Experimental Verification and Electromagnetic Characteristics Analysis of Permanent magnet Linear Oscillating Actuator by using Semi 3D Analysis Technique with Corrected Stacking Factor



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FIG. 3. 1st and 3rd harmonics magnetic behavior according to

region: (a)-(b) Outer core regions, (c)-(d) Inner core regions



Abstract

This paper proposes a semi 3D analysis method, analysis a permanent magnetic flux density in the iron core was estimated by considering the volume of the divided core. Finally, the core loss analysis of the laminated core was performed using the modified Steinmetz equation and then compared with the FEM analysis results. Additionally based on the predicted magnetic flux density, electromagnetic characteristics were compared through the experiment.

Structure of Linear Oscillating Actuator (LOA)

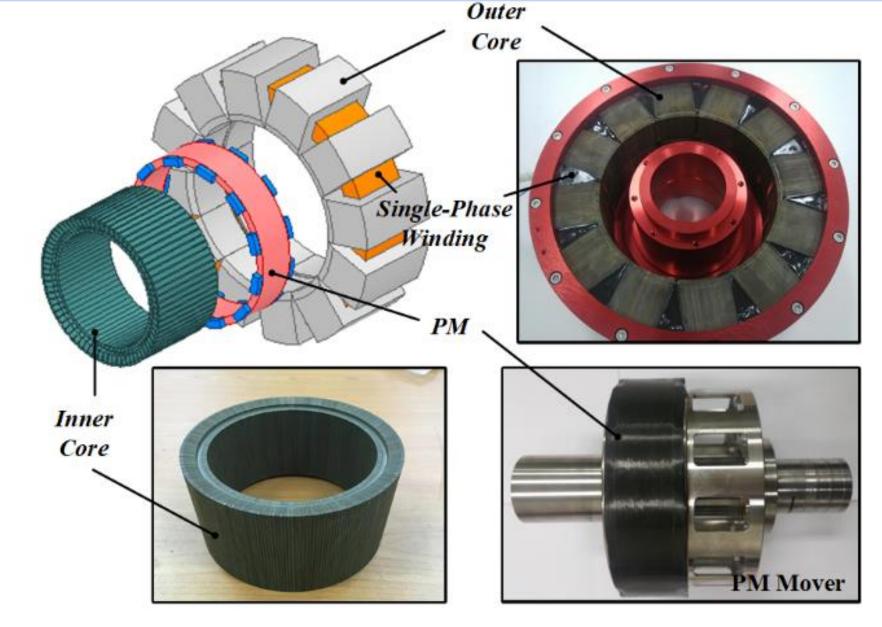


FIG. 1. Construction of LOA with radially lamination.

TABLE I REQUIRED DESIGN PARAMETER OF LOG FOR FPSE

Parameter	Value	Parameter	Value
Stroke	± 11 [mm]	PM weight	1 [kg]
Frequency	30 [Hz]	Maximum speed	3.46 [m/s]
Total piston weight	2.5 [kg]	Output Power	1500 [W]

- * In this model. Lamination of the radial direction perpendicular to the current flow direction of the coil is applied.
- * Radially laminated cores consist of 12 lamination blocks be-cause of manufacturing limitations for the stator of this model.
- **3D FEM analysis is essential for a more accurate analysis of radially stacked** LOAs.

Structure of Linear

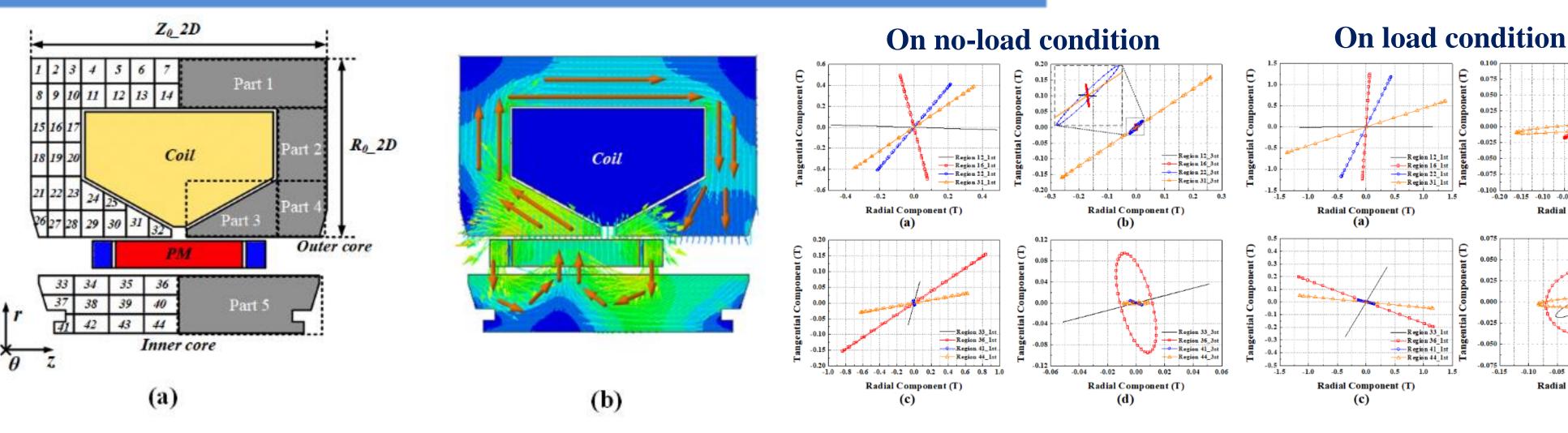
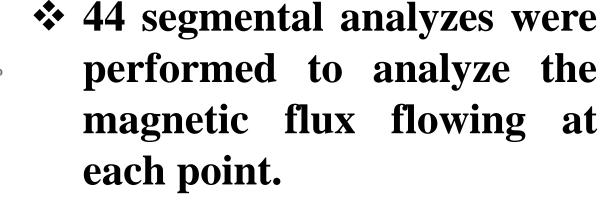


FIG. 2. (a) Analysis model for behavior and harmonics analysis of magnetic field and (b) Flux vector of LOA

❖ Fig 2 shows the 2D analysis model for semi 3d analysis. **44** segmental analyzes were



❖ Fig 3 shows the analysis of magnetic field behavior according to odd harmonics at each point.

Corrected Stacking Factor

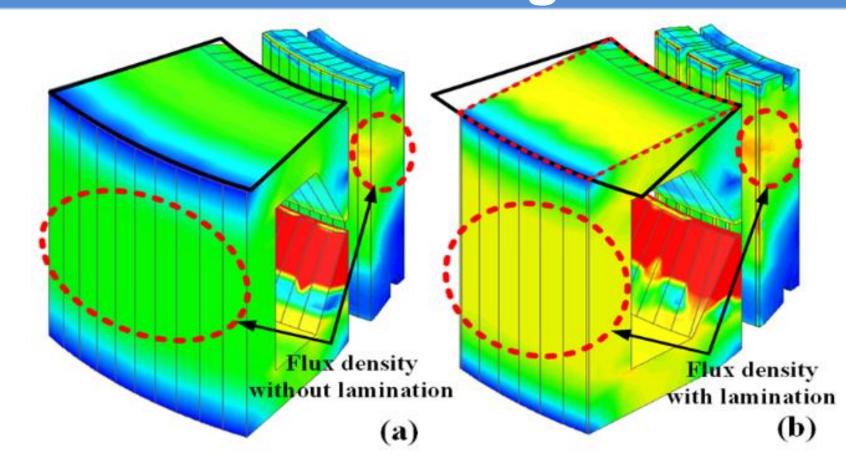


FIG. 4. Magnetic flux density at the rated condition (a) without lamination and (b) with lamination.

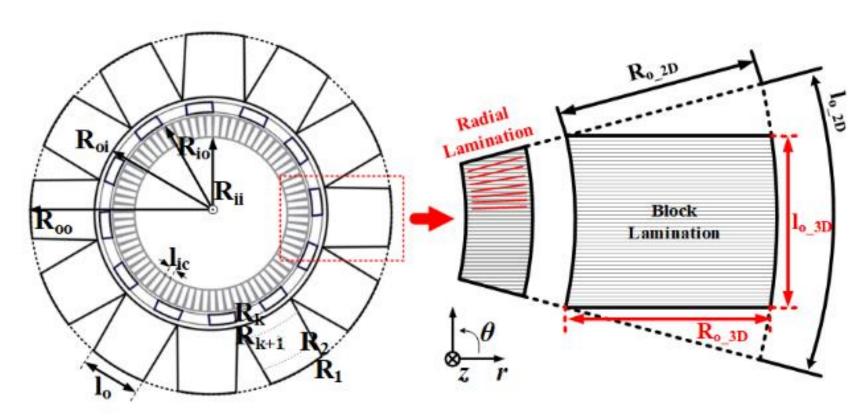
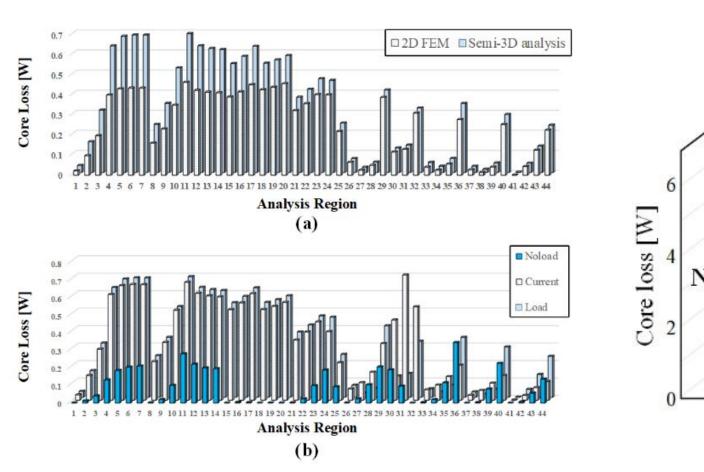


FIG. 5. Analysis model for finding of the corrected stacking factor

- **2-D** cylindrical coordinate system does not take into account the radially laminated core
- * Based on Fig. 5 , the corrected stacking factor of equation is derived.
- ***** The calculated stacking factor is applied to derive the final magnetic considering density laminated core volume.

$$\alpha_s = \frac{\pi (R_{k+1}^2 - R_k^2)}{n_c l_o (R_{k+1} - R_k)} \quad B_{3d} = \alpha_s \times B_{2d}$$

Core Loss Analysis





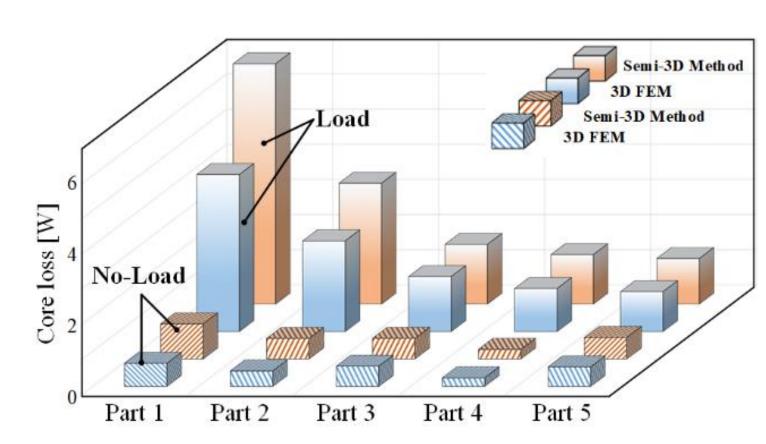


FIG. 7. Core loss results of the 3D FEM or the proposed Semi 3D analysis

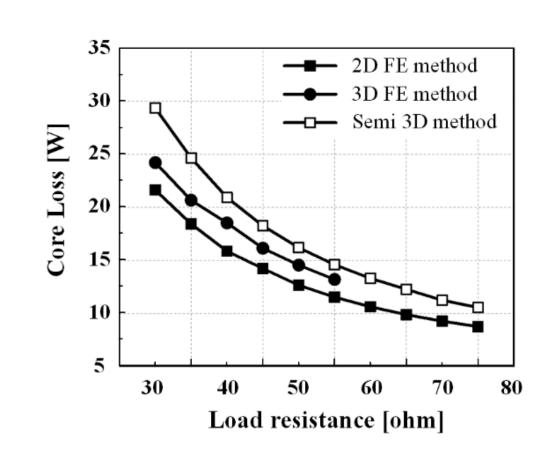
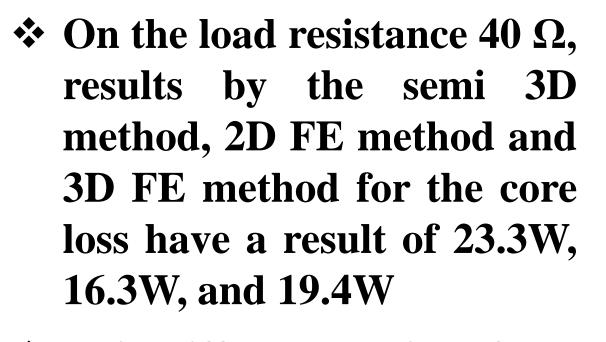


FIG. 8. Analysis results according to load resistance variation



- ***** This difference arises from consideration magnetic field behavior.
- $P_{core_semi3d} = \sum_{l} \alpha_{l} \left(k_{hl} f_{l} B_{3d}^{n_{st}} + k_{el} f_{l}^{2} B_{3d}^{2} + k_{al} f_{l}^{1.5} B_{3d}^{1.5} \right)$

❖ The predicted 3D magnetic flux density (B_3d) and applied to the modified Steinmetz equation to obtain the core loss



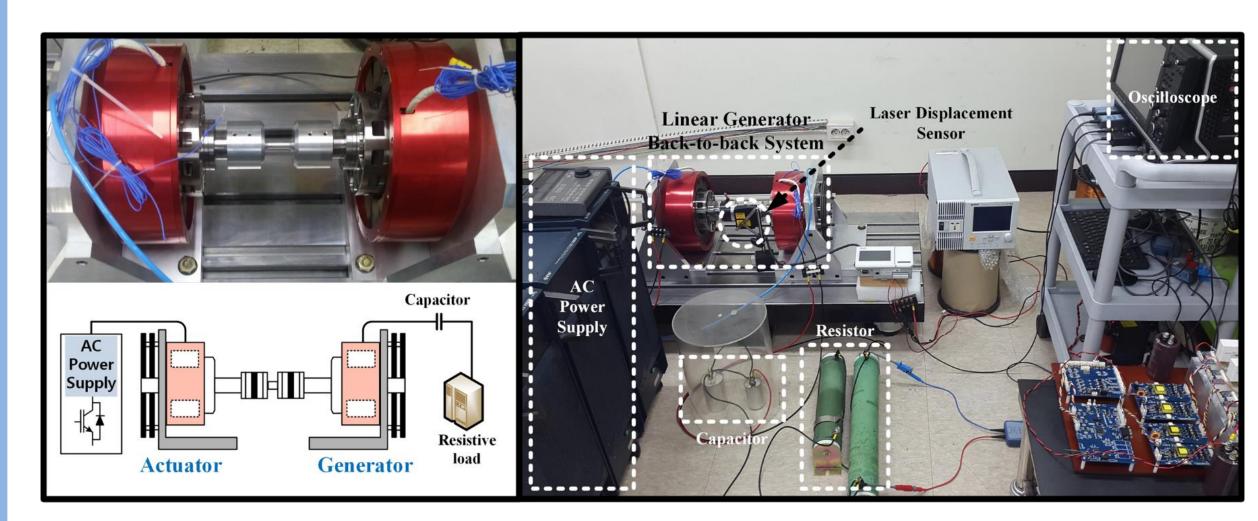


FIG. 9. Manufactured model of LOG and back-to-back experimental set.

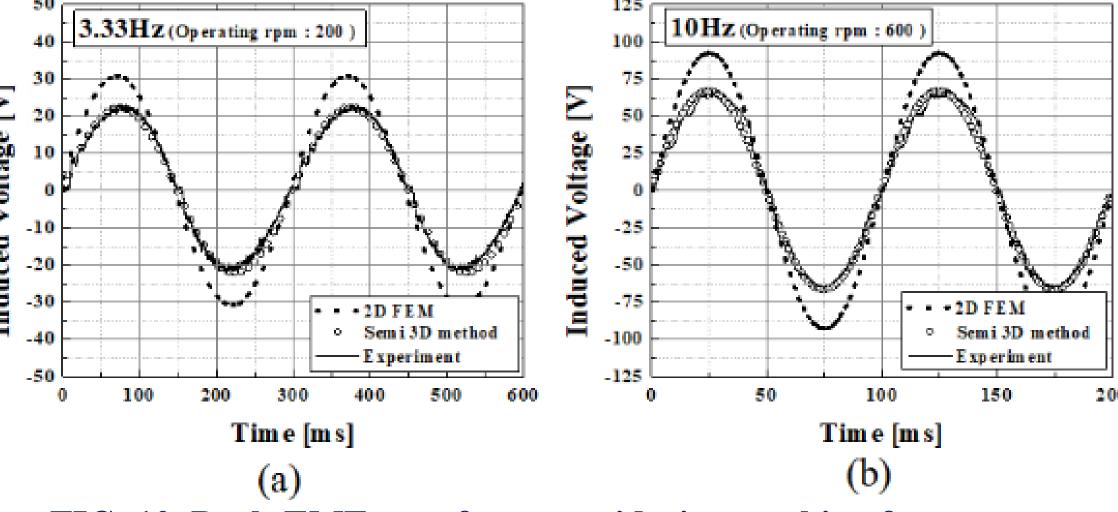


FIG. 10. Back-EMF waveform considering stacking factor at (a) 3.33Hz (b) 10Hz

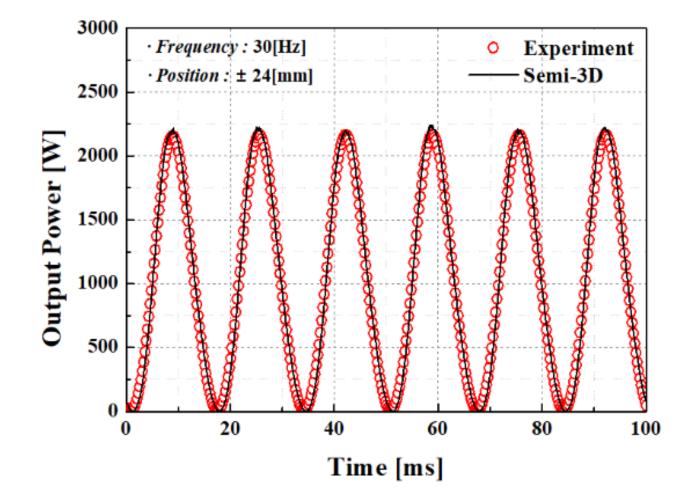


FIG. 11. Comparison of FEA result with experimental result: output power.

- * The analytical results were verified by comparison with 2D and 3D FEM results and experimental results.
- ❖ In terms of electromagnetic characteristics, the back-EMF is reduced due to the saturation of the iron core. Therefore, the inverse of the stacking factor was applied to the 2D analysis results of no-load induced voltage.
- * The back-to-back test system was composed by linear actuator, linear generator, AC power supply, capacitor and load resistance.
- * The two linear machine was connected linear coupling, and the air bearing was used for reduced friction loss
- **❖** The experimental results are agreement with the semi 3D analysis result.