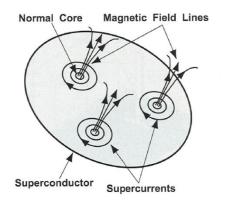
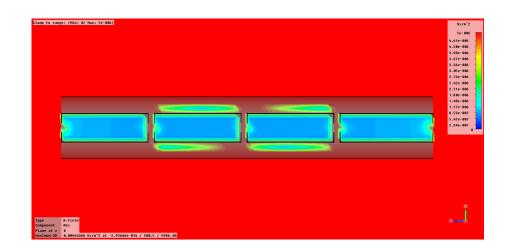




Magnetic shielding for SPL cavities Electromagnetic Simulations



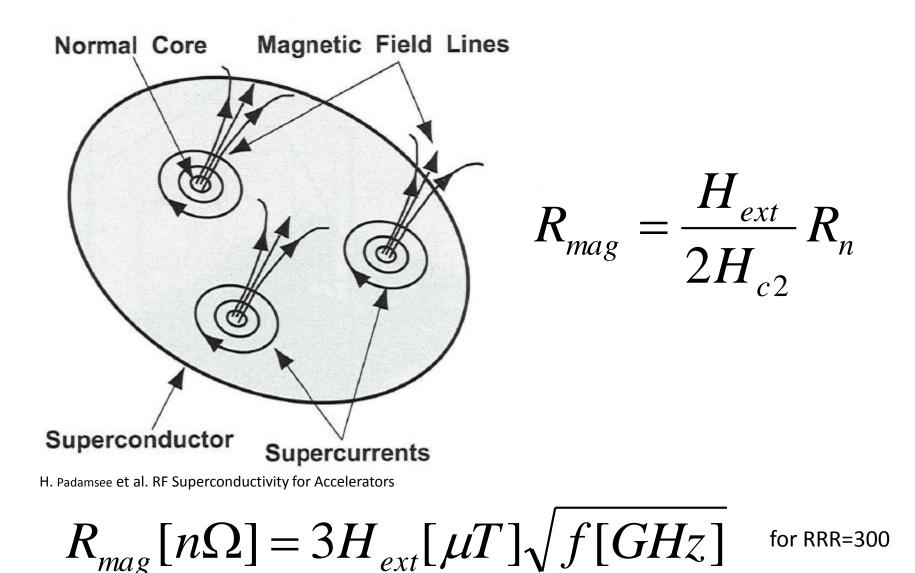


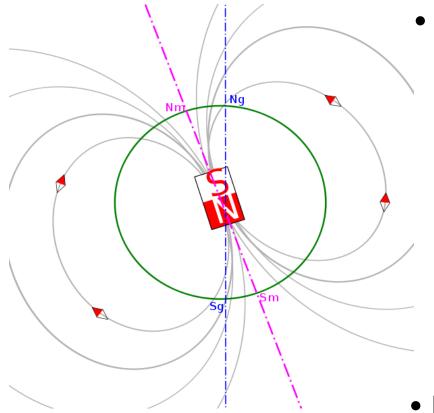
Tobias Junginger





Why do we need a Magnetic Shield?



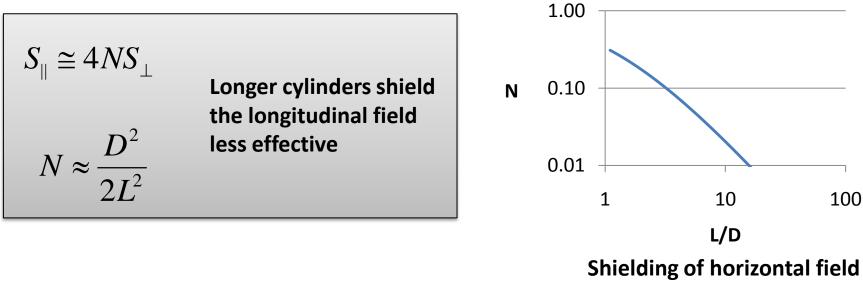


http://nl.wikipedia.org/wiki/Gebruiker:JrPol

- Assumptions
 - SPL goes straight from the South to the North (worst case)
 - Magnetic field 48 μT
 - Vertical 44 μT
 - Horizontal 20 μT

- Requirement
 - Less than 1 μT on cavity surface

$$\begin{split} R_{mag}[n\Omega] \propto \sqrt{f[GHz]} \\ S_{\perp} \cong \frac{\mu d}{D} + 1 \end{split} \\ \begin{aligned} \text{Bigger cavities need thicker} \\ \text{shields for same field!} \end{aligned}$$



is harder than of vertical

S: Shielding factors μ: Permeability of material d: Thickness of sheet D: Diameter of cylinder L: Length of cylinder N: Demagnetization coefficient

• DESY (TTF)

• 1 mm Cryoperm Shield attached to helium tank

• Remagnetisation of soft iron vacuum vessel

• PEFP/SNS

- Two amumetal magnetic shields
 - Inner shield attached to helium vessel
 - Outer shield attached to support structure

TRASCO

• 1 mm Cryoperm shield inside the helium tank

• S-DALINAC

- Vertical 0.1 mm sheets of cryoperm
- Horizontal Solenoid

	Four questions:	 Active or passive shield? One or two shields? 	
		Where to put the shield?Which material?	

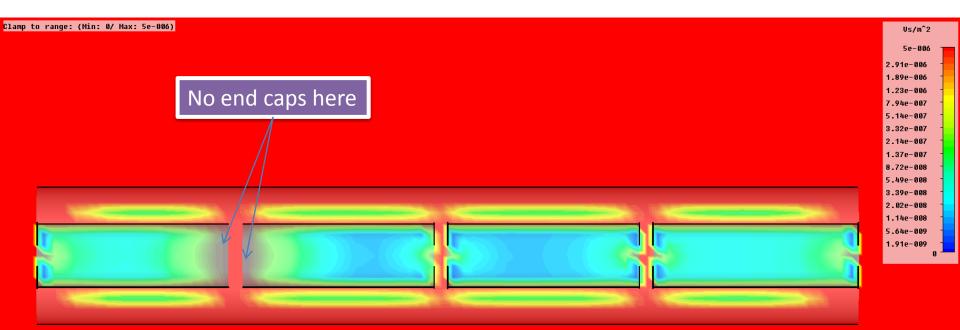
Four questions:	 Active or passive shield? One or two shields?
	- Where to put the shield? - Which material?

•One inner shield per cavity

- Horizontal field is harder to shield
- Demagnetization factor decreases quadratically with length
- Around inner thermal shield
 - As close as possible to the cavity (more effective and less expensive)
 - End caps necessary between every cavity

$$\begin{split} S_{\parallel} &\cong 4NS_{\perp} \qquad S_{\perp} \cong \frac{\mu d}{D} + 1 \\ N &\approx \frac{D^2}{2L^2} \qquad \begin{array}{l} \text{Longer cylinders shield} \\ \text{the longitudinal field} \\ \text{less effective} \end{array} \end{split}$$

End caps necessary between every cavity!



Туре	B-Field	
Component	z	
Plane at x	0	
Maximum-2D	0.001684	411 Vs/m^2 at -2.92646e-014 / 386.246 / 3006

Four questions:	 Active or passive shield? One or two shields? Where to put the shield?
	- Which material and thickness?

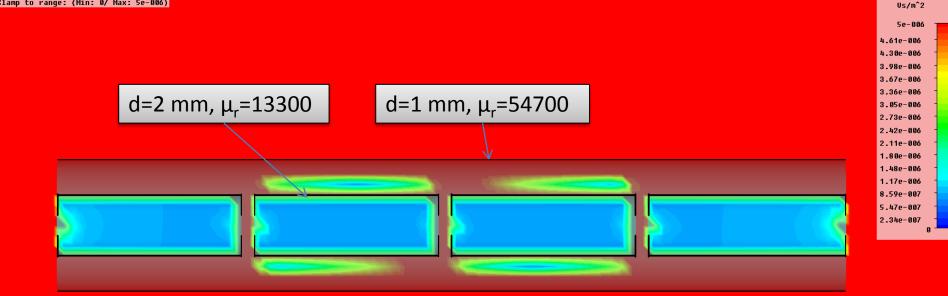
•One inner shield per cavity

- Horizontal field is harder to shield
- Demagnetization factor decreases quadratically with length
- Around inner thermal shield
 - As close as possible to the cavity (more effective and less expensive)
- End caps necessary between every cavity
- •Two passive shields
 - Outer shield helps to reduce the fields especially between two cavities
- •Amumetal or Cryoperm inside, Mumetal outside
 - For realistic μ_r values a thickness of **1 mm outside** and **2 mm inside** sufficient

My Solution

Numerical model has been crosschecked with simplified analytical expression Numerical value for magnetic field in the middle of one cavity only 4 % higher

Clamp to range: (Min: 0/ Max: 5e-006)





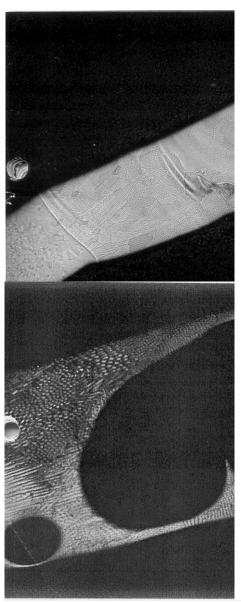
 μ_r values taken from TESLA-Report 1994-23, measured on test cylinders

8/9

Four answers:

- Passive shields
- Two shields
- One inner shield per cavity, one outer shield per module
- 2 mm Cryoperm or Amumetal inside
 1 mm Mumetal outside

Application of mumetal: LHC septa chambers



S. Sgobba – 3rd SPL Collaboration Meeting

Study of the influence of TIG welding and subsequent annealing on a Mumetal tube

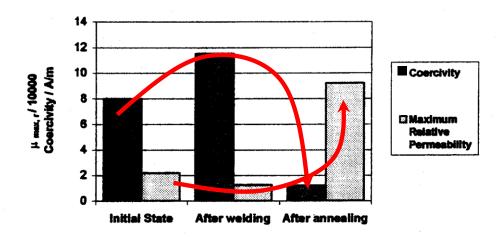
Report n. 98/10/06

EST/SM

Att. 4, page 1 of 1

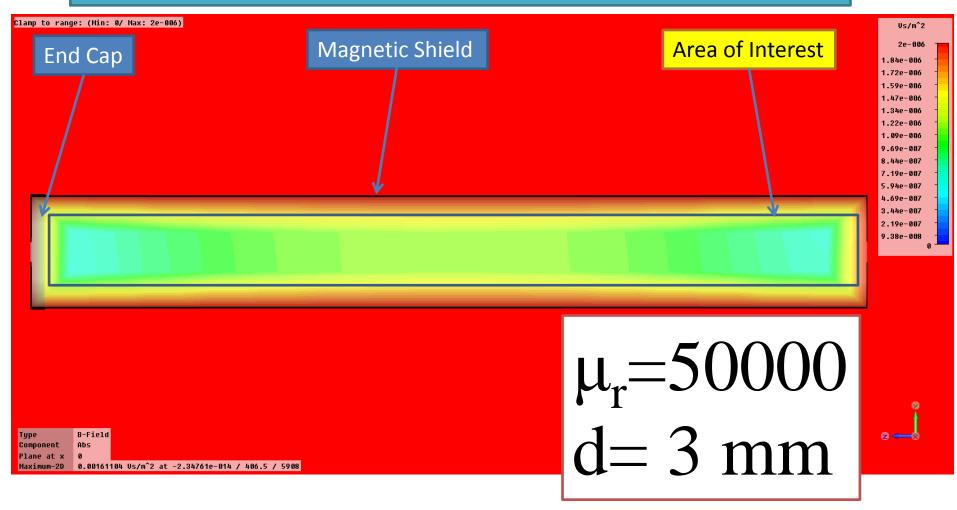
'Testing of magnetic properties and relative results

Graph, Table:	-Summary of the evolution of the measured magnetic properties on the Mumetal rings.	
Material:	Mumetal	
Samples ID:	ring 1, ring 2	
Density:	8.6	
Weight before welding:	ring (1&2) – 28.98 g	
Weight after welding:	ring 1 – 14.47 g	
	ring 2 – 14.42 g	
Permeameter:	90 turns used for excitation	
	180 turns used for detection	



Note: The properties of the initial state were measured on the two rings coupled. After the TIG welding, they were measured on both rings together and on each one separately. Since the measured values of the magnetic properties were reproducible between ring 1 and ring 2, further operations and measurements were performed only on one ring (ring 1).

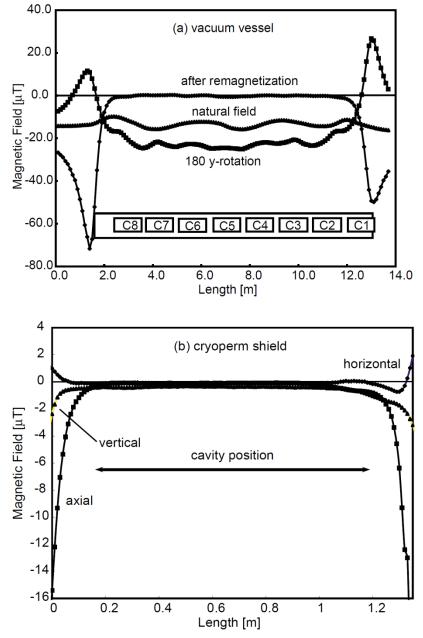
Numerical model has been crosschecked with simplified analytical expression Numerical value for magnetic field in the middle only 4 % higher



If the whole cryomodule shares one shield a maximum field value of approximately 1 μT can be achieved for $\mu_r\!=\!50000$ and d=3 mm

Tobias.Junginger@cern.ch

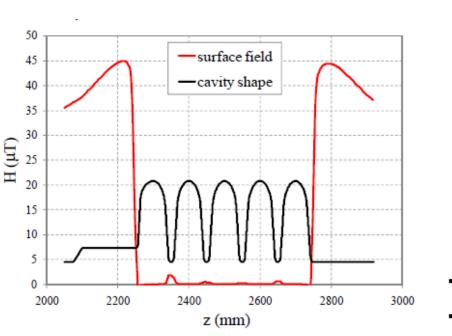
Solutions found by other labs - DESY

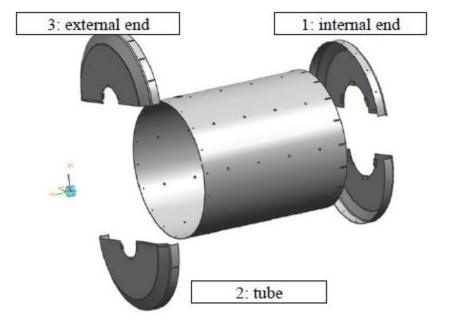


Solutions found by other labs - TRASCO



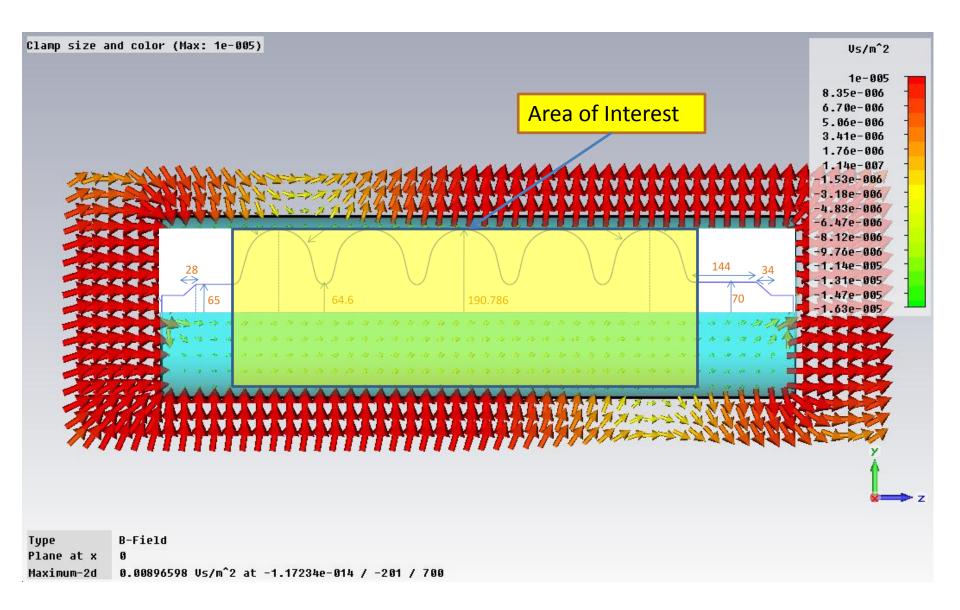
- 30 μ T field parallel to beam axis
- 1 mm thick cryoperm 10 shield (μ_r =150000)
- Two shields have already been produced and their shielding performance will be measured

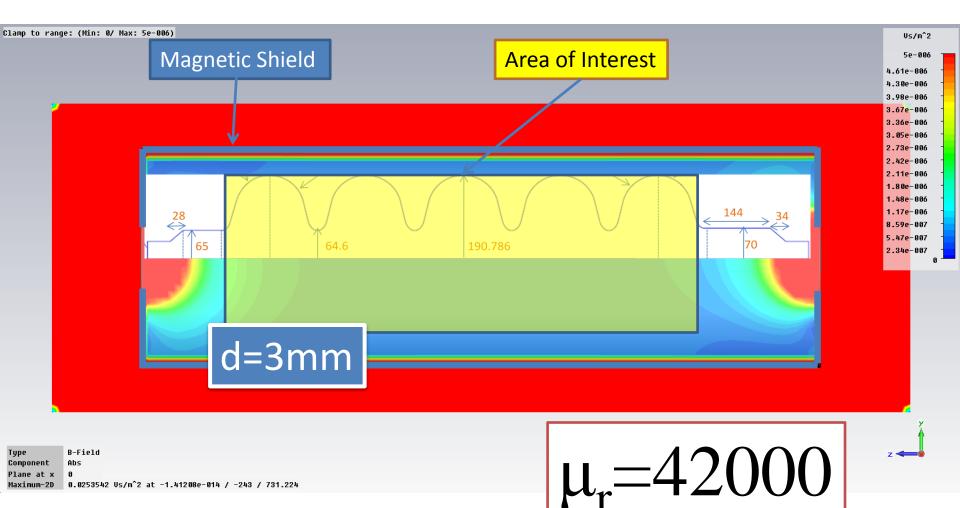


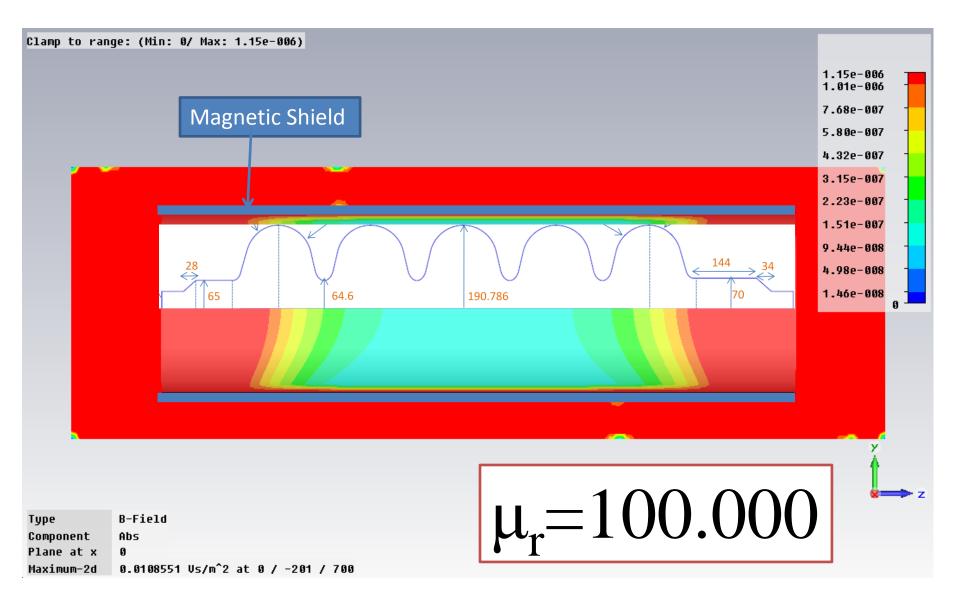


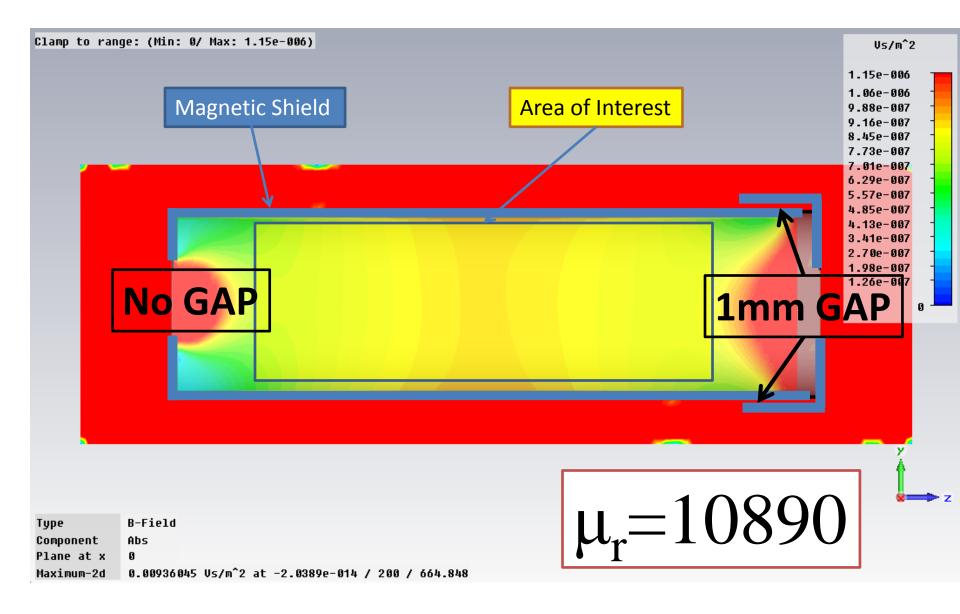
Case	< H > (μT)	Rs (nΩ)
Ideal: no gap	0.44	1.10
Not ideal: 0.1 mm gap at each end	2.08	5.23

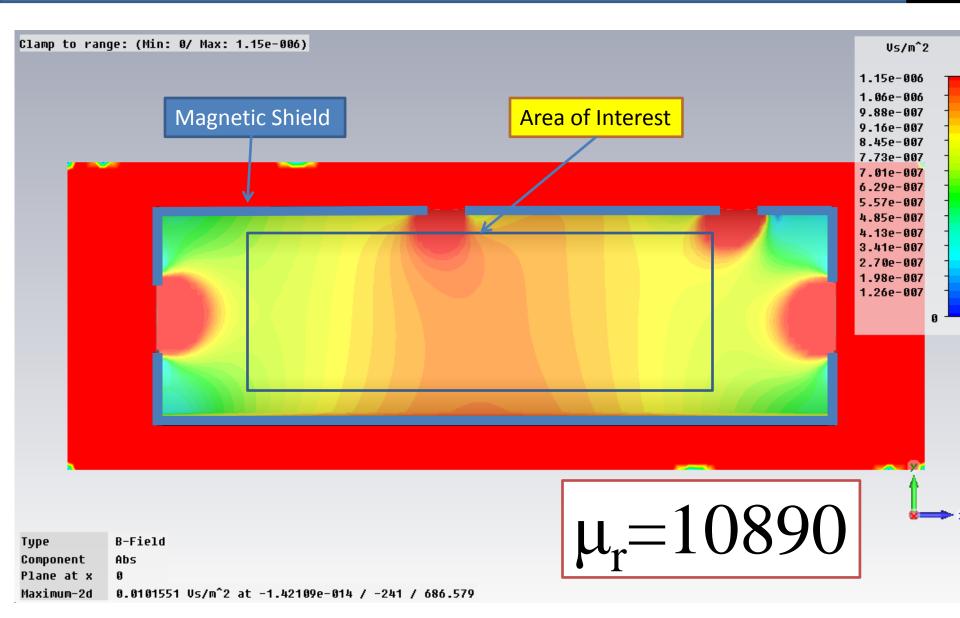
- Material: Cryoperm 10
- Thickness of sheet: 1 mm
- 206 Cavities
- 500 m² sheet
- 4.5 t of material ($\sigma=9 \text{ kg/l}$)
- 450 kCHF (100 CHF/kg)

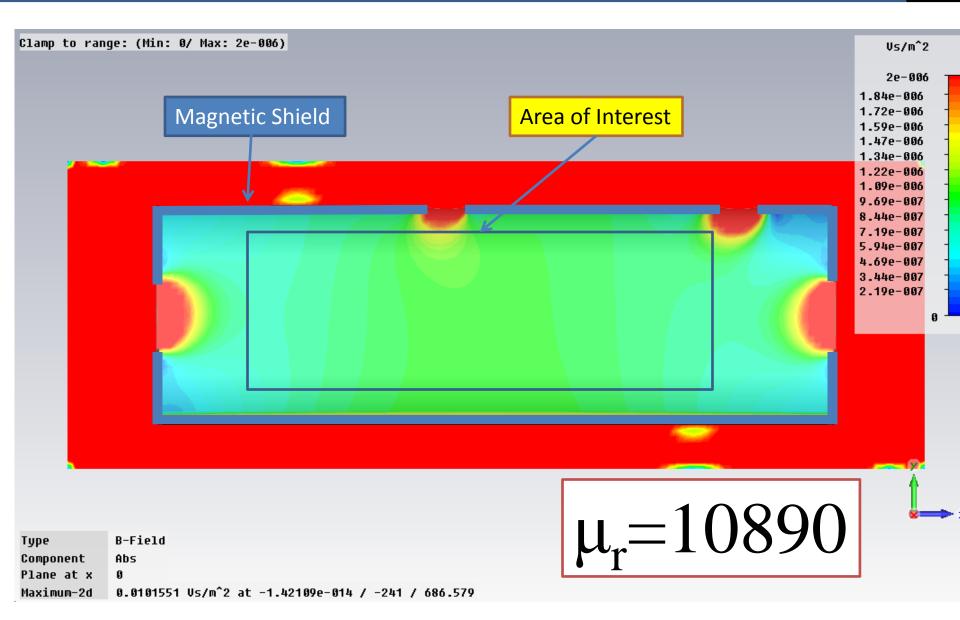












- $\mu_r = 42.000$ needed for the whole temperature range for 3 mm sheet
- End caps are necessary
- A gap of a few millimetres between end caps and cylinder can be tolerated
- Holes lead to higher field values than $1\mu T$ in spots of approximately their size

My recommendations:

- External Shield of Cryoperm (3 mm)
- As close as possible to the helium tank
- Annealing of tubes and end caps