



NOVEL DEVELOPMENTS IN R-MATRIX THEORY

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There is a worldwide effort to determine the best knowledge of nuclear reaction cross sections (nuclear data libraries)

 This is an important prerequisite for the development of new technologies in various fields (fusion research, advanced reactor techniques, medicine, safety issues, space science, materials testing,...

 General problem is the resonant behaviour at low incident collision energy, reflecting the many-body character of nuclei. (Especially, in light nuclear systems.)





Example: Neutron Cross Sections on ¹⁶O







Problems:

- Resonance range up to relatively high incident energies
- No predictive quantitative microscopic models



R-Matrix Theory

No microscopic information, but satisfies all conservation rules Proposed by Eisenbud and Wigner in the fifities of the last century



Standard R-Matrix Formalism: wave function







GECCCOS (GEneral Coupled-Channel COde System) A new comprehensive R-matrix code developed by T. Srdinko at TU Wien

New features compared with existing R-Matrix codes (SAMMY, AZUR, ...) but also compared to special codes like EDA, FRESCO, RAC, ...

New Features:

- ✓ Capability of calculabe R-Matrix calculations
- ✓ Possibility of hybrid R-Matrix approach
- ✓ Analysis procedures based on different optimization procedures
- ✓ Allowing for combined analysis of observables and S-matrices
- ✓ Transformation of R-matrices to different matching radii

Current Developments

- Development of R-matrix formulations for three-body channels (breakup)
- Reduced R-matrix parametrisations accounting for thresholds of non-explicitly treated channel



Elastic excitation functions





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Light Nuclear Systems: Further Challenge



n-induced Reactions

⁹Be(n,n)⁹Be Q= 0.0000 MeV ${}^{9}\text{Be}(n,\alpha){}^{6}\text{He}$ Q= -0.5971 MeV ${}^{9}\text{Be}(n,2n\alpha)^{4}\text{He}$ Q= -1.6636 MeV 9 Be(n,n α)(5 He) Q= -2.3073 MeV ⁹Be(n,t)⁷Li Q=-10.4373 MeV ⁹Be(n,p)⁹Li Q=-12.8248 MeV 9 Be(n,t α)t Q=-12.9049 MeV ⁹Be(n,d)(⁸Li) Q=-14.6615 MeV ⁹Be(n,t)(⁸Li) Q=-14.6615 MeV ⁹Be(n,nd)⁷Li Q=-16.6932 MeV Q=-16.8861 MeV ⁹Be(n,np)(⁸Li) ⁹Be(n,nt)⁶Li Q=-17.6871 MeV 9 Be(n, α) 6 Li Q=-19.2874 MeV ⁹Be(n,pt)⁶He Q=-20.4108 MeV ${}^{9}\text{Be}(n, {}^{3}\text{He})({}^{7}\text{He})$ Q=-21.5845 MeV ${}^{9}\text{Be}(n,p\alpha)({}^{5}\text{H})$ Q=-23.1857 MeV

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R-Matrix Formalism: Concept





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Three-body formalism of Glöckle





expansion of wave function in D: set of basis functions $\phi_{\mu}(\mathbf{r}, \mathbf{R}) = X_{\mu_{1}}(\mathbf{r}) Y_{\mu_{2}}(\mathbf{R})$ $\left[-\frac{1}{2\mu_{jk}} \frac{d^{2}}{dr^{2}} + V(\mathbf{r}) - \varepsilon_{\mu_{1}}^{i}\right] X_{\mu_{1}}(\mathbf{r}) = 0 ,$ $\left[-\frac{1}{2\mu_{i(jk)}} \frac{3}{4} \frac{d^{2}}{dR^{2}} - \varepsilon_{\mu_{2}}^{i}\right] Y_{\mu_{2}}(\mathbf{R}) = 0$

algebraic system of linear equations for the coefficients c^{i}_{μ}

$$A \cdot c = B[T_b, T(k)]$$

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Calculation of cross sections



Breakup cross section:

$$\sigma_{breakup} = 16\pi \left(\frac{\mu_{1(23)}}{m_n}\right)^2 \frac{1}{Q^2} \int_{-1}^{1} \mathrm{d}x \int_{0}^{\sqrt{2\mu_{23}E}} \mathrm{d}k_1 Q_{k_1} k_1^2 \left|\frac{T_1(k_1)}{k_1} + \frac{T_2(k_2(x))}{k_2(x)} + \frac{T_3(k_3(x))}{k_3(x)}\right|^2$$

Elastic cross section:

$$\sigma_{elastic} = 2\mu_{1(23)}m_n \left(\frac{c^2}{\hbar^2 c^2}\right)^2 \frac{1}{Q^2} |T_b|^2$$

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- E_b=-2.225 MeV
- Potential of Reid soft core type: $V(r) = -10463 \frac{e^{-\mu r}}{\mu r} - a \frac{e^{-4\mu r}}{\mu r} + b \frac{e^{-7\mu r}}{\mu r}$

a and b determined by fitting to Nijmegen phase shift data and E_b (*Phys. Rev.* C **48 (1974)**792)

for np interaction: a=1650.6 MeV, b=5371.5 MeV

for nn interaction: a=1210,4 MeV, b=4257,5 MeV

Regularization of the system of linear equations

$$\mathbf{A} \cdot \mathbf{c} = \mathbf{B}[\mathbf{T}_{b}, \mathbf{T}(\mathbf{k})] \rightarrow (\mathbf{A} + \eta) \cdot \mathbf{c} = \mathbf{B}[\mathbf{T}_{b}, \mathbf{T}(\mathbf{k})]$$

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3-Body R-Matrix Calculation: Deuteron Breakup $n+d \rightarrow n+n+p$





incident energy [MeV]

First calculation based on a three-body R-matrix:

required substantial modifications of original Glöckle formalism:

- conditions on basis functions, bound state corrections, ...
- regularisation of linear equations

PhD thesis B. Raab



3-Body R-Matrix Calculation: Elastic Scattering $n+d \rightarrow n+d$





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Summary and Outlook



Generation of basic tools for the evaluation of nuclear reaction data of light nuclear systems

- Construction of the novel R-Matrix Code GECCCOS
- Development and Implementation of the first R-Matrix analysis based on the Faddeev equations
- Novel Parametrisation of the Reduced R-Matrix for analyses of incomplete reaction data



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Tanja Stary and BA students

Thank you for your attention

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In nuclear physics the number of energetically open channels rises significantly with increasing energy.

Unitary treatment of R-matrix description becomes increasingly difficult

- a) experimental data are only available for a limited number of channels
- b) there are channels which cannot be described by R-matrix theory
- c) R-matrix analyses become numerically involved

Lane and Thomas introduced the REDUCED R-MATRIX FORMALISM

A.M.Lane, R.G. Thomas, Rev. Modern Physics 30 (1958) 257 chapter 10

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Development of adequate reduced R-matrix parametrisation





Maintaining the S-matrix elements of S_{rr} equivalent leads to the following relationship (Lane & Thomas)

$$\tilde{\mathbf{R}}_{\mathrm{rr}} = \mathbf{R}_{\mathrm{rr}} + \mathbf{R}_{\mathrm{re}} \mathbf{L}_{\mathrm{e}}^{\mathrm{O}} \left[1 - \mathbf{R}_{\mathrm{ee}} \mathbf{L}_{\mathrm{e}}^{\mathrm{O}} \right]^{-1} \mathbf{R}_{\mathrm{er}}$$
$$\tilde{\mathbf{R}}_{\mathrm{er}} = \left[1 - \mathbf{R}_{\mathrm{ee}} \mathbf{L}_{\mathrm{e}}^{\mathrm{O}} \right]^{-1} \mathbf{R}_{\mathrm{er}}$$

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Novel Parametrisation for Reduced R-Matrix Analyses



Proposal based on exact solutions for elimination of channels In 2- and 3-channel systems

$$R_{cd} = \sum_{\lambda=1}^{N} \frac{\gamma_{\lambda}^{c} \gamma_{\lambda}^{d}}{E_{\lambda} - E} \implies \tilde{R}_{c,d} = \sum_{\lambda=1}^{N} \frac{\gamma_{\lambda}^{c} \gamma_{\lambda}^{d}}{E_{\lambda} - E - \sum_{m=M_{r}+1}^{M_{r}+M_{e}} L_{m} (k_{m}a) \sum_{\mu=1}^{N} (\gamma_{\mu}^{m})^{2} \frac{E_{\lambda} - E}{E_{\mu} - E}}{L_{m} (k_{m} \cdot a) = k_{m} \cdot a \frac{O'(k_{m} \cdot a)}{O(k_{m} \cdot a)}}$$

$$c, d = 1, 2, ..., M_{r} \qquad L_{m} (k_{m} \cdot a) = k_{m} \cdot a \frac{O'(k_{m} \cdot a)}{O(k_{m} \cdot a)}$$

Important feature: $L(k_m a) = -$ real

below threshold

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Preliminary Reduced R-Matrix Analysis: n+⁹Be elastic cross section





Preliminary Reduced R-Matrix Analysis: Reaction: n+⁹Be→ ⁶He+⁴He



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Determination of R-Matrix



$$\begin{split} & u_{i}\left(r_{i}, R_{i}\right) = \sum_{\mu} c_{\mu}^{i} \phi_{\mu}\left(r_{i}, R_{i}\right) \qquad c_{\mu}^{i} = \int \int_{D} dr \ dR \ \phi_{\mu}\left(r_{i}, R_{i}\right) \ u_{i}\left(r_{i}, R_{i}\right) \\ & = \int \sum_{\mu'} C_{\mu\mu'}^{(i)} c_{\mu'}^{(i)} + \sum_{\substack{j=1 \ j\neq i}}^{3} \sum_{\mu'} V_{\mu\mu'}^{(j)} c_{\mu'}^{(j)} & \text{equation for the coefficients } c_{\mu} \\ & = \frac{1}{2\mu_{i(jk)}} QM_{\mu b} \cos(QA_{i}) - iQM_{\mu b} e^{iQA_{i}}T_{i}^{b} & T_{i}\left(k\right) \\ & - \frac{2}{\pi} \int_{0}^{\sqrt{2\mu_{jk}E}} dk \left[iQ_{k}M_{\mu k}^{(-)} e^{iQ_{k}A_{i}} + \frac{\mu_{i(jk)}}{\mu_{jk}} ikM_{\mu Q_{k}} e^{ika_{i}} \right] T_{i}(k) \\ & - \sum_{\substack{j=1 \ j\neq i}}^{3} \frac{ie^{i\sqrt{2\mu_{j(k)}E} \frac{m_{i}}{m_{i}+m_{k}}A_{i}/\sin\varphi_{j}^{*}}{A_{i}^{3/2}} T_{i}\left(\sqrt{2\mu_{jk}E}\cos\varphi_{j}^{*}\right) \\ & \times \left(N_{b}(E)M_{\mu b} \frac{2\mu_{i(jk)}}{\mu_{j(ik)}\left(E - \frac{2Q^{2}}{\mu_{j(ik)}}\sin^{2}\varphi_{j}^{*}\right)} \int_{0}^{r_{0i}} dr \ u_{i}^{b}(r)V_{i}(r) \\ & + \frac{2}{\pi}N_{k}(E) \int_{\sqrt{2\mu_{jk}E}}^{\infty} dk \ M_{\mu k}^{(-)} \frac{1}{\frac{1}{\mu_{jk}}k^{2} - 2E + 2\frac{\mu_{j(ik)}}{\mu_{j(ik)}}E\left(\frac{m_{i}}{(m_{i}+m_{k})\sin\varphi_{j}^{*}}\right)^{2}} \int_{0}^{r_{0i}} dr \ u_{k}^{(-)*}(r)V_{i}(r) \end{pmatrix} \end{split}$$

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Boundary conditions



$$2) \sum_{\mu} M_{\mu b} c_{\mu}^{(i)} \simeq \sin(QA_{i}) - 2\mu_{i(jk)} e^{iQA_{i}} T_{i}^{b}$$

$$3) \sum_{\mu} c_{\mu}^{(i)} \varphi_{\mu}(r_{i}, A_{i}) - u_{i}^{b}(r_{i}) \left[\sin(QA_{i}) - 2\mu_{i(jk)} e^{iQA_{i}} T_{i}^{b} \right]$$

$$\simeq (2\mu_{i(jk)})^{3/2} \sqrt{2\mu_{jk}} \sqrt{\frac{2}{\pi}} e^{i\frac{\pi}{4}} E^{1/4} \frac{e^{i\rho_{A}\sqrt{E}}}{\rho_{A}^{1/2}} \frac{A_{i}}{\rho_{A}} T_{i} \left(2\mu_{jk}\sqrt{E} \frac{r_{i}}{\rho_{A}} \right)$$

$$4) \sum_{\mu} c_{\mu}^{(i)} \varphi_{\mu}(a_{i}, R_{i}) \simeq (2\mu_{i(jk)})^{3/2} \sqrt{\frac{2}{\pi}} e^{i\frac{\pi}{4}} E^{1/4} \frac{e^{i\rho_{a}\sqrt{E}}}{\rho_{a}^{1/2}} \frac{R}{\rho_{a}} T_{i} \left(2\mu_{jk}\sqrt{E} \frac{a_{i}}{\rho_{a}} \right)$$

with
$$\rho_A = \sqrt{2\mu_{jk}r_i^2 + 2\mu_{i(jk)}A_i^2}$$
 $\rho_a = \sqrt{2\mu_{jk}a_i^2 + 2\mu_{i(jk)}R_i^2}$

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T-amplitudes



Transition amplitude from channel α to β :

$$T_{\beta\alpha} = \left\langle \phi_{\beta} \left| V^{\beta} \right| \Psi_{\alpha}^{(+)} \right\rangle$$

$$T_i^b = \int_0^\infty \mathrm{d}R \int_0^\infty \mathrm{d}r \; \frac{\sin(QR)}{Q} u_i^b(r) V_i(r) Q_i(r,R)$$

Elastic or rearrangement

$$T_{i}(k) = \int_{0}^{\infty} \mathrm{d}R \int_{0}^{\infty} \mathrm{d}r \; \frac{\sin(Q_{k}R)}{Q_{k}} u_{k}^{(-)*}(r)V_{i}(r)Q_{i}(r,R)$$

Breakup

with
$$Q_i(r_i, R_i) = \int_{-1}^{1} \mathrm{d}x_i \ r_i R_i \frac{1}{2} \sum_{\substack{j=1 \ j \neq i}}^{3} \frac{u_j(r_j, R_j)}{r_j(x_i) R_j(x_i)}$$

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