



The MAPP Outrigger Technical Proposal

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The MoEDAL-MAPP Collaboration

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Abstract

This is the Technical Proposal for the Outrigger Detector for the MAPP-1 (moEDAL Apparatus for Penetrating Particles) detector currently being installed in UA83 for data taking during LHC's Run-3. The Outrigger is an auxiliary detector designed to greatly improve the acceptance of the Phase-1 MAPP detector (MAPP-1) for mini-charged particles with larger fractional charges. The Outrigger Detector is comprised of four 6m scintillator planks, comprised of 60 cm x 30 cm x 5 cm scintillator slabs, deployed in three horizontal shafts joining the UA83 tunnel to the beam tunnel in the vicinity of the MAPP detector.

1 Introduction

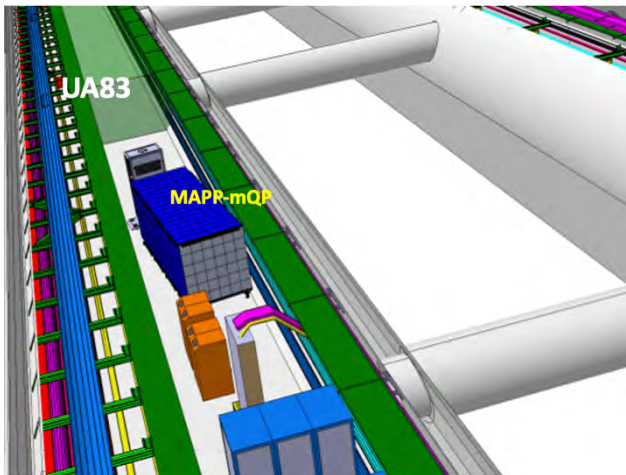
A major part of the MoEDAL Collaboration's physics program for LHC's Run-3 and beyond involves the installation of a new detector called MAPP-1 (MoEDAL Apparatus for Penetrating Particles) [1]. MAPP's purpose is to expand the physics reach of MoEDAL, that is focussed on the detection of Highly Ionizing Particle (HIP) avatars of new physics, to include the search for mini-charged particles¹ (mCPs) with charges as low as one thousandth the electron charge (e) and weakly interacting very long-lived neutral particle (LLPs) messengers of new physics. Thus the MoEDAL and MAPP detectors operating together will be able to detect: HIPs, mCPs and LLPs.

The MAPP-1 outrigger detector is an array of scintillator blocks arranged in planks placed in three ducts joining the UA83 tunnel and the beamline tunnel, in the vicinity of the MAPP detector, as indicated in Figure 1. Its purpose is to significantly increase MAPP's acceptance for feebly electromagnetically interacting particles with an effective charge greater than $\sim 0.01e$, where e is a single electric charge. This Technical Proposal describes the details of the design, construction and installation of the "Outrigger Detector."

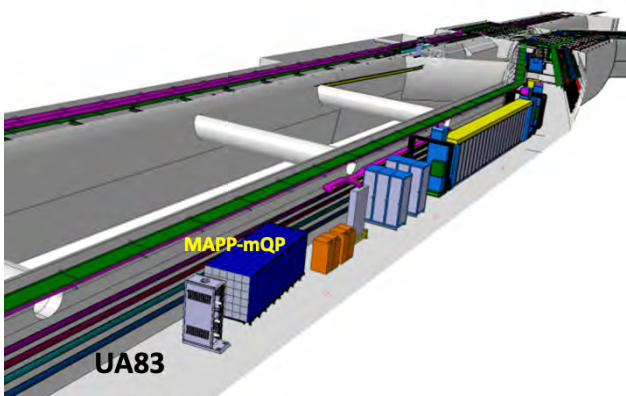
2 The Outrigger Detectors for the MAPP Phase-1 Detector

The Phase-1 MAPP detector (MAPP-1) for LHC's Run-3 is currently being installed in UA83 tunnel some 100 m from the existing MoEDAL & LHCb detectors, in order to take data during LHC's Run-3. The MAPP-1 detector and its associated electronics rack has now been included in the overall LHC machine description as shown in Figure 1. A drawing of the MAPP-1 detector is shown in Figure 2. MAPP-1 is protected from Standard Model particles from interactions at IP8 by roughly 35m to 40m of rock and from cosmic rays by an overburden of approximately 110m of limestone.

¹We use the term mini-charged rather than milli-charged to denote the lightly ionizing particle as it does not imply that the charge is $10^{-3}e$



(a)



(b)

Fig. 1: The deployment of the MAPP-mQP detector in UA83.

82 The MAPP Phase-1 detector is designed to the search for mCPs. It is made
 83 up of four collinear sections, with sensitive cross-sectional area of roughly 1.0
 84 m^2 , each comprised of 100 ($10 \text{ cm} \times 10 \text{ cm}$) plastic scintillator bars each
 85 75cm long. Each bar is readout by one low-noise 3-inch PMT. The detector is
 86 arranged to point toward the IP. Thus, each through-going particle from the
 87 IP will encounter 3.0 m of scintillator and be registered by a coincidence of
 88 4 PMTs. The 4-fold PMT coincidence essentially eliminates the background
 89 from "dark counts" in the PMTs. Additionally, the division of the detector
 90 into 4 bars virtually excludes all fake 4-fold coincidences due to radiogenic

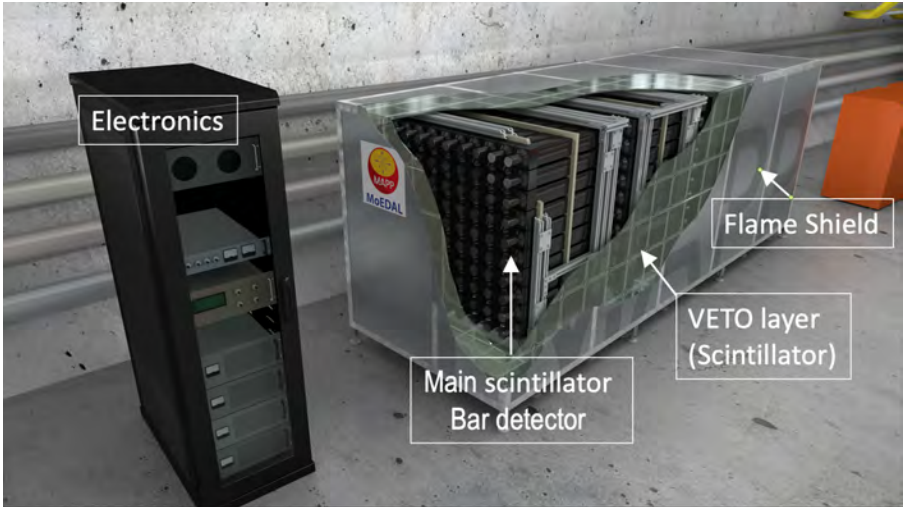


Fig. 2: A drawing of the MAPP detector showing the main elements of the MAPP detector.

91 backgrounds in the scintillator and PMTs. The MAPP-mCP “bar” detector
 92 is hermetically enclosed in a veto layer consisting of a 1 cm thick scintillator
 93 read out by embedded scintillating fibre loops with a 25 cm x 25 cm pitch.

94 The MAPP-1 Outrigger Detectors are placed adjacent to the MAPP-1
 95 detector in three ducts joining the beamline tunnel to the UA83 tunnel, as
 96 shown in Figure 3. As shown in Figure 4 the outrigger detectors cover the
 97 region between 1.7° and 5.3° at a distance of 108.5m to 135.3m from IP8.

98 2.1 Outrigger Detector Technology

99 The basic scintillator unit of the Outrigger Detector is described in Figure 5.
 100 It is comprised a block of acrylic scintillator (Bicron BC-412) of size 60 cm
 101 x 30 cm x 5 cm readout through a light guide by a single 3.5-inch low noise
 102 PMT (HZC Photonics XP82B2FNB) ² This unit is assembled on a frame with
 103 another unit for insertion on a rail into the shafts that house the Outrigger
 104 Detectors. This subdivision is chosen to facilitate manual handling. The units
 105 are held at an angle of 45° in order that the path length of particles from the
 106 IP in the scintillator is increased from 5cm to approximately 7 cm.

107 These scintillator subunits are installed in ducts 3, 4 and 5 joining the
 108 UA83 tunnel to the beam tunnel. The numbering of shafts starts from the
 109 end of UA83 nearest to IP8. Two scintillator layers are inserted in shaft 3
 110 and one scintillator layer is inserted in ducts 4 and 5, as shown in Figure 6
 111 and Figure 7. For example, a requirement for a gold-plated milli-charged par-
 112 ticle candidate would be the coincidence of all 4 layers where the scintillator

²The HZC Photonics PMT is functionally the same as the HZC XP82B20D [2]

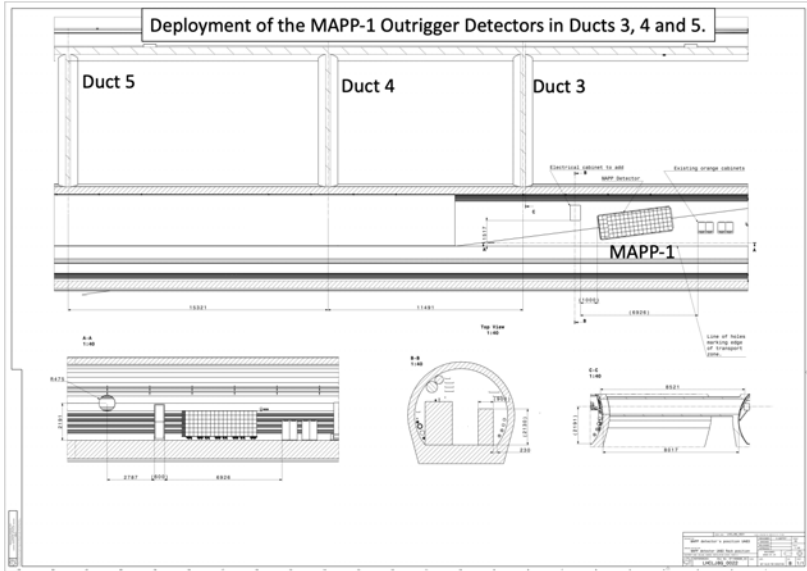


Fig. 3: The deployment of the Outrigger Detectors adjacent to the MAPP-1 detector.

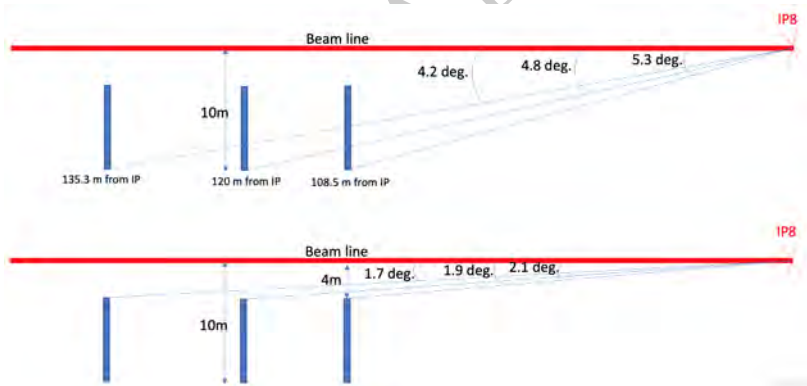


Fig. 4: The angular coverage of the Outrigger Detectors.

113 blocks responding would be those consistent with a track passing through the
 114 Outrigger Detectors.

115 Typically, a Minimum ionizing particle will lose around 2 MeV/cm in a
 116 good plastic scintillator and generate of the order of 10K to 20K photons
 117 per MeV lost. Consequently, this particle will deposit a comparatively large
 118 amount of light, of the order 1.4×10^5 photons in each scintillator block through
 119 which the muon passes. We have estimated that the light collection efficiency,
 120 including the loss due to photo-cathode efficiency, is 10%.

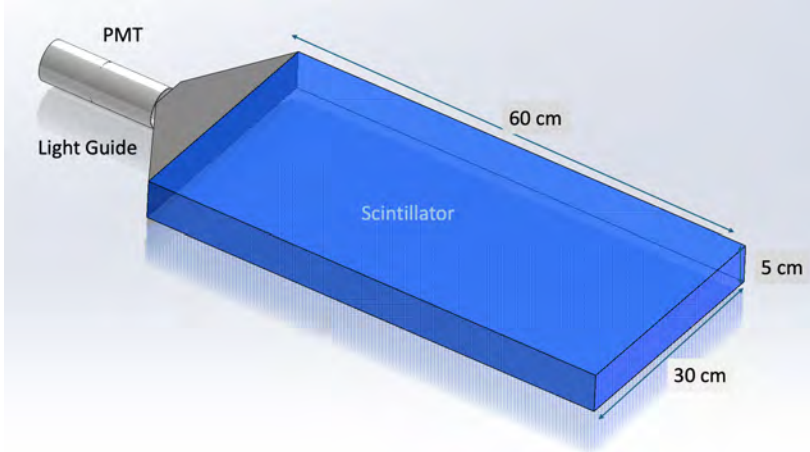


Fig. 5: The basic 5 cm thick plastic scintillator (Bicron 412) unit of the Outrigger Detector readout by a single 3.5-inch HZC Photonics (XP82B2FNB) PMT.

121 Roughly, a relativistic charged particle ionizes according to the square of
 122 its charge a particle with around $10^{-2}e$ would give approximately 14 photons
 123 in each bar. Assuming a quantum efficiency of 20% for the detecting PMT
 124 and a 50% efficiency for the photon reaching the PMT we should get of the
 125 order of one (PE). Thus, using this very approximate calculation the blocks
 126 are limited to the measurement of mCPs with a charge of $10^{-2}e$ and above.

127 However, number of other factors need to be taken in account including
 128 a detailed knowledge of the photon detection efficiency of each bar as well
 129 as factors that effect the particle by particle emission of scintillation light
 130 that depends on such factors as the charge, the velocity and Landau-Vavilov
 131 fluctuations [4] in energy loss. Indeed, at the limit of the sensitivity of the
 132 detector the most probable energy loss instead of the average energy loss is
 133 required.

134 A detailed simulation dealing with all of the above mentioned details is
 135 required especially when for small enough values of fractional charge the
 136 expected number of photons produced per MCP passing through the detec-
 137 tor is less than one, pushing the limitations of the outrigger detector. Such as
 138 simulation named SUMMA (Simulation of the UA83, MoEDAL, MAPP-mCP
 139 Arena) has been created and is under test.

140 2.2 HV, Readout, DAQ, Calibration and Trigger

141 The PMT used in the readout of the scintillator bars is a HZC Photonics
 142 P82B2FNB PMT Tube. The High Voltage divider will be resistive with an
 143 impedance of $4M\Omega$ a maximum voltage of 2000V and a current of $500\mu A$. The
 144 photocathode will be at ground potential with positive high voltage applied
 145 to the anode. The signal will be capacitively coupled to the cable.

146 The power supply will consist of a boost converter to convert from 48Vdc
147 to 250V using a coupled inductor to reduce the maximum voltage seen by the
148 controller. Several stages of a Cockcroft-Walton multiplier will then increase
149 this up to 2000V. The boost converter will be controlled by a small inexpensive
150 6 pin micro-controller which can accept serial data and synchronization pulses
151 from the DAQ. The Front end is connected to the DAQ via an MCX connector.
152 Power, signal and control will all be delivered via the same cable to reduce
153 cabling costs. In this way we avoid HV cables and connectors as well as the
154 related safety concerns

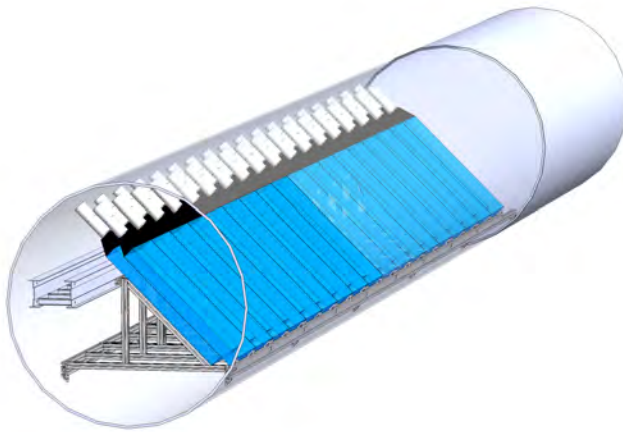


Fig. 6: The deployment of the outrigger detector in Shaft 3.

155 The technology for HV, readout, DAQ, calibration, and trigger used for the
156 main MAPP-1 detector will also be used for the Outrigger Detector. However,
157 the Outrigger will have its own software trigger and operate autonomously,
158 although the data will use the same DAQ computers and data-path out of the
159 cavern

160 A block diagram of the electronic readout and powering scheme for the
161 MAPP and Outrigger Detectors is shown in Figure 8. Each DAQ board will
162 consist of 32 identical channels. The DAQ will connect to the front end via an
163 MCX connector. A bias tee will couple the 48V dc supply to the signal line.
164 Control signals for the high-voltage power supply will also be coupled capaci-
165 tively to the signal line. The amplifier will chain will include a programmable
166 gain amplifier to allow tuning of the overall system gain, minimal shaping and
167 an anti-alias filter. The ADC will consist of a Texas Instruments ADS4249
168 dual channel amplifier running at 240MHz, and a 14bit readout to an Intel
169 (formally Altera) Cyclone IV FPGA via LVDS.

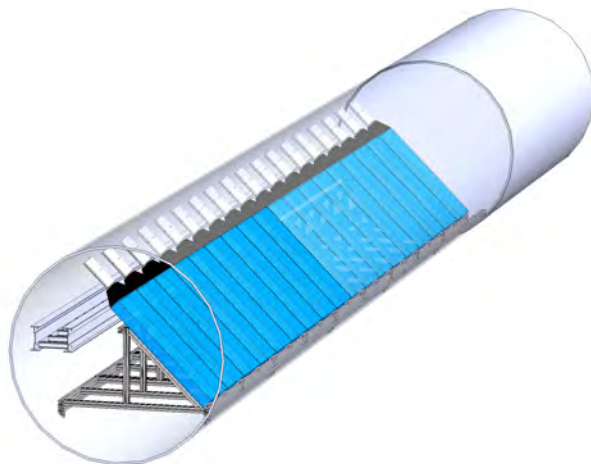


Fig. 7: The deployment of the Outrigger Detector in Shafts 4 and 5.



The FPGA will perform discrimination, coincidence and peak detection of the incoming signals, with inter-FPGA communication via backplane B-LVDS. Events that pass both the software trigger and the veto will be passed for storage via Ethernet to the PC(s). The system will run synchronously to the LHC (bunch crossing) clock. The orbit clock will also veto background events from non-colliding bunches and to synchronize health-keeping events and switching regulator noise to the abort gap.

Normally the data will be transferred via 1 Gbit/s ethernet link to an external computer. There will also be a computer in UGC1 that will take data if there is a failure in the ethernet connection. The data will be sent via the onsite storage via the internet to analysis sites in Canada, UK, USA, Spain and Italy. The 19 readout boards will be housed directly underneath the MAPP-mQP detector, in the UGC1 gallery.

The data rate is expected to be on average less than 1 Hz from each of the 400 bars of the MAPP main detector with around another 200 channels from the veto detectors and radiator at maximum. There are 80 extra channels contributed by the Outrigger Detector, corresponding to the 80 scintillator blocks comprising the detector.

Conservatively assuming a rate of, on average, 1 Hz for each of the 680 channels involved, with 200 bits per channel (or PMT pulse) being read out, the total data rate is around 140 Kbits/sec. Our system has the capacity to read out 4 million channels/s, 5900 times more capacity than needed. The data in the front end readout electronics is pipe-lined so that large fluctuations up

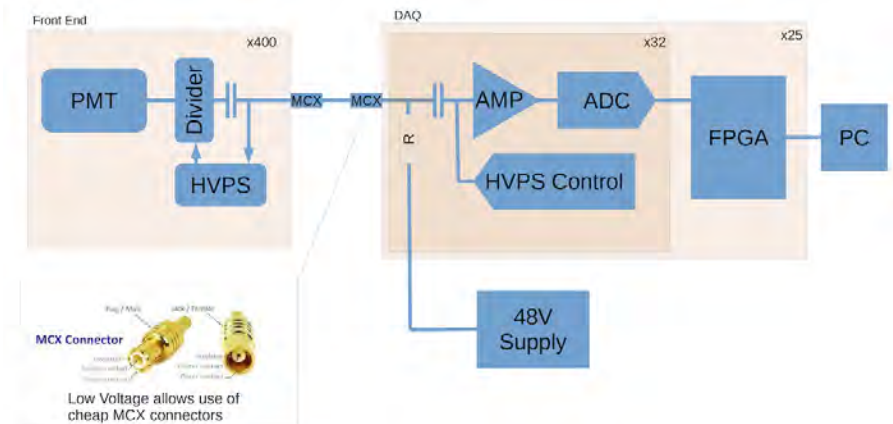


Fig. 8: A block diagram showing the basic electronics readout structure for the MAPP-mQP detector,

193 in the data rate can be handled. Thus, these boards could be used for high
 194 luminosity LHC.

195 There will be a number of software triggers carried out by FPGAs housed
 196 in the readout system. The trigger philosophy is to widen the trigger as much
 197 as possible. Additionally, we aim to take minimum bias events at the rate of
 198 approximately 5% of the total data rate. Nevertheless, we expect the amount of
 199 data readout will be somewhat less than the maximum mentioned just above.
 200 Further, higher-level “triggers”, will be applied offline to the raw data. We
 201 chose to adopt the philosophy of utilizing a very broad software trigger, rather
 202 than reading out the complete detector at each beam crossing since the flow of
 203 data through the various triggers enables us to monitor the physics response
 204 of our detector online.

205 An example of an important “software” trigger for MAPP-1 and the Out-
 206 rigger Detectors, is the through going muon-trigger. In this case the muon
 207 would pass through all four scintillator blocks pointing at the IP as well as
 208 the photon tagging boards (that can also serve as VETO detectors) that sand-
 209 wich the main scintillator detector sections. In the MAPP-1 case a basic muon
 210 trigger is formed from a coincidence of 4 contiguous scintillator sections.

211 In the case of the Outrigger Detector, the muon trigger is formed by a
 212 “hit” in each of the four scintillator layers where those hits are consistent with
 213 forming a collinear track. In the case of the Outrigger detector the trigger
 214 efficiency of a through going muon is on average around 80%, rather than
 215 the essentially 100% expected for the MAPP-1 bar detector. This is because
 216 MAPP-1 has been designed as a pointing detector, whereas the Outrigger is
 217 only approximately pointing due to the nature of its required positioning.

218 The efficiency trigger efficiency to be very near 100%.

2.2.1 The Outrigger Detector Calibration System

Like the MAPP-1 detector, the Outrigger Detector will be calibrated in two main ways. The first method utilizes an array of blue LED's emitting at the peak of the wavelength sensitivity of the scintillator blocks forming the Outrigger Detector. Each scintillator block is equipped with a LED which is pulsed in such a way as to mimic the light deposited by particles with varying fractional charge, down to the level where only single photoelectrons are being detected by the PMTs.

The second calibration method employs the small flux of high-momentum muons from IP8. Characteristically, these muons will be minimum ionizing particles (MIPs). We can simulate the light emission of a fractionally charged particle by inserting a neutral density filter between the PMT and the scintillator block. The transmittance of the filter would be chosen to reduce the amount of light entering the PMT from the muon by the same amount that a fractionally charged particle would have reduced ionization compared to a MIP. This "absolute" calibration is transferred to the LED system by comparison of the signal generated by the calibration LED in the PMT to the signal obtained when a neutral density filter is interposed.

3 Beam Induced Radiation Backgrounds in the MAPP-1 Outrigger Detector Region of the UA83 Tunnel

A prototype MAPP-mQP detector was deployed in 2018. Its main purpose was to enable us to estimate the data rate we would expect during RUN-3. The prototype was comprised of nine 10 cm x 10 cm x 120 cm scintillator bars deployed in a *horizontal* configuration in the UGC1 gallery. Each bar was read out at both ends by a PMT. A hit on a scintillator bar was counted if the PMTs at each end of the bar registered a coincident signal above the threshold. We observed that with beam-off each bar was hit at around a rate ~ 0.05 Hz. This rate was largely due to cosmic rays, despite the roughly 110m rock overburden. This level of the cosmic background was consistent with our GEANT-4 based simulations. We expect this level of cosmic ray activity in the UA83 tunnel as it lies at the same depth beneath the same rock overburden.

When the beam was turned on we observed the rate in the MAPP-mQP prototype bars increased by a factor of 4 to 5. According to the FLUKA studies presented in the above subsection on beam-induced radiation backgrounds in the MAPP-mCP region of the UA83 tunnel, the beam-induced backgrounds in the MAPP-mCP detector in UA83 should be considerably less than expected in UGC1, except in the regions where the ducts connect UA83 with the beam tunnel.

In order to study beam-induced backgrounds more fully Francesco Cerutti and Alessia Ciccotelli of the beam-Machine Interaction section of the CERN

260 Engineering Department has performed a study of the beam-induced back-
 261 grounds in the UA83 tunnel and the UGC1 gallery using the FLUKA Monte
 262 Carlo program, assuming an annual luminosity of 10 fb^{-1} .

263 A critical issue is the effect of the radiation on the detector and on its
 264 electronic readout system. A key variable here is the dose which is shown
 265 in Figure 9. As can be seen from Figure 9 the dose received by the MAPP-1
 266 detector in its new position in the UA83 tunnel is estimated to be below
 267 1 mGy/year , a factor of 300 less than its initially proposed deployment in the
 268 UGC1 gallery.

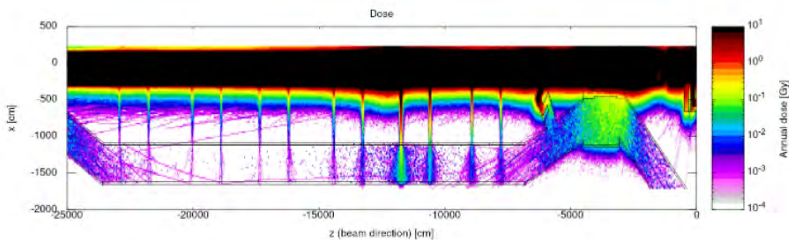


Fig. 9: The dose rate in the vicinity of MAPP-1. The top map shows the UGC1 gallery and the bottom map shows the UA83 tunnel.

269 Figure 10 depicts a map of the muon fluence component of beam-induced
 270 backgrounds expected at the UA83 ($< 10^6 \text{ cm}^{-2}$) and UGC1 ($\sim 3 \times 10^8$
 271 cm^{-2}) locations of the MAPP-mCP detector. We see a better than a 300
 272 times reduction of the muon flux in the UA83 location compared to the UGC1
 273 position.

274 Likewise the neutron flux ($5 \times 10^7/\text{year}$) and photon flux ($10^8 \text{ cm}^{-2}/\text{year}$)
 275 at the position of the MAPP-1 detector in UA83 show at least a few hundred
 276 times reduction over MAPP-1's previously proposed position in the UGC1
 277 gallery, as laid out in Figure 11 and Figure 12, respectively.

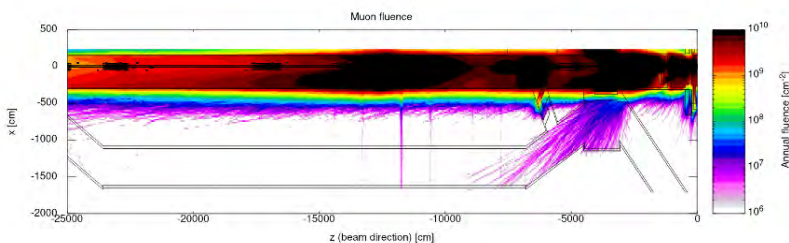


Fig. 10: The muon fluence in the vicinity of MAPP-1. The top part of map shows the UGC1 gallery and the bottom map shows the UA83 tunnel.

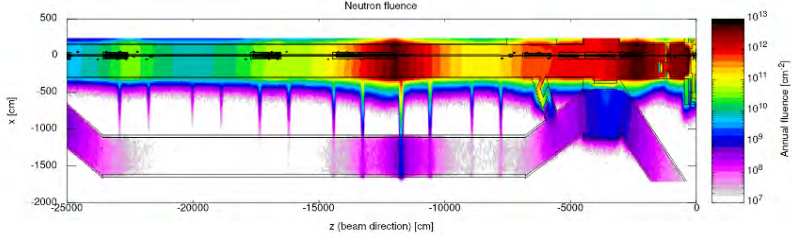


Fig. 11: The neutron fluence in the vicinity of MAPP-1. The top part of the map shows the UGC1 gallery and the bottom map shows the UA83 tunnel.

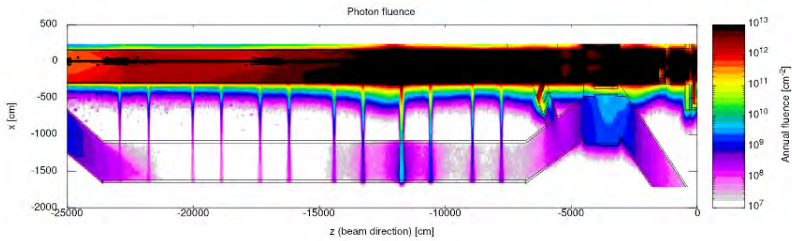


Fig. 12: The photon fluence in the vicinity of MAPP-1. The top part of the map shows the UGC1 gallery and the bottom map shows the UA83 tunnel.

3.1 Beam and Cosmic Backgrounds in the Vicinity of the Outrigger

In the region by the mouth of the ducts in the UA83 tunnel, the beam-induced backgrounds rise substantially, since radiation can travel down the shafts unimpeded. Thus, before we install the outrigger detectors in shafts 3,4 and 5 we will install 2m of shielding in the beam-tunnel side of the shaft. The result of doing this for shafts 4 and 5 are given in Figures 13, and 14 where the peak values obtained in the ducts are shown.

For shaft 3, the 2m of shielding reduces the annual dose by a factor of around 300 from 3×10^4 mGy to 10^2 mGy for a luminosity of 10 fb. The thermal neutron fluence is reduced by a factor of over 150 from 10^{11} $\text{cm}^2\text{yr}^{-1}$ to 7×10^8 $\text{cm}^{-2}\text{yr}^{-1}$ and the High Energy Hadron (HEH) flux is attenuated by a factor roughly 10 to 6×10^8 $\text{cm}^{-2}\text{yr}^{-1}$. For an instantaneous luminosity of 2×10^{33} $\text{cm}^{-2}\text{s}^{-1}$ the estimated photon fluence is diminished from 10^5 $\text{cm}^{-2}\text{s}^{-1}$ to 3×10^2 $\text{cm}^{-2}\text{s}^{-1}$. In the case of muons the fluence is reduced by a factor of about 8 to 10 $\text{cm}^{-2}\text{s}^{-1}$.

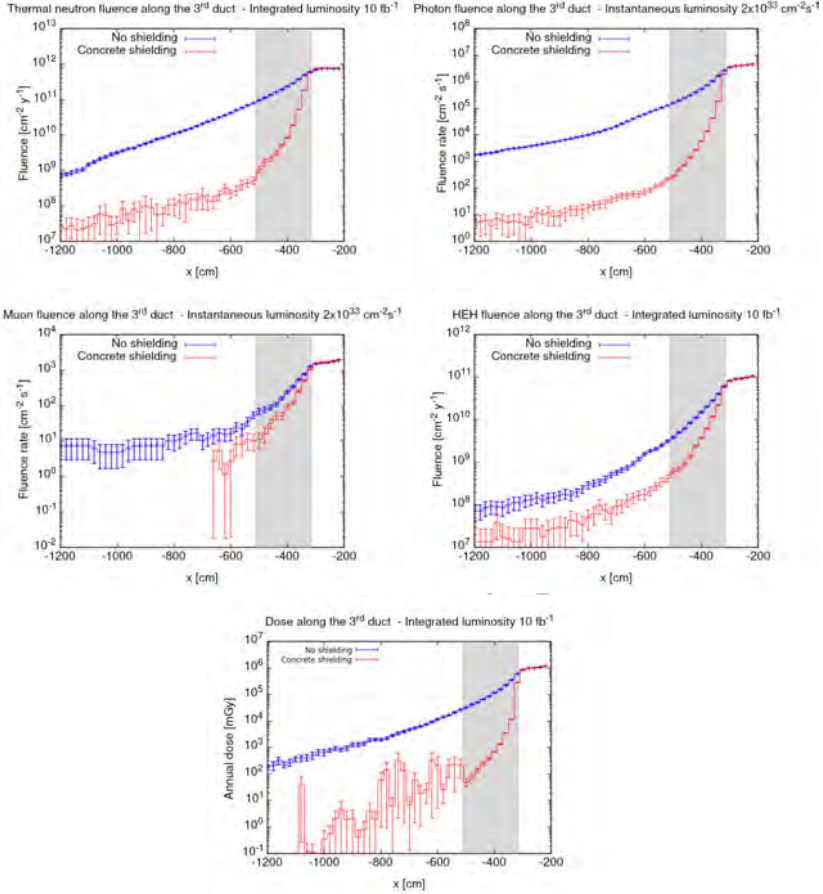


Fig. 13: The radiation levels in the 3rd duct on the UA83 tunnel.

294 As the TANB absorber is adjacent to the mouth of shaft 4 the beam back-
 295 grounds are somewhat higher than in shaft 3. For shaft 4 the 2m of shielding
 296 reduces the annual dose by a factor of nearly 300 to 0.1 Gy for a luminosity
 297 of 10 fb. The thermal neutron fluence is reduced by a factor of over 200 from
 298 $10^{12} \text{ cm}^2 \text{ yr}^{-1}$ to $2 \times 10^9 \text{ cm}^2 \text{ yr}^{-1}$ and the High Energy Hadron (HEH) flux is
 299 attenuated by a factor roughly 30 to $10^9 \text{ cm}^2 \text{ yr}^{-1}$. For an instantaneous lumi-
 300 nosity of $2 \times 10^{33} \text{ cm}^2 \text{ s}^{-1}$ the estimated photon fluence is diminished from 10^6
 301 $\text{cm}^2 \text{ s}^{-1}$ to $10^3 \text{ cm}^2 \text{ s}^{-1}$. In the case of muons, the fluence is reduced by a factor
 302 of 10 to $10 \text{ cm}^2 \text{ s}^{-1}$.

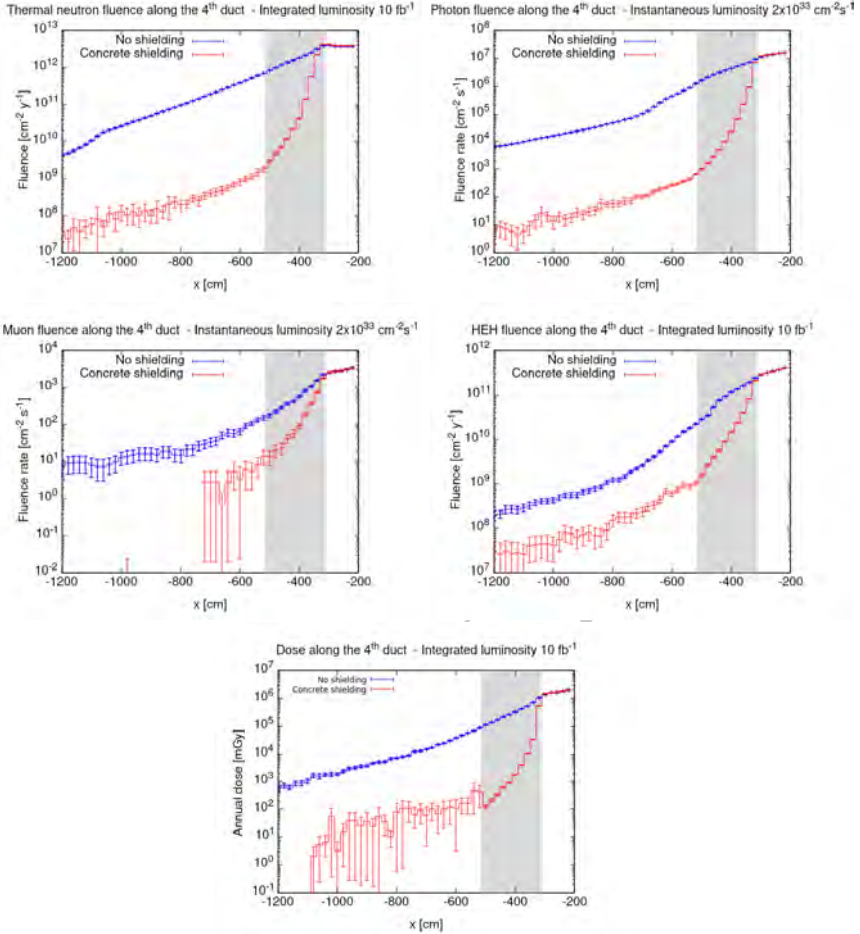


Fig. 14: The radiation levels in the 4th duct on the UA83 tunnel.

303 4 Construction and Installation of the 304 Outrigger Detector

305 The detector will be constructed and tested at the University of Alberta. It
 306 will then be broken down to its constituent elements, none of which weigh
 307 more than 20kg, and then shipped to CERN for installation in the UA83
 308 tunnel. Once situated, the detector and its readout chain will be tested in situ
 309 before data taking. T-slot extrusion (45 mm x 45 mm) is used to construct the
 310 framework to support the scintillator blocks. In practice, the basic units are
 311 assembled into 4 block (shaft 3) and 2 blocks (shafts 3 and 4) substructures
 312 for handling and insertion into the shaft. A Gantt chart showing the envisaged
 313 construction schedule is given is provided in Figure 15 and Figure 16.

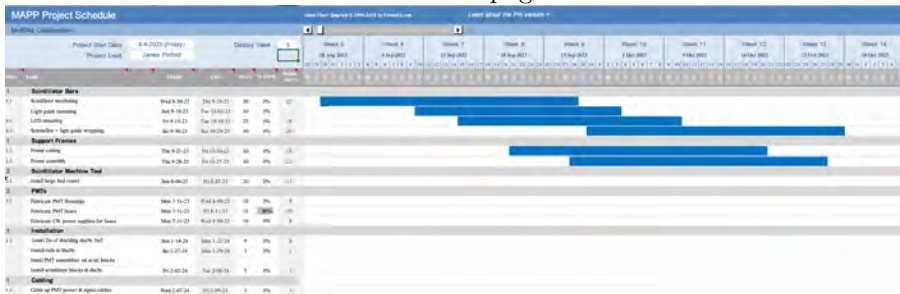


Fig. 15: The construction schedule for the Outrigger Detector scintillators.

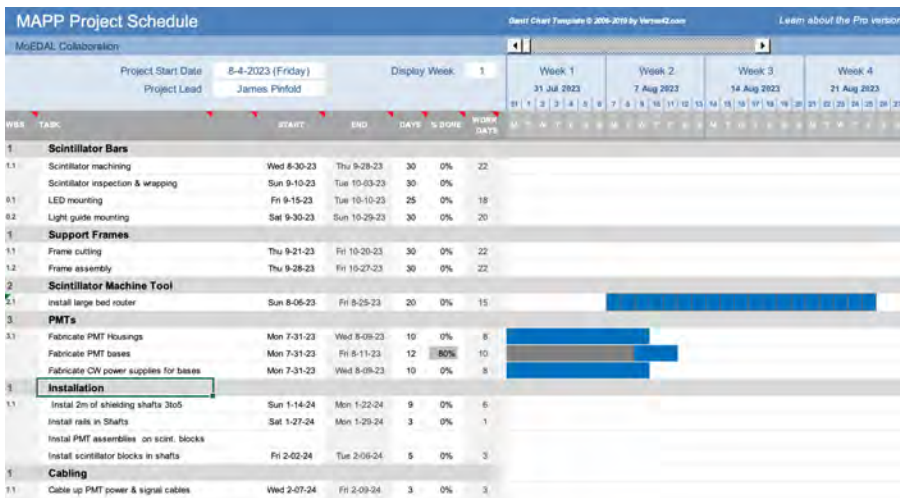


Fig. 16: The construction schedule for the Outrigger Detector PMTs and related technology.

314 4.1 Installation of Required Infrastructure

315 The substructures are inserted into the shaft along rails fixed on each side of
 316 the shaft. A total of 10 subunits (roughly 20 blocks wide) are installed in each
 317 shaft. The total area of plastic seen by particles from the IP as they impinge
 318 on shaft 3 is $20 \times [30 \times 60 \times \sin 45^\circ] = 2.5 \text{ m}^2$, compared to $\sim 1 \text{ m}^2$ for the
 319 MAPP-1 detector

320 The readout of the PMTs as well as the calibration system is connected
 321 to the main readout electronics readout rack of the MAPP detector. The elec-
 322 tronics readout and calibration system is functionally the same as that of the
 323 MAPP-1 detector. The cables carrying LV power and signals to and from the
 324 PMTs are housed in the cable rack installed the length of each shaft behind

325 the scintillator blocks. Details of the installed detector are given in Figure 6
 326 and Figure 7.

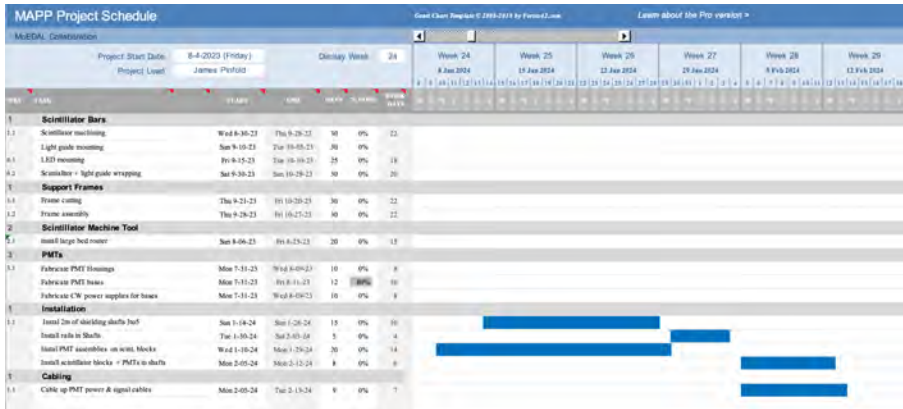


Fig. 17: The installation schedule for the shielding, the installation rails, the cable trays, the Outrigger Detectors with PMTs and cables.

327 The installation starts with the attachment of the PMTs and light-guides
 328 to the scintillator blocks during week in January 2024. Contemporaneously,
 329 the shielding will be installed, filling the 2m of ducts 3, 4 and 5 nearest the
 330 beam tunnel. After the 'shielding has been installed the rails and cable trays
 331 within the ducts will be put in place. Starting at the beginning of February
 332 2024, the scintillator PMT units will be cabled and placed in the ducts using
 333 the rails. The installation schedule for the Outrigger Detector is summarised
 334 in Figure 17

335 4.2 Staging and Temporary Storage Area

336 In order to facilitate the installation and operation of the Outrigger Detector
 337 the LHC machine side manager responsible for allocation of surface space in the
 338 SBD building agreed that MoEDAL-MAPP Experiment can be temporarily
 339 attributed about 20 m² of surface space in SBD 2855, as indicated in the
 340 photograph in Figure 18. This area will be used as buffer space for short term
 341 storage of equipment before transport and installation underground, and for
 342 storing light tooling needed for assembly and installation.

343 5 Safety Matters

344 The safety issues considered below arise from four sources, those to do with:
 345 the UA83 tunnel; the detector itself; and, detector operations.



Fig. 18: The temporary staging area in SBD 2855.

5.1 UA83 Tunnel and Detector Safety Issues

The UA83 tunnel is a full part of the LHC machine infrastructure with access via the PM85 lift directly to the floor of UA83. It has interlock access, smoke detectors, fire alarms and forced ventilation.

The MAPP-mQP and the Outrigger Detector employ conventional detector technology involving scintillator detectors and electronic readout, no gaseous detectors are involved. The safety issues directly related to the MAPP-mCP detector are presented in an approved Safety Derogation Request (SDR) [3] and described directly below. The SDR is included in Appendix (A).

The acrylic-based scintillator detector elements of the Outrigger are completely enclosed in three horizontal concrete ducts. The total mass of plastic scintillator in Shaft 3 is 400 kg, with 200kg of scintillator in each of the ducts 4 and 5. The safety sheets for acrylic plastic are included in Appendix (B). Thus the Outrigger detectors are completely surrounded by metres of concrete, except for the opening into the UA83 tunnel. An aluminium flame shield will be placed across the mouth of the opening to completely isolate the detectors.

The MAPP/Outrigger detector electronics rack and MAPP detector are monitored by an IR + Visible light digital camera placed in the vicinity of MAPP in the UA83 tunnel. The Outrigger detectors which do not obtrude into the UA83 tunnel are situated in ducts that will be equipped with smoke and temperature detectors, that are monitored in the same way as the MAPP-1 temperature and smoke sensors.

368 **5.1.1 Safety Issues Related to the Readout Electronics & HV**

369 The readout electronics and power supplies are isolated and deployed up to
370 30m from the Outrigger Detectors in the electronics racks servicing the MAPP-
371 1 detector. There are no HV cables or HV connectors as there is a “Cockcroft-
372 Walton” type converter in the base of each PMT that converts LV power
373 to HV power for the PMT. The power supplies are low voltage (24V), are
374 current and the temperature limited (turn off when current or temperature
375 goes out of a predetermined range), and provide an alarm signal when current
376 or voltage moves out of some predefined operating window. The MAPP-mQP
377 and Outrigger detector electronics consume only 1800 watts of power.

378 All cabling is halogen-free according to the provisions in IS23 ³. The only
379 other heat source in the UA83 gallery arises from the MAPP-mQP detector
380 electronics and amounts to only 1400 watts.

381 **5.2 Safety Issues Relating to Detector Installation**

382 MAPP-1’s outrigger detector is designed to be installed in situ from pieces
383 weighing a maximum of approximately 20 kgs each. Thus the whole Outrigger
384 detector can be taken underground using the machine side elevator at IP8. We
385 envisage that a maximum of four people will need to be present in the UA83
386 gallery for installation of the MAPP Phase-1 detector. MoEDAL-MAPP’s
387 installation personnel will, of course, be equipped with all the required safety
388 gear and will operate according to the safety rules and guidelines described in
389 the safety courses that each member of the team will have taken and passed.

390 **5.3 Safety Monitoring After Detector Installation**

391 The MAPP-1 Outrigger detector is readout over ethernet through the same
392 pathways as the MAPP-1 detector. It does not require a team to operate it
393 during data taking. However, it is important that the detector is monitored to
394 ensure safe operation at all times. The safety systems that will be installed to
395 ensure that the detector is operating safely are as follows:

- 396 • The power supplies are current limited. In addition, alarm conditions are
397 defined that signal non-standard operating characteristics. The power sup-
398 plies output and alarm conditions are monitored remotely with a feed
399 supplied to the CERN Control Centre (CCC);
- 400 • Three temperature probes will be placed at the end, middle and entrance
401 of each of the three shafts housing the outrigger detector. Alarm conditions
402 are defined that signal if any monitored temperature moves above normal
403 ambient temperature in the UA83 tunnel. The temperature probe outputs
404 and alarm conditions are monitored remotely with a feed supplied to the
405 CCC;
- 406 • A smoke detector that can be monitored remotely will be placed within the
407 mouth of each of the ducts containing Outrigger Detectors;

³<https://edms.cern.ch/document/335745/4>

- 408 • An IR camera will be installed on site to monitor the whole MAPP-1
409 detector region. Again, the feed from the camera will be supplied to the
410 CCC.

411 5.4 MoEDAL-MAPP Safety Organization

412 The MoEDAL-MAPP safety organization at CERN will be established prior
413 to installation. It will consist of:

- 414 • An experimental Safety Officer (EXSO, formerly GLIMOS) as the point of
415 contact for all experimental safety issues and communication with the EP
416 Safety Office. The EXSO for MoEDAL for installation and the first year of
417 running, will be the Technical Coordinator, Richard Soluk;
- 418 • Both the EXSO and the MoEDAL-MAPP Spokesperson will be available
419 for urgent safety interventions required during the detector installation;
- 420 • All the activities of installation will be declared via IMPACT request and
421 analyzed via the usual work package analysis and VIC (Visite Inspection
422 Commune) procedures ;
- 423 • The MoEDAL-MAPP safety files will be created on EP safety office EDMS
424 and shared with the LHCb LEXGLIMOS.

425 6 Organization of Construction, Installation 426 and Running of the Detector

427 The two bulleted lists below describe the basic organization of the construction
428 and installation of the Phase-1 MAPP-mCP detector:

- 429 • Project Managers:
 - 430 – MoEDAL Spokesperson - James Pinfeld;
 - 431 – MoEDAL Technical Coordinator - Richard Soluk;
 - 432 – Chief engineer - Mitchel Baker;
 - 433 – Chief electronics engineer +Trigger and DAQ coordinator - Paul Davis;
 - 434 – CERN based administrator - Veronique Wedlake;
 - 435 – CERN based liaison with Machine - Francois Butin;
 - 436 – EXSO(GLIMOS) - Richard Soluk; Safety Officer - Richard Soluk
- 437 • Installation Crew
 - 438 – Richard Soluk - Crew leader and responsible for mechanics installation;
 - 439 – Paul Davis - Readout electronics, power supplies and FPGA-based trigger;
 - 440 – Aditya Upreti - General team member to assist in all aspects of installa-
441 tion;
 - 442 – Emanuela Musumeci - General team member to assist in all aspects of
443 installation
 - 444 – Michael Staelens - General team member to assist in all aspects of
445 installation
 - 446 – Mitch Kelly - General team member to assist in all aspects of installation

- 447 – Phd-student/Post Doctoral student 1 - General team member to assist in
448 all aspect of installation;
- 449 – Phd-student/Post Doctoral student 2 - General team member to assist in
450 all aspect of installation.

451 **7 Maintenance and Operation of the Outrigger** 452 **Detectors for MAPP-1 During Run-3**

453 The MAPP-1 and Outrigger detector will be read out via ethernet during
454 the run to large-scale onsite disk storage at CERN. The UA83 gallery is not
455 accessible during LHC running periods. In the event of a failure or malfunction
456 of the Outrigger Detector, we will not be able to effect repair until we have
457 a TS, or a YETS in which access to the UA83 tunnel is possible. Typically,
458 there are a few Technical Stops (TSs) within the year besides the YETS.

459 We could continue running with the failure of a large fraction of the readout
460 channels although understandably this would compromise the physics perfor-
461 mance of the detector. In order to reduce the risk of shutdown of data taking
462 during the run we have included in our electronics design a redundant power
463 supply system and a redundant DAQ computer, to ensure robust operation of
464 the overall detector.

465 In order to continue data taking in the event of a disruption of the ethernet
466 connection, the DAQ server will have 60TB of local disk storage. Data will
467 be written to this disk until the ethernet connection is re-established. During
468 normal running the data rate will be below 0.5 TB/day allowing an extended
469 running period without exporting data to remote storage. Initially, the fewest
470 possible restriction will be applied to the trigger, and storage write speeds will
471 limit the data rate.

472 The MAPP detector is designed to be operated remotely and to shut down
473 if any MAPP-1 or Outrigger Detector power supply draws more than a set
474 maximum current. Nevertheless, the MAPP-1 and Outrigger detectors must
475 be monitored 24/7 by personnel based on site primarily for safety purposes -
476 as described in Subsection 5.4. This team would be enhanced by an average
477 of 0.5 FTE person, formed from MoEDAL-MAPP collaboration members who
478 are visiting CERN and have the required safety training. For planned upgrades
479 or maintenance during running periods, we will call on manpower resources
480 described in Subsection 6.

481 **7.1 The Outrigger Detector Control Centre**

482 The base of operations of the MAPP detector is the MAPP Control Centre
483 (MCC) in Bat. 17 R-007, the location of which is shown in Figure 19. MAPP's
484 CERN-based operators have access through their on-call cell phones to the
485 monitoring and alarm system as well as simple controls that allow them to turn
486 off the power and alert the CCC. The on-call MAPP operator, the off-duty
487 operator, and the Technical Coordinator + Spokesperson are also connected
488 to this system at all times via cellphone. During the day the on-call MAPP-1



Fig. 19: The location of the MAPP-1 and Outrigger Detector Control Room (Bat. 17 R-007).

489 Outrigger operator will usually sit in the control room. During the evening and
490 night, the on-call will be connected by cell phone to the MAPP-1 and Outrigger
491 control and monitoring services. The on-call cell phone will be switched on at
492 all times.

493 **8 Funding Plans for the MoEDAL-MAPP** 494 **Phase-1 Installation**

495 The MAPP-1 Outrigger detector project has been made possible by contri-
496 butions of equipment from other experiments, including long-term loans of
497 scintillator from EXO-200 and surplus HZC PMTs from a cancelled astroparticle
498 physics experiment. We will use the same electronic readout and calibration
499 technology utilized by MAPP-1, including electronic readout, DAQ, cali-
500 bration and safety systems. The funding needed for extra readout boards,
501 PMT bases, LED calibration units and power supplies will; be provided from
502 MoEDAL-MAPP M&O funds, MoEDAL-MAPP-1's NSERC Discovery Grant;
503 and, contributions from the UofA DUP funds. All required funding for the
504 project is now in place.

505 Regarding manpower, our project electronics engineer, mechanical engineer
506 and detector technologist are funded by our existing NSERC MRS grant. We
507 have sufficient funds in hand to deploy the Outrigger detector (as described
508 above) to take data in Run-3.

509 **9 Physics Issues**

510 In order to fully understand the sensitivity of the MoEDAL-MAPP detector
511 to we are performing studies of a number of relevant physics benchmarks.
512 Examples of initial benchmark studies are presented below. To complete these

513 physics studies we need to fully and accurately simulate: the detector and its
514 response; the passage of primary and secondary particles through the inter-
515 vening infrastructure; and, the transport of cosmic ray particles through the
516 105 m overburden. The complete Simulation package UA83-MAPP-MoEDAL
517 Arena (SUMMA) is discussed below.

518 **9.1 The Full Simulation of the UA83, MoEDAL,** 519 **MAPP-mCP Arena (SUMMA)**

520 The previous version of SUMMA, with the MAPP-mCP detector deployed in
521 the UGC1 region, was nearing completion in Spring of 2021 when the decision
522 was made to move MAPP's location to the UA83 tunnel. The move required an
523 extensive update to the SUMMA code to take into account the MAPP-mCP's
524 new final position approximately 100m away (UA83) from the IP. Additionally,
525 the modelling of the intervening infrastructure had to be completely redone.
526 However, SUMMA's existing cosmic ray simulation module did not require
527 extensive updates.

528 The SUMMA simulation is derived from: the final CAD drawings of the
529 MAPP-mCP detector; accurate CAD drawings of the machine infrastructure;
530 and, the existing model of cosmic ray transport through the overburden. In all,
531 the simulation involves over 2500 elements. The SUMMA code will be ready
532 for use in mid-December 2021.

533 The Physics Processes included in SUMMA, are:

- 534 • Primary Interaction and secondary particles, factory lists :
 - 535 – FTFP_Bert model of hadronic showers
 - 536 – QGSP_BERT_HP for neutron fluxes
- 537 • Transportation and Decay;
- 538 • Electromagnetic Interactions.
 - 539 – Gamma conversion, Compton scattering, photo-electric effect for gammas;
 - 540 – Multiple scattering, ionization, bremsstrahlung for electrons and annihila-
541 tion for a positron;
 - 542 – Multiple scattering, ionization, bremsstrahlung and pair production for
543 muons;
 - 544 – Multiple scattering and ionization for other particles.
- 545 • Scintillation processes
 - 546 – Scintillation and Cerenkov for particles;
 - 547 – Absorption, Rayleigh scattering, Mie scattering and boundary processes
548 for optical photons.

549 The SUMMA ionization energy loss calculation for milli-charged particles
550 is based on the approach adopted in Reference [5]

9.2 Mini-Charged Particles from Dark QED - a Physics Benchmark

In an initial study of the sensitivity of the MAPP-1 Outrigger detector to mCPs. We here consider a class of Feebly Interacting Particle (FIP) that has a mini-charge (mCP) as small as $10^{-3}e$, or lower. A common scenario is from a Dark Sector model where one considers a mCP coupled through a very light kinetically mixed dark photon [6][7]. Although the mCP does not carry SM electroweak quantum numbers, it behaves as a particle with a tiny electric charge. The Feynman diagrams for the most important production mechanism of mCPs at the LHC are shown in Figure 20.

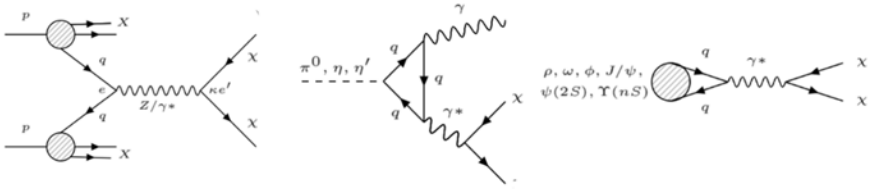


Fig. 20: The Feynman diagrams for the most important production mechanism of mCPs at the LHC: (left) DY production; (middle) Dalitz decays of pseudoscalar mesons; and, (right) direct decays of vector mesons.

The DY process provides the main production channel for GeV-range mCPs at the LHC. The sensitivity of the MAPP-mCP detector deployed at UA83 to mini-charged particles produced in this way is shown in Figure 21. The sensitivity of the MAPP-mCP detector deployed at UA83 to mini-charged particles produced by DY production is shown in Figure 21. The Outrigger Detectors provide a clear improvement over the whole higher mass region of $1 \text{ GeV}/c^2$ and above.

If we include all of the processes shown in Figure 20 the sensitivity of MAPP-1 for masses below $1 \text{ GeV}/c^2$ improves considerably and in a very competitive way. However, we should note that the efficiency of the MAPP-1 and Outrigger Detectors is assumed to be 100%, with zero background. The milliQan analysis on the other hand has considered detector efficiency and backgrounds. The final MAPP-1 efficiency and backgrounds

Backgrounds

A potential source of background mentioned previously is the dark count from the PMT. For the HZC-phonics, the dark count rate is typically 600 cps. Considering the mCP trigger, that consists of requiring an mCP signal in 4 collinear blocks in coincidence, with a trigger window of 25 ns and a beam crossing rate of 40 MHz, we would expect a trigger rate due to the dark count rate in the PMTs, of roughly 0.003, in a data-taking year of 1.5×10^7 s.

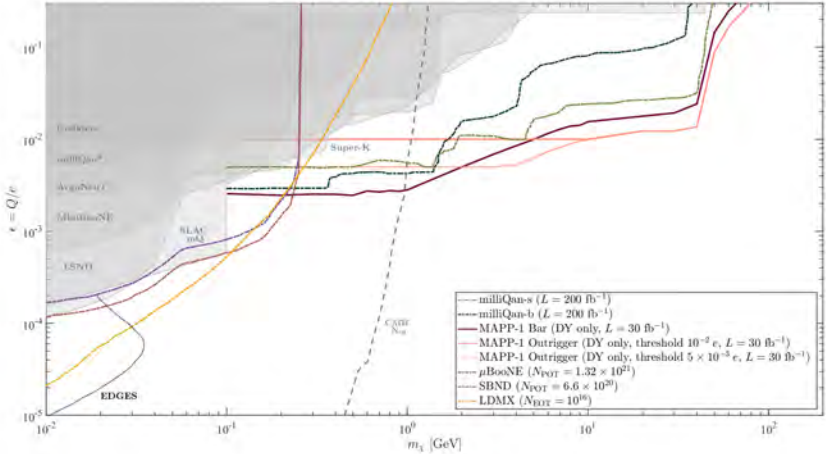


Fig. 21: Direct bounds from accelerator-based searches and indirect bounds from the effective number of neutrinos from Planck are shown. The projected sensitivity for mCPs, for models with a massless dark photon, are presented for milliQan (for the slab (s) and bar (b) detectors and MAPP-mCP (for the MAPP-mCP bar (B) and Outrigger (O) detectors) at Run-3. The existing bounds are provided for approved detectors or detectors in the process of approval [8].

581 The MAPP-mCP detector is protected from cosmic ray backgrounds by
582 a 105 m overburden. MilliQan, by comparison, is deployed near to the CMS
583 detector at a depth of 73m. The cosmic ray background expected in the MAPP-
584 mCP detector has been assessed by the MoEDAL-MAPP simulation group
585 to be $(4.04 \pm 0.06) \times 10^{-5} \text{ cm}^{-2} \text{ s}^{-1}$. This amounts to about 2 muons/s
586 incident of the top of the MAPP-mCP veto detector, with area $\sim 4.5 \text{ m}^2$.
587 This rate is inconsistent with measurements taken in the UGC1 gallery in
588 2018. Considering the trigger requirement for mCPs and the high efficiency of
589 the MAPP-mCP veto system the background from uncorrelated CR muons is
590 expected to be negligible.

591 The most important source of background is thought to be due to cosmic
592 ray events with high muon multiplicity where a number of muons penetrate
593 underground together, This has been observed, for example, by the ALICE [10]
594 TPC with effective CR muon detection area of 17 m^2 and 28 m rock overburden,
595 where the corresponding figures for the MAPP-mCP detector at 4.4 m^2 and
596 105 m. The concern is that a number of particles could impinge on the detector
597 together increasing the probability of satisfying the mCP trigger conditions.
598 However, the greater the multiplicity of muons impinging on the MAPP-mCP
599 detector region, the greater the chance one of these muons would VETO the
600 event. There are several additional factors that act to reduce this potential
601 source of background:

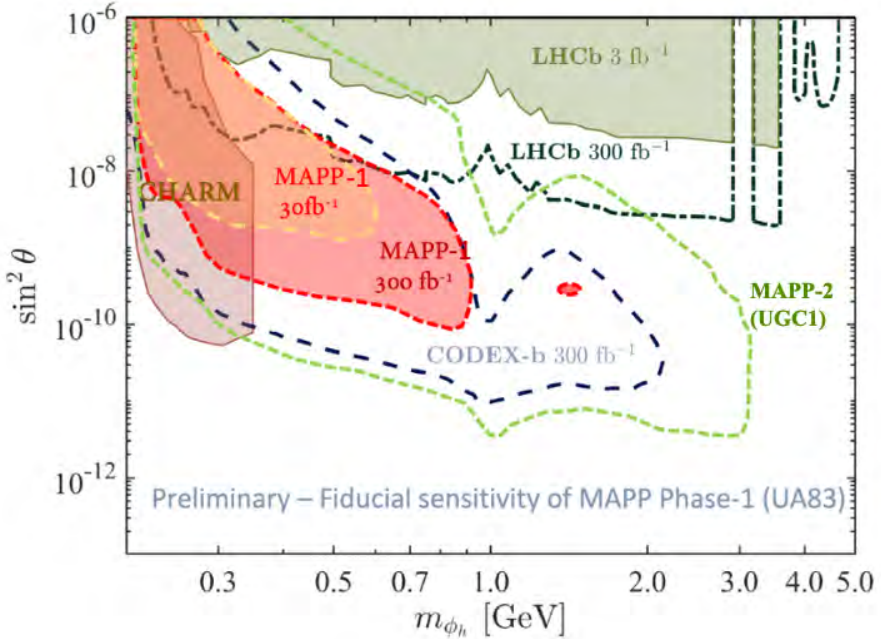


Fig. 22: 95% C.L. exclusion bounds on dark Higgs bosons produced at the HL-LHC at a center-of-mass energy of $\sqrt{s} = 14$ TeV for the MAPP-2 detector (considering a total integrated luminosity of $L = 3 \text{ ab}^{-1}$), compared to previous results obtained for MAPP-1 and CODEX-b [9]

r

- 602 • The rate of these showers is very small compared to the rate of single uncor-
- 603 related particles given above. For example, the ALICE data shows over six
- 604 orders of magnitude fall in the number of events with a multiplicity of 20
- 605 muons compared to just a few muons;
- 606 • For cosmic ray muons from above or below to reach a bar and give even
- 607 a small mCP signal the charged CR particle would normally need to cross
- 608 two VETO counters which have an efficiency better than 99.7% and “clip”
- 609 a bar. This would need to happen four times in four contiguous bars within
- 610 the trigger time window, without hits from other CR muons in the shower
- 611 registering in the VETO system;
- 612 • The rate of horizontal cosmic rays is greatly suppressed compared to the
- 613 downward flux. If horizontal cosmic ray muons do reach the MAPP detector
- 614 they must pass through four vertical veto walls of thickness 2.5 cm that are
- 615 placed in front of MAPP and between each MAPP section, and also the
- 616 back wall of the cosmic ray VETO detector of thickness 1 cm, to satisfy the
- 617 mCP trigger;
- 618 • Neutrons associated with the muon shower can evade the VETO system and
- 619 cause, for example, a nuclear recoil that can give rise to a small signal in a

620 bar. This would need to happen in four contiguous bars within the trigger
621 time window. At the same time, the accompanying charged particles in the
622 shower would have to miss the VETO system.

623 As stated above in Section 2 we can monitor the VETO system, with collisions-
624 off and collisions-on, for any penetration of the VETO system. If necessary we
625 can utilize the outer layer of scintillator bars in MAPP-mCP detector as an
626 additional VETO system.

627 Importantly, can study non-beam-related background sources experimen-
628 tally by running in the winter while the beam is off. In this way, we can directly
629 register background events that mimic a signal. These runs can be used to
630 hone our estimates of non-beam-related backgrounds.

631 10 Conclusion

632 The MAPP-1 Outrigger Detector is designed to enhance the acceptance
633 above a mCP mass of approximately $5 \text{ GeV}/c^2$ as shown in Figure 21 for
634 the standard benchmark process [6][7] of DY production of mCP pairs. The
635 MAPP-mCP detector and Outrigger Detector is very competitive with the
636 milliQan detector [11] that will also be deployed for Run-3 and covers a dif-
637 ferent pseudo-rapidity range. In the event of the discovery of a mini-charged
638 particle by MAPP-mCP and milliQan, a signal seen in two different detectors
639 with their different systematics would provide the necessary confirmation of a
640 discovery. Indeed, the use of multiple experiments to provide verification for
641 important experimental findings has been adopted at LEP (ALEPH, DELPHI,
642 L3 and OPAL) as well as the LHC (ATLAS and CMS).

643 Additionally, although MAPP-1 is designed primarily to detect feebly ion-
644 izing particles such as mCPs, its has some but useful sensitivity for neutral
645 LLPs, s shown in Figure 22. It could in some circumstances provide a con-
646 firmation of a signal observed by FASER [12] or vica versa. We are currently
647 investigating the use of the Outrigger Detectors to enhance the sensitivity of
648 MAPP-1 to neutral LLPs.

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683 Appendix A Safety Derogation Request

EDMS 2631839 v.1 status Released access Restricted
 PDF from EDMS 2631839: MoEDAL_1841_derogation_material_lfre_v1.docx modified 2021-10-06 09:27



HSE
 Occupational Health & Safety
 and Environmental Protection Unit

Safety Derogation Request Form		
Date	Requested by	Dpt/Group
27 août 2021	MoEDAL- MAPP Experiment EP Safety Office	EP

DESCRIPTION OF THE REQUEST
<p>Location / Project : UA83</p>
<p>Regulation related to the derogation: Plastic materials needed for the MoEDAL Detector are not conforming to CERN IS41, and specifically needed due to their physical properties.</p>
<p>Brief description of the Detector : The MAPP detector is comprised of 400 x (10 cm x 10 cm x 75 cm) scintillator bars, wrapped in Tyvek and then black tape. Each bar is connected via a short light guide to a 3-inch PMT. The bars are arranged in 4 sections, each with 100 bars with overall sensitive area of 1m². The scintillator bars (NUVIA polystyrene based scintillator) in each section are held in a square array by three support grids made of High-Density Polyethylene (HDPE). A drawing of one of the basic HDPE support grids is shown in Figure 1. The grid separates the bars one from the other by 5m to 7 mm. The air fills the interspaces between the scintillator bars.</p>
<p style="text-align: center;">Figure 1: The drawing of one of 12 HDPE support grids of the MAPP-nOP detector.</p>

The weight of the scintillator in each section is supported by an aluminium T-bar support structure and a 0.5 cm aluminium plate that forms the base of each section. Additionally, each section is protected from the other by the lead-scintillator radiator plane that includes 2 x 1 mm of aluminium sheet and 5 x 2mm layers of lead. The active detector is completely encapsulated in VETO detectors comprised of 1 cm thick acrylic scintillator (Eljen-200 PVT based scintillator), with area roughly 30m². The above arrangement is shown in Figure 2. The support structures and metal plate elements are shown in blue. The HDPS support grids and metal support structures are further emphasized in Figure 3.

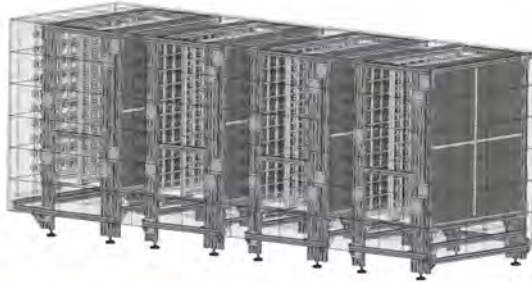


Figure 2: The basic structures of the MAPP-mQP with the outer VETO layer and the support structures emphasized.



Figure 3: The basic structures of the MAPP-mQP without the outer VETO layer, the support structures emphasized.

The MAPP detector and VETO layer are completely enclosed in the MAPP-mQP flame shield as shown in Figure 3. The size of the shield is roughly 1.3 x 1.5 x 4m. The flame-shield is fabricated out

of 1mm thick aluminium sheet and has a total area of $\sim 30 \text{ m}^2$. The aluminium encloses the plastic scintillator completely. There is no break in the flame shield for cable exit. The cables exit via a patch panel.



Figure 4 The flame shield around the MAPP-mQP detector

In order to provide a hermetic environment all joints in the flame shield are sealed using heavy duty aluminium tape shown in Figure 5. Any fires within the flame shield volume would be suppressed due to lack of oxygen. The slight electrical heating arising from the PMT bases within the volume of the flame shield – the only electrical elements in the region – amounts to a few hundred Watts that is dissipated by conduction and radiation from the flame shield surface

The foreseen location in UA83 is shown in Figure 5 and Figure 6 here below.



Figure 5: Proposed location in UA83



Figure 6: Proposed layout of the MAPP-mQP setup in UA83.

Further details on the materials used and other cases of applications at CERN are available in the document: **"Information Relating to Safety of the MAPP Detector With Respect to Flammability"** From J.Pinfold, available in this same EDMS node.

Further details on the installation in the UA83 are given in the ECR "LHC-X8MAPP-EC-0001 MoEDAL MAPP mQP detector in UA83" (EDM5 2617044).

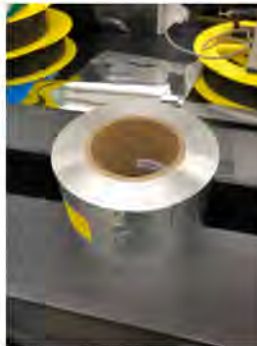


Figure 7 Heavy duty aluminium tape (0.25 mm thick) used to seal the flame shield

Gap compared with the reference regulation

Description:

Materials specifically needed for the MoEDAL Detector in virtue of their physical properties are not conforming to CERN IS 41:

Polystyrene (PS)

https://edms.cern.ch/ui/file/2631839/1/Polystyrene_Material_Data_Sheet-AMCRYS.pdf



High Density Polyethylene (HDPE) https://edms.cern.ch/uj/file/2631839/1/Recycled_HDPE_Material_Safety_Data_Sheet.pdf	
Polyvinyl Toluene (PVT) https://edms.cern.ch/uj/file/2631839/1/EJ-200-SDS_PVT_Material_Safety_Data_Sheet.pdf	
<u>Cause and justification of the gap:</u> PS is required for the operation of scintillation detectors in order to perform physics in MoEDAL Experiment	
Quantity : (kg or m ³) 3,000 kgs of PS HDPE 326kg PVT 406kg	Dimensions : (length, width, diameter, thickness): PS: 10 x 10 x 75 cm / 100 units x 4 HDPE: support spacers grids --various measures described in Figure 1. PVT: set of plates, 1cm thick, total 30m ²
Ignition sources: Low Voltage circuitry Distance to the nearest external powered system: An uninterruptible power supply, part of other LHC equipment, is at a distance ~1.5 m	
Are there other previous derogation requests for the equipment/building/installation...? (Not for this installation (A previous derogation has been made for MoEDAL in UX85 EDM5 893563))	
What are the alternatives that have been investigated and why were they not put into place ? The scintillators for the detector are housed within a flame-resistant metal casing, to prevent the propagation of fire. This mitigation is considered in the context of the derogation request required from HSE. This measure is integral to the detector and does not require any external mitigation measures. The material properties of PS are required for scintillator detectors of this type, no other alternative is possible.	
Documents provided by the requestor: Click or tap here to enter text.	

APPLICABLE SAFETY DOMAIN		
<i>(a single domain per derogation)</i>		
<input type="checkbox"/> Mechanical (pressure, lifting, machines, HVAC...) <input type="checkbox"/> Cryogenics <input type="checkbox"/> Structural, civil engineering <input checked="" type="checkbox"/> Fire Safety <input type="checkbox"/> Chemical	<input type="checkbox"/> Workplace <input type="checkbox"/> Flammable gas <input type="checkbox"/> DDH <input type="checkbox"/> Electrical <input type="checkbox"/> Noise	<input type="checkbox"/> Non-ionising radiation <input type="checkbox"/> Environmental protection <input type="checkbox"/> Others: <input type="checkbox"/> Click or tap here to enter text.



SPECIALIST OPINION	
Specialist: Fabio CORSANÉGO HSE-DHS-IB Jonathan Guillely HSE-DHS-PE	
Specialist opinion: Acceptable with the conditions agreed here below	
Compensatory measures defined in collaboration with the requestor: <i>safeguards: hardware/software interlocks</i> power supplies are low voltage (24V), are current and temperature limited (turn off when current or temperature goes out of range) and provide an alarm signal when current or voltage moves out of some predefined <i>operating window</i> . <i>handover of alarms generated by the system</i> Three types of warning/alarm information will be provided to the CCC: <ol style="list-style-type: none">1) The current/voltage and temperature readings/alarms from the power supplies,2) The hermetic metal flame shield is monitored by temperature sensors placed on the outside of the shield. The output of these temperature sensors will also be provided to the CCC,3) There is a plan (not yet confirmed) to monitor the detectors + electronics with an IR camera whose output is provided to the CCC. <i>Other safeguards:</i> <ol style="list-style-type: none">1) The power supplies, readout electronics and other non MoEDAL live equipment present in UA83 are separated by a distance of 1,5 m from the detector,2) The only entities that use power in the detector volume are PMT bases. Power supplied to the bases is LV and only stopped up in the base,3) The detector volume is completely encased in a hermetic (sealed to exclude air movement) flame shield. Cables enter the volume via a patch panel. Metal planes separate each of the four compartments of the detector. A strong metal plate forms the base of the scintillator bar compartments.	
Conditions for the validity of the derogation : <input type="checkbox"/> Temporary derogation - expiry date : Click on the document number <input checked="" type="checkbox"/> Permanent derogation	
Description of the conditions for retaining validity: Observance of the conditions defined in this document	
Documents applicable to the reply:	

TRACEABILITY
Reference and version EDMS : https://edms.cern.ch/document/2531839/1

STATUS OF THE DEROGATION
See EDMS

Appendix B Safety Data Sheet for Acrylic Plastic

Acrylite Acrylic Material Safety Data Sheet

1. Chemical Product and Company Identification

ACRYLITE® FF Acrylic Sheet

Supplier:
A & C Plastics, Inc.
6135 Northdale
Houston, TX 77087-5095

Product Information Number 1-207-490-4242
24 Hour Emergency Number, CHEMTREC 1-800-424-9300

® is a registered trademark

Product Use: building glazing, light advertising, furniture, trade-fair booth design, displays, decoration, industrial Use

2. Composition/Information on Ingredients

This material is classified as not hazardous under OSHA regulations.

<u>Ingredients</u>	<u>CAS Reg. No.</u>	<u>Weight %</u>
acrylic copolymer	trade secret	100

NJTSR # 56705700001-6897 P

See Section 8, Exposure Controls/Personal Protection

3. Hazards Identification

Emergency Overview

Color: colorless or colored
Appearance: solid in various forms
Odor: odorless

Under normal conditions of use, this product is not expected to create any unusual industrial hazards.

Primary Routes of Exposure

Eye contact (if exposed to chips)

Potential Health Effects

Inhalation

No hazard expected in normal use.

Eye Contact

No hazard expected in normal use.
Material can cause the following:
- mechanical irritation



Acrylite Acrylic Material Safety Data Sheet

Skin Contact

Material can cause the following:
- cuts (when using cut sheets)

Ingestion

No hazard expected in normal use.

Potential Environmental Effects

See SECTION 12, Ecological Information

4. First Aid Measures

First Aid Procedures

Inhalation

No specific treatment is necessary since this material is not likely to be hazardous by inhalation.

Eye Contact

If mechanical irritation occurs flush eyes thoroughly with a large amount of water, consult a physician if irritation persists. (possible during machining processes)

Skin Contact

No specific treatment is necessary since this material is not likely to be hazardous.

Ingestion

Ingestion is not considered a potential route of exposure.

5. Fire-Fighting Measures

Flash point	> 250 °C (ASTM D1929-68) > 482 °F (ASTM D1929-68)
Autoignition Temperature	> 400 °C (ASTM D1929-68) > 752 °F (ASTM D1929-68)
Lower explosion limit	not applicable
Upper explosion limit	not applicable
OSHA Flammability Classification	none

Other Flammable Properties

Use water spray to cool containers exposed to fire.

Extinguishing Media

Use the following extinguishing media when fighting fires involving this material:
water spray - foam - dry chemical - carbon dioxide

Fire Fighting Procedures

As in any fire, wear self-contained breathing apparatus pressure-demand, MSHA/NIOSH (approved or equivalent) and full protective gear.



Acrylite Acrylic Material Safety Data Sheet

6. Accidental Release Measures

Procedures

Collect material and place in a disposal container. Obey relevant local, state, provincial and federal laws and regulations.

See Material Safety Data Sheet section 8, Exposure Controls/Personal Protection.

7. Handling and Storage

Handling

During thermal processing and/or machining local exhaust ventilation at processing machines is necessary.

Storage

Storage: dry.

8. Exposure Controls/Personal Protection

Exposure Limit Information

ACRYLIC COPOLYMER

trade secret

No Occupational Exposure Values established (ACGIH, OSHA, Canada and Mexico).

Engineering Controls (Ventilation)

If use operations generate dust, use adequate ventilation.

Respiratory Protection

A respiratory protection program meeting OSHA 1910.134 and ANSI Z88.2 requirements must be followed whenever workplace conditions warrant a respirator's use.

Eye Protection

goggles for machining operations

Hand Protection

protective gloves against mechanical risks

Other Protective Equipment

To identify additional Personal Protective Equipment (PPE) requirements, it is recommended that a hazard assessment in accordance with the OSHA PPE Standard (29CFR1910.132) be conducted before using this product.

9. Physical and Chemical Properties

Appearance	colorless or colored
Physical state	solid in various forms
Odor	odorless
Flash point	> 250 °C (ASTM D1929-68) > 482 °F (ASTM D1929-68)
pH-value	not applicable



Acrylite Acrylic Material Safety Data Sheet

Viscosity (dynamic)	not applicable
Specific gravity (water = 1)	1.19 g/cm ³ at 20 °C / 68 °F
Vapor density (air = 1)	not applicable
Vapor pressure	not applicable
Softening Temperature	approx. 102 °C / 216 °F
Boiling Temperature	not applicable
Solubility in water	insoluble
n-Octanol/water partition coefficient	not applicable
Evaporation rate	not applicable
Odor threshold	not available
Further information	none
See Section 5, Fire Fighting Measures	

10. Stability and Reactivity

Stability

This product is stable under normal storage conditions.

Conditions To Avoid

This material is considered stable.

Incompatibility With Other Materials

Oxidizing agents. No known incompatibility with other materials.

Hazardous Decomposition Products

In case of thermal decomposition, combustible vapours are formed, which are irritating to eyes and respiratory system, mainly consisting of methyl methacrylate

Hazardous Polymerization

Product will not undergo polymerization.

11. Toxicological Information

Further Information on Toxicology

The product has not been tested toxicologically. When handled and used as directed the product will not cause hazardous effects to health according to studies on similar products and practical experience.

12. Ecological Information

Information on Elimination (Persistence and Degradability)

Ecotoxicological Effect

Further information on Ecology

The product has not been tested ecotoxicologically.

On the basis of the products consistency as well as its low water solubility a bio availability is unlikely. Studies on products with similar composition confirm this assumption.

Acrylite Acrylic Material Safety Data Sheet

13. Disposal Considerations

Procedures

Waste must be disposed of in accordance with federal, state and local regulations. Incineration is the preferred method. A & C Plastics encourages the recycle, recovery and reuse of materials, where permitted, as an alternate to disposal as a waste.

14. Transport Information

Further information

Not subject to the regulations on dangerous goods.

15. Regulatory Information

INVENTORY INFORMATION

EINECS (EU)	listed or exempted listed or exempted listed or exempted
TSCA (USA)	
DSL (CDN)	

US FEDERAL REGULATORY INFORMATION

Component / CASRN	TPQ (lbs)	CECLARQ (lbs) (40CFR302.4)	SARA 302 List of EHS	SARA 313 (40CFR172)	TSCA 12b)
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NONE

COMPONENT CLASSIFICATION UNDER CLEAN AIR ACT SECTION 112

Component / CASRN	Weight %	HAP	EHAP
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NONE

PRODUCT CLASSIFICATION UNDER SECTION 311/312 OF SARA (40CFR370)

NONE

US STATE REGULATORY INFORMATION

Component / CASRN	New Jersey RTK	Pennsylvania RTK	Massachusetts RTK	California Proposition 65 Cancer	California Proposition 65 Reproductive
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acrylic polymer / Trade secret	NO	NO	NO	NO	NO
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This product contains (a) chemical(s) known to the State of California to cause cancer and birth defects or other reproductive harm.

Acrylite Acrylic Material Safety Data Sheet

CANADIAN REGULATION

This product has been classified in accordance with the hazard criteria of the Controlled Products Regulation and the MSDS contains all information required by the Controlled Products Regulations.

This is a non-controlled product.
WHMIS: NO

Component / CASRN _____ NPRI _____

NONE

16. Other Information

	Health	Flammability	Physical Hazard
HMIS-Ratings	0	1	0
NFPA-Ratings	0	1	0

HMIS Hazard Ratings

4 = severe
3 = serious
2 = moderate
1 = slight
0 = minimal
N = no rating for powders
* = chronic health hazard

NFPA Hazard Ratings

4 = extreme
3 = high
2 = moderate
1 = slight
0 = insignificant
N = no rating for powders

This MSDS was prepared in accordance with ANSI Z400.1-1998.

Places marked by || have been amended from the last version.

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