



Evaluation of Joint Resistance and Bending Performance of Various Ultrasonic Weld CC Joints

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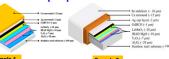
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Introduction

- ☐ In practical applications, the superconducting coils and magnets impose to use joints to connect the unit lengths of 2G CC tapes and to constitute the termination of winding units such as in the cases of pancakes and double pancakes coils.
- ☐ Relevant joining technique that recently emerged in superconducting tape joints is ultrasonic welding. The localized high frequency ultrasonic vibration and pressure generated frictional heat and achieve metallurgical bond at contacting interfaces without melting the base metal.
- ☐ In this study, to further enhance the capability of the UW method to Cu stabilized REBCO CC tape joints, lap- and bridge-joints intended to be embedded in the coils using intermediate CC tapes were considered. The Taguchi Method, as design of experiments in optimizing the welding process parameters, was adopted to minimize the number of experiments.
- ☐ Joint resistance. R and critical current. I. measurements of UW CC joints were measured at 77 K. Bending performance of UW CC bridge ioints as a practical evaluation for magnet and coil applications were carried out and discussed.

Experimental procedure

Sample specifications



GdBCO film (t) Substrate, (t)

Ag/GdBCO/LaMnO./ Homo-epi MgO/IBAD MgO/ Y₂O₃/AlO₃/Stainless steel/Cu stabilized ~ 1 um Stainless steel. ~100 um Cu surround, ~15 um Sn-Cu stabilized Dimension, t x w (mm 0.140 mm x 4.05 m 0.130 mm x 4.05 mm Critical current (I,) ~ 220 A

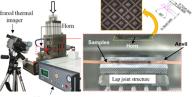
Joint configuration

Intermediate CC tape

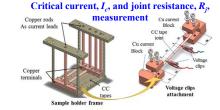
RCE-DR

Bridge-joint structure

Ultrasonic welding set-up and procedure



□Ultrasonic welder (KORMAX, Korea: KM-2035): frequency of 20 kHz



- □ Lap-ioint: overlapping CC tapes on top of one another. GdBCO film sides facing each other, face-to-face structure
- ☐ Bridge-joint: indirect joint using an intermediate material
- ☐ 4-mm and 12-mm bridges: Suitable if the joint is required to extend or replace the CC tapes in the coil winding, like in the case of double pancake coils

Double bending test

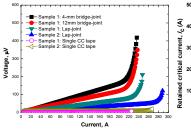


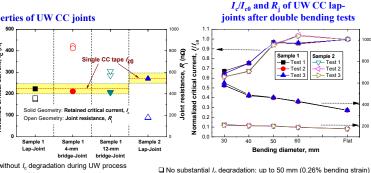
 $\varepsilon_b = \frac{\iota}{2r+t} \times 100\%$ Where: \mathcal{E}_{+} = bending strain (+/-) r = bending radius t = thickness of CC tapes at the joint region

- ☐The welder can generate power up to 3.5 kW varying the vibration amplitude at fixed frequency of 20 kHz
- ☐ Multiple I_c measurement fixture was used:
- √ Voltage taps were clipped instead of soldering for an easier attachment
- √ I₂ was measured using four-probe method at 77 K (LN₂) with a voltage criterion of 1 uV/cm
- ✓ The R_i was derived from the initial part slope of the V-I curve

Results and Discussion

Electromechanical properties of UW CC joints





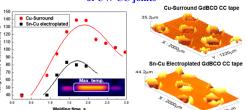
Bending diameter, mm

 \square Abrupt I_c degradation (~70% of I_{c0}) at 40 mm bending diameter

-Test 2

- □ All UW CC joints retained I_c (from single CC tape) without I_c degradation during UW process $\square R$ for Sample 1 UW lap-joint is 340 n Ω and is about twice of Sample 2. R = 170 n Ω
- \square Ri for Sample 1 bridge joint is 820 n Ω and 600 n Ω for 4 mm and 12 mm bridges, respectively

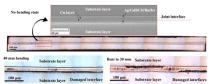
Temperature history distribution and surfaces images of UW CC ioints



- □ Results optimized by Taguchi method: good indicators of weld quality: ~130 J and 288 W for Sample 1 and ~80 J and ~170 W for Sample 2
- ☐ Max temp of ~140°C for Sample 1 and ~85°C for Sample 2: recorded temp are not enough to after the weld quality nor damage the CC tapes
- □ Horn tip penetration: ~7.5µm deep to Cu-stabilizer of Sample 1, while ~10um to Sn-stabilizer of Sample 2 (Vickers hardness value difference)

(0.62% bending strain) ☐ Sample 2: showed bending tolerance at the smaller diameters. increasing in a less sensitive way down to a 30-mm bending diameter

Cross-sectional views of Sample 1 at UW CC lap-joint interfaces



- Ic degradation also affects the increase of Ri bending diameter decreases
- 50-60 mm bending dia w/out I2 degradation is consider safe as required in various CC tapes utility devices
- ☐ Incomplete bonding and damages along the interfaces, even in the unbend UW CC joints
- the joint interface ☐ After bending, damage interface was only visible along the Ag/GdBCO/Buffer layer at 40 mm bending dia

☐ High R_i for bridge-joints

were perhaps due to

complex current transfer

nath and R from voids at

□ 30 mm, multiple locations of damages were observed at the interface

Summary

- ☐ The retained /s of CC joints did not show any degradation after the UW process.
- 🗖 A ioint resistance value ranging from ~100 to ~200 nΩ could be obtained for a lap-joint structure using the UW method. The double bending test of UW CC joints demonstrated a large tolerance to smaller bending diameter up to 50 mm without any L degradation, which particularly within the minimum 100 mm required bending diameter in various CC device applications.
- ☐ The results were considered suitable for practical 2G CC device applications. To further improve the joint quality, hybrid UW variants and other joint configurations in CC coil winding application involving intermediate material, such as butt, inclined, etc., are still needed.

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