

DE LA RECHERCHE À L'INDUSTRIE

cea



Conceptual Design Review of R2D2

1

- Introduction -

<https://indico.cern.ch/event/1003865/>

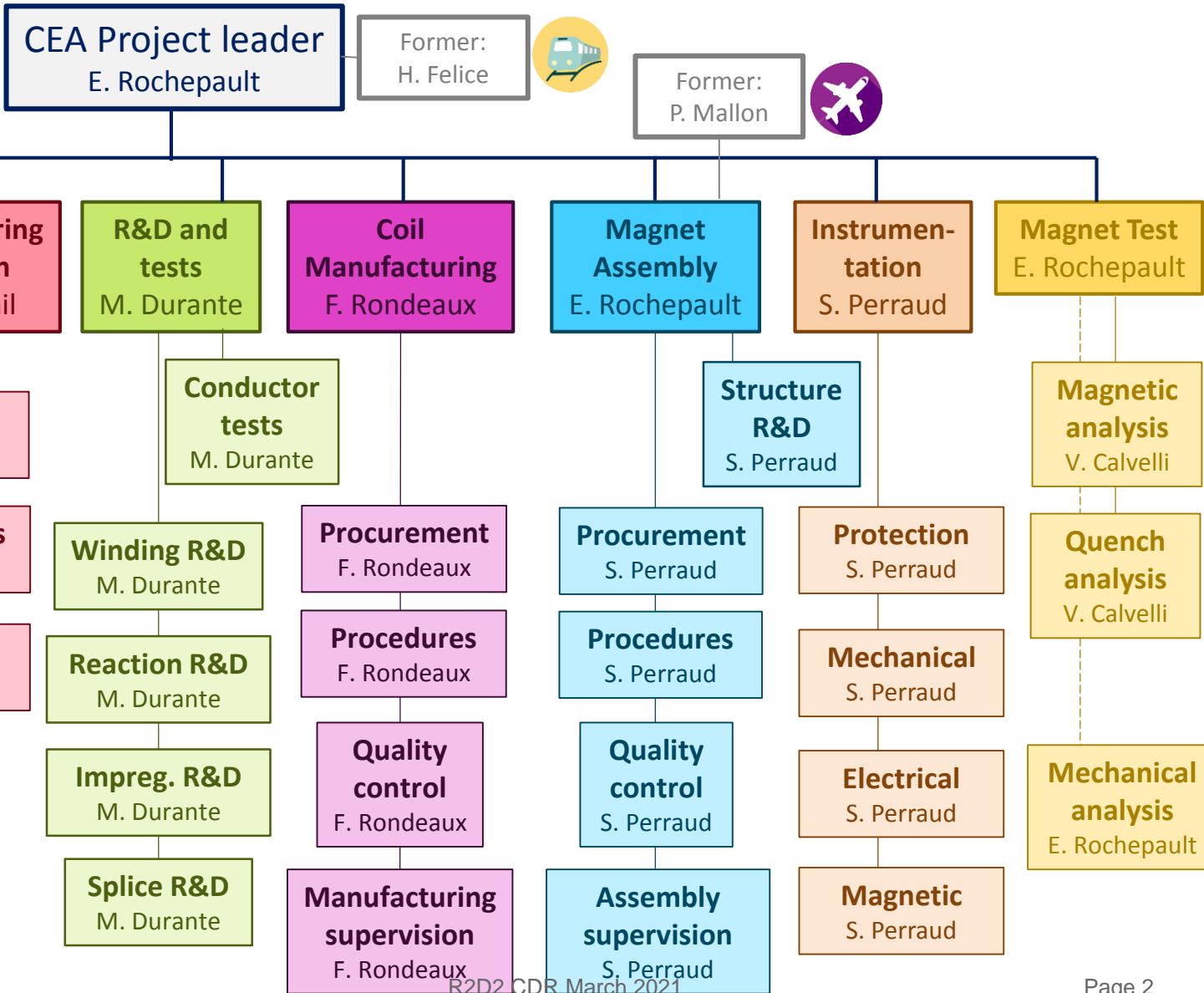


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CEA: E. Rochepault, V. Calvelli, M. Durante, H. Felice,
P. Mallon, P. Manil, G. Minier, G. Maitre, B. Prevet, S.
Perraud, F. Rondeaux

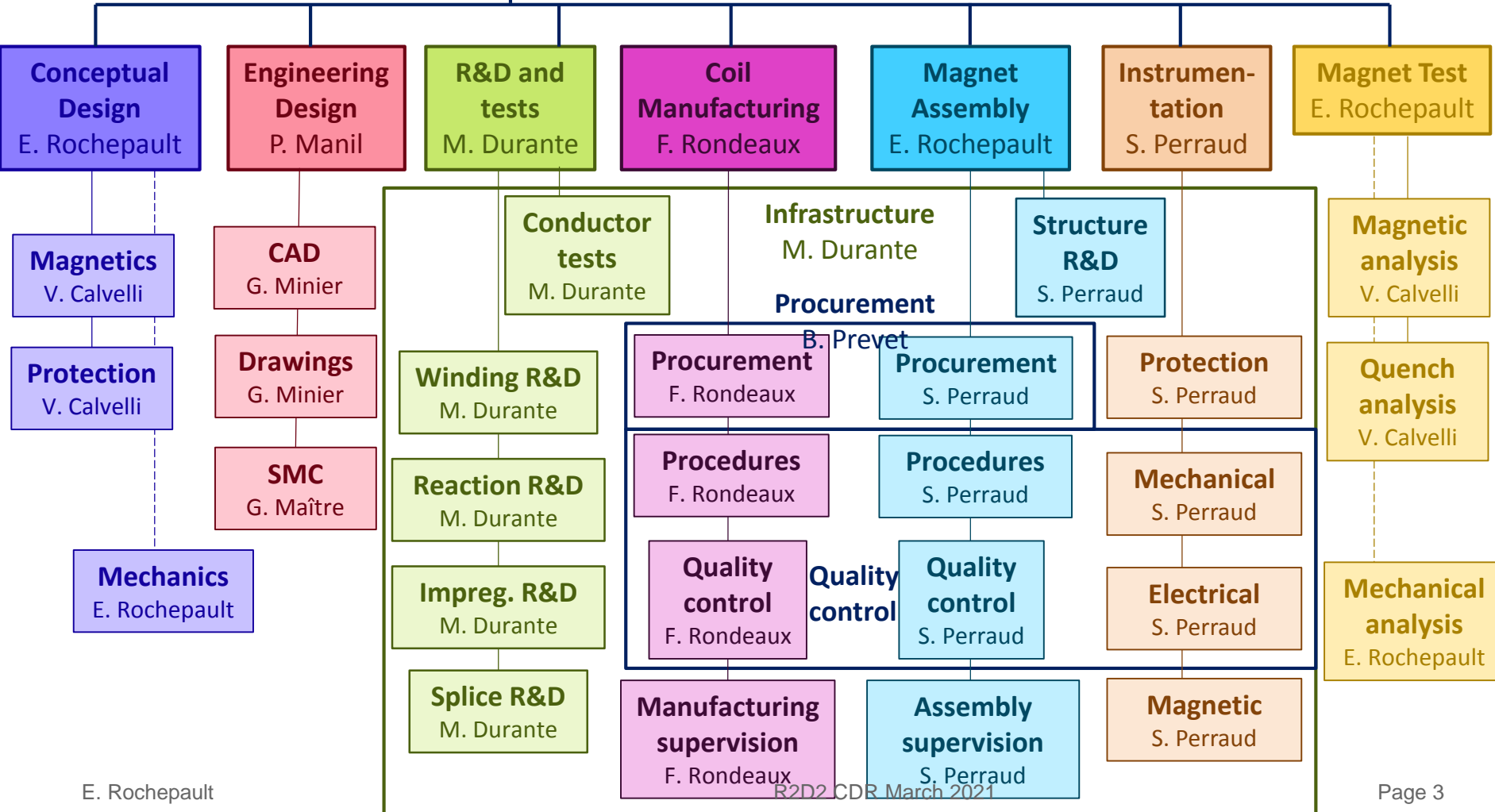
CERN: S. Izquierdo Bermudez, J.C. Perez, D.
Tommasini, J. Fleiter, H. Felice

08/03/2021

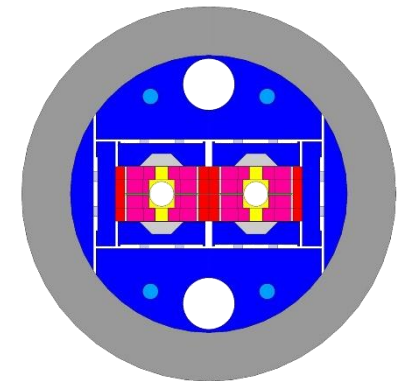


CEA Project leader
E. Rochepault

CERN collaboration: Steering, technical support, conductor, tests...

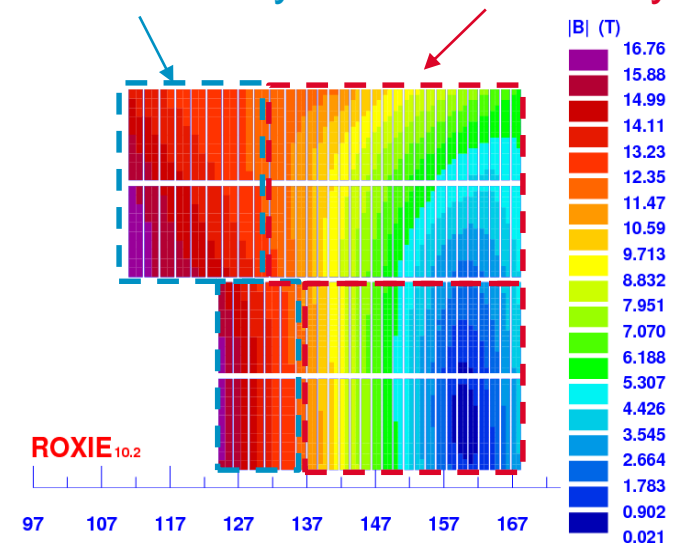


- Starting point: **block-coil option for FCC**
 - 16 T \rightarrow max. achievable field
 - Graded coils \rightarrow most compact possible
 - High-Jc cables
 - Double aperture \rightarrow accelerator type
 - Conceptual design
- CEA-CERN collaboration:
 - Probe the **16 T limit**
 - Test grading** in block-coils
 - State-of-the-art cables
 - develop and build** a demonstrator
 - Single aperture
 - Short models



High Field "HF"
blocks, low
current density

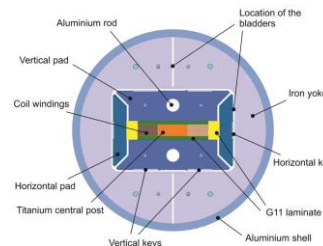
Low Field "LF"
blocks, high
current density



1. SMC 11T (=Short Model Coil)

Racetrack coils

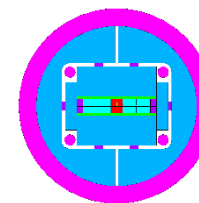
No grading → **Demonstrate field ≥ 12 T**



+Grading

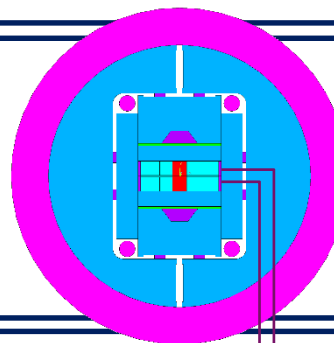
2. R2D2 (=Research Racetrack Dipole Demonstrator)

Racetrack + **Grading** = 12 T



3. FD (=Flared Dipole)

Grading + **Flared-end coils** ≥ 14 T

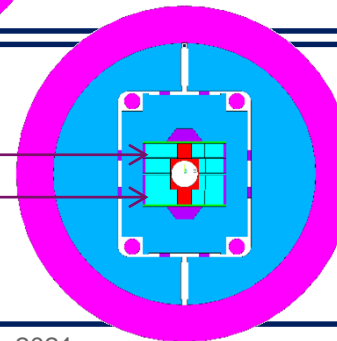


+Flared ends

4. F2D2 (=FCC Flared-ends Dipole Demonstrator)

Reuse FD coils + structure

Grading + Flared-end coils + **Aperture** = 16 T

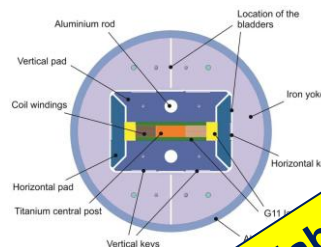


+Aperture

1. SMC 11T (=Short Model Coil)

Racetrack coils

No grading → **Demonstrate field ≥ 12 T**

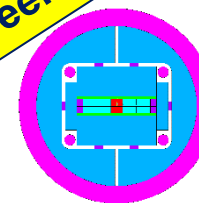


Current collaboration agreement

+Grading

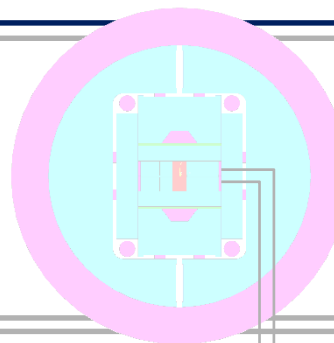
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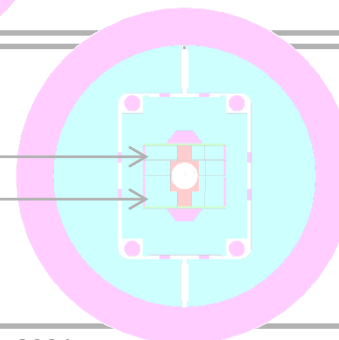


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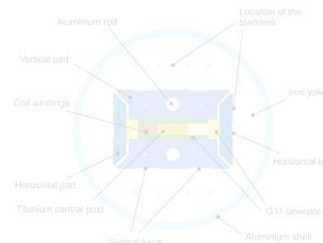


+Aperture

1. SMC 11T (=Short Model Coil) [10]

Racetrack coils

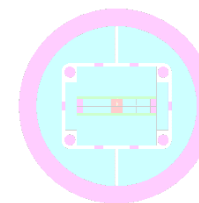
No grading → **Demonstrate field ≥ 12 T**



+Grading

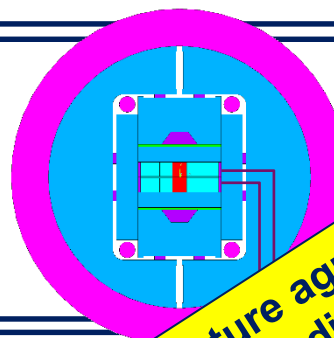
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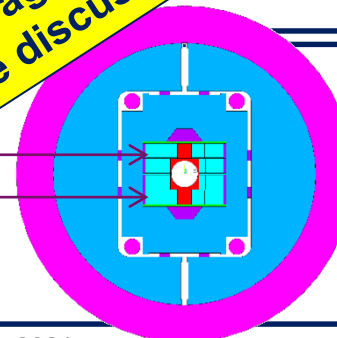


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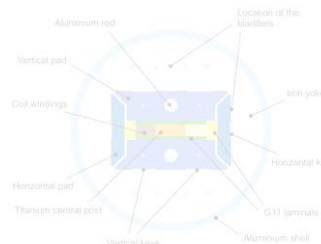
+Aperture

Future agreement to be discussed

1. SMC 11T (=Short Model Coil) [10]

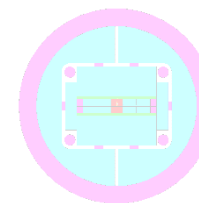
Racetrack coils

No grading → **Demonstrate field ≥ 12 T**



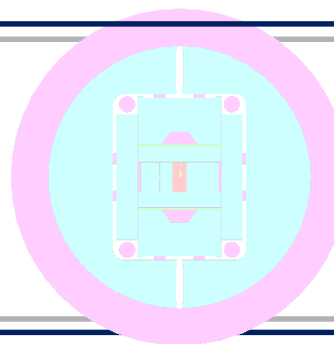
2. R2D2 (=Research Racetrack Dipole Demonstrator)

Racetrack + **Grading** = 12 T



3. FD (=Flared Dipole)

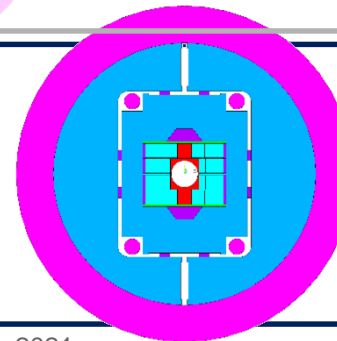
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Reuse FD coils + structure

Grading + Flared-end coils + **Aperture** = 16 T

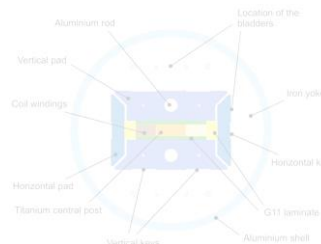


**First part
of this talk**

1. SMC 11T (=Short Model Coil) [10]

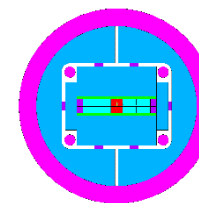
Racetrack coils

No grading → **Demonstrate field ≥ 12 T**



2. R2D2 (=Research Racetrack Dipole Demonstrator)

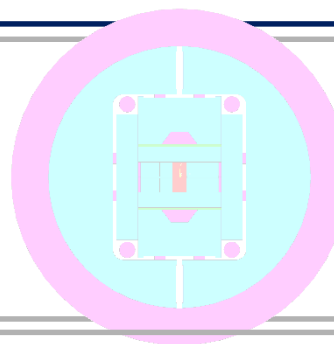
Racetrack + **Grading = 12 T**



Focus of the CDR

3. FD (=Flared Dipole)

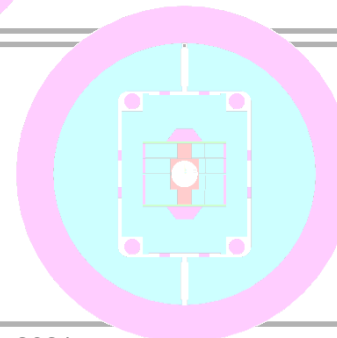
Grading + **Flared-end coils ≥ 14 T**



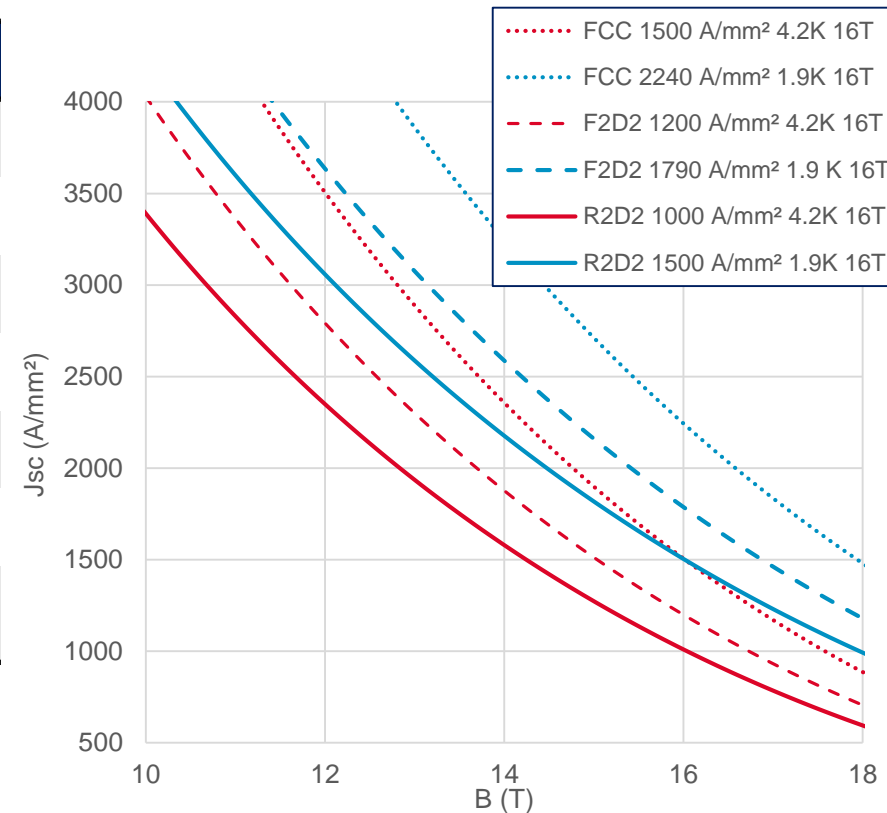
4. F2D2 (=FCC Flared-ends Dipole Demonstrator)

Reuse FD coils + structure

Grading + Flared-end coils + **Aperture = 16 T**



Expected Parameters	HF	LF
# strands	21	34
∅ strands	1.1 mm	0.7 mm
Pitch angle	16.5 deg	16.5 deg
Transposition pitch	85.0 mm	85.0 mm
Cu/Sc ratio	0.8	2
Insulation	0.15 mm	0.15 mm
Expected Dimensions (reacted & insulated)	2.36 x 13.04 mm	1.61 x 13.04 mm



- Cu cables expected T1 2021
- LF cable very similar to the 11-T cable
- HF cable new, 1.1 mm strand
- risk of changes in dimensions, mitigated with dimensional margins (see 4, P. Manil)
- J_c and RRR extrapolated
- risks of impact on the design, mitigated with design margins (see 2, V. Calvelli)

- 16 T target for FCC [1], proposed strategy:

1. Rely on proven technology [2]:

- State-of-the-art cables
- Block-coils
- Bladders and keys

→ Concepts proposed within EuroCirCol [3]

2. Develop grading:

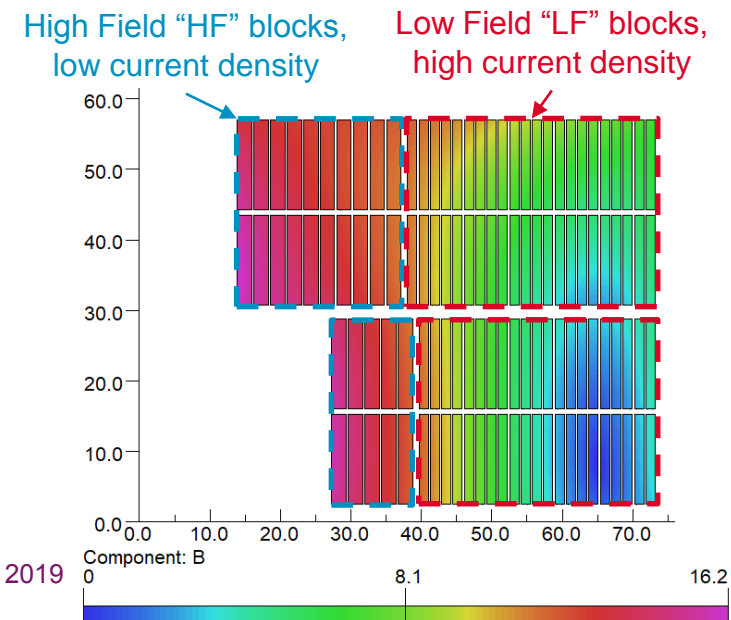
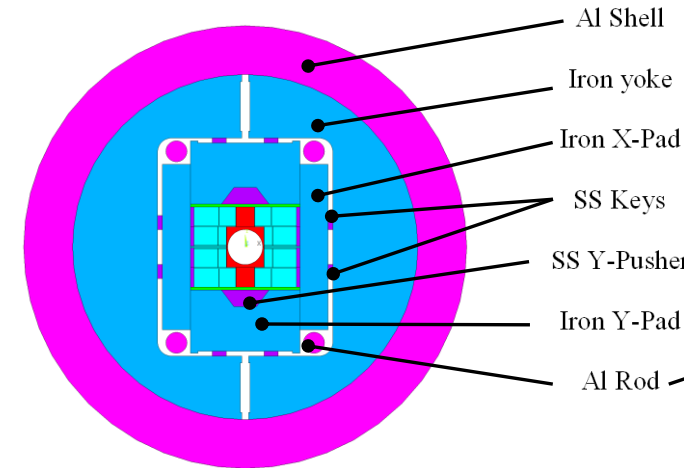
- Compact, high current density

3. Build and test a short model [4]

- CERN-CEA collaboration

→ Design/fabrication at CEA

→ Test at CERN



[1] D. Schoerling et al., "The 16 T Dipole Development Program for FCC and HE-LHC", IEEE TAS, 2019

[2] Plenary H. Felice, MT26: "Advances in Nb3Sn Superconducting Accelerator Magnets"

[3] M. Segreti et al., "2D and 3D Design of the Block-coil Dipole Option for the Future Circular Collider", IEEE TAS, 2019

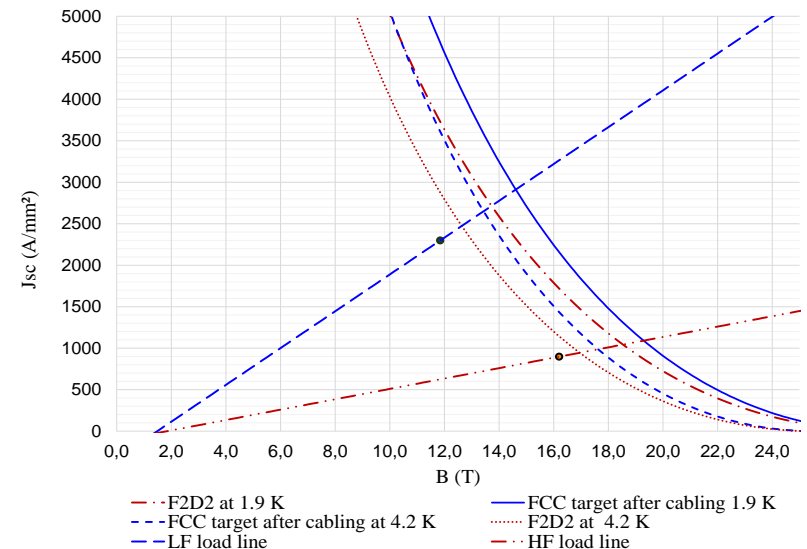
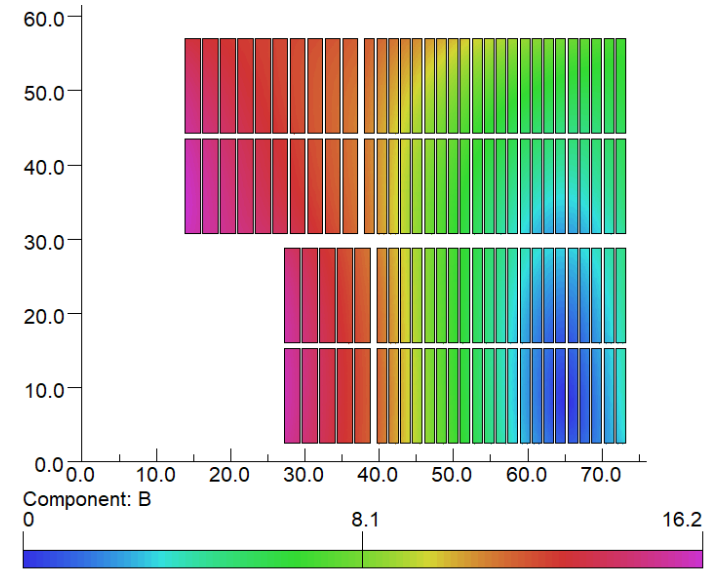
[4] H. Felice et al. "F2D2: a Block-coil Short Model Dipole Toward FCC", IEEE TAS, 2019

1. Maximize central field with margins:

- 15,5 T with available conductor (1200 A/mm² @ 16T, 4,2K)
- At least 14 % margin on the load-line
- Margins balanced HF/LF

V. Calvelli

Nominal Current I_{nom}	10378 A
Short sample current I_{ss}	12118 A
Bore field B_{y_0} at I_{nom} (I_{ss})	15.54 (17.81) T
Peak Field at I_{nom} (HF/LF)	16.20 / 11.85 T
Peak Field at I_{ss} (HF/LF)	18.58 / 13.62 T
Loadline Margin at I_{nom} (HF/LF)	14.0 / 15.4 %
Stored Energy I_{nom}	1.4 MJ/m



- EPFL-CERN Program: **R&D on internal joint** technologies [6]
 - Ultrasound (US), Soldering (CRS), Diffusion bonding (DB)
 - DB promising but: pressure required during heat treatment

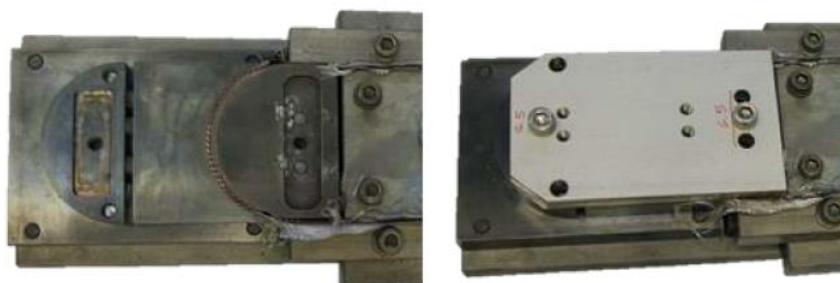
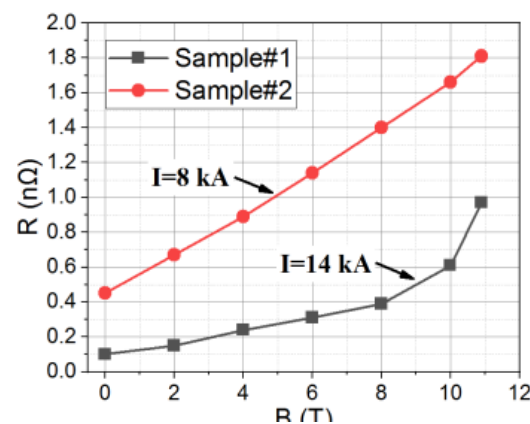
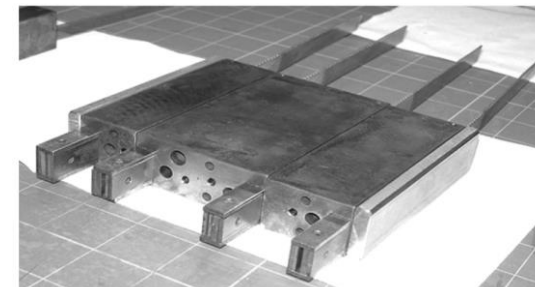
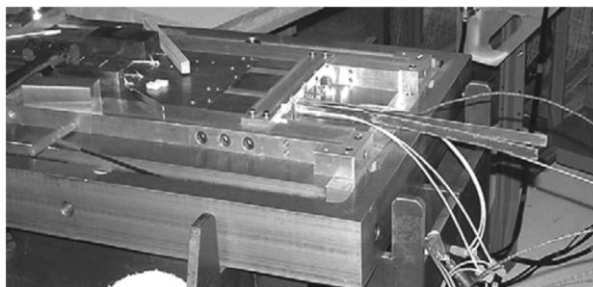
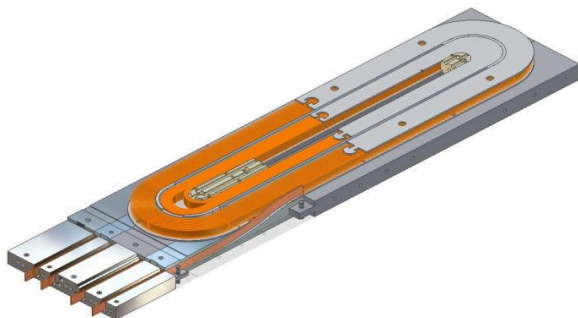


Figure 5. Sample#2 during the disassembly of the heat treatment sample holder and assembly of the test sample holder without manipulation of the components in contact with the splice.

Courtesy
V. D'Auria

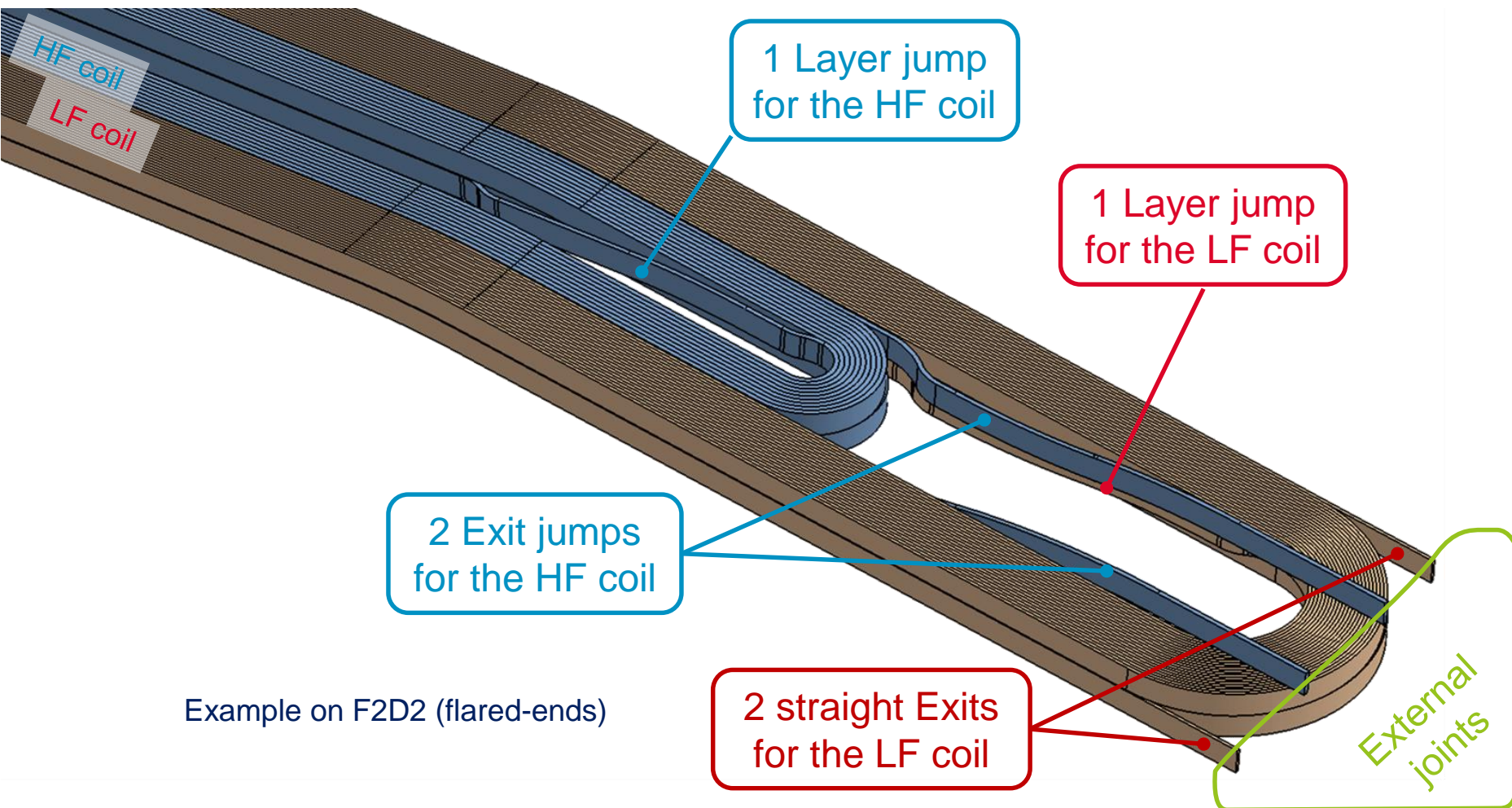


- TAMU magnets: grading with external splices



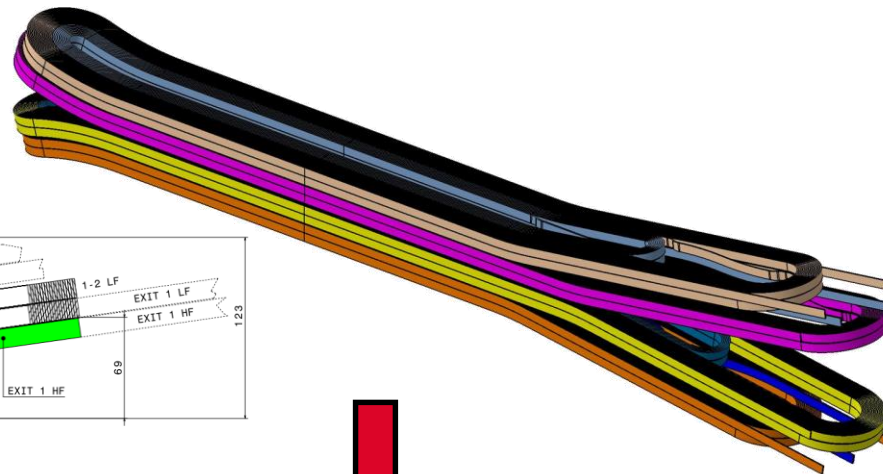
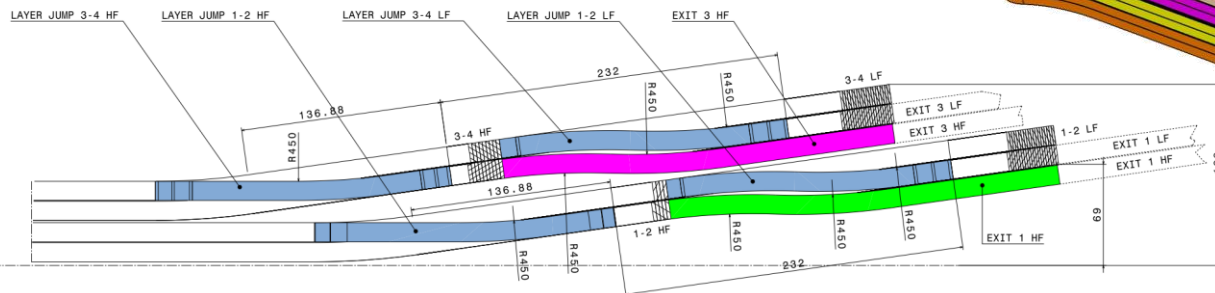
[6] V. D'Auria et al. "Progress on Tests on Splices between Nb₃Sn Rutherford Cables for Graded High-Field Accelerator Magnets", submitted to IEEE TAS
 [7] P. Noyes et al., "Construction of a Mirror-Configuration Stress-Managed Nb₃Sn Block-Coil Dipole", IEEE TAS 2006

- **CEA proposal: external joints** to better fit in schedule [4]
→ Possibility to implement internal joints in a second phase



Example on F2D2 (flared-ends)

1. Preliminary CAD model of the coils



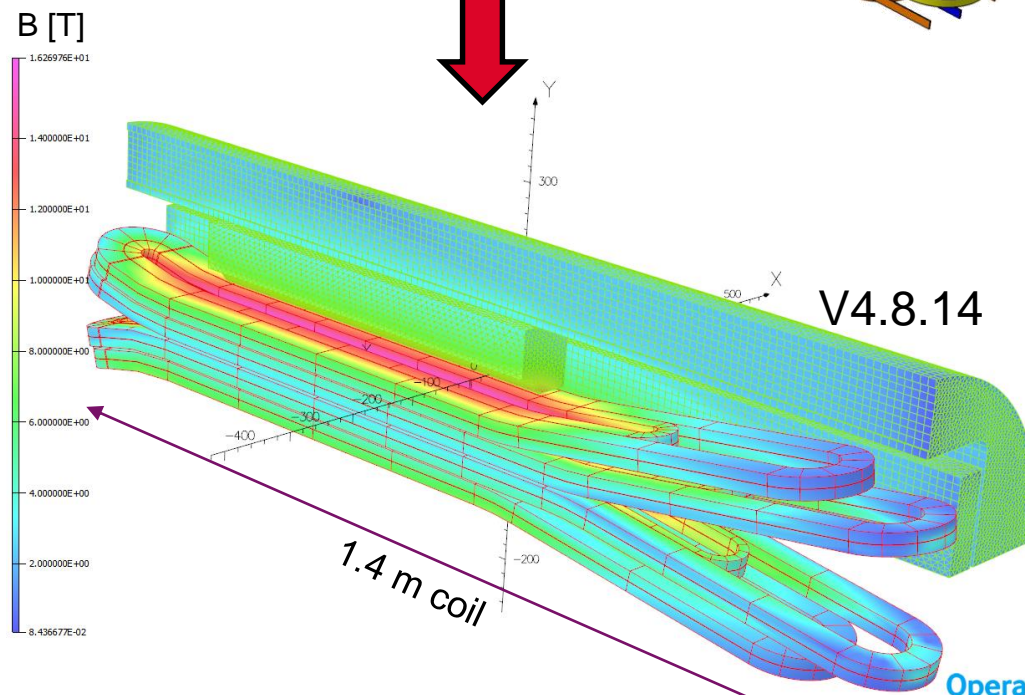
2. 3D simplified Opera FEM:

a. Central field:

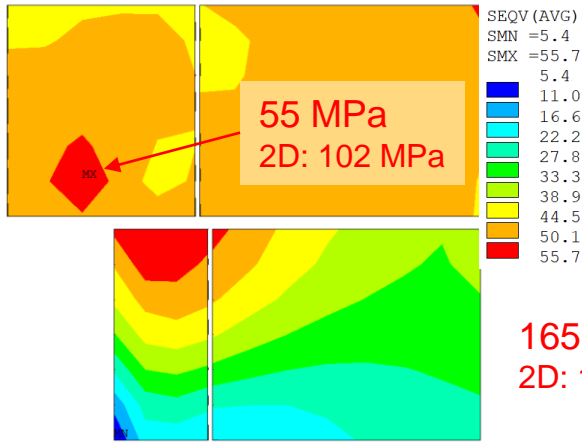
- Magnetic Length = 1042 mm
- Uniform field ($\pm 1\%$) = 249 mm

b. Field in critical areas:

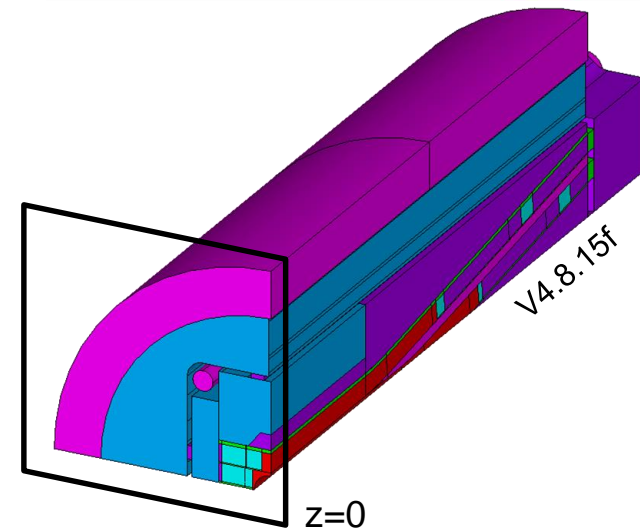
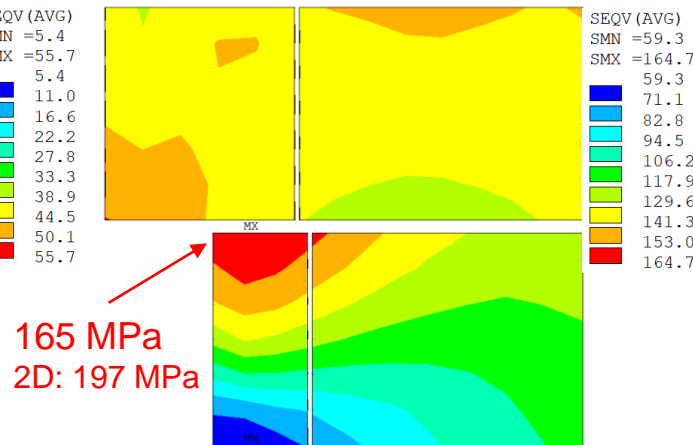
- ✓ **Field in the layer jumps < 14 T**
- Advantage of flared ends:
- ✓ **Peak field not in coil-ends**



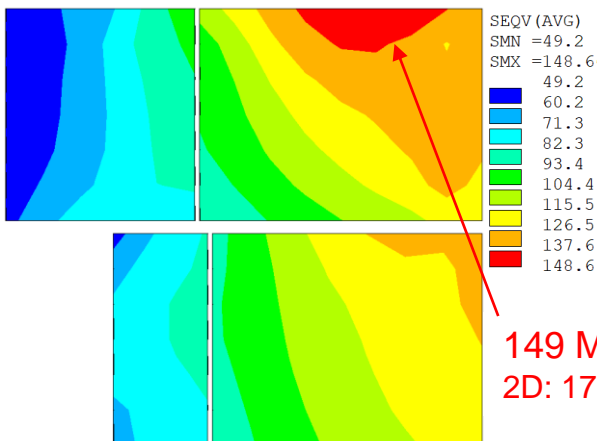
- 0.6 mm interference
 σ Von Mises [MPa]



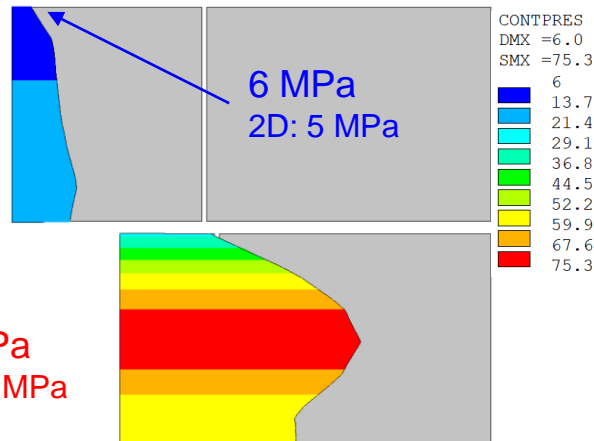
- 1.9 K
 σ Von Mises [MPa]



- Nominal operations: 10.4 kA, 14% margin, 15.5 T
 σ Von Mises [MPa]



- Contact pressure [MPa]



- Verified consistency with 2D model at z=0
- Coil peak stress within targets at z=0

- Next step: estimate stress-induced current limit with 3D stress [5]

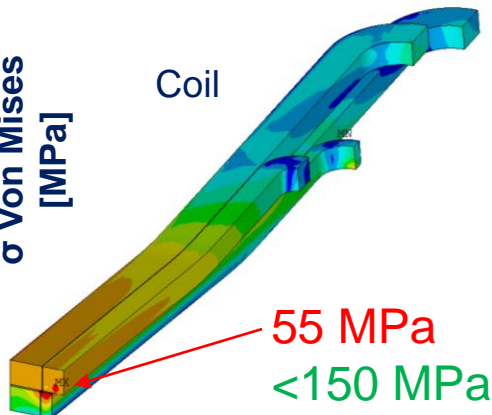
• 0.6 mm interference

• 1.9 K

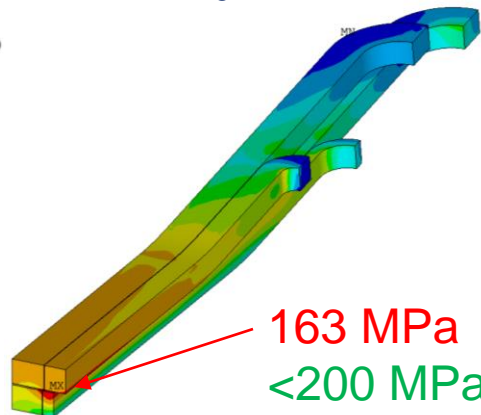
• 15.5 T

σ Von Mises [MPa]

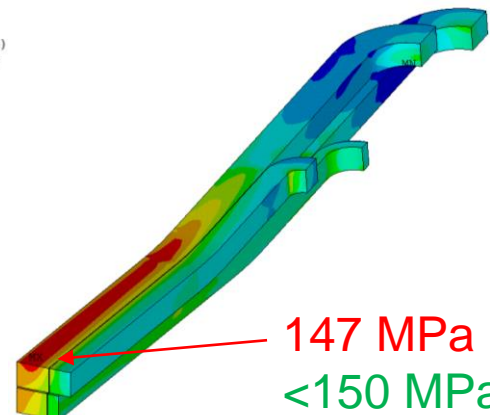
Coil



```
STEP=1
SUB =1
TIME=1
SEQV (AVG)
PowerGraphics
EFACET=1
AVRES=Mat
DMX =.157656
SMN =1.51076
SMX =55.0586
1.51076
7.46052
13.4103
19.36
25.3098
31.2596
37.2093
43.1591
49.1089
55.0586
```



```
STEP=2
SUB =1
TIME=2
SEQV (AVG)
PowerGraphics
EFACET=1
AVRES=Mat
DMX =2.22503
SMN =4.08463
SMX =163.46
4.08463
21.793
39.5014
57.2097
74.9181
92.6264
110.335
128.043
145.752
163.46
```

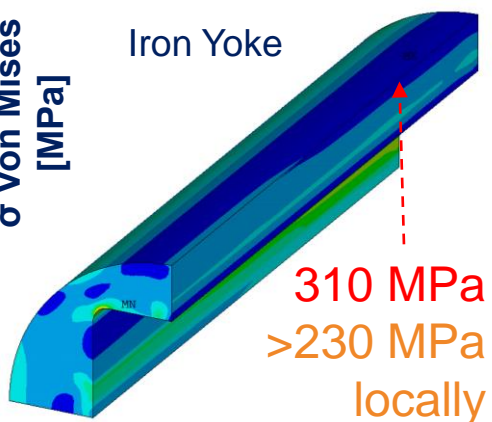


```
STEP=3
SUB =1
TIME=3
SEQV (AVG)
PowerGraphics
EFACET=1
AVRES=Mat
DMX =2.17473
SMN =6.42149
SMX =147.387
6.42149
22.0844
37.7472
53.4101
69.0729
84.7358
100.399
116.062
131.724
147.387
```

• 0.6 mm interference

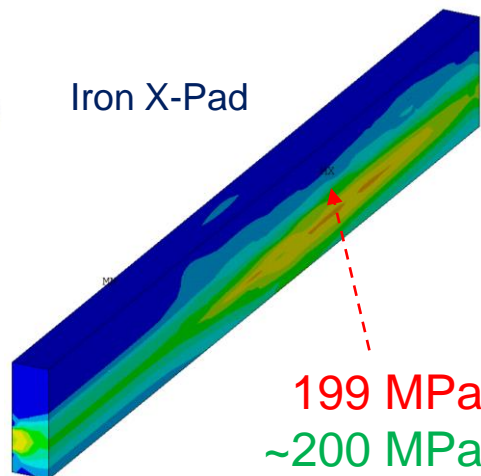
σ Von Mises [MPa]

Iron Yoke



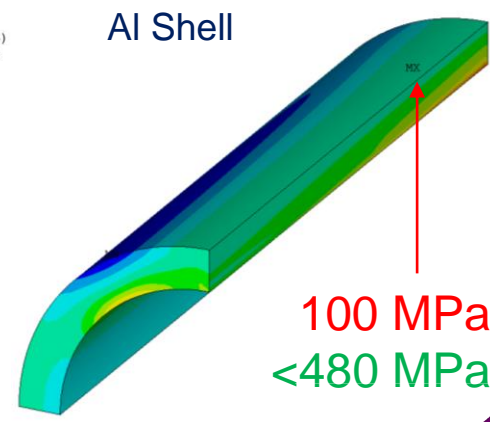
```
STEP=1
SUB =1
TIME=1
SEQV (AVG)
PowerGraphics
EFACET=1
AVRES=Mat
DMX =.546965
SMN =2.15664
SMX =310.116
2.15664
36.3743
70.592
104.81
139.027
173.245
207.463
241.68
275.898
310.116
```

Iron X-Pad



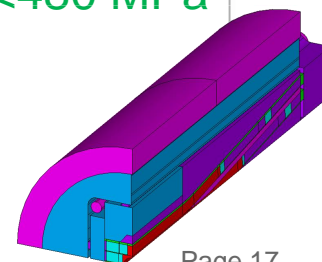
```
Build 19.0
NODAL SOLUTION
STEP=1
SUB =1
TIME=1
SEQV (AVG)
PowerGraphics
EFACET=1
AVRES=Mat
DMX =.187071
SMN =.384803
SMX =199.452
.384803
22.5034
44.622
66.7407
88.8593
110.978
133.096
155.215
177.334
199.452
```

Al Shell

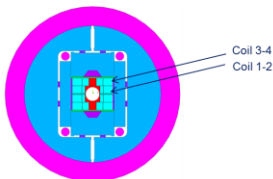


```
STEP=1
SUB =1
TIME=1
SEQV (AVG)
PowerGraphics
EFACET=1
AVRES=Mat
DMX =.525836
SMN =17.5058
SMX =100.518
17.5058
26.7293
35.9528
45.1764
54.3999
63.6234
72.8469
82.0705
91.294
100.518
```

- Peak stress in coil and critical components within targets
- Accepted local plasticization of the iron yoke



- CEA-RD-2.1: Demonstrator **conceptual design** (F2D2)
- CEA-RD-2.2: FD engineering design (F2D2 **partial assembly with coils 3-4 only**) + associated tooling
- CEA-RD-3.1: Fabrication of one Cu coil 3-4
- CEA-RD-3.2: Fabrication of one Nb₃Sn coil 3-4
- CEA-RD-4.1: Procurement and validation of the F2D2 support structure
- CEA-RD-4.2: Assembly of the Nb₃Sn coil with the Cu coil in a "FD" configuration (coils 3-4 at the right position + coils 1-2 filler) and delivery at CERN by end of 2021



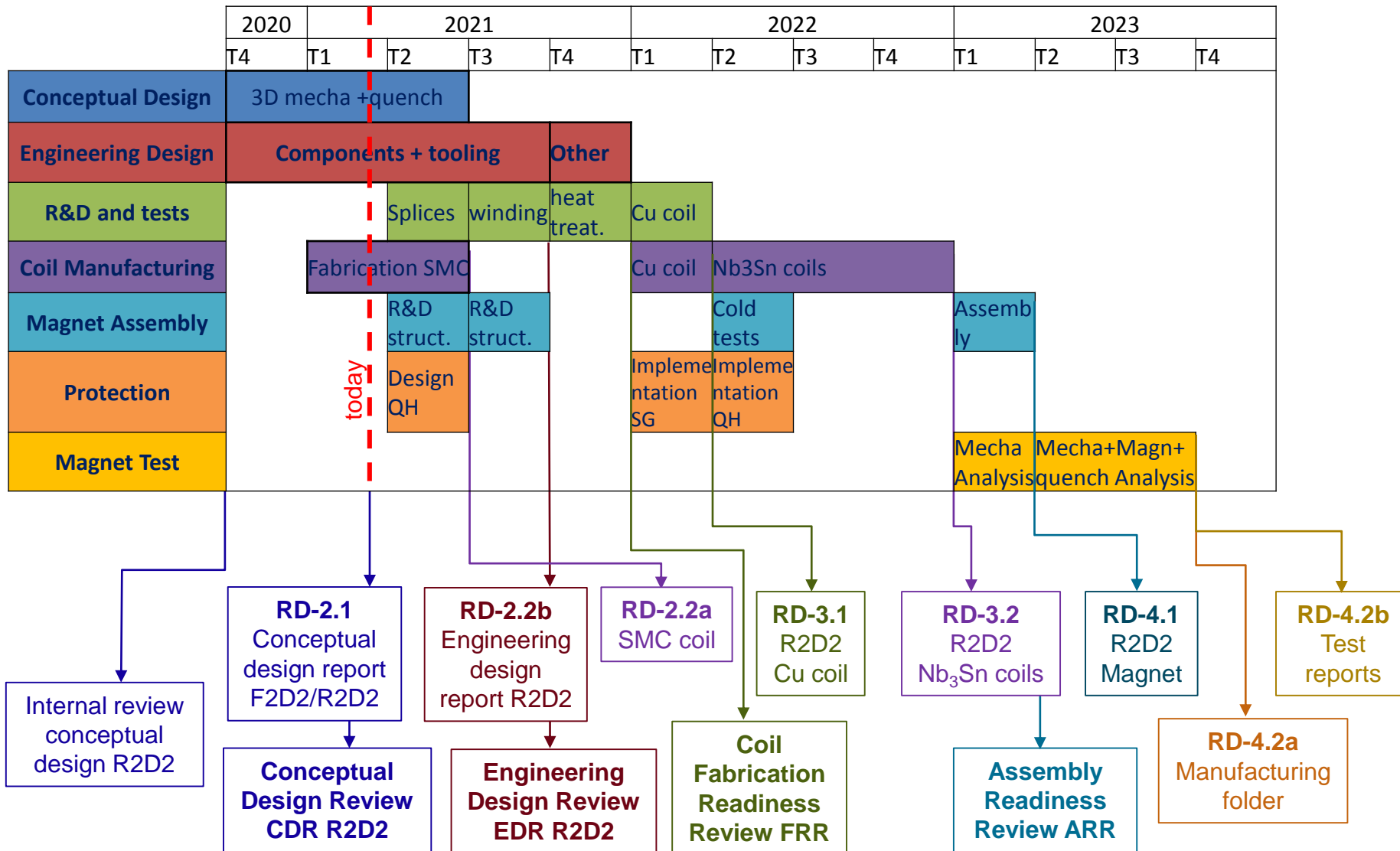
- CERN acknowledged good progress on the design
- Concerns expressed by CERN based on HL-LHC experience:
 - High risk of conductor loss
 - Call for a further improvement of the technology
 - Demonstrating progress is paramount to the credibility of the HFM development programs
 - LS2 activities impacts CERN ability to support technically the collaboration
- CEA agrees

Courtesy H. Felice

Steering committee recommendation on May 9th 2019:

- **re-examine the modified proposal**, discuss the idea of completing the F2D2 engineering design, but wind SMC/eRMC/RMM class coils that would allow “unitary tests” of novel technology (grading) with relevant cable and field
- **Call for a technical discussion** (timescale 2 weeks) for final agreement by steering committee by the end of June 2019

R2D2 SIMPLIFIED SCHEDULE



- a. What are the safe bending parameters for **coil winding**? (see 5, M. Durante)
- b. How to handle cables in **graded coils** ? (see 4 P. Manil + 5)
- c. How to deal with longitudinal contraction during **heat treatment**? (see 5, M. Durante + EDR)

Splices R&D

- d. How to guide and secure the **exits** to the outside of the coils?
- e. How to provide **margins** (geometric, magnetic, mechanical...) to the exit path? (see 2, V. Calvelli + 4, P. Manil + EDR)
- f. How to perform all the **joints** in a compact area? (see 5, M. Durante)

- g. How to apply **longitudinal pre-stress** without damaging the joint area? (see 4, P. Manil + EDR)

- h. What will be the **mechanical behavior** of the coils?
- i. What level of **transverse pre-stress** to apply?
- j. How to guarantee the **pre-stress** is controlled and reproducible?

Structure R&D,
further review

- a. Have the goals of the project been clearly stated/explained?
- b. Is the design overall solid? Magnetic design, protection, and mechanics.
- c. Are the field and current levels sufficient to validate the grading concepts?**
- d. Are there unidentified risks associated to the design?
- e. Is there a sufficient level of tests and R&D?
- f. Does the maturity of the design allow moving to the engineering design phase? For example: winding two grades, dealing with contraction during heat treatment, concept of longitudinal support...
- g. In particular: is the concept of external splices adequate for R2D2? Are there enough tests foreseen?**
- h. Does the schedule seem reasonable for the engineering and fabrication steps?
- i. Are the design tools appropriate for this project?
- j. Is the team sufficiently benefiting from past experiences?

What is outside of the CDR scope:

- Conceptual design of F2D2 → design for the long term
- Detailed (engineering) design of R2D2 → covered in the EDR
- Fabrication of SMC → covered in the FRR

Pacific time	Paris time	Title	Presenter	Duration
Day 1: Monday, March 9				
7:00-7:20	16:00-16:20	Introduction	E. Rochepault	20'
7:20-8:20	16:20-17:20	Magnetic Design and protection	V. Calvelli	40'+20'
8:20-8:50	17:20-17:50	Mechanical design	E. Rochepault	20'+10'
Day 2: Tuesday, March 10				
7:00-7:40	16:00-16:40	Engineering design	P. Manil	30'+10'
7:40-8:10	16:40-17:20	Coil R&D	M. Durante	30'+10'
8:10-9:00	17:20-18:00	Wrap-up and Discussion	All	40'

- Goals of the project:
 1. Rely when possible on **proven technology**
 2. **Develop grading** → Compact coils, high current density
 3. **Build and test a short model**
- Rescoping from F2D2 to R2D2
 - Reducing the overall difficulty
 - Conceptual design finalized
- Difficulties related to grading:
 - External joints, need for R&D
 - Longitudinal preload

Are these concepts sufficiently solid for the project?

DE LA RECHERCHE À L'INDUSTRIE

cea



BACKUP SLIDES

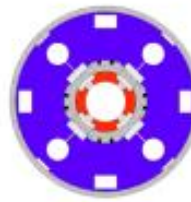
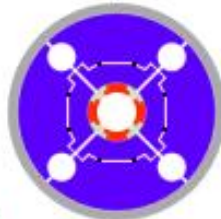
www.cea.fr

Subscale Quadrupole SQ
0.3 m long
110 mm bore



LBNL Subscale Magnet SM
0.3 m long
No bore

Technology Quadrupole TQS - TQC
1 m long
90 mm bore

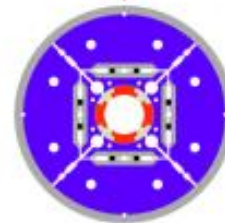


Long Racetrack LRS
3.6 m long
No bore

Technology selection:
Shell based support structure for LARP

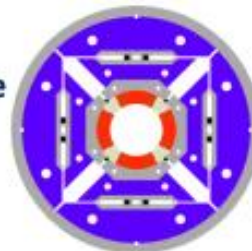
1st assembly: 2009
Last assembly: 2012

Long Quadrupole LQS
3.7 m long
90 mm bore



1st assembly: 2010
Most recent: 2013

High Field Quadrupole
1 m long
120 mm bore



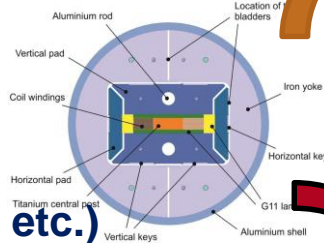
Courtesy H. Felice

IDEAS ON AN INTEGRATED STRATEGY



SMC 11T

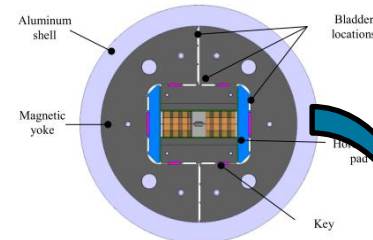
- Conductors
- Pre-stress
- Materials (Insulations etc.)



+Field

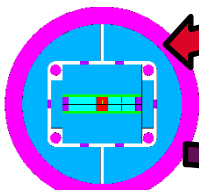
ERMC

(= 'reduced' RMM)
 ✓ Demonstrate 16 T



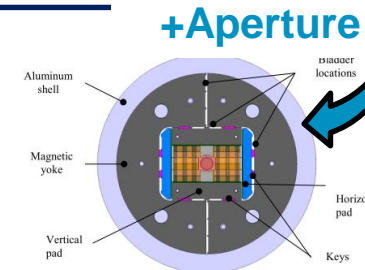
R2D2

Demonstrate Grading ≥ 12 T



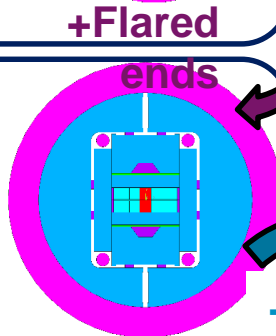
RMM

Demonstrate aperture = 16 T



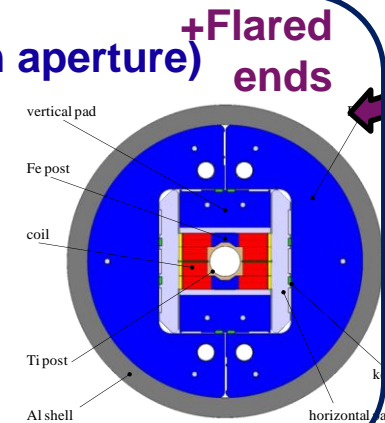
'Reduced' demo. (FD?)

Grading + Flared-ends ≥ 14 T



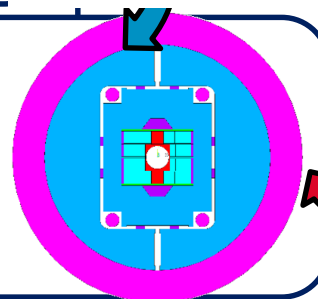
FRESCA2 (but 100 mm aperture)

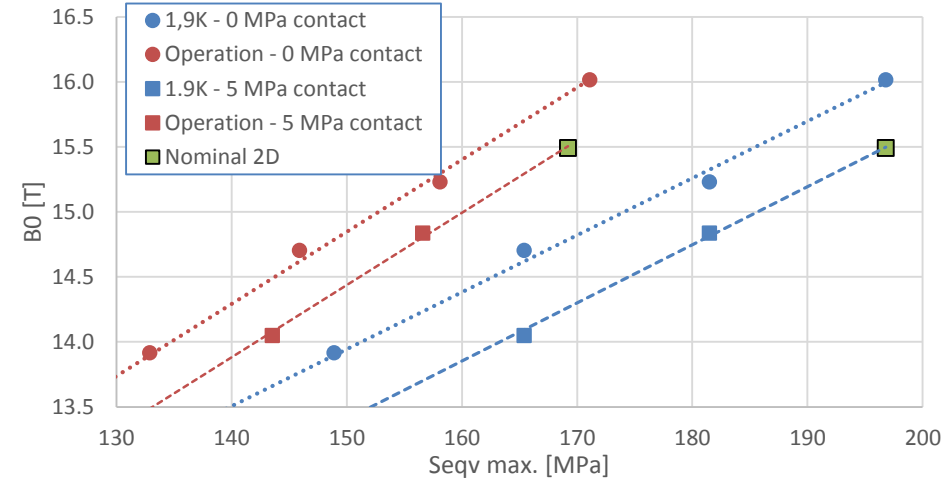
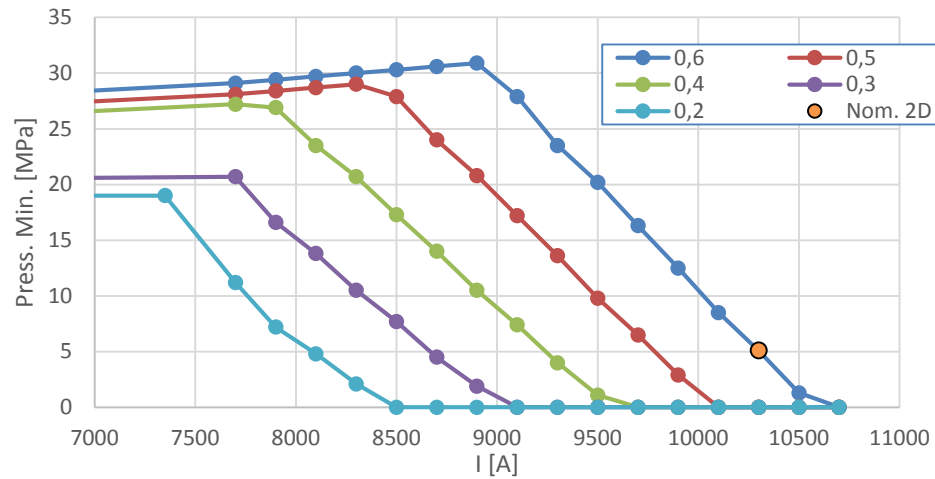
✓ Flared-ends
 + aperture ≥ 14 T



"Demonstrator" (F2D2?)

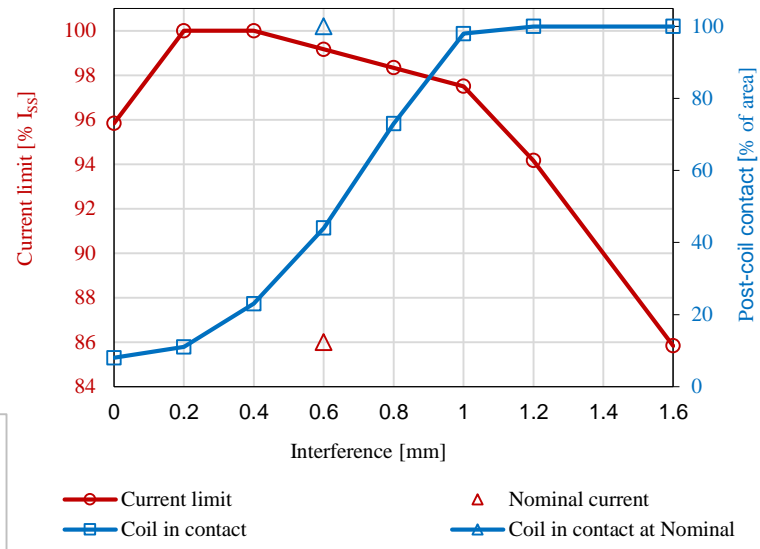
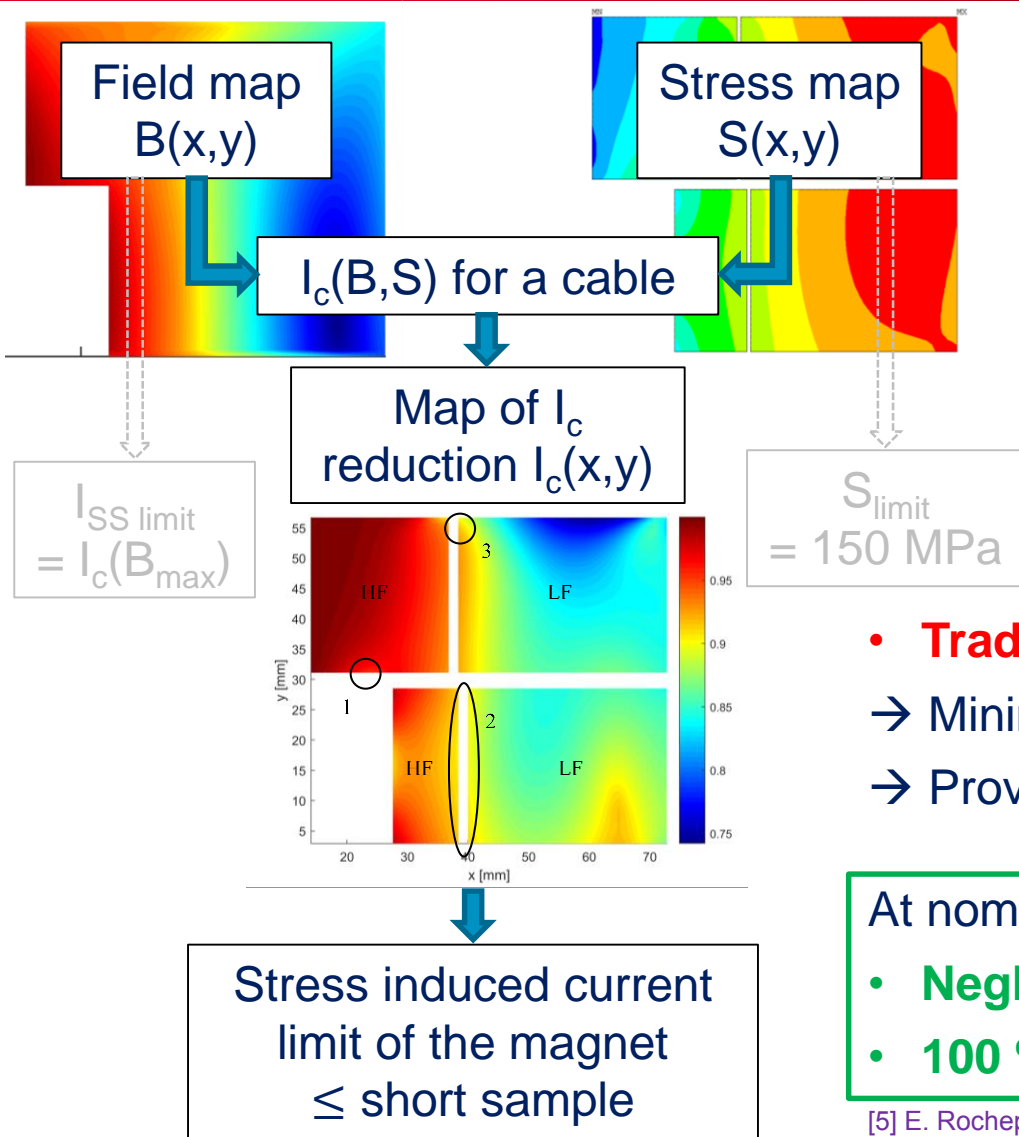
Grading + Flared-ends + Aperture = 16 T





Different fields depending on stress conditions:

Criterion	Interf. [mm]	Seqv peak [MPa]		Min. Press. [MPa]	Margin @1.9 K [%]	B ₀ [T]
		1.9 K	Operation			
150 MPa at 1.9 K	0,31	150	135	0	24	14.0
150 MPa at operation	0,44	171	150	0	18	14.9
Nominal 14% margin	0,53	186	162	0	14	15.5
Nominal 14% margin	0,6	197	170	5	14	15.5
200 MPa at 1.9 K	0,62	200	173	0	10	16.1
Short sample	0,84	237	202	0	0	17.7



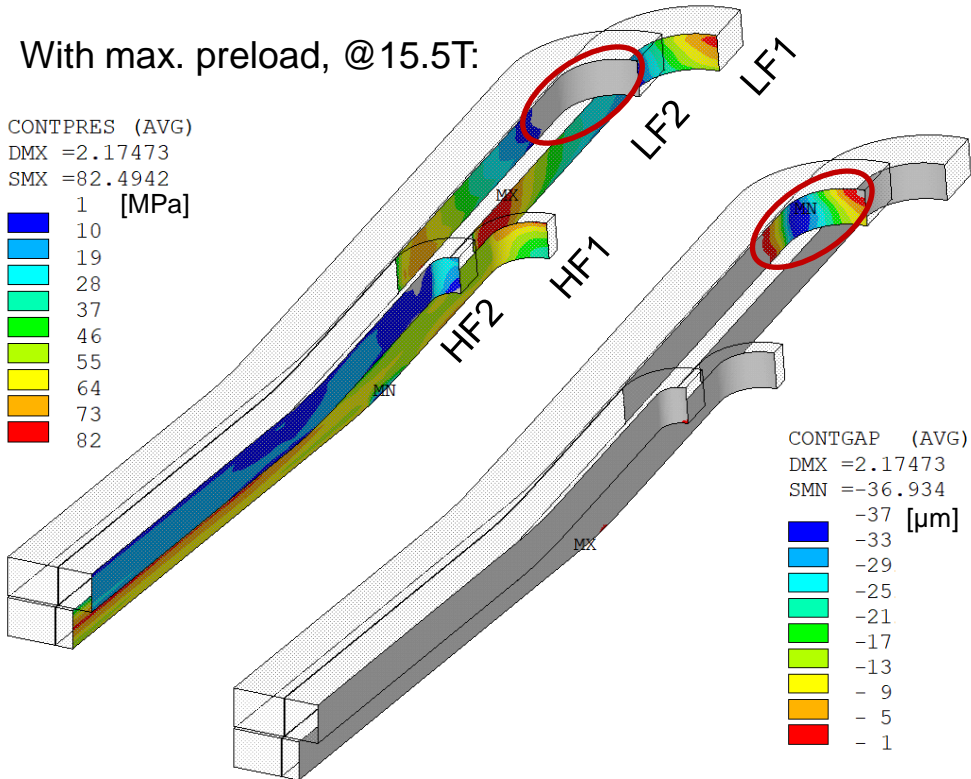
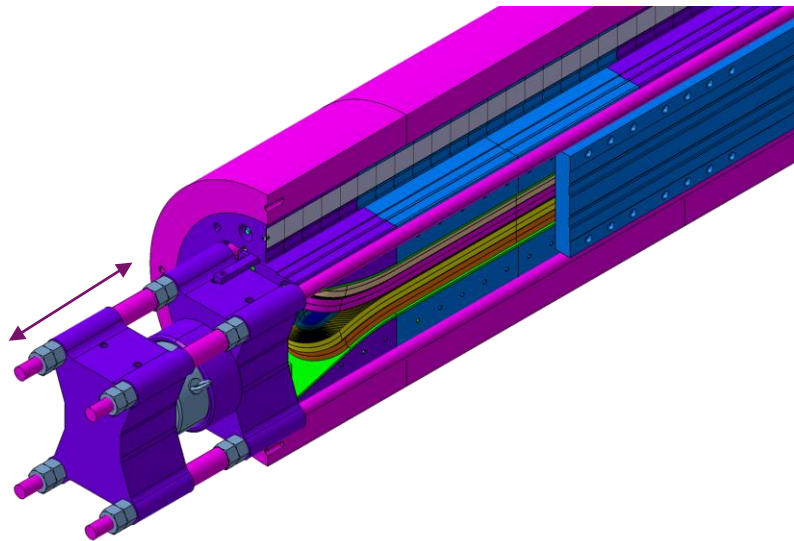
- **Trade-off on the pre-stress:**
- Minimize I_c reduction
- Provide sufficient pre-stress

At nominal current :

- **Negligible I_c reduction $\rightarrow I_{limit} = 99\% I_{SS}$**
- **100 % coil in contact with the post**

[5] E. Rochepault et al., "Computation of Current Limits in Nb3Sn Superconducting Magnets Using Magnetic Field and Stress" to be published in IEEE TAS.

Criterion	Rod, Pre-load		Rod, Cool-Down		Contact pressure at 15.5 T [MPa]			
	F_z [%]	S_z [MPa]	F_z [%]	S_z [MPa]	HF1	LF1	HF2	LF2
Criterion	<109	<480	<157	<690	>0	>0	>0	>0
Min. preload	4	15	33	146	9	0 (no gap)	0 (no gap)	0
100% of EM forces	64	281	100	440	29	1	0 (no gap)	0
Max. preload	109	480	151	662	45	4	1	0



- Longitudinal preload tuned with the tie-rods, up to 150 % if necessary
- Difficult to maintain contact in LF2