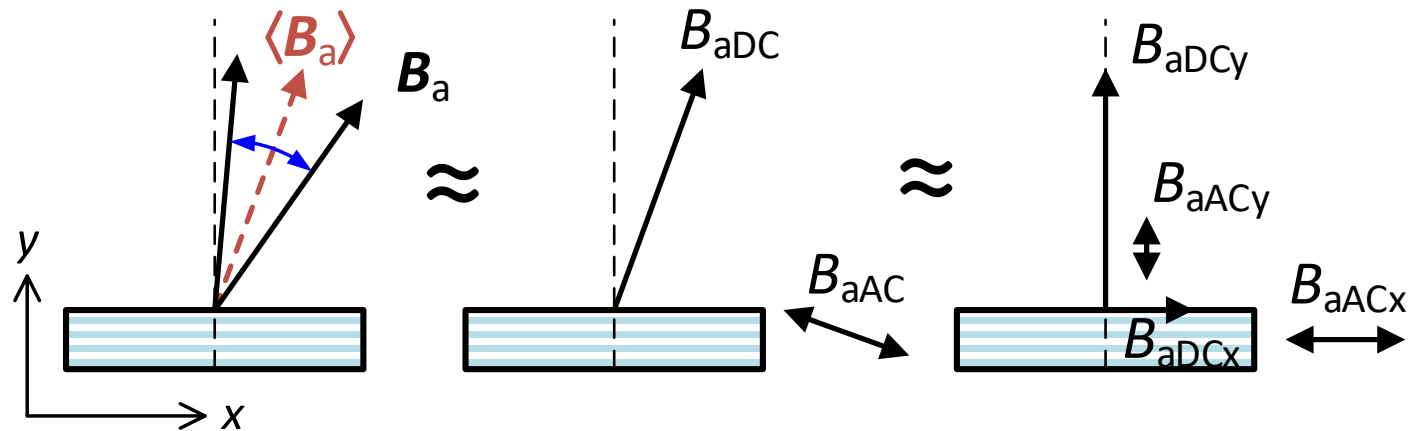
- a) flux density distribution for **sectioned stack**,
- b) flux density distribution for **wide stack**.



The peak of the trapped flux at the air gap by the sectioned and wide stack magnetized in an electrical motor. There are 4 distinctive zones on the graph representing characteristic different points between the stacks.

It is evident that using wider tapes in a real motor environment is not always is beneficial at lower flux trapped components (in our case 0.65 T)

# Problem of Crossed-field demagnetization “AC case”



- Stacks in applications experience AC magnetic field that causes demagnetisation, but experimental studies for characterising the effect at complex operating conditions (such as magnetic-superconducting architectures) are still lacking.
- Figure above shows the external AC field experienced by a stack in applications. The field can be decomposed into perpendicular and parallel field components. It is the  $B_{aACx}$  component that causes largest demagnetisation rate.

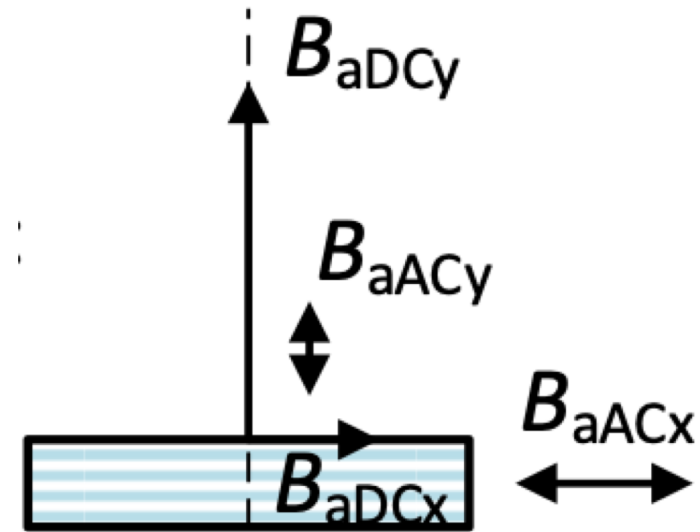


# HTS Stack in rotor application “paramagnetic current”

The effect of the  $B_{aACy}$  component on trapped field magnets is understood and current distribution in the interior of the sample does not fundamentally change

If direction of the external applied field is perpendicular to the tape layers  $B_{aACx}$ , even a small applied field exceeds the penetration field of a single tape in that orientation, that reduces the magnetisation along the y axis.

However, stacks in applications experience an AC magnetic field that causes demagnetization, there is data suggesting that the **demagnetization rate is actually slower in stacks of tape than in bulk** HTS superconductors.

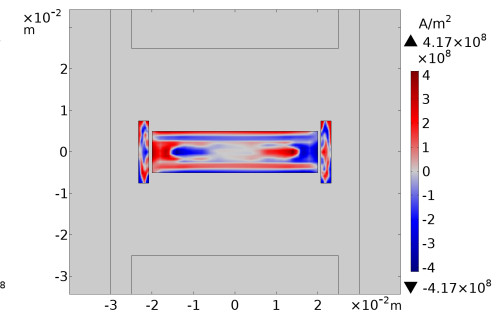
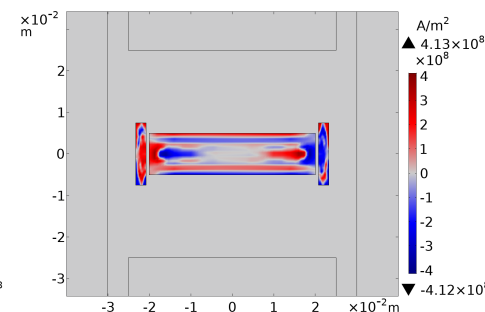
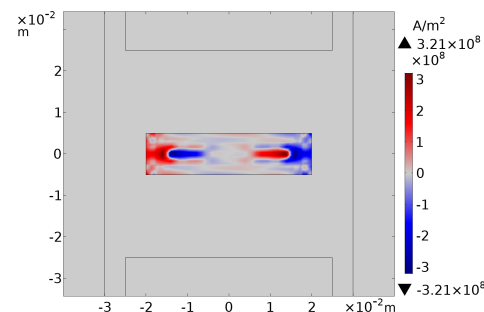
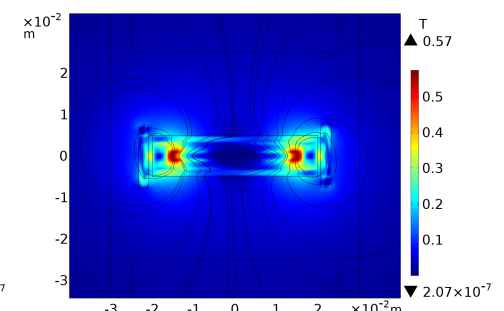
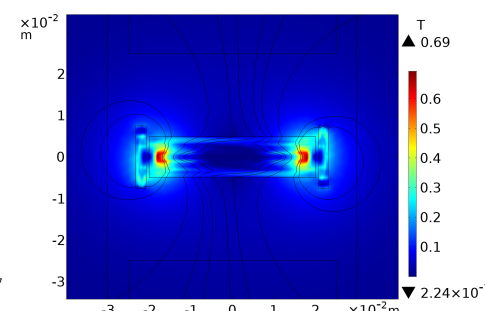
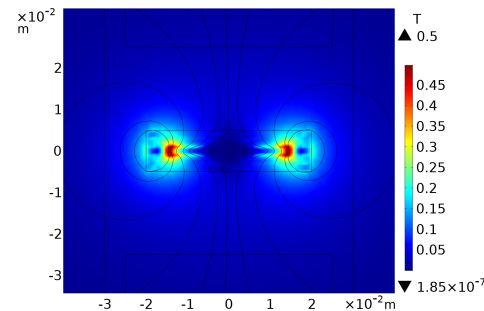
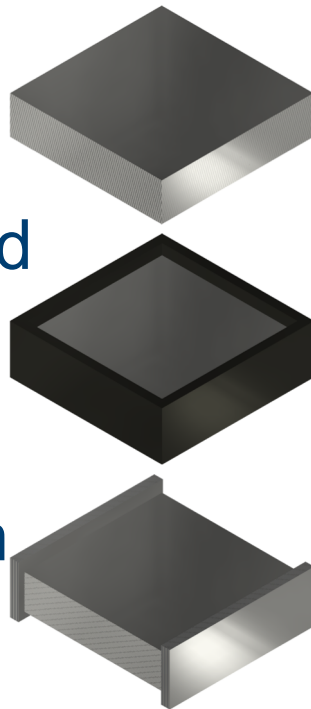


# Protection against demagnetisation: *stack shielding*

unshielded

closed

open



Unshielded

Closed shield

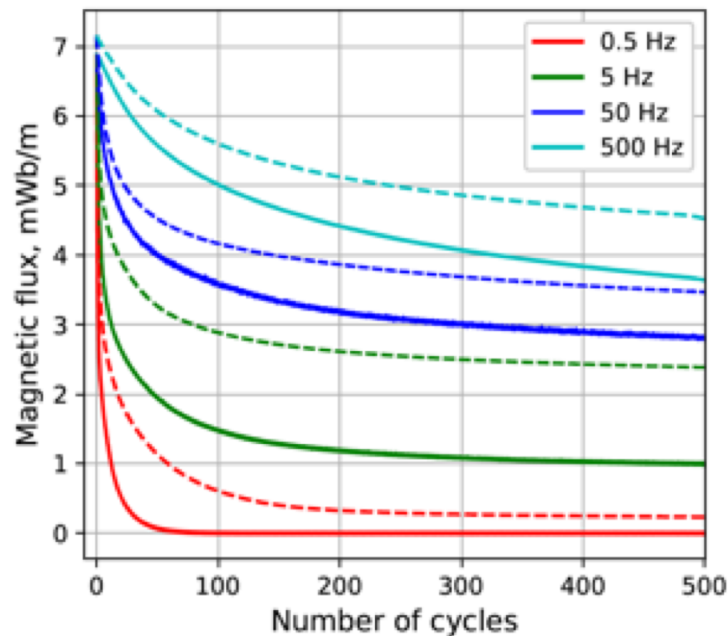
Open shield

Shielding variants

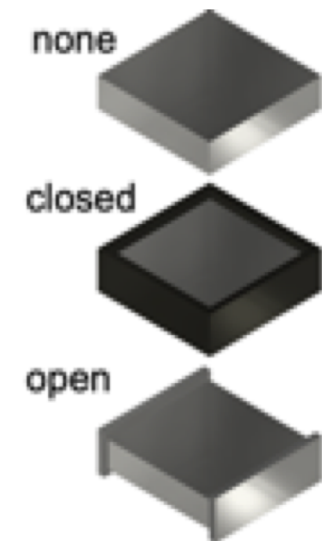
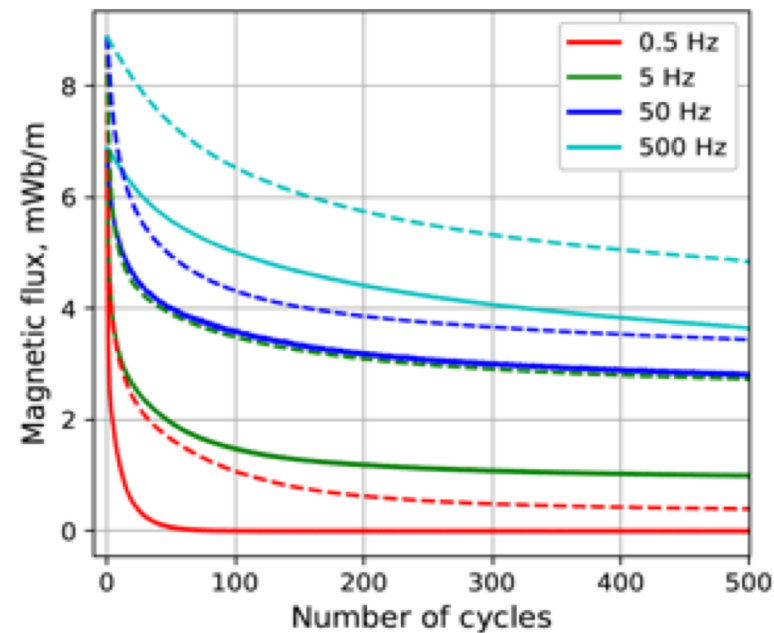
Distributions of magnetic induction and electric current density

# Stack screening in rotor applications dynamic demagnetization

open shield

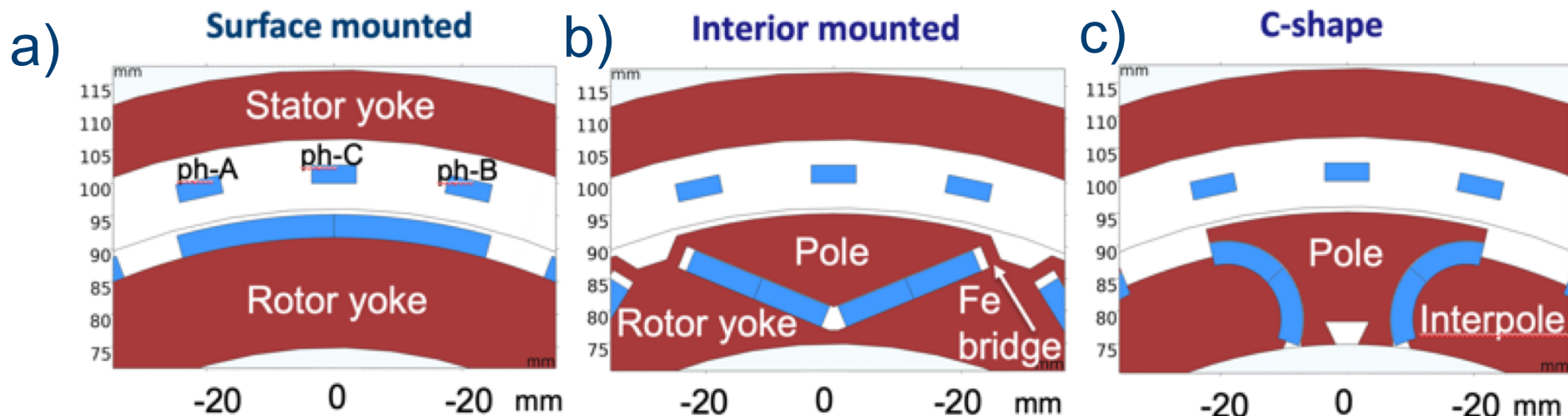


closed shield



Magnetic flux vs number of cycles for the stack shielded with: a) an open shield, b) a closed shield (**solid lines - unshielded, dashed lines - shielded**); c) variants of shielding; unshielded stack, closed shield, open shield

# HTS Stack architecture in **rotor** application C-shape



- Easy assembly
- Easy magnetization
- Easy demagnetization
- High losses
- Difficult construction

- Easy assembly
- Difficult magnetization
- Little demagnetization
- Low losses

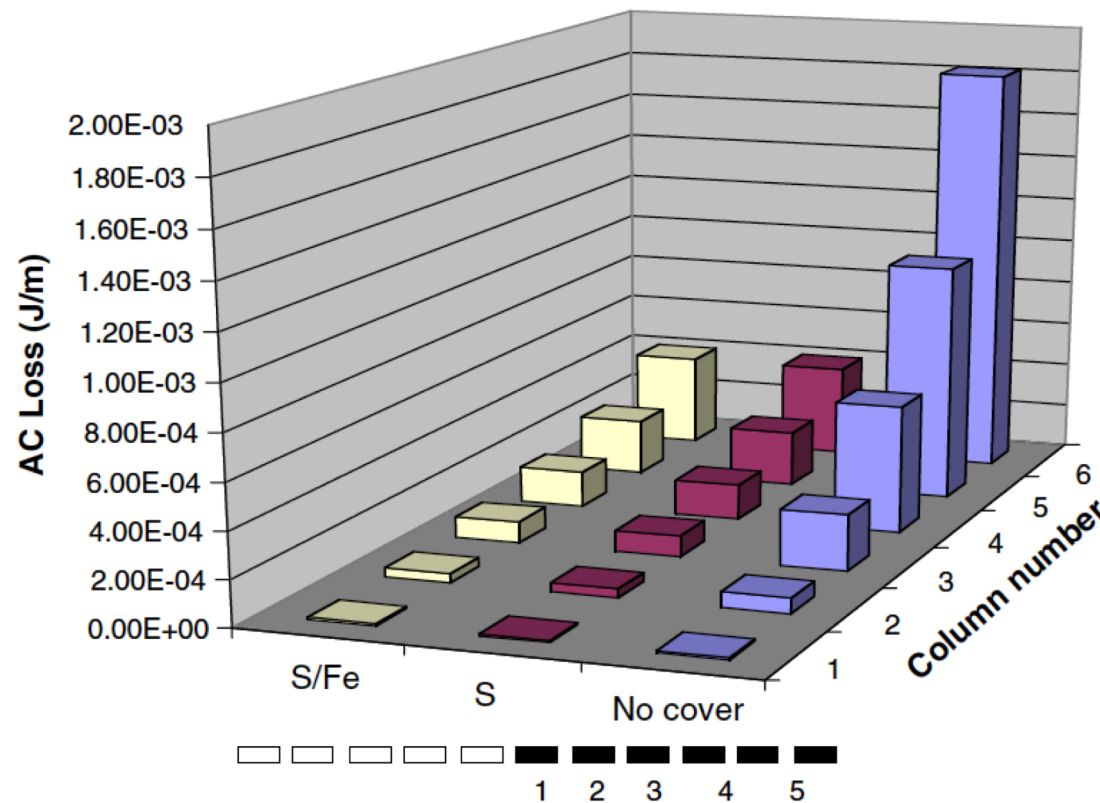
- Difficult assembly
- Easier magnetization
- Lower demagnetization
- Low losses
- Novel geometry

Classical geometries considered for the ASuMED fully superconducting 1 MW, 3-phase motor demonstrator cooled by  $\text{LH}_2$ : a) surface mounted stacks; b) interior mounted stacks and c) C-shape (geometry finally accepted).

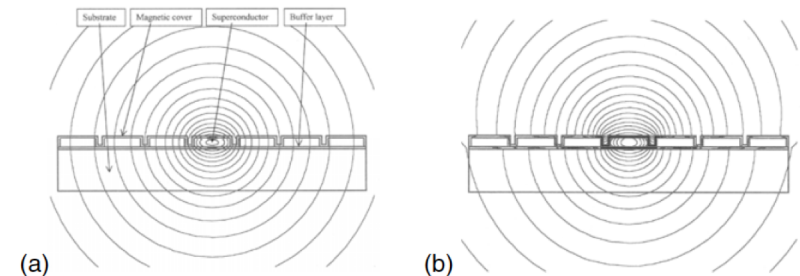


# Magnetic superconducting architecture on losses

## stator case



Proximity of ferromagnetic materials may benefit the performance of superconducting conductors in respect of the critical current and AC losses



YBCO cc

AC loss distribution in individual filaments when they are covered with Fe layers and without the covering. (S/Fe—total losses, S—component of the losses in the superconductor only.)

# Conclusions

- HTS stacks for DC applications have a great potential if the pulse magnetisation procedures were optimised for desired temperature range.
- HTS stacks for AC applications are promising but in complex magnetic-superconducting architectures such as it is in rotating machines, much more novel tailored R&D is required to prevent detrimental demagnetization effect.

**WIDER TAPES ARE NEEDED – they will be most likely based on RABiT substrates 10 - cm width**