

# FEA Analysis Summary

## SFGD BOX

A. Gendotti

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08.02.2021

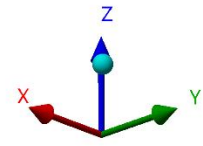
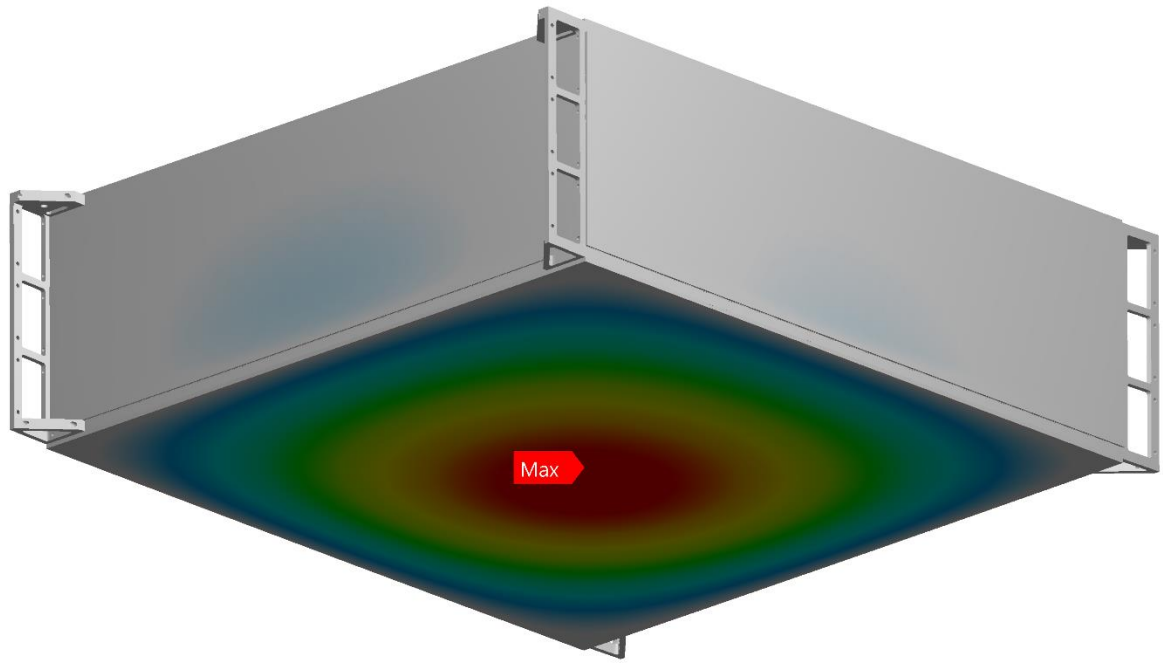
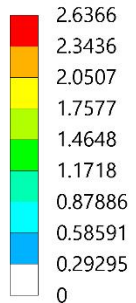
- FEA studies Static and Dynamic
- All Materials were tuned including effect of the holes (implementing various tests that has been done)
- Simplification at the model were done trying to be conservative
- First Analysis: Static Structural **1.** Self Weight **2.0.65g** in each direction:
  1. Cubes simulated as a Force
  2. it's practically considering as 100% the Mass participation of the cubes with a 0.65g acceleration in each direction
    - Deformations always under 5mm
    - Stresses always below the limit (SF included)
- Second Analysis: Tentative to implement the cubes as a solid and perform a dynamic random vibration test using the PSD spectrum given by KEK.
  - Acceleration response always below the 0.65g calculated in the static structural analysis

# STATIC STRUCTURAL ANALYSIS

- The fact that the maximum allowed deformation of the Box was set as 5mm, has brought a very stiff design. Here below images of deformation at different scenarios

**C: Static with G and Nominal Cubes Weight**  
Total Deformation  
Type: Total Deformation  
Unit: mm  
Time: 1  
Custom  
Max: 2.6369  
Min: 0

Self Weight Only



## STATIC STRUCTURAL ANALYSIS

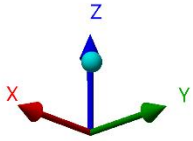
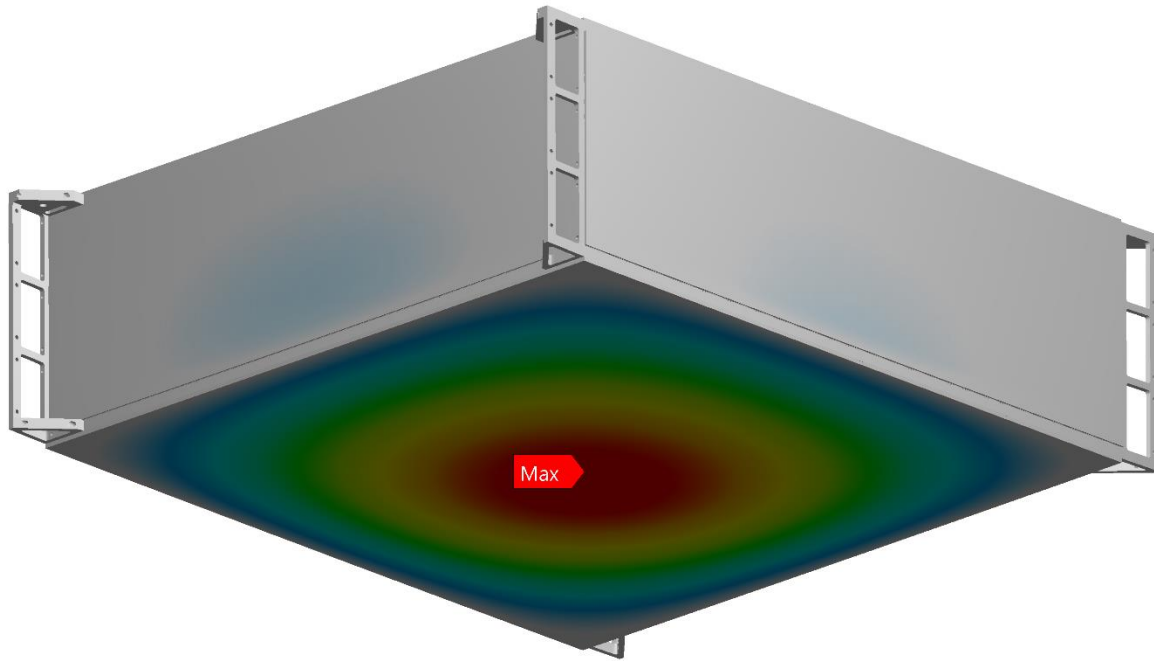
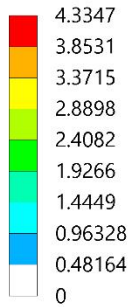
Scenario 1	Material	Yield Stress [MPa]	Von Mises [MPa]	SF	SFM	$MoS = \frac{\sigma_m}{\sigma \cdot SF \cdot SFM} - 1 \geq 0$
Earth gravity +0.65g in -Z direction	AISI 316L	290	118.28	1.1	1.1	1.026
	ALU 6061-T651	276	36.351	1.1	1.1	5.275
	FR4/G10	300	5.5928	1.1	2.0	23.382
	PMMA/Acrylic	62	3.4881	1.1	2.0	7.075
	Divynycell H250	9.2	3.0395	1.1	2.0	0.3758
						Inverse Reserve Factor <1
	Carbon Fiber					0.1144

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### D: Static Earthquake Load Bottom Panel

Total Deformation  
 Type: Total Deformation  
 Unit: mm  
 Time: 1  
 Max: 4.3347  
 Min: 0

### Self Weight + 0.65g Z-direction

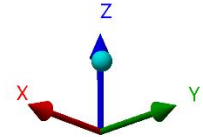
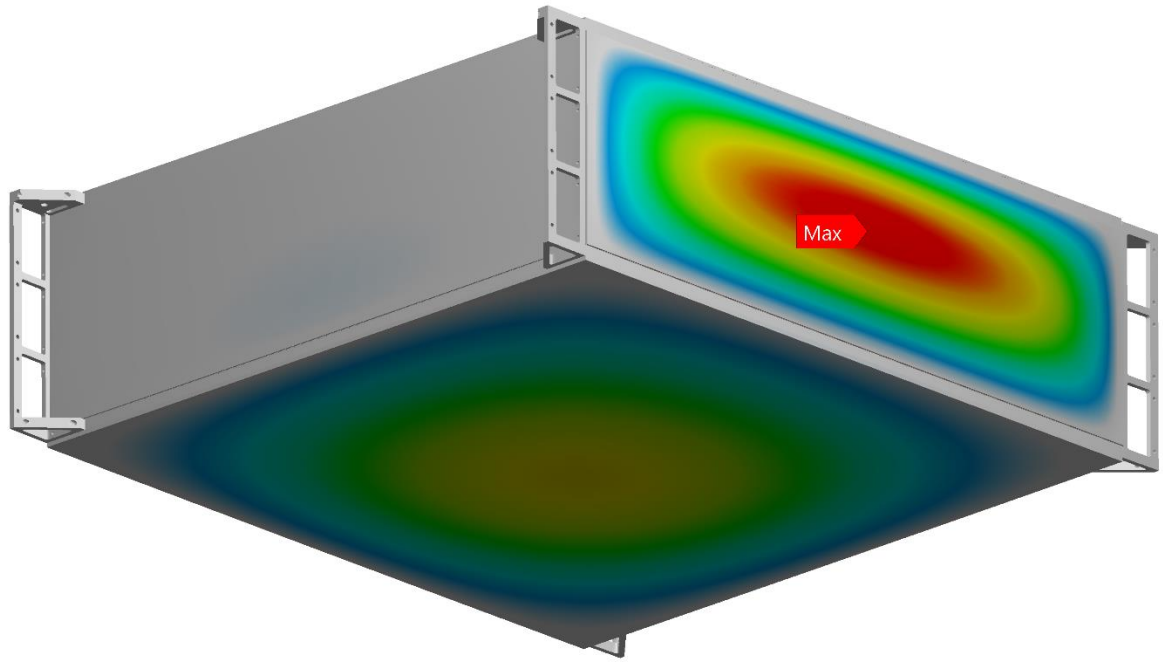
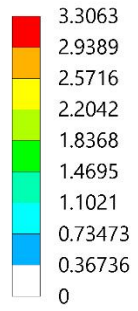


## STATIC STRUCTURAL ANALYSIS

Self Weight + 0.65g Y-direction

### E: Static Earthquake Load Y Direction

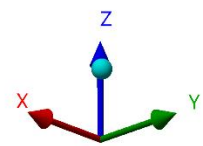
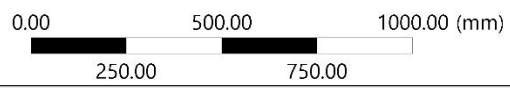
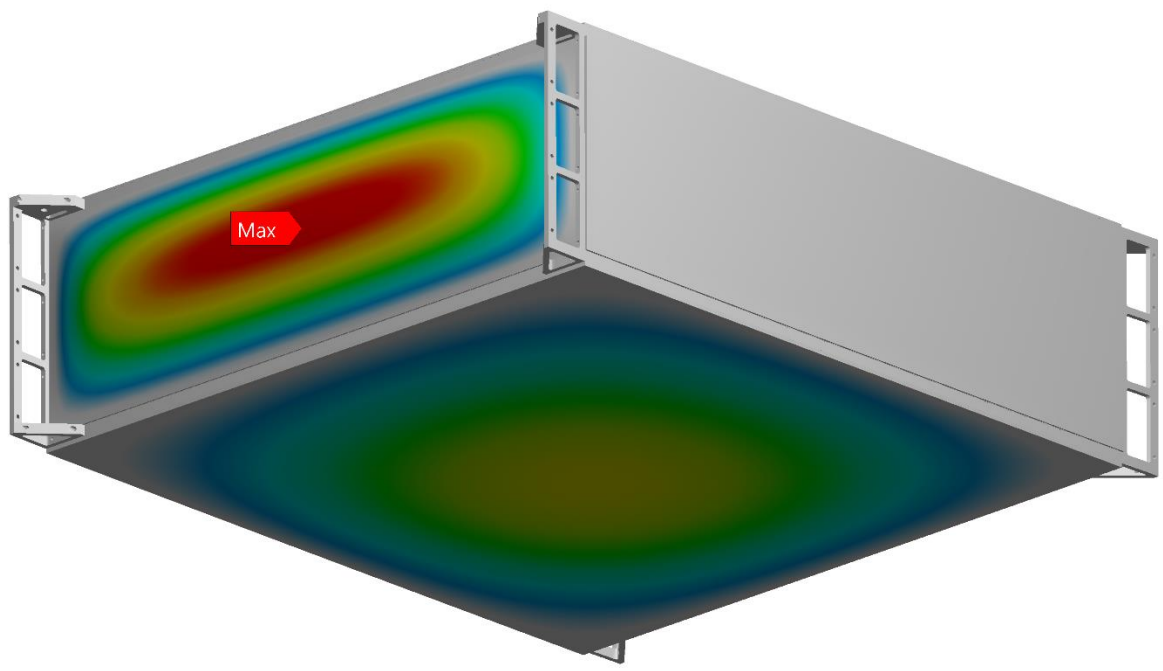
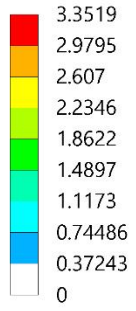
Total Deformation  
Type: Total Deformation  
Unit: mm  
Time: 1  
Max: 3.3063  
Min: 0



## STATIC STRUCTURAL ANALYSIS

Self Weight + 0.65g X-direction

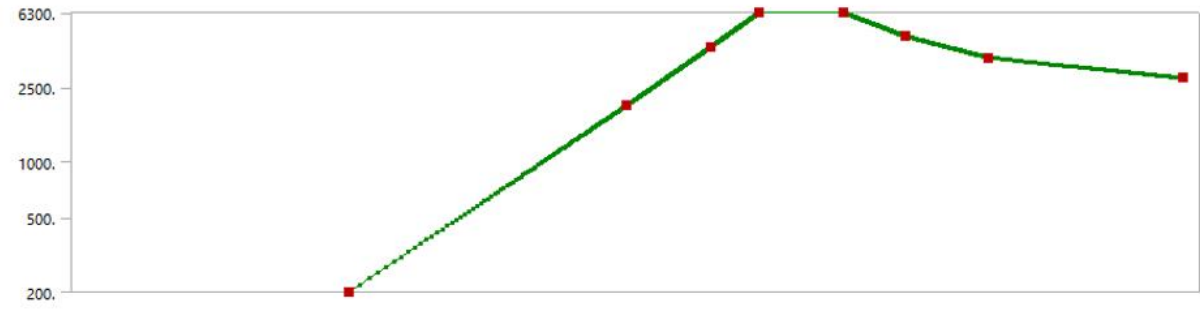
**F: Static Earthquake Load X Direction**  
Total Deformation  
Type: Total Deformation  
Unit: mm  
Time: 1  
Max: 3.3519  
Min: 0



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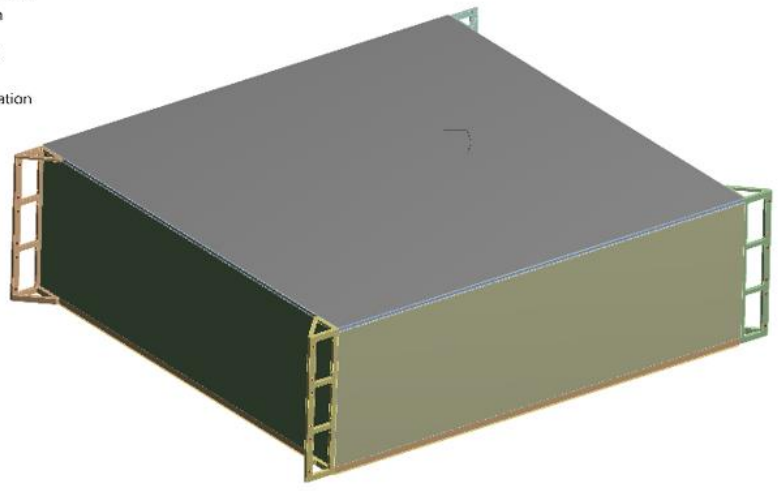
## DYNAMIC STRUCTURAL ANALYSIS

PSD Spectrum given by KEK

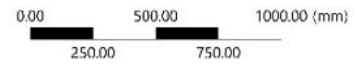


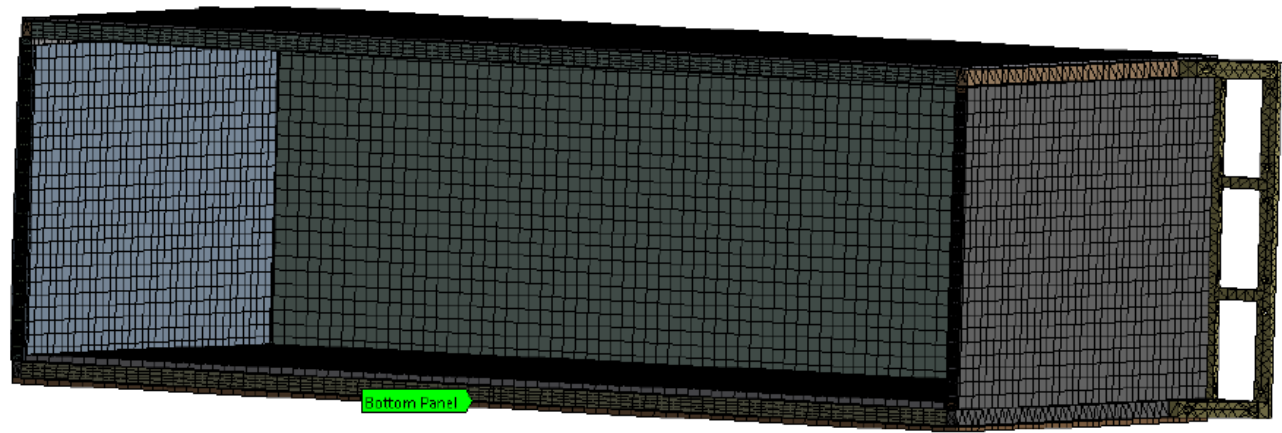
E: Random Vibration  
PSD Acceleration  
Time: 1. s  
19.10.2020 11:23

■ PSD Acceleration



	Frequency [Hz]	✓ Acceleration [(mm/s <sup>2</sup> ) <sup>2</sup> /Hz]
1	0.1	200.
2	1.	2000.
3	2.	4100.
4	3.	6300.
5	6.	6300.
6	10.	4700.
7	20.	3600.
8	100.	2800.
*		





## DYNAMIC STRUCTURAL ANALYSIS (no\_cubes)

PSD acceleration response (Z-axis) at center of Bottom Panel

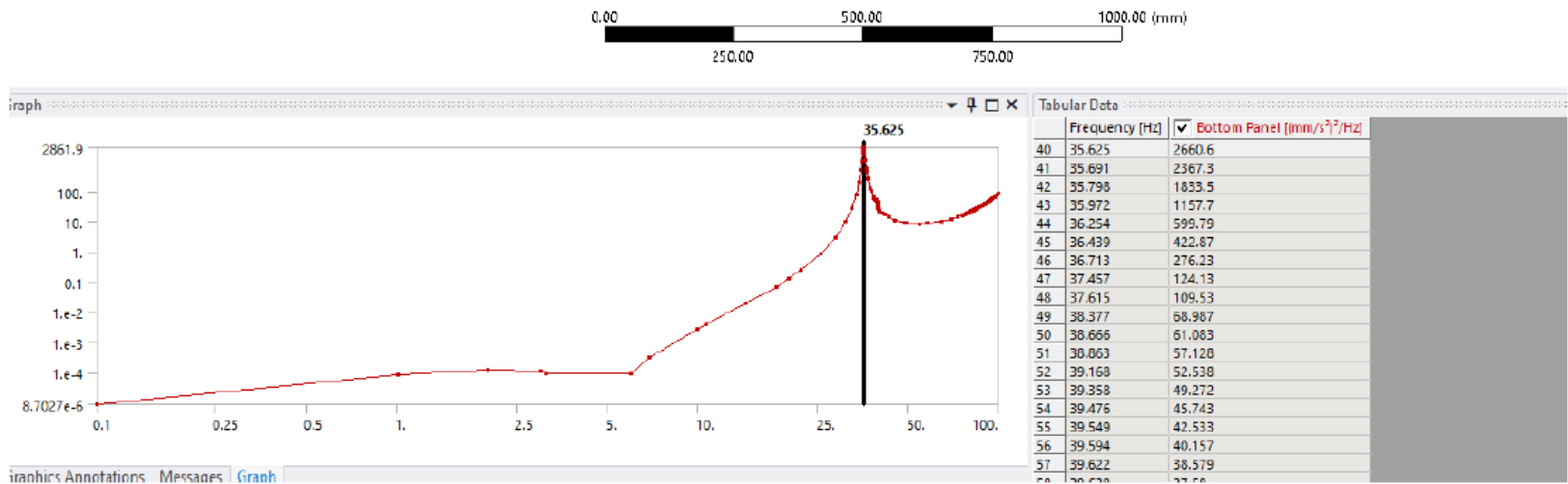
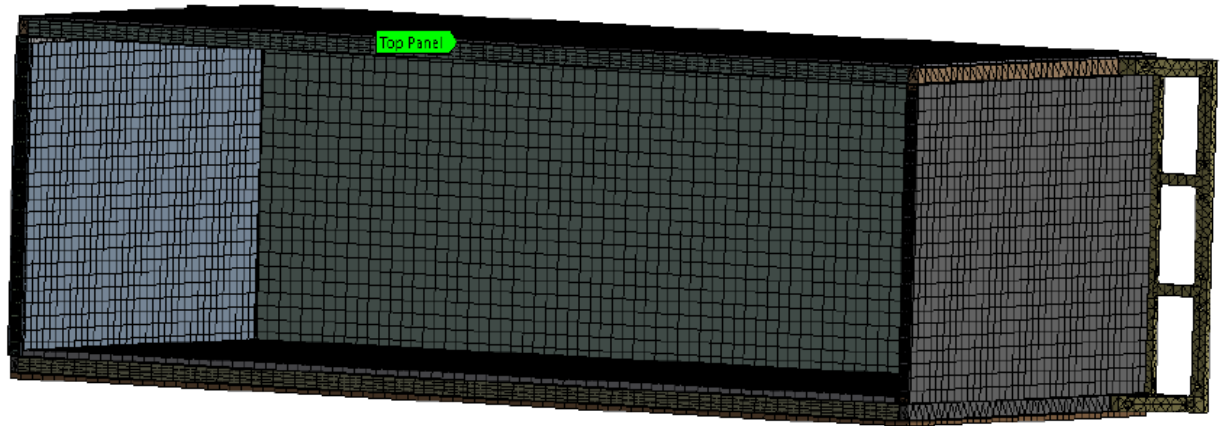


Figure 3-13 Bottom Panel PSD response; cubes weight as a Force – PSD results of acceleration

A peak is found at 36.625 [Hz] with a PSD response of 2660.6 [(mm/s<sup>2</sup>)<sup>2</sup>/Hz]

Indicatively vibrational acceleration derived of the Top Panel →  $a = 0.308 \text{ m/s}^2$





DYNAMIC STRUCTURAL ANALYSIS  
(no\_cubes)

PSD acceleration response (Z-axis) at center of Top Panel

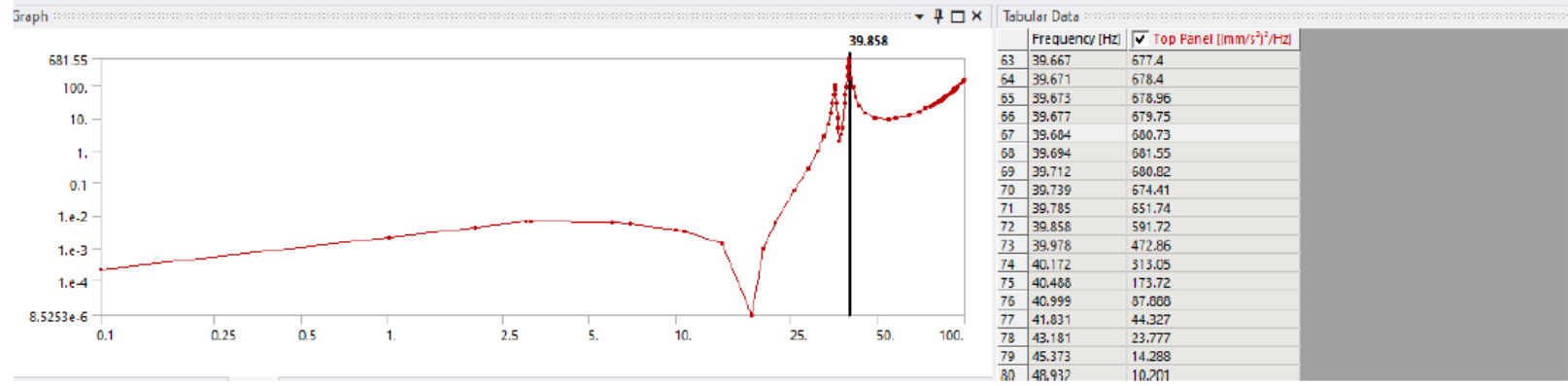
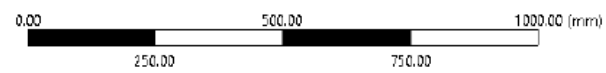
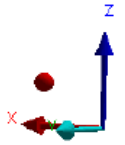


Figure 3-14 Top Panel PSD response; no cubes effect – PSD results of acceleration

A peak is found at 39.684 [Hz] with a PSD response of 680.73 [(mm/s<sup>2</sup>)<sup>2</sup>/Hz]

Indicatively vibrational acceleration derived of the Top Panel → a= 0.164 m/s<sup>2</sup>

Linear System with all contact bonded

PSD amplitude response (Z-axis) at Top and Bottom Panel

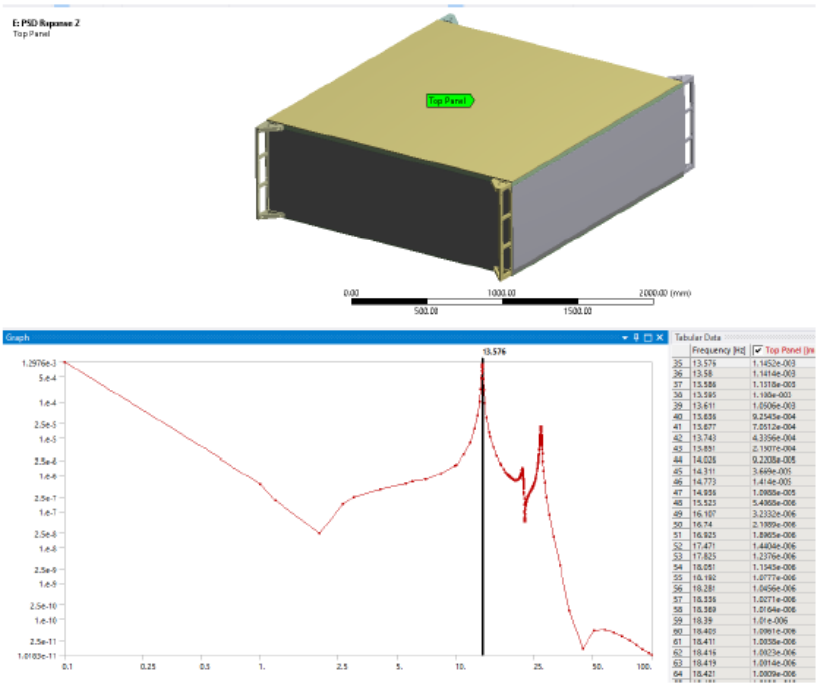


Figure 3-7 Scenario 1 – Vibration in Z direction – Results at the Top Panel

A peak is found at 13,576 [Hz] with a PSD of 1.1452e<sup>-3</sup> [(mm²)/Hz]

Indicatively vibrational amplitude derived of the Top Panel → A= 0.140 mm

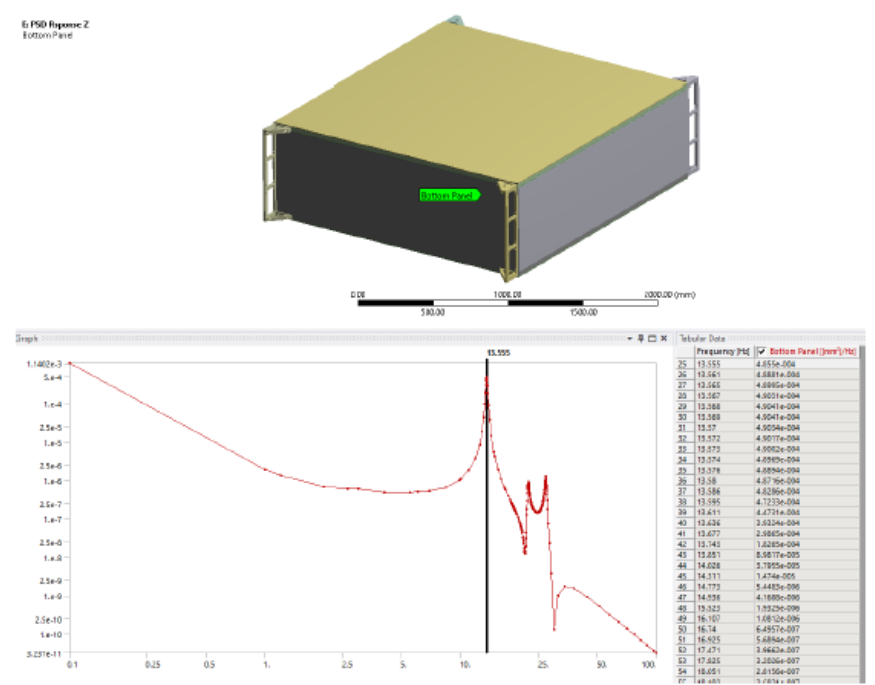


Figure 3-8 Scenario 1 – Vibration in Z direction – Results at the Bottom Panel

A peak is found at 13,555 [Hz] with a PSD of 4.855e<sup>-4</sup> [(mm²)/Hz]

Indicatively vibrational amplitude derived of the Top Panel → A= 0.081 mm

## Linear System with all contact bonded

### PSD amplitude response (Y-axis) at Top and Bottom Panel

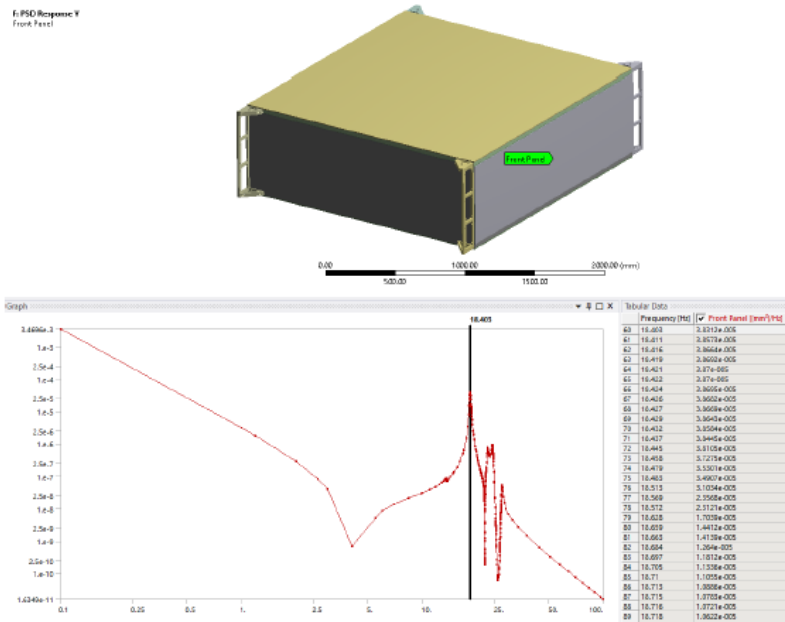


Figure 3-9 Scenario 2 – Vibration in Y direction – Results at the Front Panel

A peak is found at 18.403 [Hz] with a PSD of  $3.83122e^{-5}$  [(mm<sup>2</sup>)/Hz]

Indicatively vibrational amplitude derived of the Top Panel → A= 0.026 mm

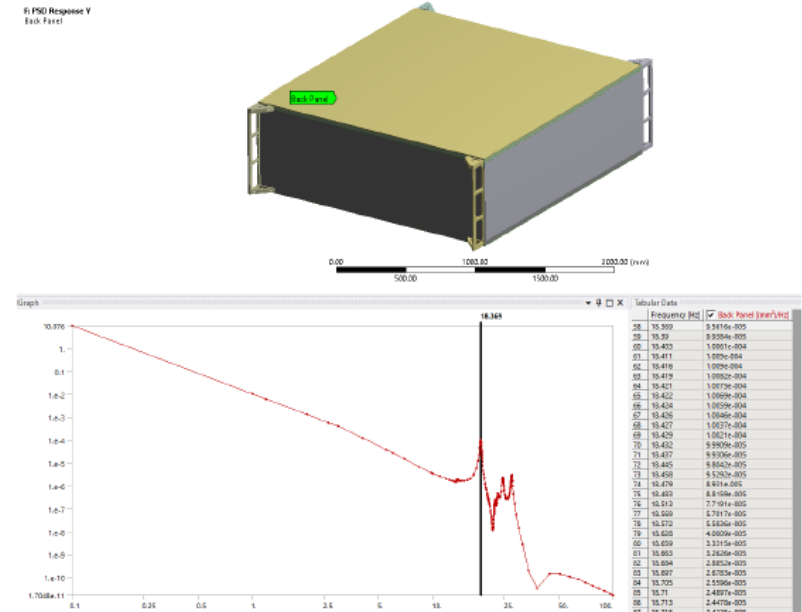


Figure 3-10 Scenario 2 – Vibration in Y direction – Results at the Back Panel

A peak is found at 13,369 [Hz] with a PSD of  $9.5616e^{-5}$  [(mm<sup>2</sup>)/Hz]

Indicatively vibrational amplitude derived of the Top Panel → A= 0.042 mm

## Linear System with all contact bonded

### PSD amplitude response (X-axis) at Top and Bottom Panel

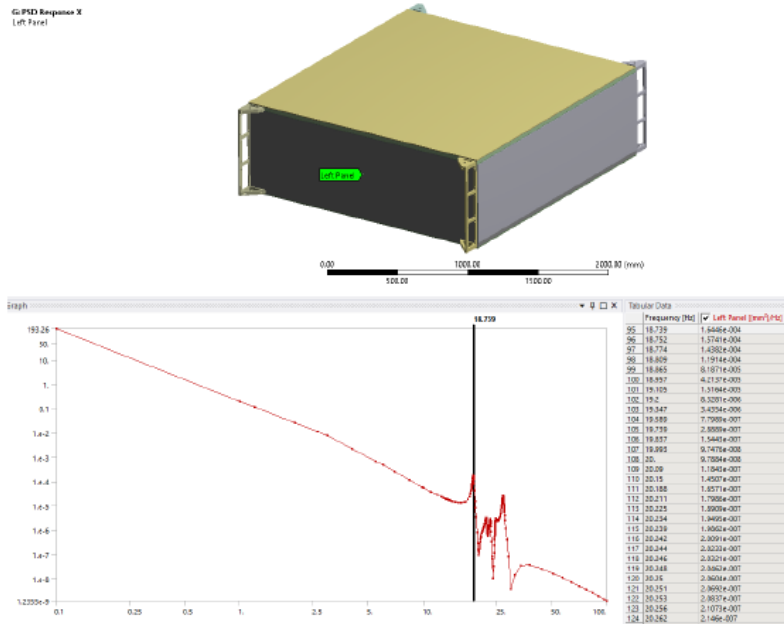


Figure 3-11 Scenario 3 – Vibration in Y direction – Results at the Left Panel

A peak is found at 18.739 [Hz] with a PSD of  $1.6446e^{-4}$  [(mm<sup>2</sup>)/Hz]

Indicatively vibrational amplitude derived of the Top Panel → A= 0.056 mm

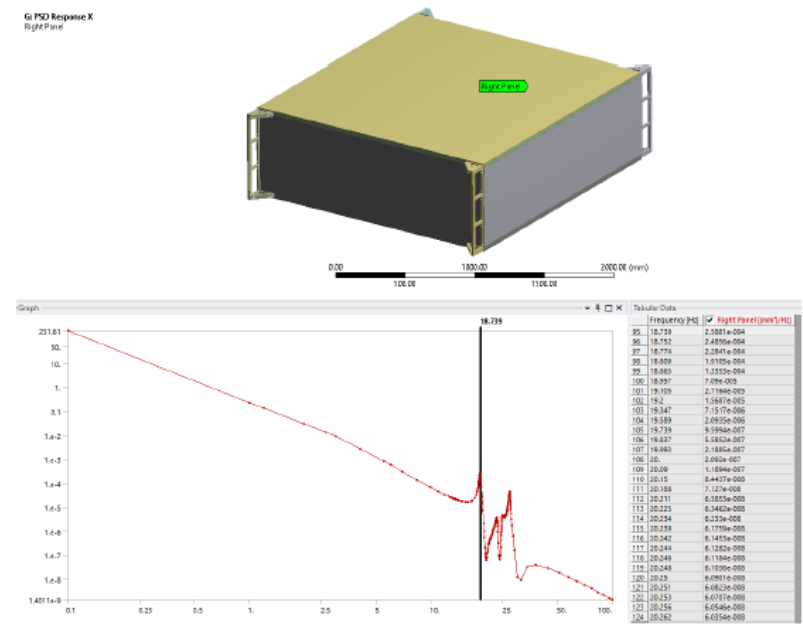


Figure 3-12 Scenario 3 – Vibration in Y direction – Results at the Right Panel

A peak is found at 18.739 [Hz] with a PSD of  $2.5881e^{-4}$  [(mm<sup>2</sup>)/Hz]

Indicatively vibrational amplitude derived of the Top Panel → A= 0.070 mm