

Superconducting magnet optimisation and modelling of magnetic shields with GetDP



TECHNISCHE
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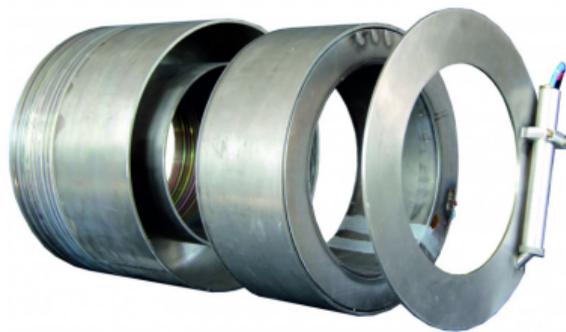
Superconducting confinement magnet

- 2D magnetostatics and optimization



Cryogenic current comparator

- 2.5D magnetostatics



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PUMA in a nutshell I

This project is part of the PUMA experiment

PUMA: antiProton Unstable Matter Annihilation

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PUMA: antiProton Unstable Matter Annihilation

What does PUMA aim at?

Measurement of the **neutron/proton ratio** at the **surface** of heavy nuclei

PUMA in a nutshell I

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PUMA: antiProton Unstable Matter Annihilation

What does PUMA aim at?

Measurement of the **neutron/proton ratio** at the **surface** of heavy nuclei

Why antiprotons?

High probability that antiprotons interact at the **surface** of a nucleus

PUMA in a nutshell II

How will it work?

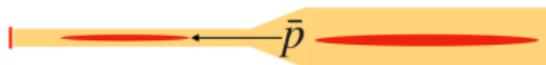
1. Store antiprotons in a reservoir trap



PUMA in a nutshell II

How will it work?

1. Store antiprotons in a reservoir trap
2. Transfer some antiprotons to a collision trap



PUMA in a nutshell II

How will it work?

1. Store antiprotons in a reservoir trap
2. Transfer some antiprotons to a collision trap
3. Introduce the heavy nuclei in the collision trap

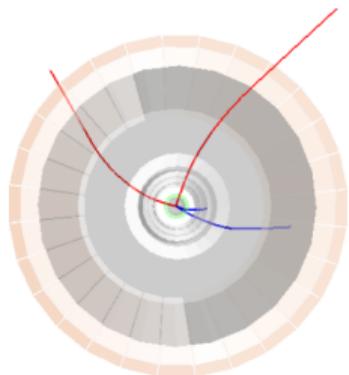
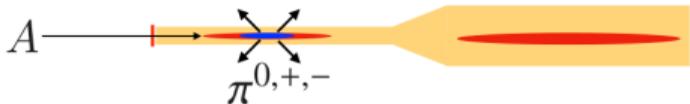


PUMA in a nutshell II

How will it work?

1. Store antiprotons in a reservoir trap
2. Transfer some antiprotons to a collision trap
3. Introduce the heavy nuclei in the collision trap
4. Antiprotons interact with **surface** nucleons \longrightarrow emission of **pions** (subatomic particles)

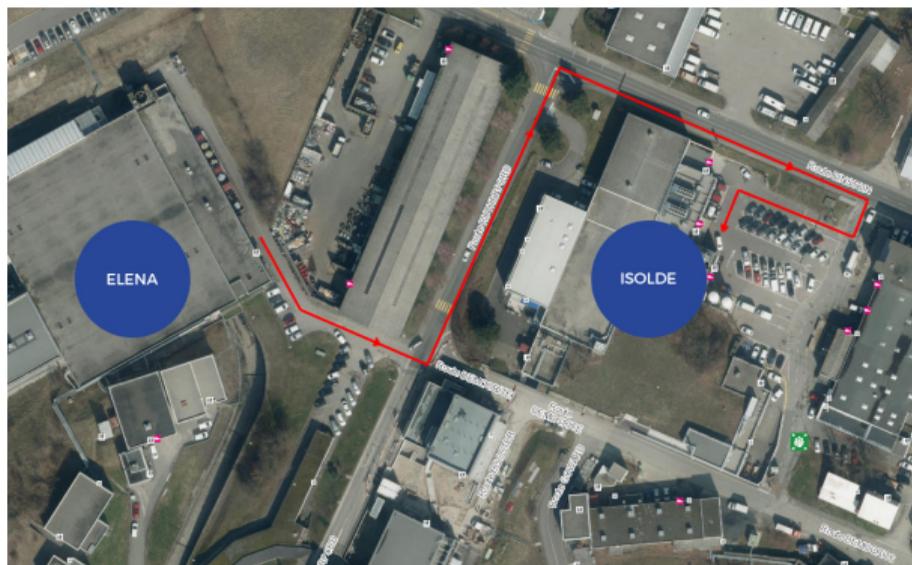
The **charge of a pion** tells us if we annihilated a proton or a neutron



PUMA in a nutshell III

Where do we find heavy nuclei and antimatter?

- At CERN :-)
 - PUMA has been recently accepted as a new CERN experiment (17/03/2021)
 - **No beamline** allowing collisions between antimatter and heavy nuclei



Transportable antimatter trap

PUMA in a nutshell IV

Which question did we try to answer in this project?

Is it possible to build a **confinement magnet** with both

- active shielding
- passive shielding

given **constraints** on the

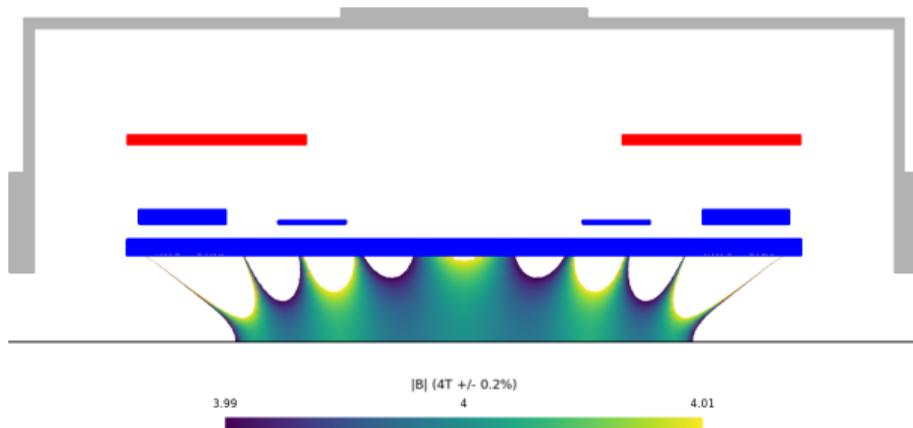
- the weight
- the geometry (bore radius, total length, ...)
- the **b**-field (strength, quality, far field)?

→ Lots of iterations with the team designing the experiment :-)!

PUMA in a nutshell V

Magnetic pre-design with GetDP

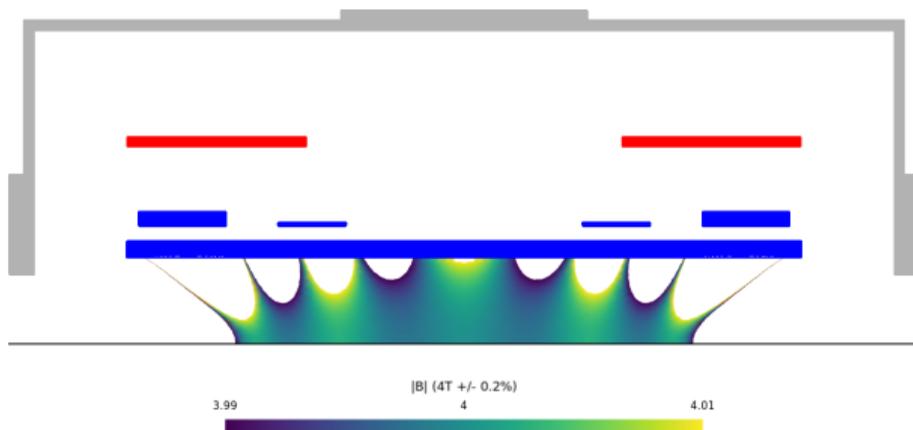
- Axisymmetric 2D magnetostatics



PUMA in a nutshell V

Magnetic pre-design with GetDP

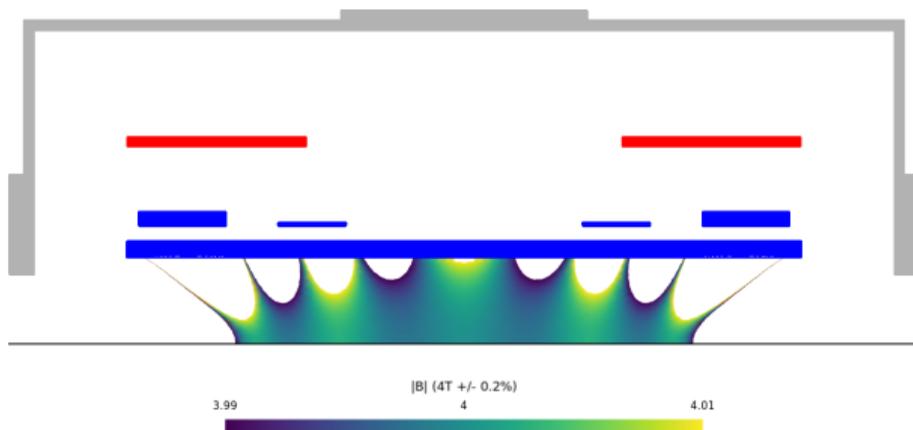
- Axisymmetric 2D magnetostatics
- Optimization problem



PUMA in a nutshell V

Magnetic pre-design with GetDP

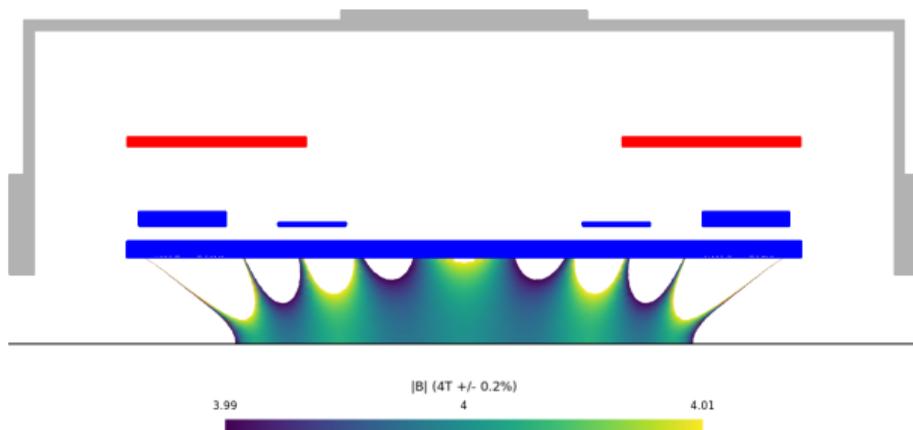
- Axisymmetric 2D magnetostatics
- Optimization problem
 - As light as possible
 - As compact as possible



PUMA in a nutshell V

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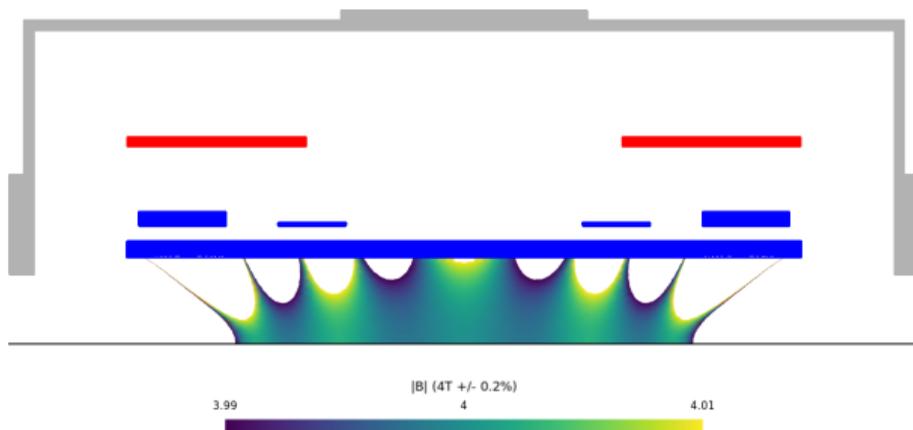
- Axisymmetric 2D magnetostatics
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 - As light as possible
 - As compact as possible
 - 4T with 2 homog. regions
 - Low far field



PUMA in a nutshell V

Magnetic pre-design with GetDP

- Axisymmetric 2D magnetostatics
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 - As light as possible
 - As compact as possible
 - 4T with 2 homog. regions
 - Low far field
 - Avoid shield saturation
 - Quench margin (load line)

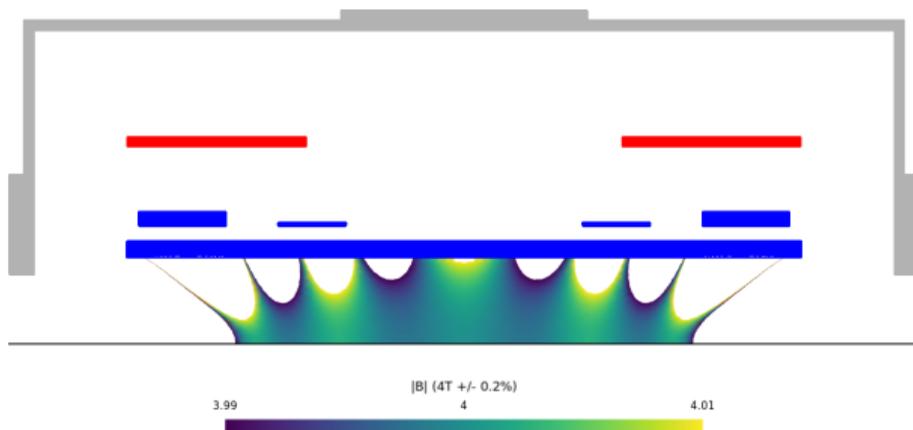


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25 parameters



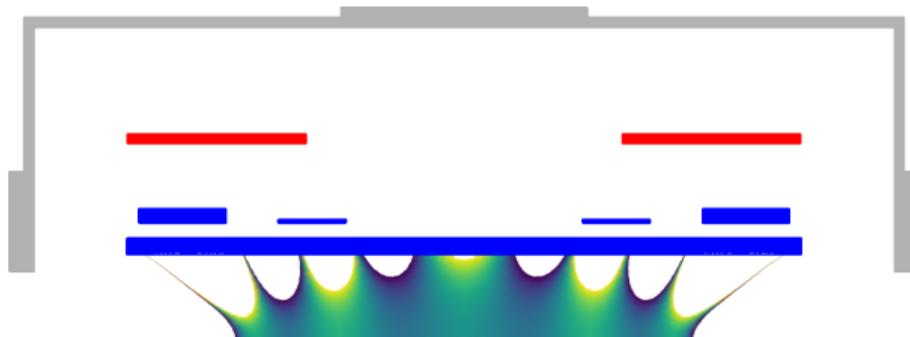
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Magnetic pre-design with GetDP

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25 parameters

- Final design by Bilfinger Noell
 - Coils and shield: $\sim 1t + \sim 2t$
 - Total: $\sim 7t$



Formulation of the problem

Find τ and j_s that minimize W such that:

[SI units]

$$\begin{aligned}\tau_{\min} &\leq \tau \leq \tau_{\max} \\ j_{s,\min} &\leq j_s \leq j_{s,\max} \\ 3.992 &\leq b_{R1} \leq 4.008 \\ 3.800 &\leq b_{R2} \leq 4.200 \\ b_{3m} &\leq 2 \times 10^{-4} \\ b_{sh} &\leq 1.5 \\ Ll &\leq 0.8 \\ \mathbf{b} &= \mathbf{curl} \mathbf{a}\end{aligned}$$

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$$Ll \leq 0.8 \longrightarrow \text{Quench margin (load line criterion) @6K}$$

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$$\mathbf{b} = \text{curl } \mathbf{a} \longrightarrow \text{GetDP!}$$

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- $\mathbf{b}_{sh} \leq 1.5$ \longrightarrow Avoid shield saturation
- $Ll \leq 0.8$ \longrightarrow Quench margin (load line criterion) @6K
- $\mathbf{b} = \mathbf{curl} \mathbf{a}$ \longrightarrow GetDP!

With $\mathbf{a} \in H_0(\mathbf{curl}, \Omega)$ such that:

$$\int_{\Omega} \nu \mathbf{curl} \mathbf{a} \cdot \mathbf{curl} \mathbf{a}' d\Omega - \int_{\Omega} \mathbf{j}_s \cdot \mathbf{a}' d\Omega = 0 \quad \forall \mathbf{a}' \in H_0(\mathbf{curl}, \Omega)$$

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Note that we assume that each coil has its **own power source**

→ Some technological details were unknown (e.g. cable cross section, fill factor, ...)

→ Optimizing for the same current in each coil is also possible

GetDP: Jacobian and 2D axisymmetric problems

```
Jacobian{  
  { Name Jac; Case{ { Region All; Jacobian VolAxiSqu; } } }  
}
```

VolAxiSqu

→ Cylindrical coordinate system $(x, y, z) \rightarrow (r, z, \theta)$

→ together with the transformation $r \rightarrow \sqrt{\rho}$

$$\text{Leads to } \lim_{\rho \rightarrow 0} \det J \rightarrow \frac{1}{2}$$

instead of $\lim_{r \rightarrow 0} \det J \rightarrow 0$

[Henrotte et al., 1999]

GetDP: *bh* law

```
Function{
  mu0 = 4 * Pi * 1e-7;

  nu[NonMagnetic] = 1/mu0;
  nu[Magnetic]    = nuMag[$1]; // $1 = b
  dnu[Magnetic]   = 2 * dNudB2[$1] * SquDyadicProduct[$1];
}
```

- Differential reluctivity for Newton-Raphson: $\delta\nu = 2 \frac{\partial\nu}{\partial\|\mathbf{b}\|^2} \mathbf{b} \otimes \mathbf{b}$
- nuMag[] and dNudB2[] obtained by **linear interpolation** of a set of points $(\nu, \|\mathbf{b}\|^2)$ (list NuB2)
 - InterpolationLinear[SquNorm[\$1]]{List[NuB2]} for nuMag
 - dInterpolationLinear[SquNorm[\$1]]{List[NuB2]} for dNudB2

GetDP: FunctionSpace for a

```
FunctionSpace{
  { Name HCur12D; Type Form1P; // "1-form perpendicular to the domain"
    BasisFunction{
      { [...]; Function BF_PerpendicularEdge; Entity NodesOf[All]; }
      { [...]; Function BF_PerpendicularEdge_2E; Entity EdgesOf[All]; }
    }
    Constraint{ [...] }
  }
}
```

Perpendicular edge functions

2nd-order contributions

GetDP: Magnetostatic formulation (vector potential)

```
Formulation{
  { Name MVP; Type FemEquation;
    Quantity{ { Name a; Type Local; NameOfSpace HCur12D; } }
    Equation{
      Galerkin{ [nu[{d a}]*Dof{d a}, {d a}];          [...] }
      Galerkin{ [-js[], {a}];                          [...] }
      // Jacobian for Newton-Raphson
      Galerkin{ JacNL[dnu[{d a}]*Dof{d a}, {d a}]; [...] }
    }
  }
}
```

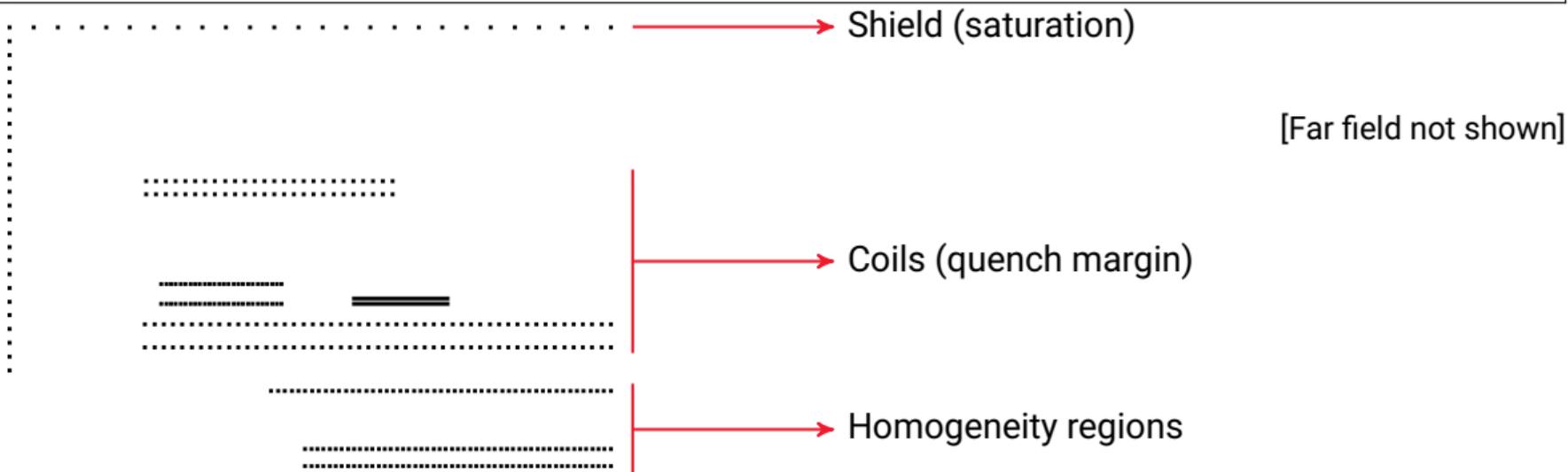
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One-to-one correspondence !

GetDP: Post-processing

```
PostOperation MVP UsingPost MVP{  
  For i In {1:MTot} // For each sampling line: bMag = Norm[{d a}]  
    Print[bMag, OnLine{ /*start point*/ } /*end point*/ } /*# of samples*/ },  
          File Sprintf["bMag%g.txt",i], Format SimpleTable];  
EndFor
```



Where were we?

We can now compute \mathbf{b} :-)

Do we have everything we need to optimize then?

- We used a **gradient-based** optimizer: (GC)MMA
- Implementation from the conveks library (part of ONELAB)
→ We need the **sensitivity** of \mathbf{b} with respect to τ and \mathbf{j}_s

[Kuci et al.]

Sensitivity analysis

[Kuci et al., 2017]

Sensitivity analysis I

Finite differences

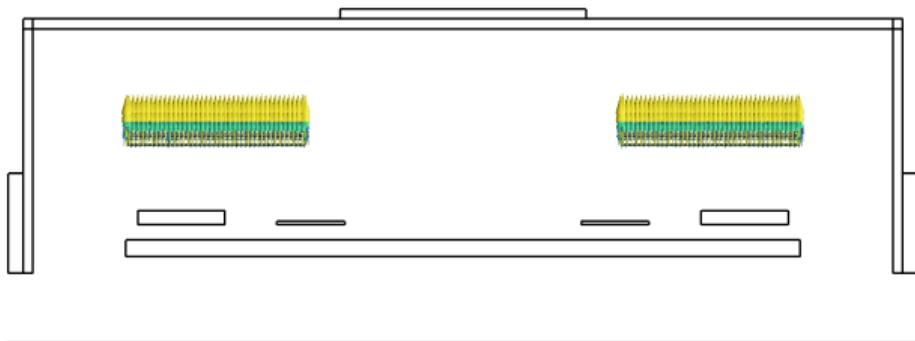
1. We **perturb** each design variable
2. **For each** perturbed design variable, we carry out a full **nonlinear** solve
3. We extract the sensitivity with a finite difference scheme

Easy to implement but slow

Sensitivity analysis II

Lie derivatives

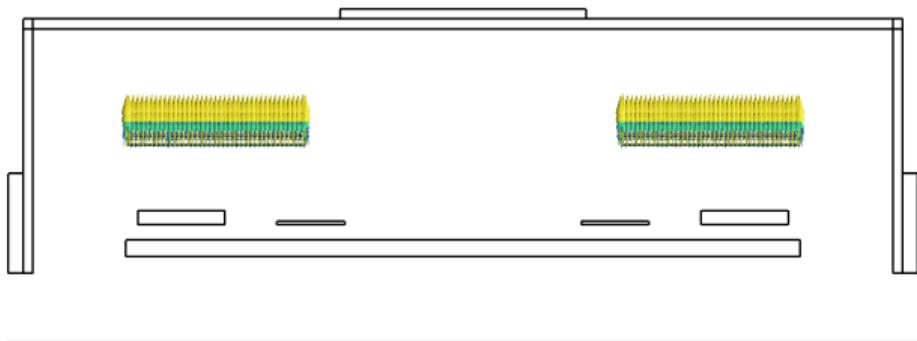
1. We define a **velocity field** for each design variable
→ How does the domain move when perturbing a variable?



Sensitivity analysis II

Lie derivatives

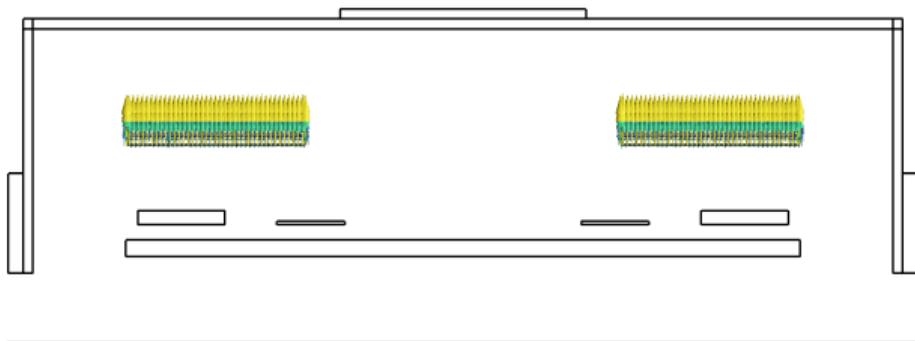
1. We define a **velocity field** for each design variable
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2. We solve a **finite element problem** to extract the derivative



Sensitivity analysis II

Lie derivatives

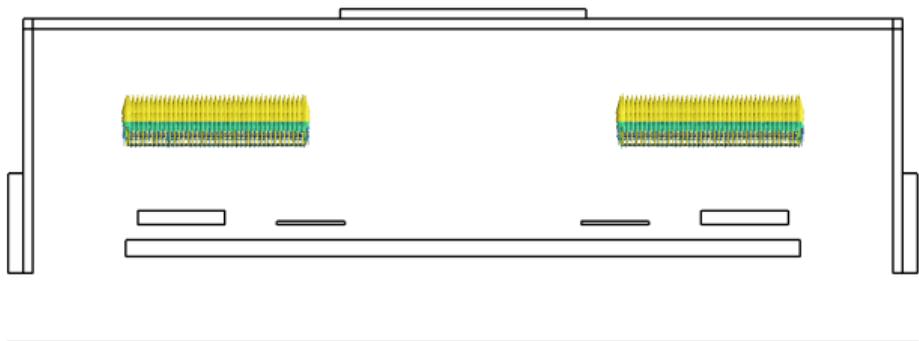
1. We define a **velocity field** for each design variable
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2. We solve a **finite element problem** to extract the derivative
3. **Same system matrix** as the one obtained at the last Newton iteration when computing \mathbf{a}
→ LU factorization can be **reused**



Sensitivity analysis II

Lie derivatives

1. We define a **velocity field** for each design variable
→ How does the domain move when perturbing a variable?
2. We solve a **finite element problem** to extract the derivative
3. **Same system matrix** as the one obtained at the last Newton iteration when computing \mathbf{a}
→ LU factorization can be **reused**



Fast sensitivity analysis!

GetDP: sensitivity analysis I

1. We compute the velocity field \mathbf{v} associated with each parameter τ_i
→ Done by Gmsh: one .msh file per **perturbation** of τ_i
2. New FunctionSpace (same as \mathbf{a})
3. New Formulation

GetDP: sensitivity analysis II

```
Resolution{
  { Name Optimization;
    System{
      { Name MVP; NameOfFormulation MVP; } // Compute b = curl a
      { Name LIE; NameOfFormulation LIE; } // Sensitivity analysis
    }
    Operation{
      // MVP //
      //////////////
      InitSolution[MVP];
      IterativeLoop[NL_maxit, NL_stop, NL_relax]{ // Newton-Raphson
        GenerateJac[MVP];
        SolveJac[MVP];
      }
      PostOperation[MVP]; // Evaluate bMag
      [...]
    }
  }
}
```

GetDP: sensitivity analysis III

```
[...]
// Sensitivity analysis //
////////////////////////////////////
InitSolution[LIE];

// Shape variables
For i In {0:NShapeVariables-1}
  GmshRead[Sprintf("velocity_%g.msh", i), Vi]; // Velocity field i
  Generate[LIE];                               // Only RHS relevant
  SolveAgainWithOther[LIE, MVP];              // Reuse LU of MVP
  PostOperation[Get_Lie~{i}];                 // Evaluate d(B)
EndFor
[...]
```

→ With design variables that are not related to shape (J_s): $\mathbf{v} = \mathbf{0}$

Where were we?

We can now carry out the sensitivity analysis :-)

Let's glue everything together!

Optimizer/GetDP/Gmsh coupling I

Overview

```
c      = onelab.client(__file__)           # New client
design = getDesignVariables(c.getAllParameters()) # Design variables
solver = Solver(c, design, 'magnet.geo', 'magnet.pro') # Homemade wrapper
[...]
```

Optimizer/GetDP/Gmsh coupling I

Overview

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[...]
while it <= maxIter:
    solver.setVariables(conveks.mma.getCurrentPoint()) # New var. from opt.
```

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[...]
while it <= maxIter:
    solver.setVariables(conveks.mma.getCurrentPoint()) # New var. from opt.
    solver.mesh()      # Mesh
    solver.velocity()  # Velocity fields (mesh perturbation)
    solver.solve()     # GetDP (B-field and sensitivity)
```

Optimizer/GetDP/Gmsh coupling I

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    solver.solve()        # GetDP (B-field and sensitivity)

obj       = solver.objective()      # Objective function (weight)
dObj      = solver.dObjective()     # Derivatives of objective function
cons      = solver.constraints()    # Constraints (<0: OK / >0: KO)
dCons     = solver.dConstraints()   # Derivatives of constraints
```

Optimizer/GetDP/Gmsh coupling I

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c          = onelab.client(__file__)           # New client
design     = getDesignVariables(c.getAllParameters()) # Design variables
solver    = Solver(c, design, 'magnet.geo', 'magnet.pro') # Homemade wrapper
[...]

while it <= maxIter:
    solver.setVariables(conveks.mma.getCurrentPoint()) # New var. from opt.
    solver.mesh()          # Mesh
    solver.velocity()     # Velocity fields (mesh perturbation)
    solver.solve()        # GetDP (B-field and sensitivity)

obj       = solver.objective()      # Objective function (weight)
dObj      = solver.dObjective()     # Derivatives of objective function
cons      = solver.constraints()    # Constraints (<0: OK / >0: KO)
dCons     = solver.dConstraints()   # Derivatives of constraints

conveks.mma.updateCurrentPoint(obj, dObj, cons, dCons) # Call optimizer
```

Optimizer/GetDP/Gmsh coupling II

A few useful methods of Solver

```
def solve(self):
    """Call GetDP"""
    self.c.runSubClient('myGetDP', 'getdp magnet.pro -solve Optimization')

def mesh(self):
    """Call Gmsh (need -parametric for mesh perturbation)"""
    self.c.runSubClient('myGmsh', 'gmsh -parametric magnet.geo -')

def objective(self):
    """Objective function (computed by Gmsh, transferred via ONELAB)"""
    return self.c.getNumber('Optimization/Objective')
```

- Same ideas for dObjective, constraints and dConstraints
- Constraints handled with text files instead of ONELAB

Optimizer/GetDP/Gmsh coupling III

User data file

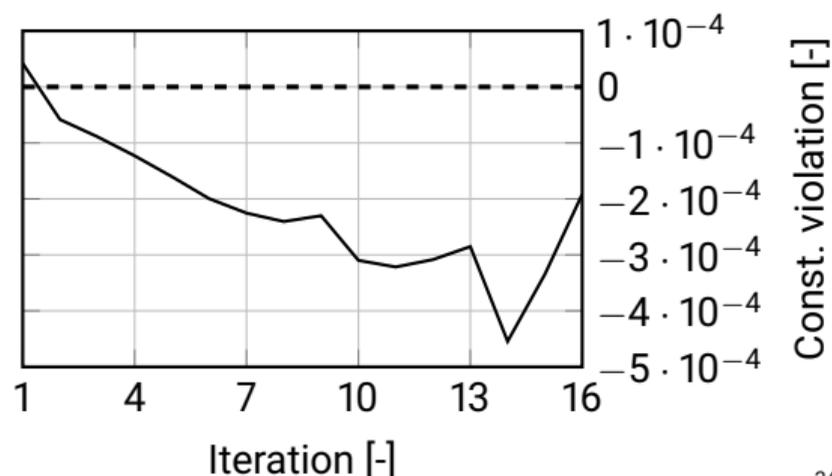
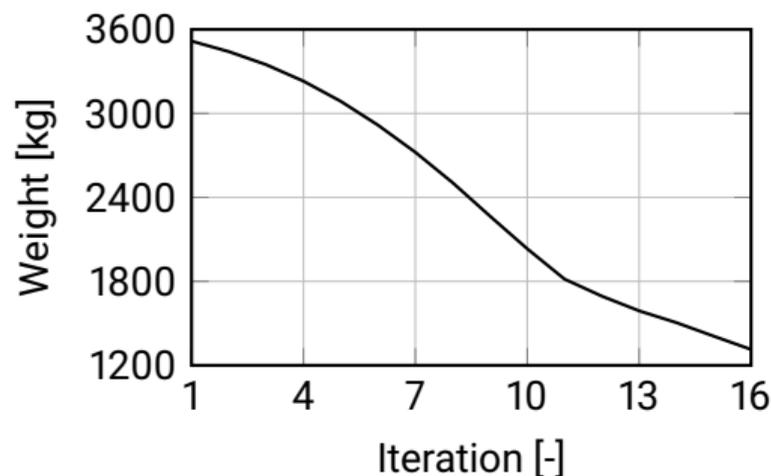
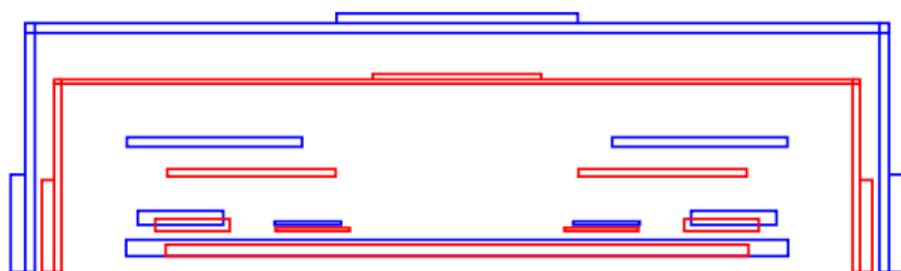
```
mm = 1e-3;  
DefineConstant[  
  [...]  
  H5 = { 20*mm, Name "0Geo/SH5", Opti "1", OptiLw "5e-3", OptiUp "*2" }  
  [...]  
];
```

User defined attributes: Opti, OptiLw and OptiUp

- `c.getAllParameters()`: fetches all variables and their attributes (pre- and user-defined)
- `getDesignVariables(...)`: homemade parser (regular expressions)

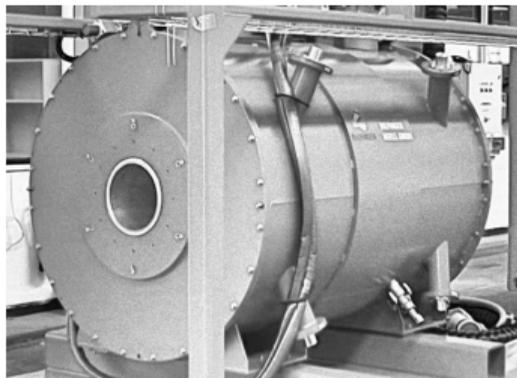
Optimizer: example

Example test case: optimization for a field magnitude of **2T** instead of **4T**



Superconducting confinement magnet

- 2D magnetostatics and optimization



Cryogenic current comparator

- 2.5D magnetostatics



CCC: cryogenic current comparator

What is a cryogenic current comparator (CCC)?

- One of the most sensitive instrument to measure **very low electric currents** with high accuracy

CCC: cryogenic current comparator

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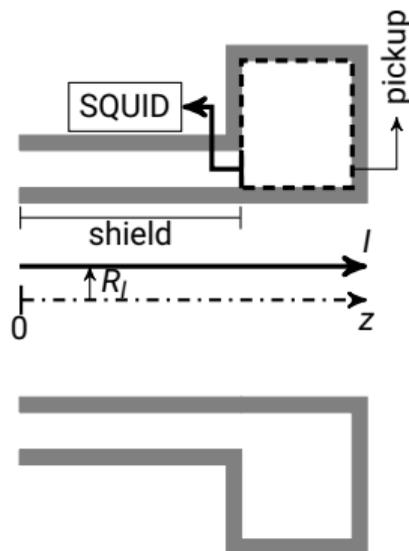
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- Diagnostics device: @CERN AD (in use), @FAIR (planned), ...

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Its key components are a magnetometer and a superconducting shield

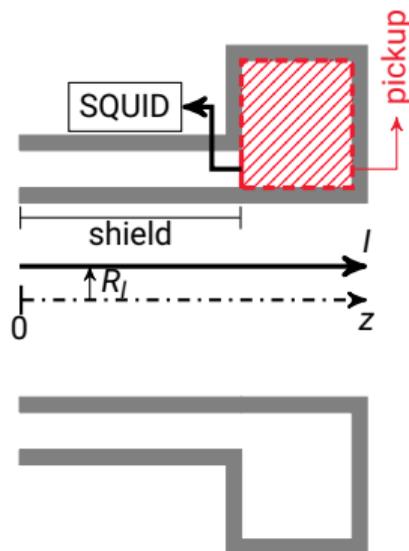


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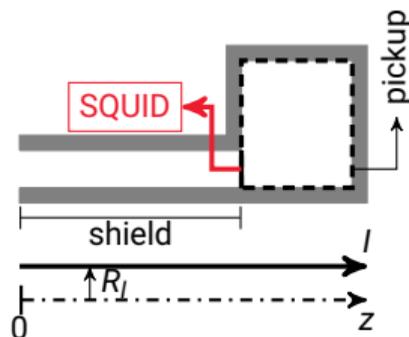
- Magnetometer
→ Superconducting pickup coil (flux transformer)

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■ Magnetometer

- Superconducting pickup coil (flux transformer)
- Superconducting Quantum Interference Device

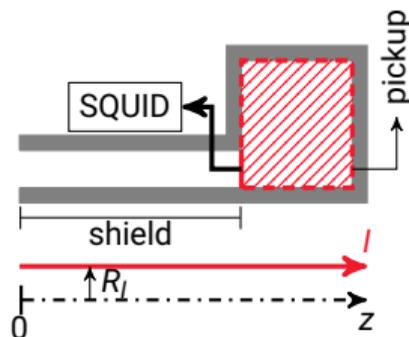


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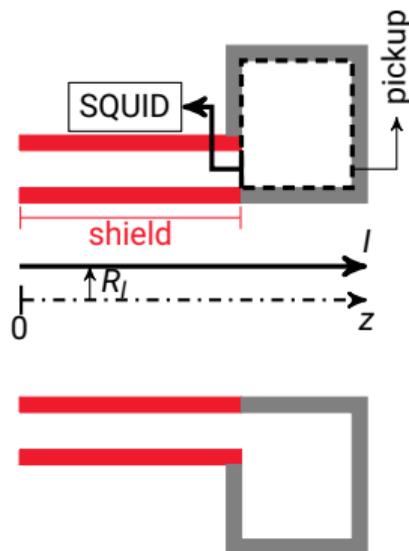


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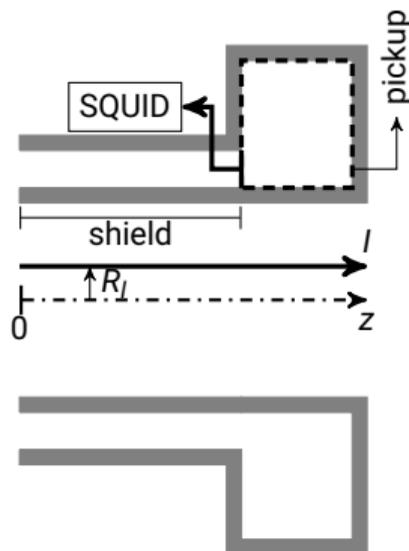
- Magnetometer
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 - Measures the \mathbf{b} -field induced by the current
- Shield acts as a magnetic filter
 - Damps all components of \mathbf{b} but the azimuthal one
 - We see \mathbf{b} as if I was located on the symmetry axis

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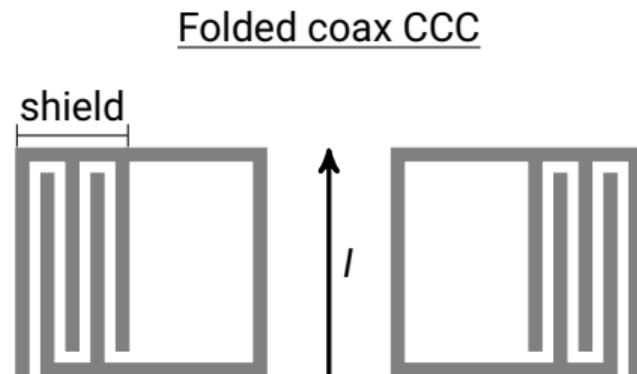
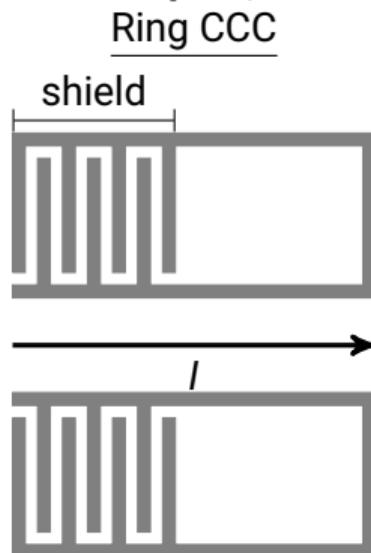


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Good position independence property

CCC: folded coaxial shield

For the CCC to be compact, the shield is usually folded into a meander structure



Unlike the ring design, the damping of the folded coax is theoretically unknown*

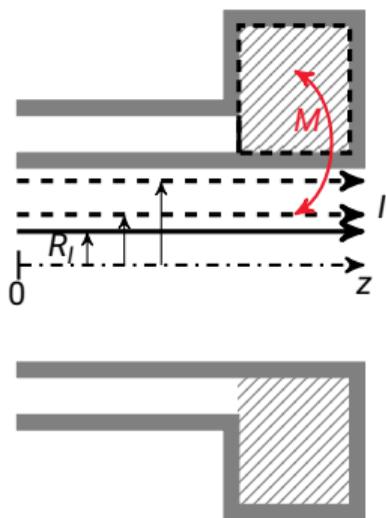
* to the best of our knowledge

→ Let's build a FE model :-)!

Why 2.5D FEM?

How can we determine the shield performance?

- Test different position of the current carrying wire and compute the mutual inductance M



Can we exploit symmetries?

- The CCC is axisymmetric
- But the excitation (the current carrying wire) is not

Use 2.5D modeling

2.5D FEM in a nutshell

Main idea

→ Decompose the full 3D field into a **Fourier series** along the **azimuthal direction** φ

$$\mathbf{a}(r, \varphi, z) = \begin{bmatrix} a_r^0(r, z) \\ a_\varphi^0(r, z) \\ a_z^0(r, z) \end{bmatrix} + \sum_{n=1}^{\infty} \left(\begin{bmatrix} a_r^n(r, z) \cos(n\varphi) \\ a_\varphi^n(r, z) \sin(n\varphi) \\ a_z^n(r, z) \cos(n\varphi) \end{bmatrix} + \begin{bmatrix} a_r^{-n}(r, z) \sin(n\varphi) \\ a_\varphi^{-n}(r, z) \cos(n\varphi) \\ a_z^{-n}(r, z) \sin(n\varphi) \end{bmatrix} \right)$$

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$$a_\varphi^{*,n} = r a_\varphi^n$$

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→ Make the following **ansatz** (not unique):

$$\mathbf{a}_\varphi^{*,n} = r \mathbf{a}_\varphi^n$$

→ By substitution into the magnetostatic weak formulation (vector potential), we end up with

For all $\mathbf{a}'_{rz} \in H_0(\mathbf{curl}, \Omega)$ and $\mathbf{a}_\varphi^{*,\prime} \in H_0^1(\Omega)$, find $\mathbf{a}_{rz}^n \in H_0(\mathbf{curl}, \Omega)$ and $\mathbf{a}_\varphi^{*,n} \in H_0^1(\Omega)$, such that:

$$\int_{\Omega} r \nu_0 \mathbf{curl} \mathbf{a}_{rz}^n \cdot \mathbf{curl} \mathbf{a}'_{rz} \, dr dz + n^2 \int_{\Omega} r^{-1} \nu_0 \mathbf{a}_{rz}^n \cdot \mathbf{a}'_{rz} \, dr dz + n \int_{\Omega} r^{-1} \nu_0 \mathbf{grad} \mathbf{a}_\varphi^{*,n} \cdot \mathbf{a}'_{rz} \, dr dz \\ + n \int_{\Omega} r^{-1} \nu_0 \mathbf{a}_{rz} \cdot \mathbf{grad} \mathbf{a}_\varphi^{*,\prime} \, dr dz + n \int_{\Omega} r^{-1} \nu_0 \mathbf{grad} \mathbf{a}_\varphi^{*,n} \cdot \mathbf{grad} \mathbf{a}_\varphi^{*,\prime} \, dr dz = \int_{\Omega} r \mathbf{j}_{rz}^n \cdot \mathbf{a}'_{rz} \, dr dz$$

where Ω is an **angular slice** of the 3D domain and where **curl** and **grad** are **2D** operators.

2.5D FEM: GetDP I

This is easily translated into GetDP scripting language

```
Jacobian{  
  { Name Vol; Case{ { Region All; Jacobian Vol; } } } }
```

→ Standard Jacobian, but more sophisticated weak formulation

2.5D FEM: GetDP II

```

Formulation{
  { Name MagStaA; Type FemEquation;
    Quantity{
      { Name aRZ; Type Local; NameOfSpace HCurl; }
      { Name aPhiS; Type Local; NameOfSpace HGrad; }
      { Name xi; Type Local; NameOfSpace HGradXi; } // Gauge !
    }
    Equation{ // R[] = X[]
      Galerkin{ [ R[]*Nu0*Dof{d aRZ}, {d aRZ}]; In Omega; [...] } // Integrals tested by aRZ
      Galerkin{ [$N^2/R[]*Nu0*Dof{ aRZ}, {aRZ}]; In Omega; [...] } // |
      Galerkin{ [$N^1/R[]*Nu0*Dof{d aPhiS}, {aRZ}]; In Omega; [...] } // |
      Galerkin{ [$N^1/R[]*Nu0*Dof{aRZ}, {d aPhiS}]; In Omega; [...] } // Integrals tested by aPhiS
      Galerkin{ [ 1/R[]*Nu0*Dof{d aPhiS}, {d aPhiS}]; In Omega; [...] } // |
      Galerkin{ [-R[] * Ji[$N], {aRZ}]; In Src; [...] } // RHS

      // Gauge condition! (Coulomb)
      Galerkin{ [ +R[]*Dof{d xi}, {aRZ}]; In Omega; [...] } // Integral tested by aRZ
      Galerkin{ [-$N/R[]*Dof{xi}, {aPhiS}]; In Omega; [...] } // Integral tested by aPhiS
      Galerkin{ [ +R[]*Dof{aRZ}, {d xi}]; In Omega; [...] } // Integrals tested by xi
      Galerkin{ [-$N/R[]*Dof{aPhiS}, {xi}]; In Omega; [...] } // |
    } } }
  
```

$$\int_{\Omega} r \nu_0 \mathbf{curl} \mathbf{a}_{rZ}^n \cdot \mathbf{curl} \mathbf{a}'_{rZ} \, drdz + \int_{\Omega} n^2 r^{-1} \nu_0 \mathbf{a}_{rZ}^n \cdot \mathbf{a}'_{rZ} \, drdz + \int_{\Omega} n r^{-1} \nu_0 \mathbf{grad} \mathbf{a}_{\varphi}^{*,n} \cdot \mathbf{a}'_{rZ} \, drdz \\
 + \int_{\Omega} n r^{-1} \nu_0 \mathbf{a}_{rZ} \cdot \mathbf{grad} \mathbf{a}_{\varphi}^{*,'} \, drdz + \int_{\Omega} n r^{-1} \nu_0 \mathbf{grad} \mathbf{a}_{\varphi}^{*,n} \cdot \mathbf{grad} \mathbf{a}_{\varphi}^{*,'} \, drdz - \int_{\Omega} r j_{rZ}^n \cdot \mathbf{a}'_{rZ} \, drdz = 0$$

2.5D FEM: GetDP III

```
Resolution{
  { Name MagStaA;
    System{
      { Name A; NameOfFormulation MagStaA; }
    }
    Operation{
      Evaluate[$MTot = 0];           // Init
      For i In {0:NTot-1}           // Loop on modes
        Evaluate[$N = i];           // --> Mode i
        Generate[A];                // --> Generate
        Solve[A];                   // --> Solve
        PostOperation[ComputeM];    // --> Compute M
        Evaluate[$MTot = $MTot + $M]; // --> Add contribution to MTot
      EndFor
    } // NB: mode-per-mode analysis is also possible
  }
}
```

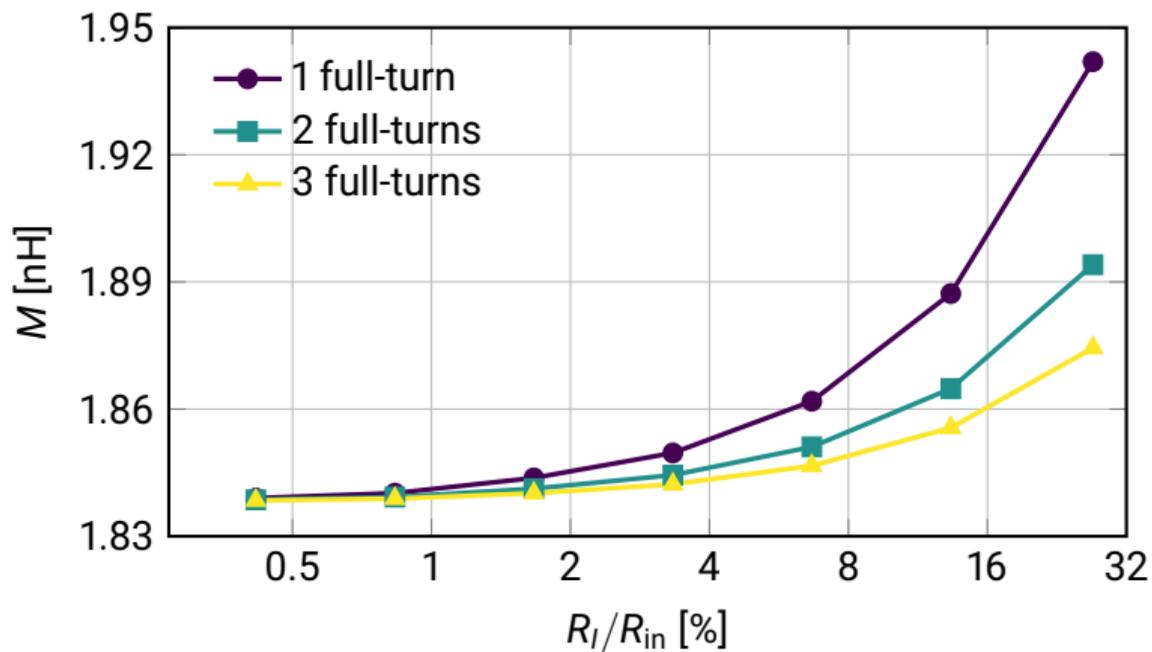
2.5D FEM: GetDP IV

```
PostProcessing{
  { Name MagStaA; NameOfFormulation MagStaA;
    PostQuantity{
      [...]
      { Name Phi; Value{ Integral{ [{aRZ}*Tangent[]];          [...] } } }
      { Name M;   Value{      Term{ [$Phi/I0]; Type Global; [...] } } }
    } } }
```

```
PostOperation ComputeM UsingPost MagStaA{
  Print[Phi[Loop], OnGlobal,          Format Table, StoreInVariable $Phi];
  Print[M,          OnRegion Dummy, Format Table, StoreInVariable $M,
    SendToServer "Output/02Modal M"];
}
```

2.5D FEM: Solution

Test case: M with 4 modes



CCC: mechanics I

Large CCCs are not axisymmetric because of mechanical deformations and vibrations

Do **deformations** and **vibrations** have a non-negligible impact on the performance of the CCC?

→ 3D elastodynamics eigenmode analysis + magnetostatics (assuming perfect screening)

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Linear elastodynamics

- 3D displacement field
 - One `FunctionSpace` per component
- Resolution
 - `EigenSolve[A, NEig, Reθ, Imθ]`

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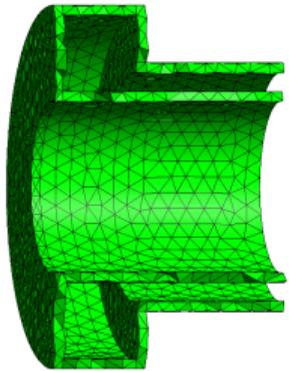
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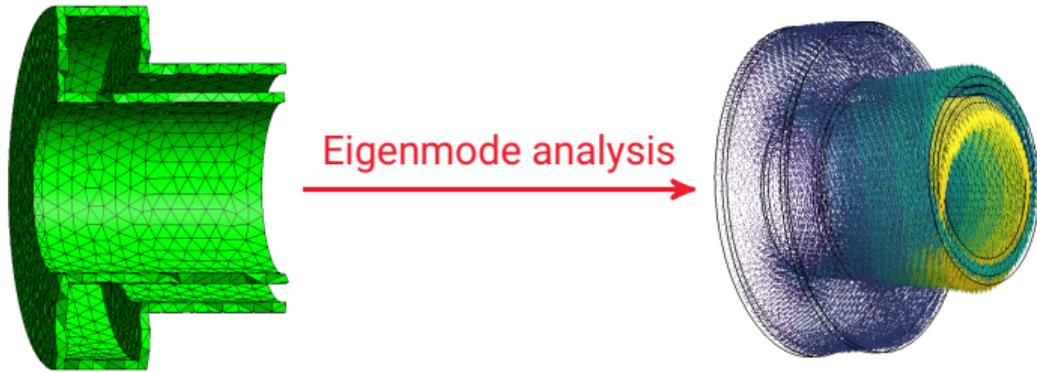
Magnetostatics

- 3D vector potential
 - M is straightforward
- Gauge condition (spanning tree):
 - `EdgesOfTreeIn (GetDP)`
 - `Plugin(SpanningTree) (Gmsh)`

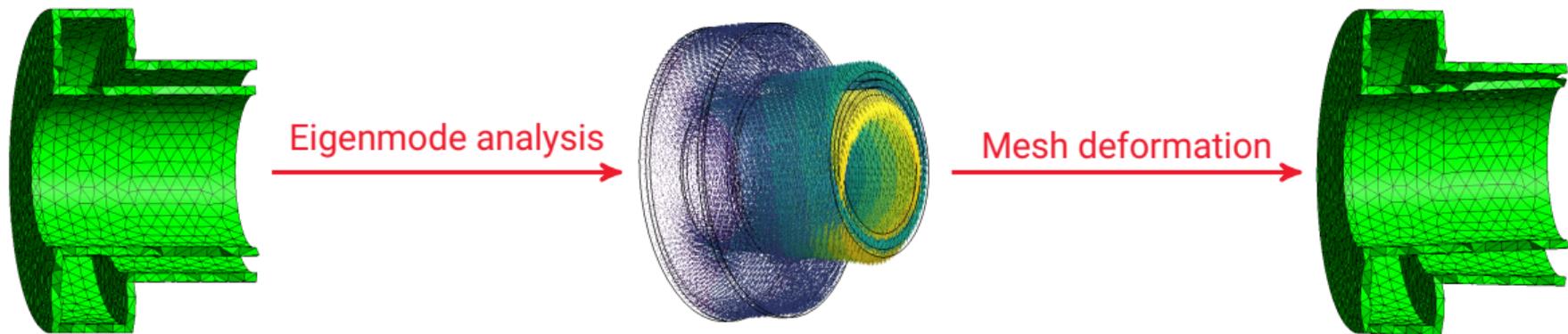
CCC: mechanics II



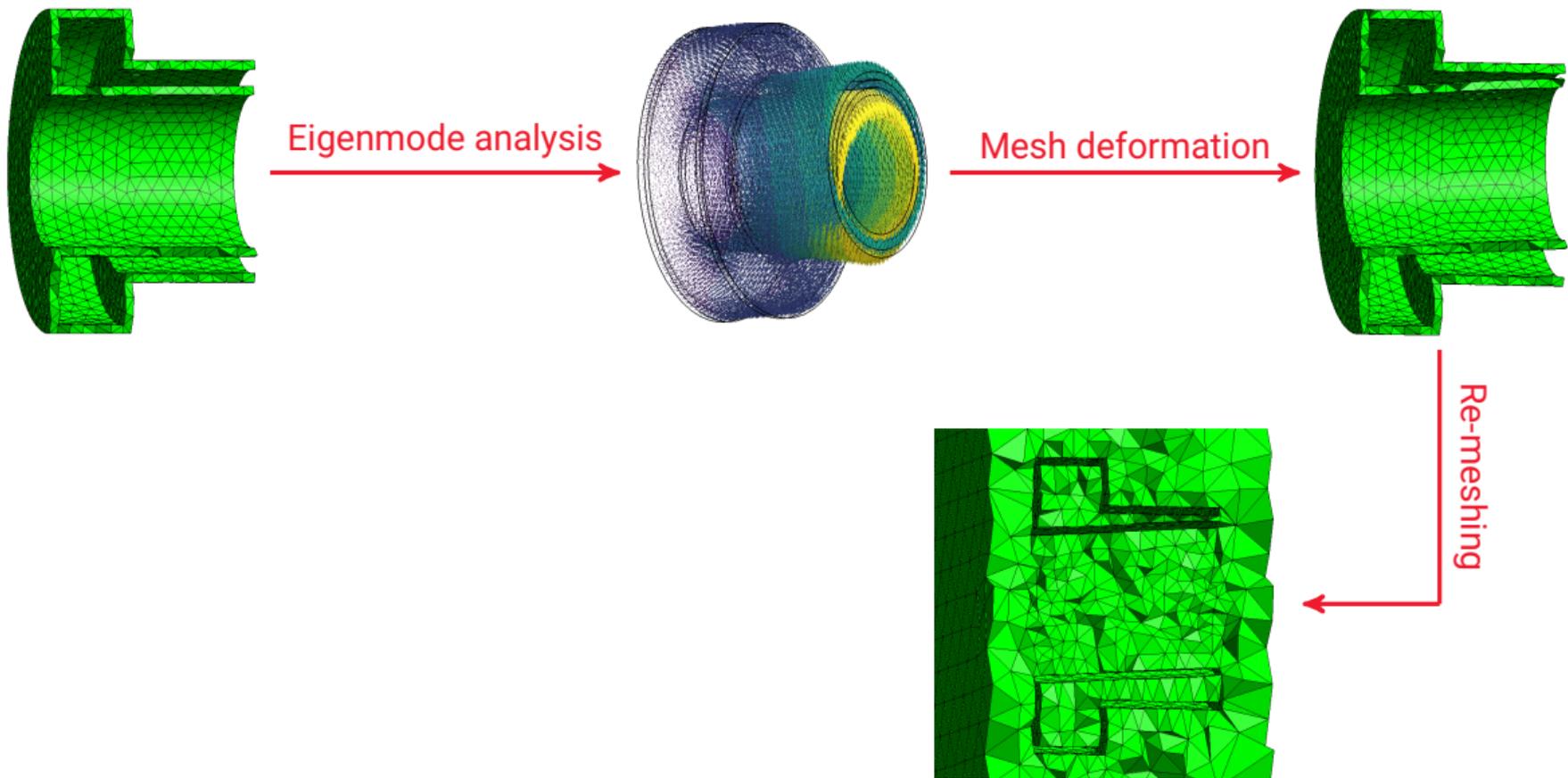
CCC: mechanics II



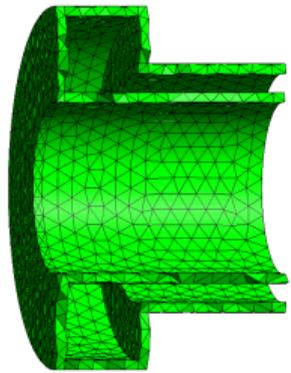
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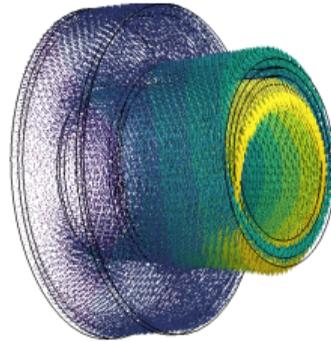
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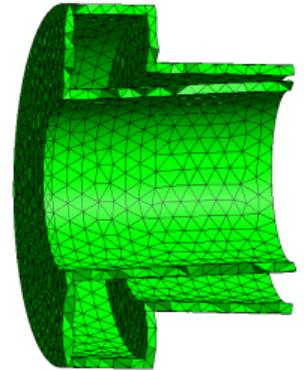
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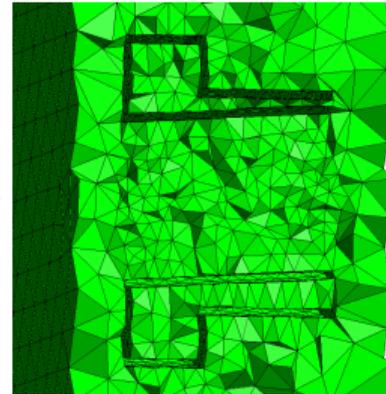
Eigenmode analysis



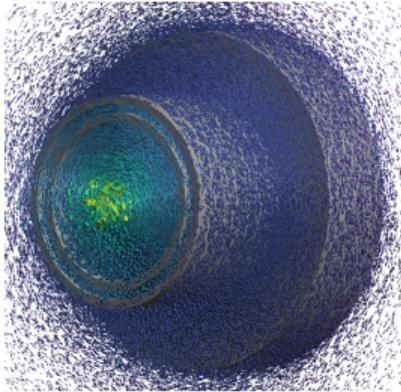
Mesh deformation



Re-meshing



MStatic



Conclusion

Why GetDP?

- Straightforward implementation of a given weak formulation
- Simple integration within broader frameworks via ONELAB
- Scripting language in a single binary (or two if we count Gmsh)

And last but not least...

Special thanks to Erin Kuci and Erik Schnaubelt!