

18 T hybrid dipole for an LHC energy doubler

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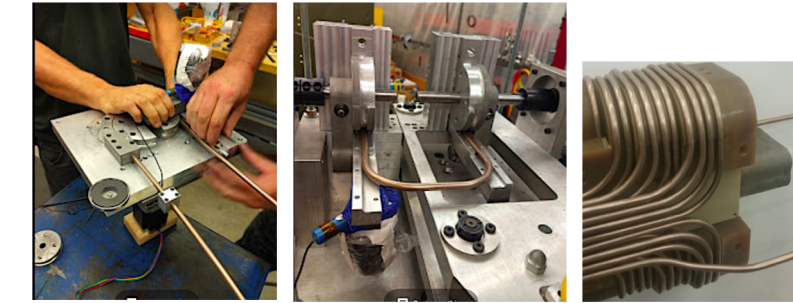
Abstract: We report the design for a hybrid block-coil dual dipole using advanced cable-in-conduit windings. The dipole is designed for use in the arcs of an energy-doubling lattice in the LHC tunnel. The block-coil design facilitates configuration of hybrid sub-windings of Bi-2212, Nb₃Sn, and NbTi, each operating to the same fraction of critical current. The cryogenics utilizes supercritical helium, operating in the window 4.2-4.6 K. A novel support structure provides robust support and stress management. The three sub-windings can be separately wound and heat-treated and then assembled and preloaded to complete the dipole.

I. Cable-in-Conduit Technology = SuperCIC



1. Perforated center tube (SCHe flow).
2. Cable wires onto center tube, SS tape over-wrap. Repeat step 2 for layer 2.
3. Pull cable through sheath tube as loose fit.
4. Draw sheath tube onto cable to compress wires against center tube.
5. Finished 140 m segment of 13 kA CIC for JLEIC dipole.

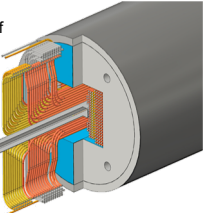
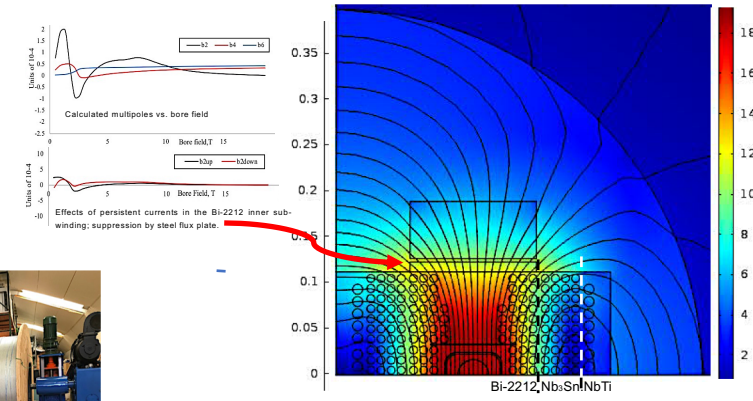
II. SuperCIC Coil Technology



180° U-bend 90° flare of U-bend Completed 24-turn CIC winding

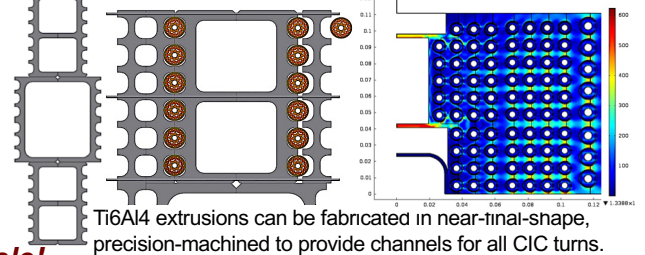
ATC manufactures 140 m lengths of SuperCIC – product for sale!

III. 18 T hybrid-coil dual dipole



Coil current	28	kA
Operating temp range	4.2-4.6	K
2-layer CIC sub-windings:		
NbTi:	# layers, turns/bore	1 14
	# wires, wire dia.	16+22 1.2 mm
	B _{max} in sub-winding	7.3 T
Nb ₃ Sn:	# layers, turns/bore	4 80
	# wires, wire dia.	17+23 0.88 mm
	B _{max} in sub-winding	12.4 T
Bi-2212	# layers, turns/bore	4 68
	# wires, wire dia.	17+23 0.88 mm
	B _{max} in sub-winding	19.4 T

IV. Stress management



Ti6Al4 extrusions can be fabricated in near-final-shape, precision-machined to provide channels for all CIC turns. Stress in wires is everywhere <120 MPa.

V. Developing 2-layer SuperCIC using Nb₃Sn, Bi-2212

NbTi: It is critically important to interpose a multi-layer spiral wrap over-wrap that provides a slip-surface between inner and outer layers, and also a spiral over-wrap on the outer layer that provides a slip-surface. For 2-layer cable, those issues required a multi-layer over-wrap between wire layers

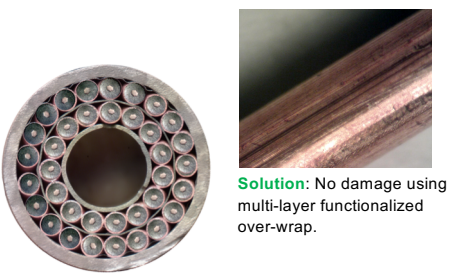
Nb₃Sn: It is critically important to interpose a multi-layer spiral wrap over-wrap that provides a slip-surface between inner and outer layers, and also a spiral over-wrap on the outer layer that provides a slip-surface. For Nb₃Sn it was necessary to adopt different materials for the slip-planes and sheath tube from what worked for NbTi SuperCIC.

Bi-2212: Bi-2212/Ag wire is soft and has limited strength. Multi-layer over-wrap foils are used to provide two distinct functions: Haynes 214 diffusion barrier foil prevents diffusion between wires and the center tube and sheath tube; slip-surface foil enables wires to re-arrange small-radius ends are formed. The Haynes 233 sheath on the Bi-2212 SuperCIC provides pressure containment during 880 C over-pressure heat treatment – **no need for high-pressure furnace.**

The Bi-2212 and Nb₃Sn sub-windings are fabricated and heat-treated as separate sub-assemblies. The SuperCIC cables of NbTi, Nb₃Sn, Bi-2212 are powered in series with the same critical current in each sub-winding - **minimum quantity of CIC turns, expensive superconductor.**

Total superconductor cross-section, wire cost for one 15 m dual dipole
(present-day commercial quotes for small quantity)

Superconductor	Wire cross-section	Wire cost/m	Wire cost for one dual dipole
NbTi	24 cm ²	\$3.60/m	\$119 K
Nb ₃ Sn	78 cm ²	\$6.56/m	\$1,345 K
Bi-2212	66 cm ²	\$64.77/m	\$11,275 K



2-layer Nb₃Sn CIC: cross-section half-way around a bend

VI. Super-critical He cryogenics

All windings are cooled by flow of SCHe through the 4.2 mm ID center tube in the SuperCIC. The Nb₃Sn sub-winding has the longest length:

Heat load/bore	1	W/m
SCHe flow	0.3	m/s
Temperature rise	0.3	K
Pressure drop	0.8	bar
PdV work	0.03	W