

# First elements towards a two dimensional model of field quality in MCBXF

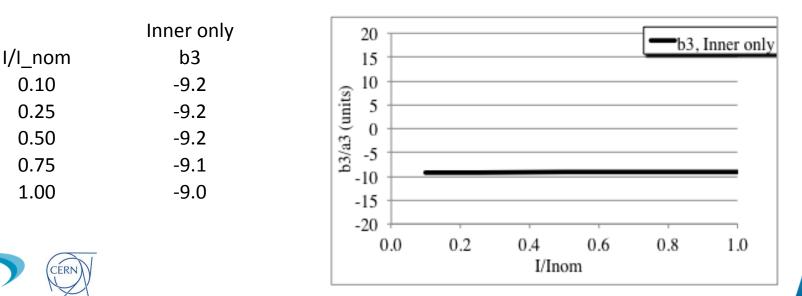
E. Todesco, F. Toral, J. Garcia Matos, J. C. Perez



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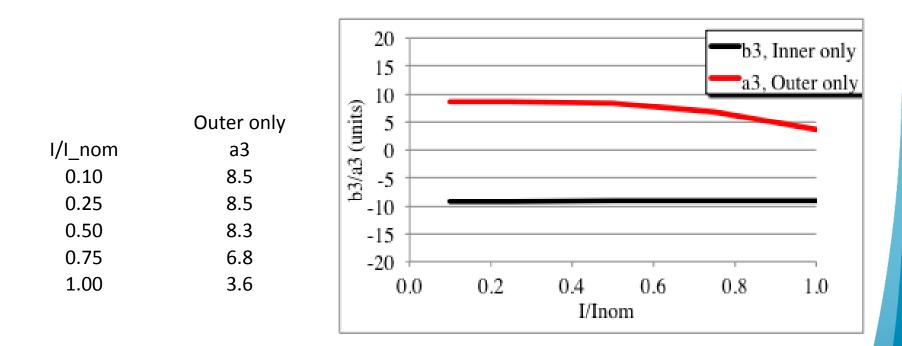
# SIMULATION RESULTS

- The main critical nonlinear components in MCBXF are b<sub>3</sub> and a<sub>3</sub>
  - Normalization is done with respect to (x,y) coordinate system, first allowed given by inner dipole is b3, and of the outer dipole is a3
  - MCBXFA and MCBXFB have similar field quality features
- For the inner dipole the iron is quite far and therefore saturation is negligible in single powering mode
  - The geometric can change as an offset according to the shimming



## SIMULATION RESULTS

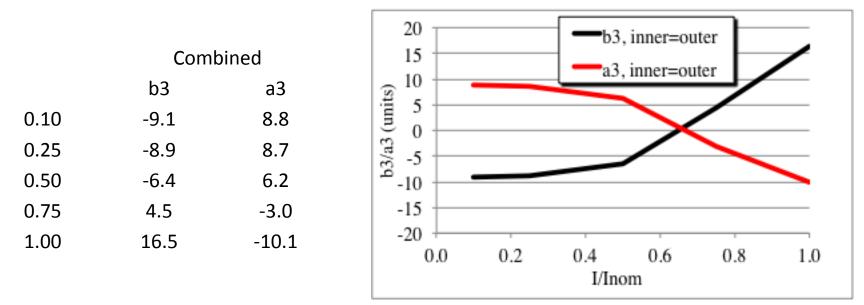
- For the outer dipole the iron is closer and therefore saturation induces a change of a<sub>3</sub> of -5 units
  - The geometric can change as an offset according to the shimming





# SIMULATION RESULTS

- In combined powering saturation strongly affects both b<sub>3</sub> (+25 units) and a<sub>3</sub> (-20 units)
  - The geometric can change as an offset according to the shimming
  - The change due to saturation begins at 50% of nominal current



 We are planning to have simulations also on the loadlines with ratio 0.5 and 2 between inner dipole and outer dipole integrated field

# TUNING POSSIBILITIES

- The geometric in the nominal design is placed at -10 units
  (b<sub>3</sub>) and +10 units (a<sub>3</sub>) to minimize the impact of saturation
  - Our initial specification were a window of ±20 units recent work by Frederick and Massimo shows that 20 units could affect dynamic aperture
- We can change the geometric b<sub>3</sub> and a<sub>3</sub> by changing the midplane/pole shim of inner and outer
  - Two free parameters for optimizing preload and a3 or b3 but also the shimming in the heads is essential, so there is not a total freedom



## A POSSIBLE MODEL

- One should find suitable forms for the functions
  - $a_3 = a_3(f; \alpha)$
  - $b_3 = b_3(f;\alpha)$
  - The functional fit should use the *erf* as done in Fidel (but this is a three parameter fit ...)
  - A simple  $a_3 = a_{3geo} + a_{3sat} * f^n$  could also be a good approximation, but it is not clear how  $a_{3sat}$  depends on  $\alpha$
- Where f is the ratio current/nominal current and r is the angle of the loadline
  - $\alpha = 0$  for inner only
  - $\alpha$ =90 for outer only
  - α=45 for inner dipole intergrated field=outer dipole integrated field



#### A POSSIBLE MODEL

- Another option could be have a table of values and interpolate linearly in between
- A feedback is needed on the best way to proceed

It would be interesting to run a sensitivity analysis on b<sub>3</sub>/a<sub>3</sub> versus dynamic aperture (maybe with nominal field and half field), so that we know what are the limits

