

# Impedance effects during injection, energy ramp & store

LHC-CC10, 4<sup>th</sup> LHC Crab Cavity Workshop  
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- longitudinal stability and impedance budget
- transverse impedance budget

Acknowledgments: E. Ciapala, W. Hofle, J. Tuckmantel

# Beam and machine parameters

Energy	TeV	0.45	7.0
RF frequency	MHz	400.8 (200.4)	400.8
RF voltage	MV	8.0 (3.0)	16.0
synchrotron frequency $f_s$	Hz	66.08 (28.64)	23.86
revolution frequency $f_0$	kHz	11.245	11.245
betatron tune $Q_\beta$ H/V		59.3/64.28	59.3/64.31
longitudinal emittance	eVs	0.6 (1.0)	1.0-2.5
rms bunch length	ns	0.4	0.275
nominal (ultimate) bunch current	mA	0.2 (0.3)	0.2 (0.3)
number of bunches (symmetric) M		2808 (3564)	2808 (3564)
nominal (ultimate) beam current (with symmetric bunches) $I_0$	A	0.7 (1.05)	0.7 (1.05)

# RF systems in LHC

## SPS

- Acceleration in the SPS is done by the 200 MHz RF system. The high harmonic 800 MHz RF system is used as Landau cavity for beam stability.
- For nominal bunch intensities **controlled longitudinal emittance blow-up** from 0.4 eVs to 0.65 eVs is required in addition. Larger emittance (0.8 eVs) will be needed for stability of ultimate intensities in SPS
- Maximum voltage (7.5 MV) to shorten bunch for transfer to LHC

## LHC

- Acceleration in the LHC is done by the 400 MHz RF system. Maximum voltage 16 MV/beam (coast)
- Capture 200 MHz RF system (8 bare cavities exist, 3 MV/beam,) => **postponed** - not ideal solution: impedance, reliability, maintenance, cost, transfer to 400 MHz and **reduced beam stability**

# Longitudinal stability in LHC

## - general remarks

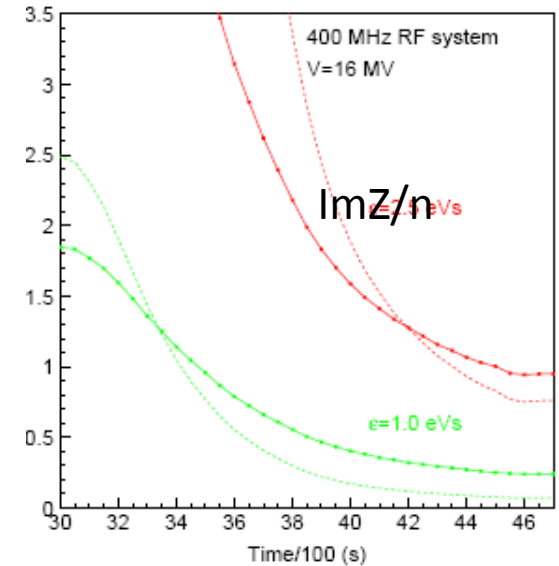
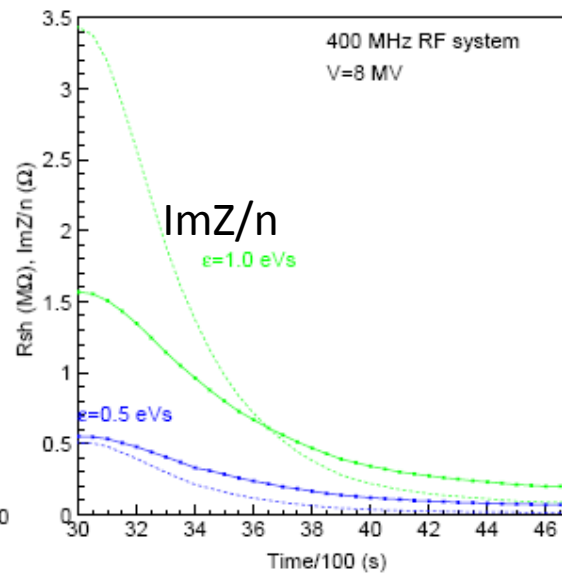
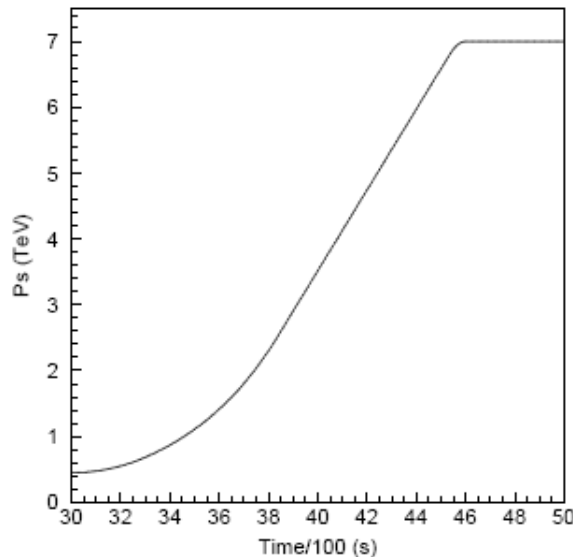
- We have feedback and feedforward systems and longitudinal damper at 400 MHz ( $\sim 1$  MHz bandwidth)
  - **No longitudinal bunch-by-bunch feedback** - difficult to do better than natural damping
- **We rely only on Landau damping** due to synchrotron frequency spread inside the bunch:
- **$\text{Im}Z/n$**  of broad-band impedance leads to the loss of Landau damping: measured in 2010
  - controlled longitudinal **emittance blow-up** during the ramp: in 2010 0.6 eVs @0.45 TeV → 1.75 eVs @3.5 TeV
  - proposal for **Landau cavity** at 800 MHz

# Impedance limit during the cycle for nominal bunch and beam current and different emittances

Momentum

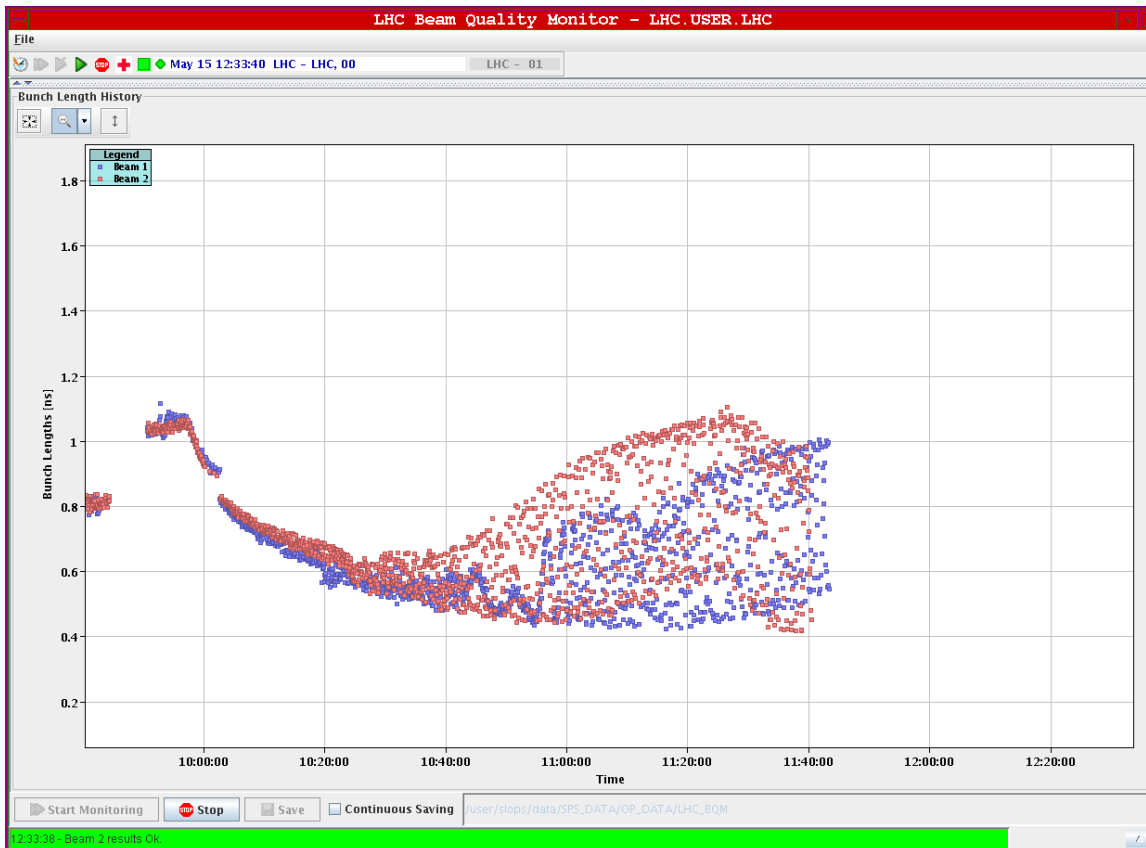
V=8 MV@400 MHz

V=16 MV@400 MHz



→ Threshold narrow- and broad-band impedances **decrease with beam energy**:  
 $R_{sh} \sim (\epsilon^2/E)^{3/4}$ ,  $ImZ/n \sim (\epsilon^2/E)^{5/4}$  → controlled emittance blow-up:  $\epsilon \sim E^{1/2}$

# Loss of Landau damping: during the ramp (@1.8 TeV)



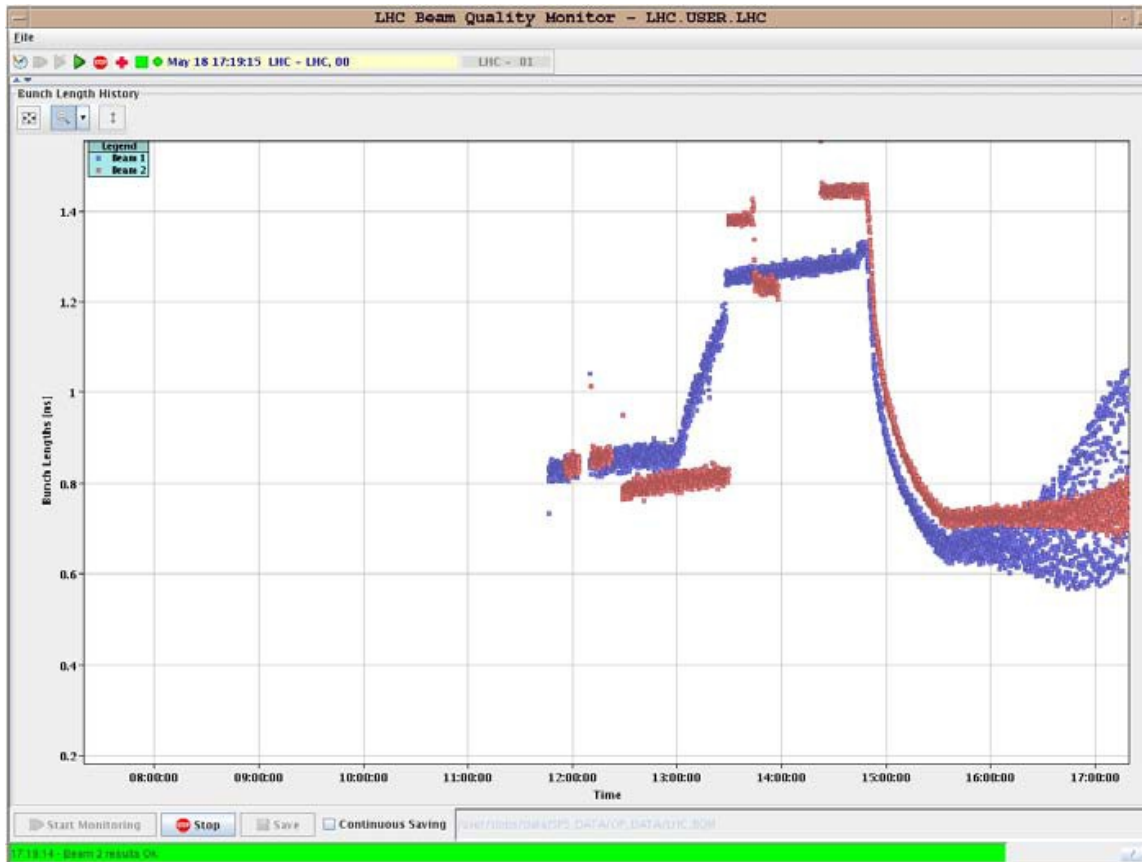
Single bunch:

Beam1 -  $1.1 \times 10^{11}$

Beam2 -  $1.05 \times 10^{11}$

1.05 ns  $\rightarrow$  0.35 eVs  
(0.45 TeV, 5 MV)

# and on flat top



**Beam 1** -  $1.1 \times 10^{11}$

•450 GeV, 5 MV:

1.25 ns - 1.3 ns  $\rightarrow$  0.5 eVs

•3.5 TeV, 8MV:

0.65 ns  $\rightarrow$  0.5 eVs

**Beam 2** -  $1.05 \times 10^{11}$

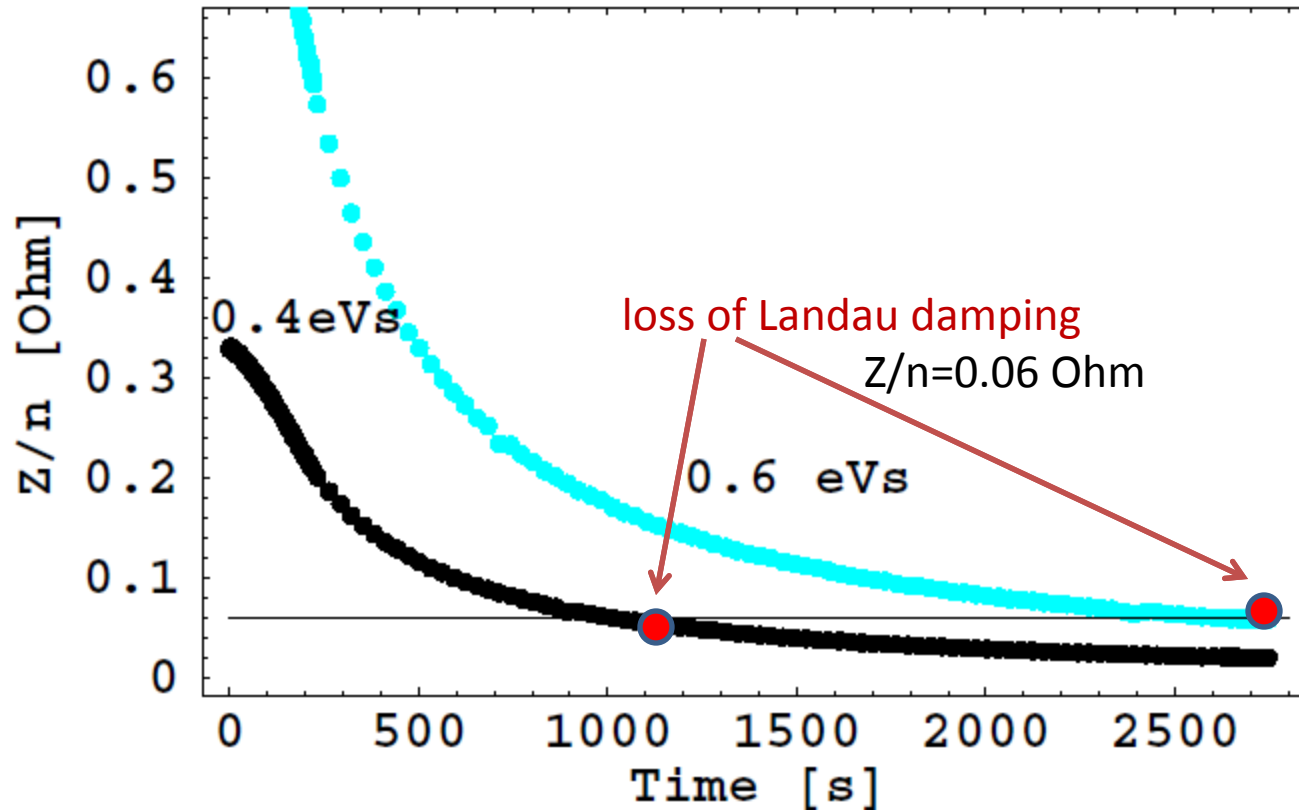
•450 GeV, 5 MV:

1.45 ns  $\rightarrow$  0.6 eVs

•3.5 TeV, 8 MV:

0.72 ns  $\rightarrow$  0.6 eVs

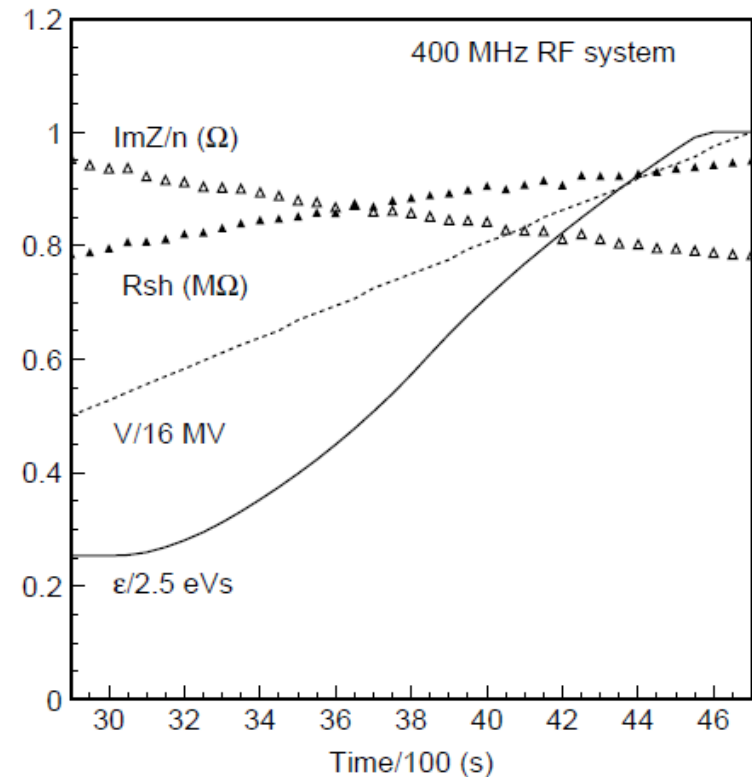
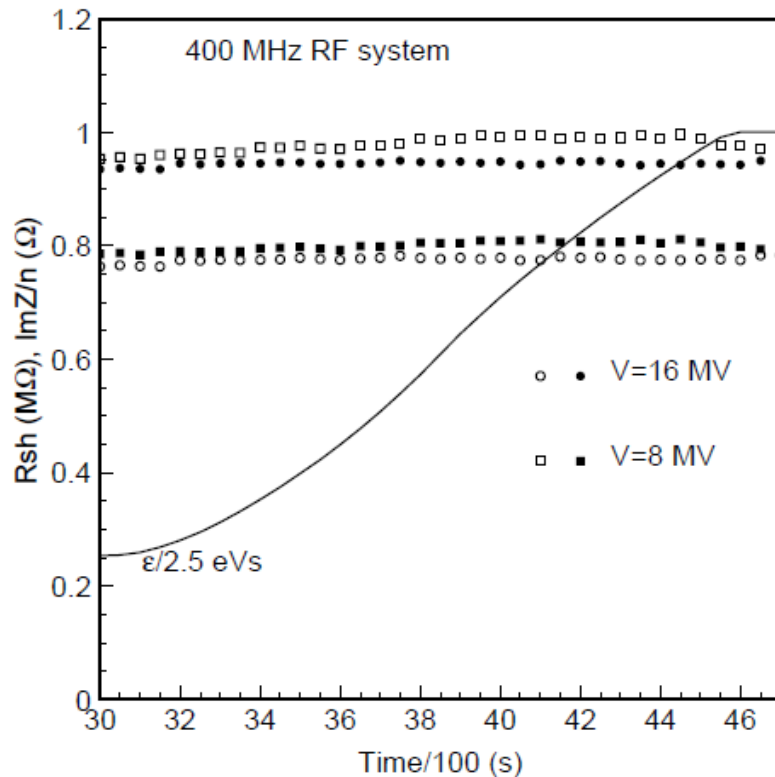
# Loss of Landau damping: threshold through the cycle



- mode  $m=2 \rightarrow 0.09$  Ohm. LHC DR impedance budget - 0.08 Ohm
- Minimum emittance for ultimate intensities is **1.5 eVs @ 7 TeV**

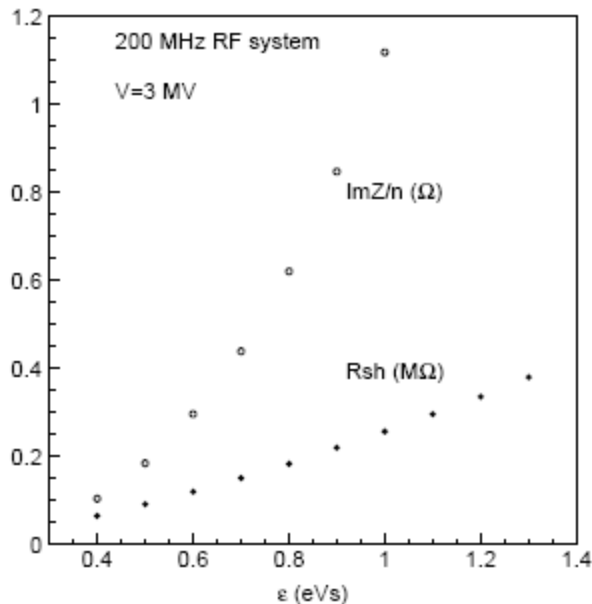


# Constant thresholds during the cycle for $\varepsilon \sim \sqrt{E}$

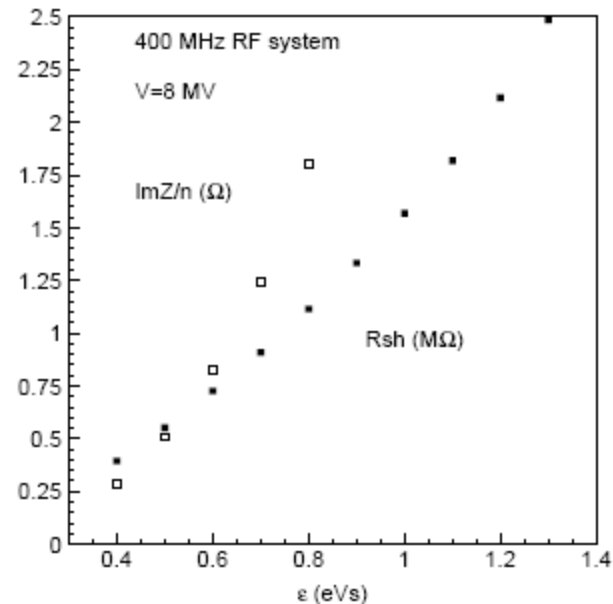


# Stability on 450 GeV flat bottom

200 MHz RF system

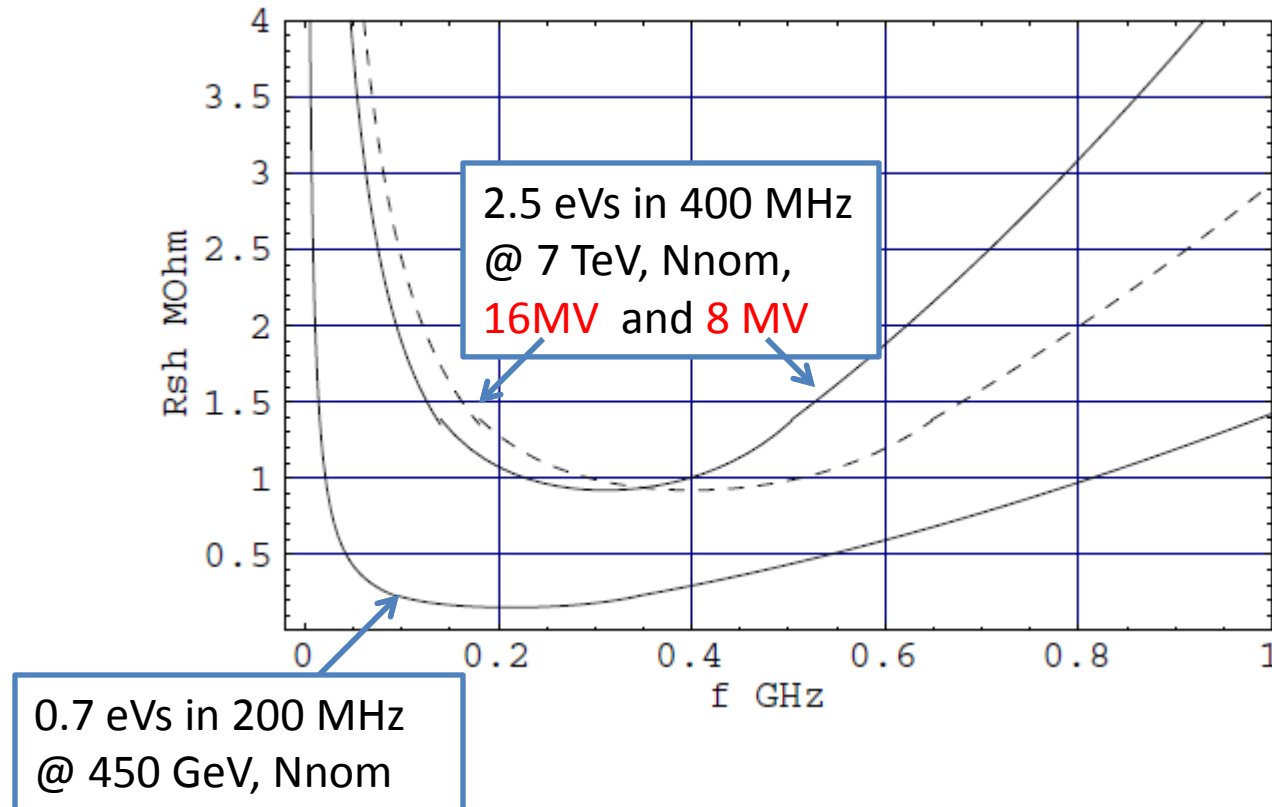


400 MHz RF system



- 200 MHz: 120 kOhm limit for emittance of 0.7 eVs and nominal intensity or 1 eVs and ultimate intensity (symmetric filling) + factor  $\frac{1}{2}$  for different distribution (F). The 400 MHz RF can be used as Landau system
- 400 MHz: 600 kOhm limit for 0.7 eVs, nominal intensity (sym. filling)

# Impedance budget: frequency dependence



# Beam stability in 400 MHz RF system

- Limit of **600 kOhm** for 2.5 eVs at 7 TeV, nominal intensity (symmetric bunches)
- Factor **1/2** for different bunch distribution (formfactor F)
- Factor **2/3** for ultimate intensity
- **200 kOhm** in frequency range (100-600) MHz, relaxed  $\sim (2\tau f_r)^{5/3}$  outside minimum at  $f_r \approx 0.4/\tau$ , ( $\tau$  is  $4\sigma$  bunch length)

# Summary:

## longitudinal impedance budget

- LHC Design Report: HOM damping below **60 kOhm**  
(defined by stability in a single 200 MHz RF at 0.45 TeV)
  - For nominal intensity
    - 400 MHz RF: **300 kOhm** for 2.5 eVs @ 7 TeV  
(**100 kOhm** for 1.5 eVs – possible from single bunch stability – loss of Landau damping)
    - 200 MHz RF: **60 kOhm** for 0.7 eVs @0.45 TeV  
(the 400 MHz RF can be used as Landau system)
- **Limit: 40 kOhm** for ultimate intensity  
or **20 kOhm for two** identical cavities (HOMs)

# Transverse coupled-bunch instability (narrow-band impedances)

- **Instability thresholds** are determined by
  - betatron frequency spread:
    - system nonlinearities
    - octupoles
    - space charge
    - long range beam-beam
  - synchrotron frequency spread ( $m > 0$ )
  - chromaticity
- In LHC there is a **bunch-by-bunch transverse feedback system** (20 MHz bandwidth) to damp injection oscillations and unstable rigid bunch motion
- Estimate which **growth rate** can be damped without significant transverse emittance blow-up with present transverse damper HW

# Instability growth rate (1/2)

- A resonant transverse impedance with resistive part  $Z_T$  [Ohm/m] at resonant frequency  $\omega_r = 2\pi f_r$  will drive coupled-bunch mode  $(n, m)$   $f_r = (n + pM + Q_\beta)f_0 + mf_s$  with the growth rate

$$\frac{1}{\tau_m} = \frac{1}{m+1} \frac{1}{4\pi Q_\beta} \frac{cI_0 Z_T}{E/e} F(\omega_r \tau - \omega_\xi \tau)$$

$f_0$  and  $f_s$  are revolution and synchrotron frequency,

$M$  is number of (symmetric) bunches,

$Q_\beta$  is betatron tune,  $\omega_\xi = Q_\beta \omega_0 \xi / \eta$ ,  $\xi$  is chromaticity,

Formfactor  $F(x)$  for water-bag bunch:  $F(0)=1$  (the worst mode  $m=0$ ),

$F(x > 0.5) \approx 0.5$

# Instability growth rate (2/2)

- Growth rate  $\sim 1/E \rightarrow$  maximum at **low energy**
- At 450 GeV, for nominal intensity and  $Z_T = 1 \text{ MOhm/m}$  ( $\xi=0$ ):  
minimum  $\tau_{\text{inst}} = 0.15 \text{ [s]}$
- Condition  $\tau_{\text{inst}} > \tau_d$  gives
$$Z_T [\text{MOhm/m}] < 0.15 / (1-x/1.6) / \tau_d, \quad x = (f_r - f_\xi)\tau < 0.8$$
$$Z_T [\text{MOhm/m}] < 0.3 (0.5+x) / \tau_d, \quad x > 0.8$$

$\tau_d$  [s] is the damping time by transverse damper,  
 $\tau$  is the bunch length, typically  $1.0 \text{ ns} < \tau < 1.5 \text{ ns}$
- For ultimate intensity factor 2/3

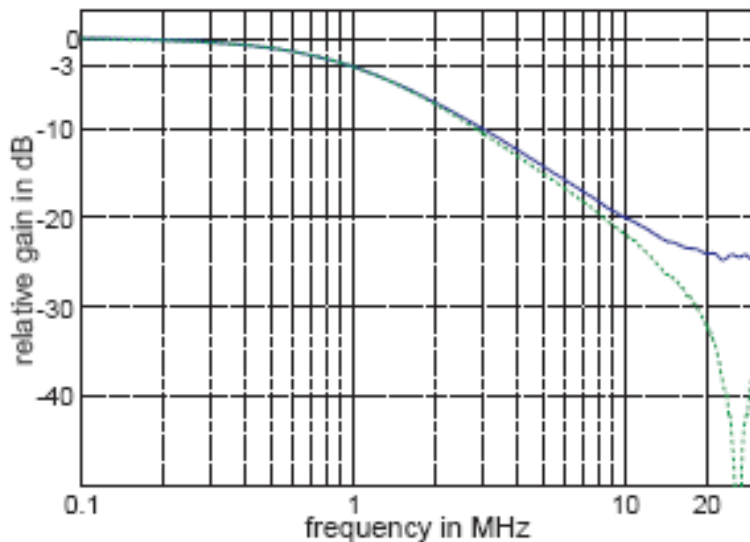


# Damping time (1/2)

- Specifications of the transverse feedback (W. Hofle et al.):  
damping time  $\tau_d = 3.6$  ms, but
  - simultaneous injection oscillation damping
  - resistive wall instability growth time  $\sim 17$  ms at injection for ultimate intensity (E. Metral, 2008)
  - decoherence time 68 ms (for tune spread  $1.3 \times 10^{-3}$  and chromaticity  $\xi \neq 0$ )
  - strict budget for transverse emittance blow-up (2.5%), 2.2% blow-up at ultimate intensity
  - gain roll-off for high frequencies
- Damping times achieved in LHC in 2010 in talk of W. Hofle

# Damping time (2/2)

Power amplifier  
frequency characteristics



→ roll-off of gain for **kicker** and **tetrode anode** voltage (W. Hofle et al., EPAC'08)

- Frequency roll-off: -1 dB at 1 MHz and -24 dB at 20 MHz  
→  $\tau_{d \max} = 60 \text{ ms}$
- Crab cavity impedance (for  $x=0$ )  
 $Z_T < 2.5 \text{ [M}\Omega\text{/m]}$   
(The same threshold from betatron frequency spread)
- Formfactor  $F_m$  for different longitudinal particle distribution (not water-bag) – up to factor  $1/4$
- $n_c$  identical cavities: factor  $1/n_c$
- **Weight function**  $\beta / \langle \beta \rangle$  if beta-function at Crab cavity location is different from average

# Summary:

## transverse impedance budget

- For nominal intensity at 450 GeV threshold determined by the damping time of 60 ms is 2.5 MOhm/m. With margin for particle distribution - 0.6 MOhm/m
- Approximate **frequency dependence**
  - $0.6 / (1 - f_r / 1.6)$  MOhm/m for  $f_r$  [GHz] < 0.8
  - $1.2 (0.5 + f_r)$  MOhm/m for  $f_r$  [GHz] > 0.8

→ 0.8 MOhm/m at 0.8 GHz for ultimate intensity and **0.4 MOhm/m** for 2 identical cavities
- Additional factor proportional to local beta-function  $\beta / \langle \beta \rangle$

# Conclusion

## Longitudinal impedance budget

- determined by preserving natural Landau damping
- most strict requirement from capture 200 MHz RF system (not installed)
- worst at high energy - controlled emittance blow-up to keep threshold constant during the cycle

## Transverse impedance budget

- determined by bunch-by-bunch FB damping time
- worst at low energy

# Spare slides

# Longitudinal stability

## Threshold for coupled-bunch instability

(equally spaced bunches) due to resonant impedance with frequency

$$f_r = f_0 n_r = p M f_0 + n f_0 + m f_s$$

$$R_{sh} < \frac{|\eta| E}{e I_0} \left( \frac{\Delta p}{p} \right)^2 \frac{\Delta \omega_s}{\omega_s} \frac{F}{f_0 \tau} x G(x),$$

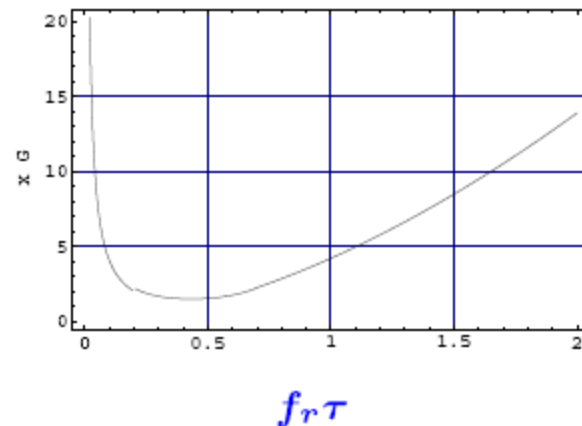
$f_0$  is the revolution frequency,  $\eta = 1/\gamma^2 - 1/\gamma_t^2$ ,  $I_0$  is the average beam current,  $\frac{\Delta p}{p}$  is the relative momentum spread,  $\frac{\Delta \omega_s}{\omega_s}$  is the relative synchrotron frequency spread,  $F \sim 0.3$  is defined by the particle distribution.

(V. Balbekov, S. Ivanov, 1984)

## Function

$$x G(x) = x \min\{J_m^{-2}(\pi x)\},$$

$$x = f_r \tau$$



# Warning: definition of transverse shunt impedance $R_s$

- Resonant impedance in [Ohm/m]

$$Z_T(\omega) = D(\omega) R_s / [1 + jQ(\omega - \omega_r^{-1})],$$

where  $\omega = \omega_r \omega_r$

$$\rightarrow Z_T(\omega_r) = D(\omega_r) R_s$$

- A. Chao, K.Y. Ng

$$D(\omega) = c/\omega, \quad D(\omega_r) = c/\omega_r$$

- A. Zotter, S. A. Kheifets

$$D(\omega) = \omega_r / (j\omega), \quad D(\omega_r) = 1/j$$

- S. Y. Lee

$$D(\omega) = 2c / (b^2 \omega), \quad D(\omega_r) = 2c / (b^2 \omega_r),$$

$b$  – beam pipe radius

- G. Dome

$$D(\omega) = \omega_r^2 / (c\omega), \quad D(\omega_r) = \omega_r / c$$

- At the resonant frequency

$$R_s = |V_T|^2 / (2P),$$

where  $P$  is the power loss in the cavity walls and HOM damper for a given level of deflecting voltage  $V_T$  on the cavity axis (“circuit” definition, = 1/2 “linac”  $R_s$ )

- Measured  $R_s$  [Ohm] =  $Z_T c / \omega_r$
- Calculated - ...