

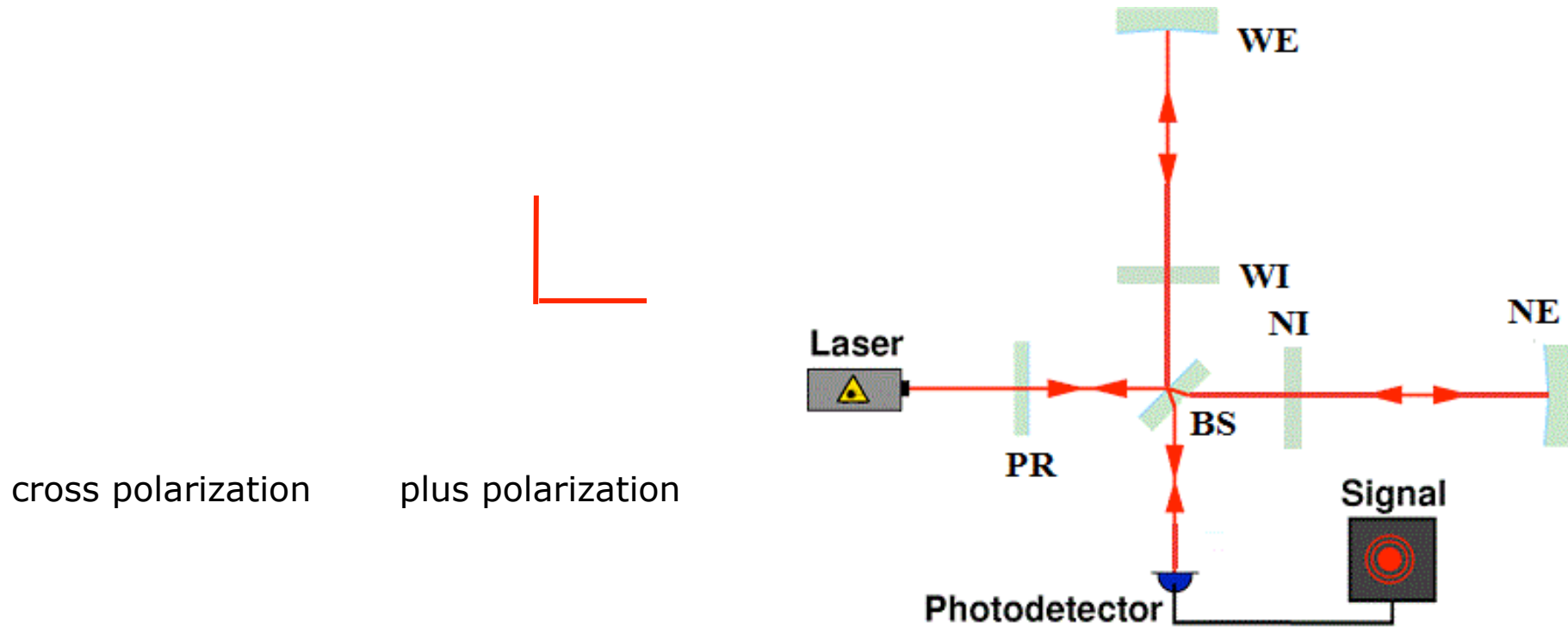
Seismic attenuation technology for the advanced Virgo gravitational waves detector

Mark Beker (mbeker@nikhef.nl), Mathieu Blom, Jo van den Brand,
Henk Jan Bulten, Eric Hennes, Frans Mul.

9 June 2011
TIPP 2011, Chicago



Virgo is a 3 km arm-length interferometer designed to measure gravitational waves



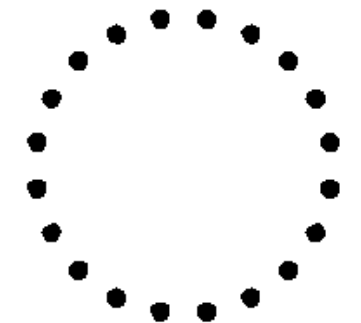
Global detector network:

LIGO - USA:

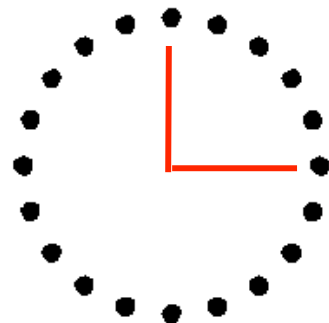
- 4 km Hanford
- 4 km Livingston

GEO 600 m - Germany
(LCGT 3 km - Japan)
(AIGO 4 km - Australia)

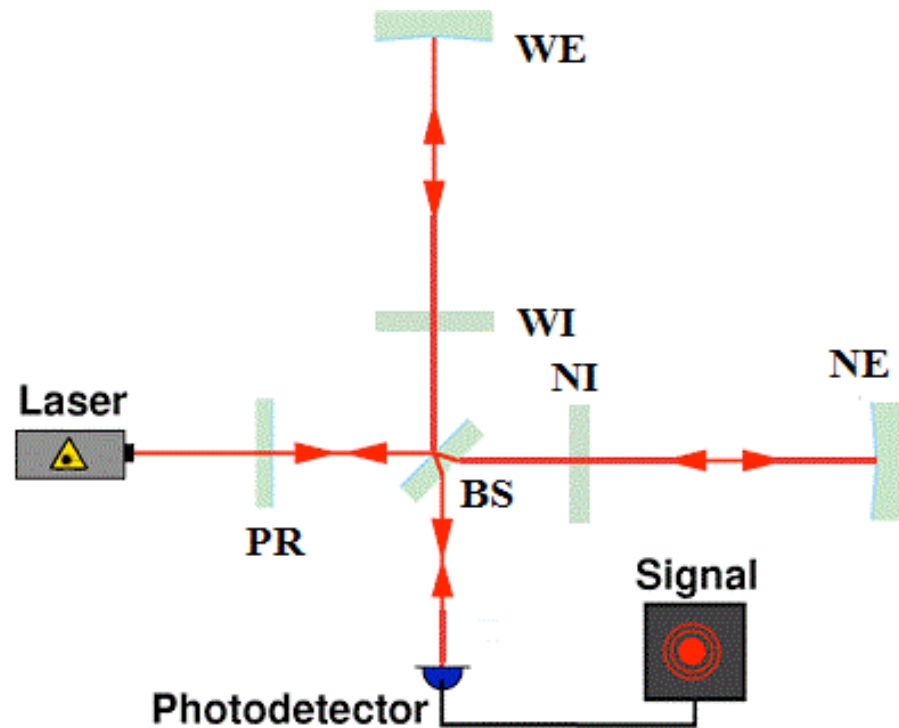
Virgo is a 3 km arm-length interferometer designed to measure gravitational waves



cross polarization



plus polarization



Global detector network:

LIGO - USA:

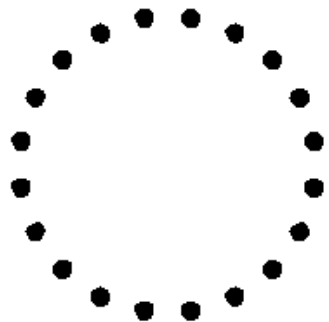
- 4 km Hanford
- 4 km Livingston

GEO 600 m - Germany

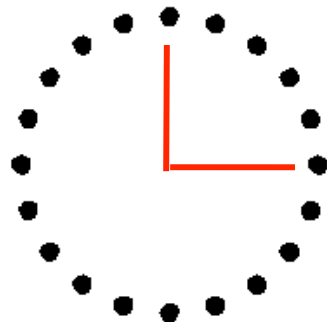
(LCGT 3 km - Japan)

(AIGO 4 km - Australia)

Virgo is a 3 km arm-length interferometer designed to measure gravitational waves

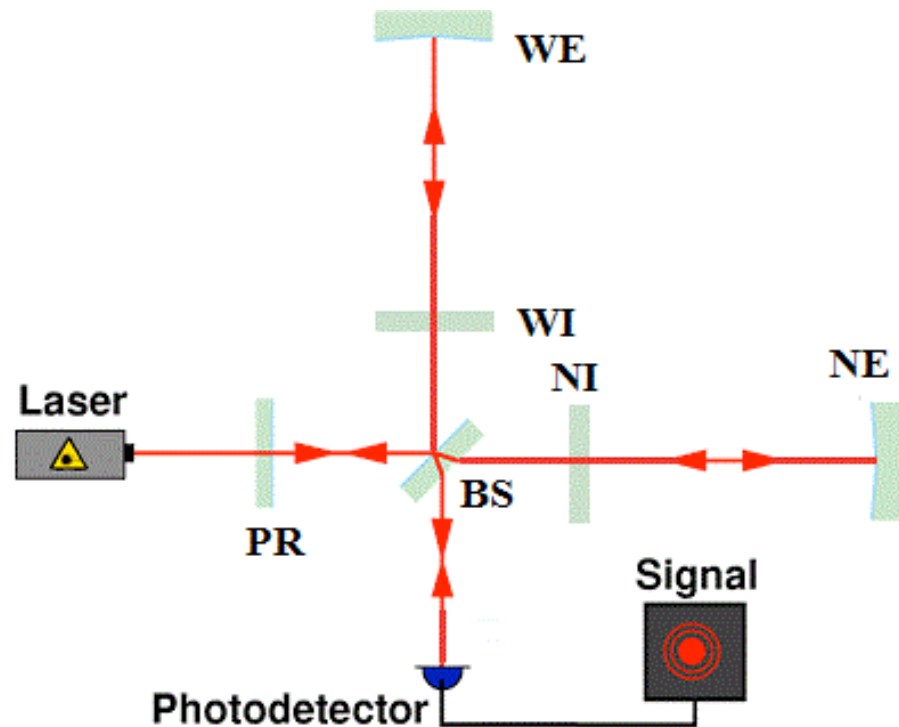


cross polarization



plus polarization

$$\text{Strain, } h = \Delta L/L \approx 10^{-22}$$



Global detector network:

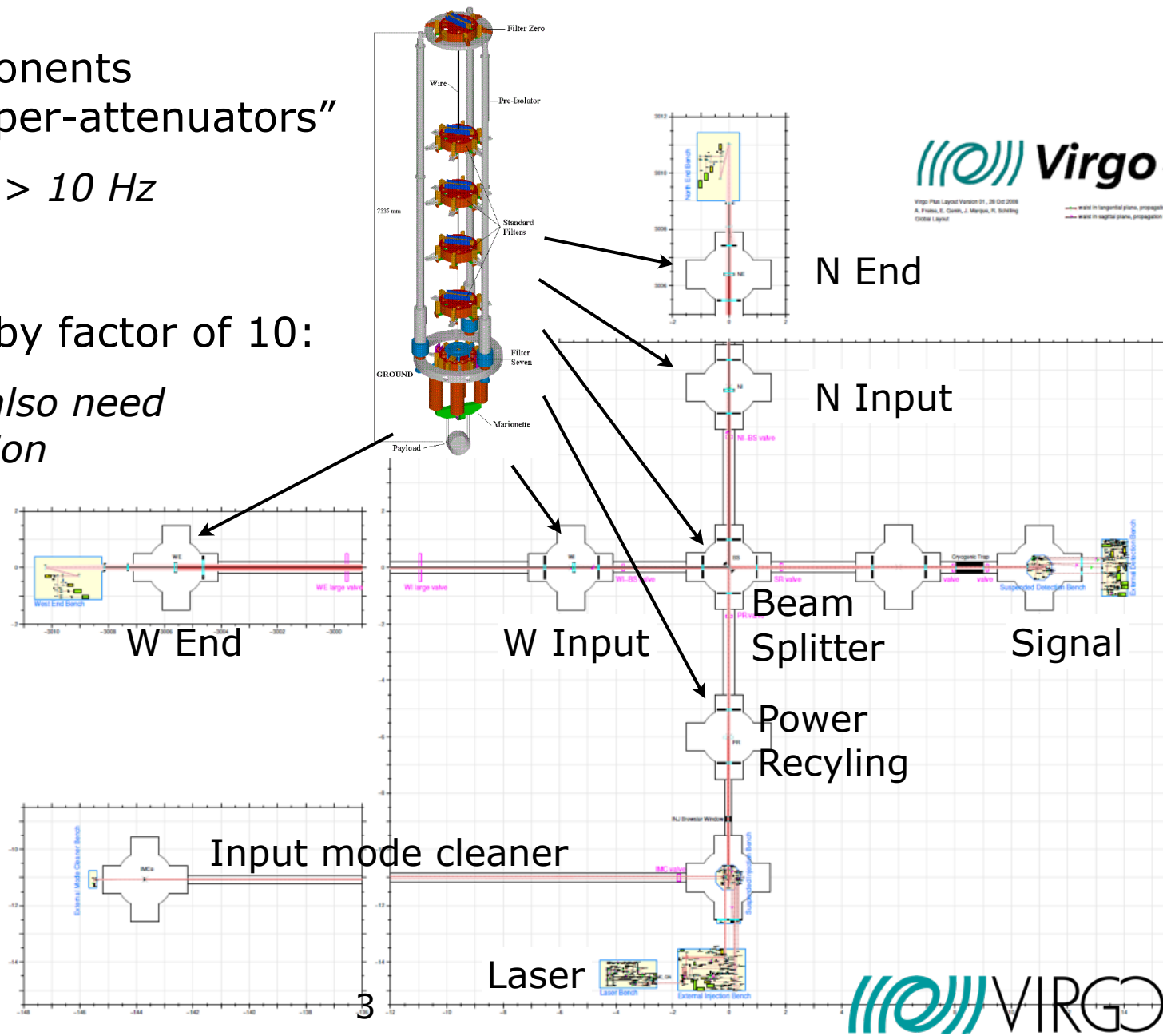
LIGO - USA:

- 4 km Hanford
- 4 km Livingston

GEO 600 m - Germany
(LCGT 3 km - Japan)
(AIGO 4 km - Australia)

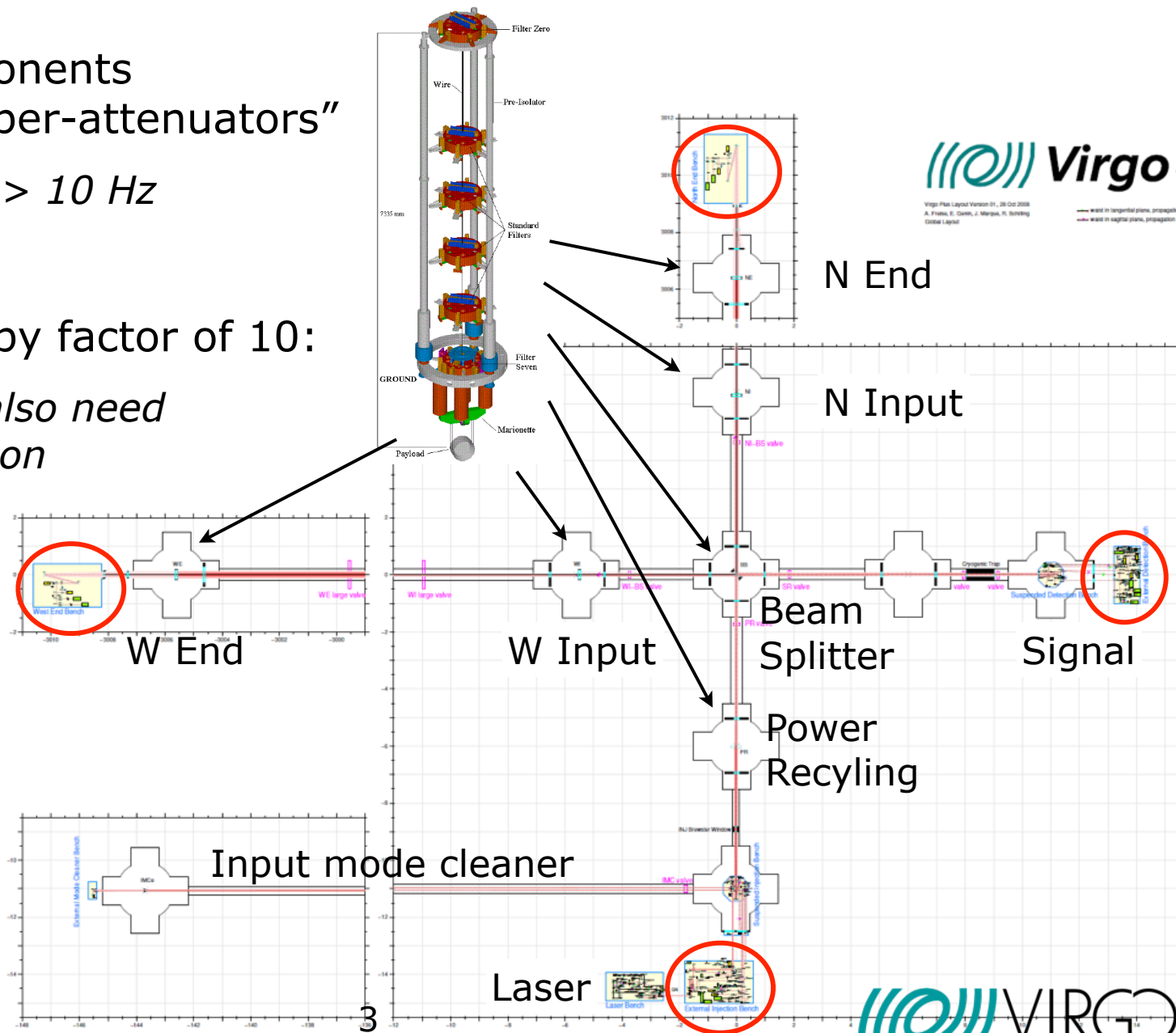
Seismic noise limits low frequency sensitivity of Virgo through vibration of optical components

- Main optical components suspended by “Super-attenuators”
 - 10^{14} suppression > 10 Hz
- To improve strain by factor of 10:
 - *Optical benches also need seismic suppression*
 - 4 external
 - 2 internal
 - Requirement: 40 dB > 10 Hz



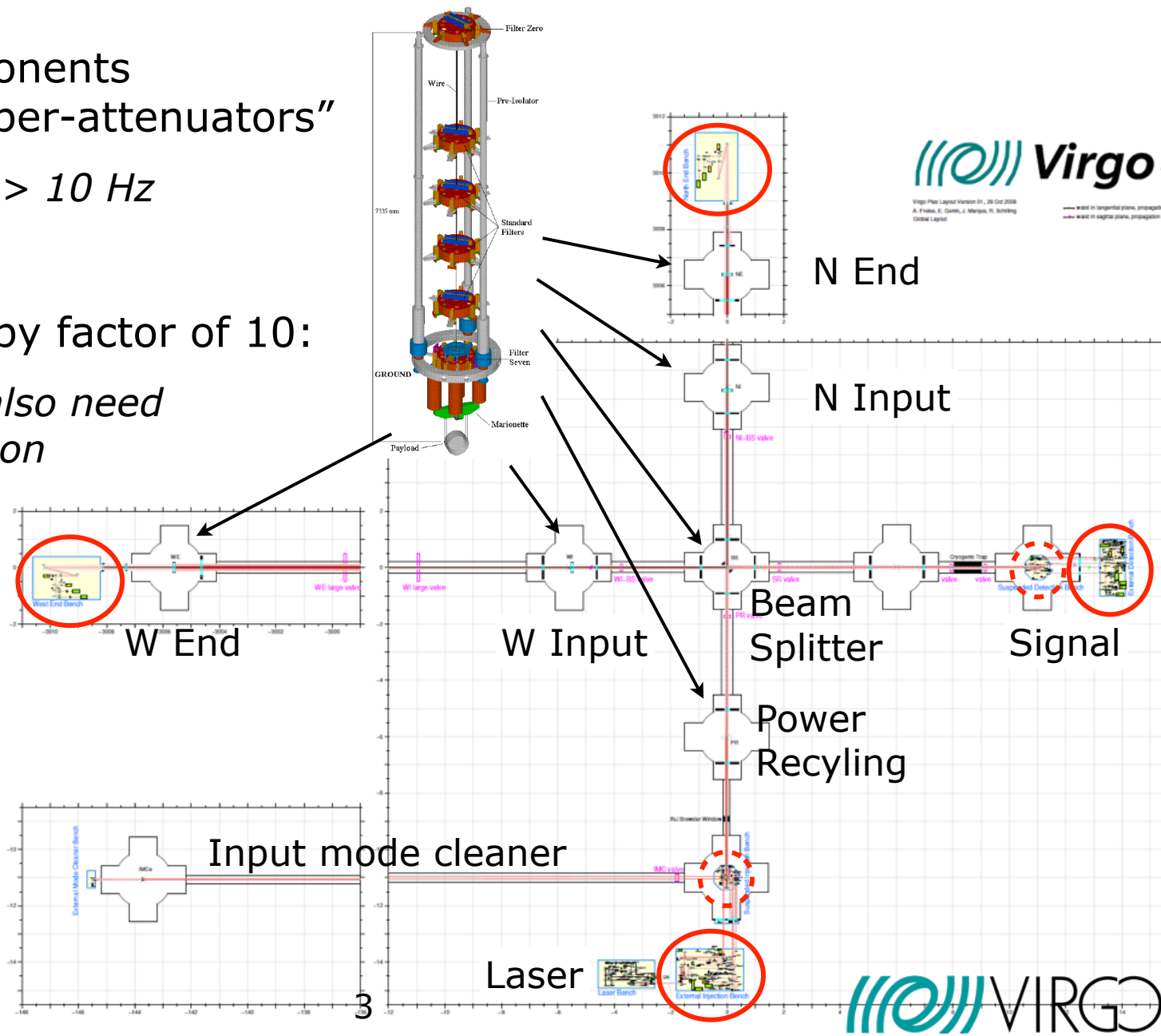
Seismic noise limits low frequency sensitivity of Virgo through vibration of optical components

- Main optical components suspended by “Super-attenuators”
 - 10^{14} suppression > 10 Hz
- To improve strain by factor of 10:
 - *Optical benches also need seismic suppression*
 - 4 external
 - 2 internal
 - Requirement: 40 dB > 10 Hz



Seismic noise limits low frequency sensitivity of Virgo through vibration of optical components

- Main optical components suspended by “Super-attenuators”
 - 10^{14} suppression > 10 Hz
- To improve strain by factor of 10:
 - *Optical benches also need seismic suppression*
 - 4 external
 - 2 internal
 - Requirement: 40 dB > 10 Hz



Seismic isolation systems also needed for future high-energy experiments

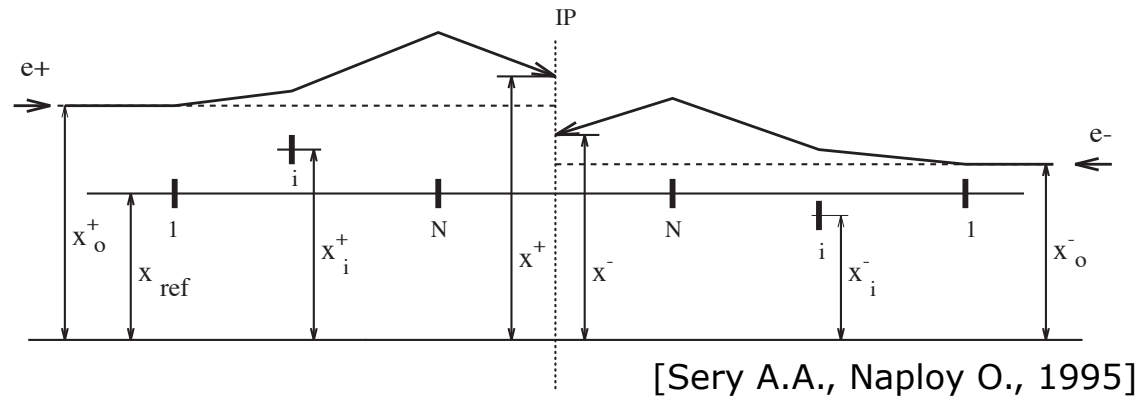


Figure 7: Layout of the e^+ and e^- parts of a linear collider near interaction region.

Seismic isolation systems also needed for future high-energy experiments

- Linear Colliders CLIC / ILC
 - *Sub nano-meter interaction points*
 - *Quadrupole movement (ATL law)*

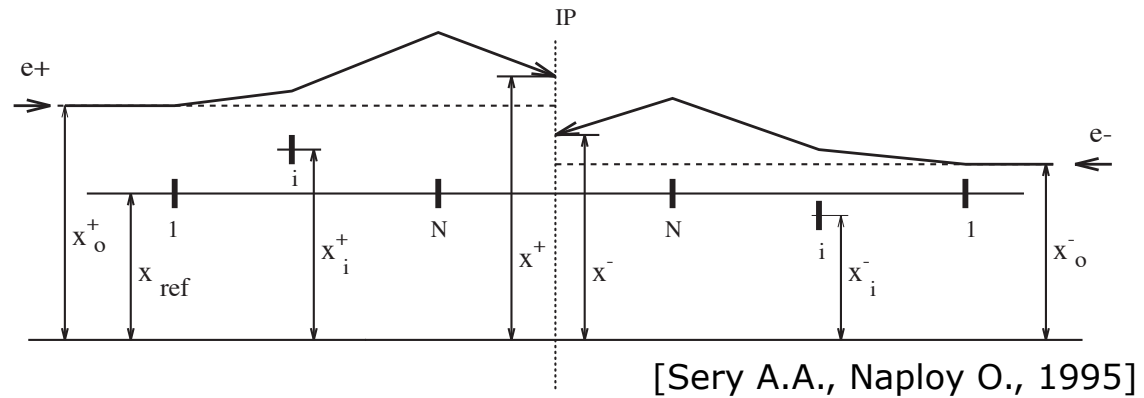
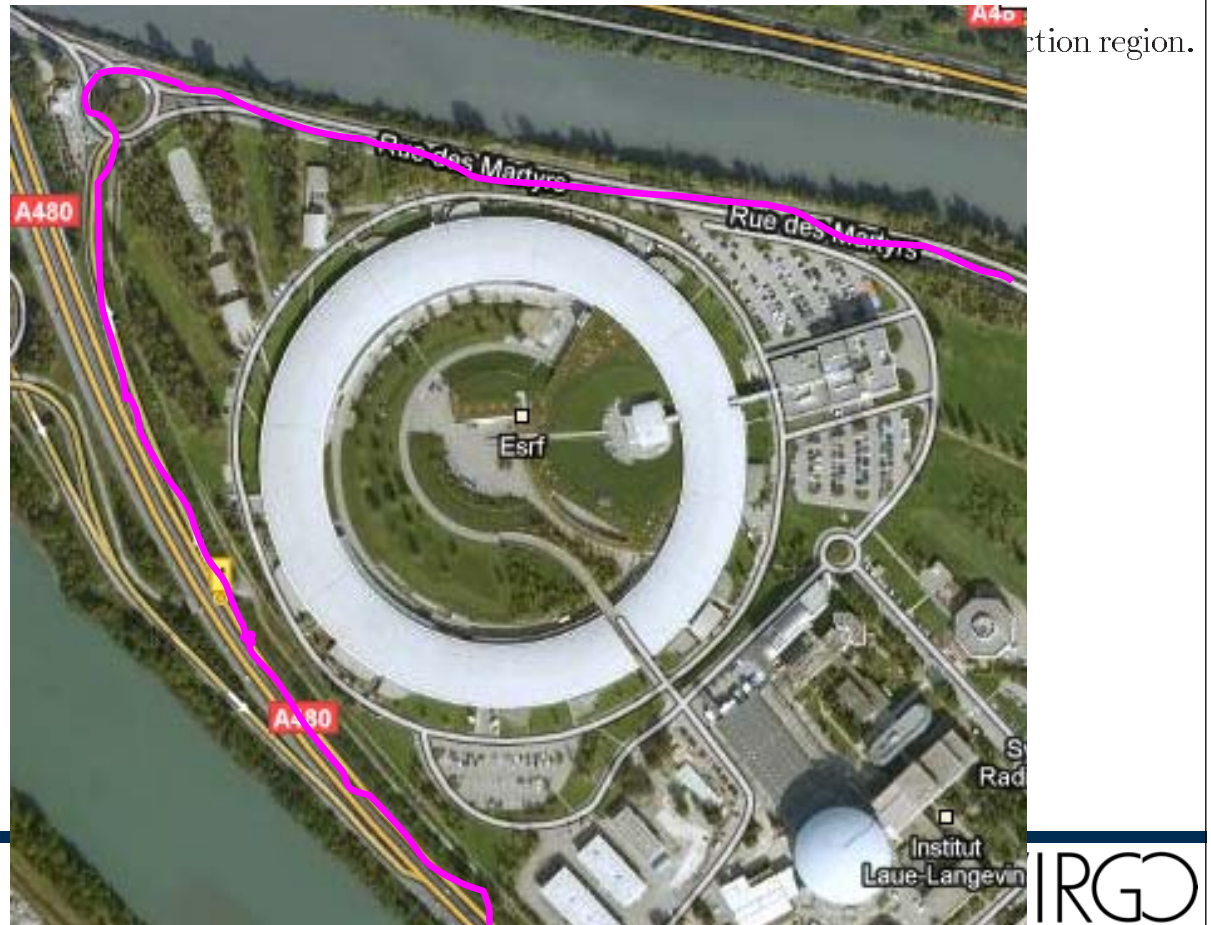
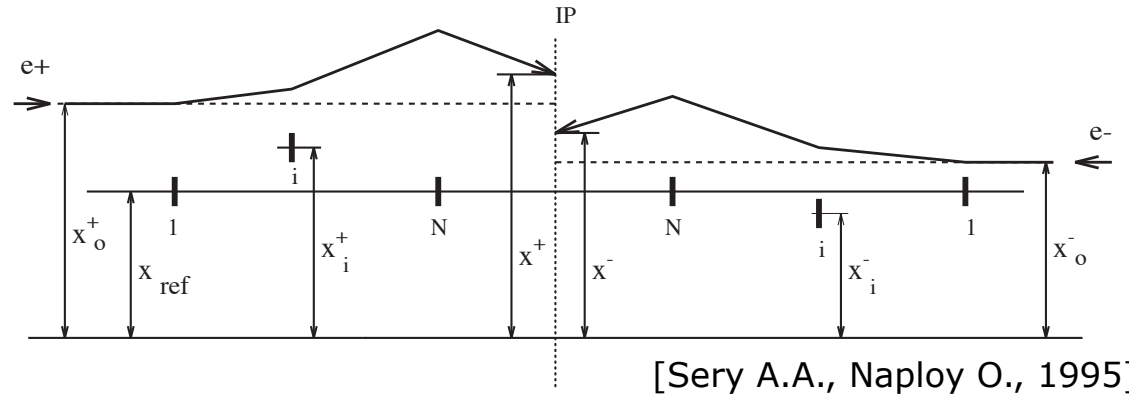


Figure 7: Layout of the e^+ and e^- parts of a linear collider near interaction region.

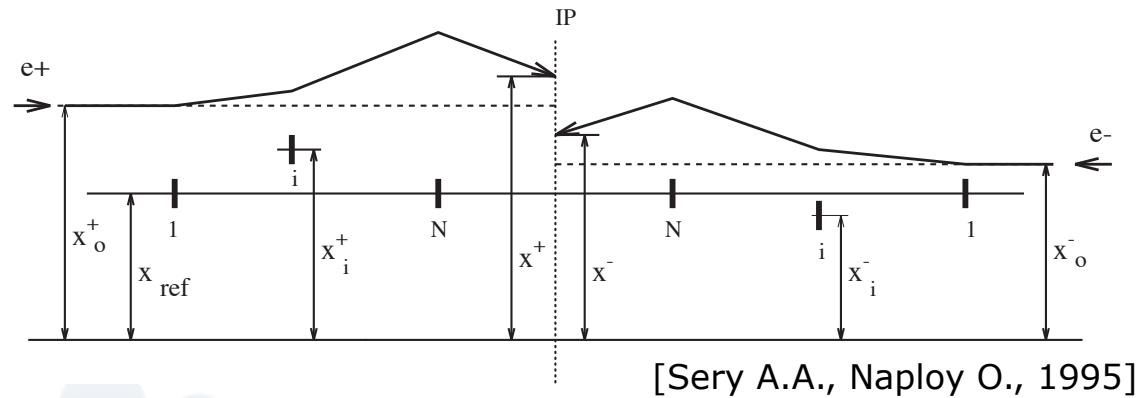
Seismic isolation systems also needed for future high-energy experiments

- Linear Colliders CLIC / ILC
 - *Sub nano-meter interaction points*
 - *Quadrupole movement (ATL law)*
- Synchrotrons
 - *ESRF e-beam and X-ray vibration stability*



Seismic isolation systems also needed for future high-energy experiments

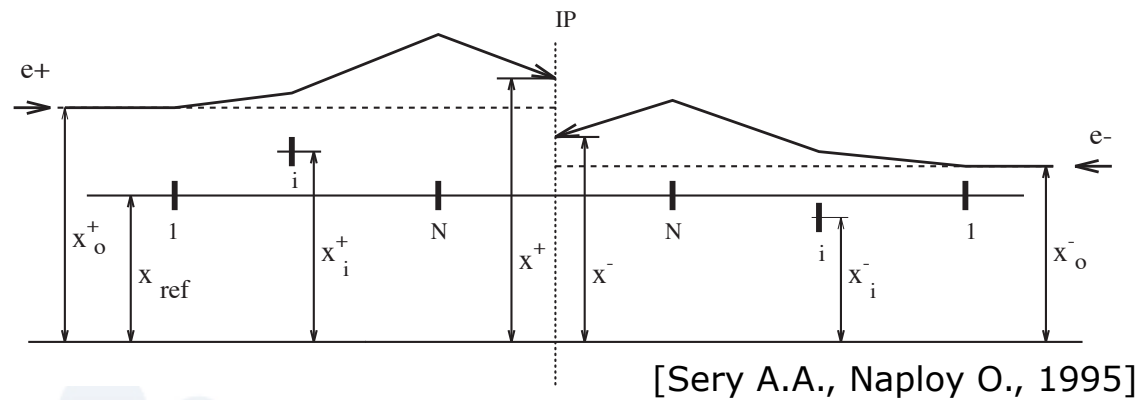
- Linear Colliders CLIC / ILC
 - *Sub nano-meter interaction points*
 - *Quadrupole movement (ATL law)*
- Synchrotrons
 - *ESRF e-beam and X-ray vibration stability*



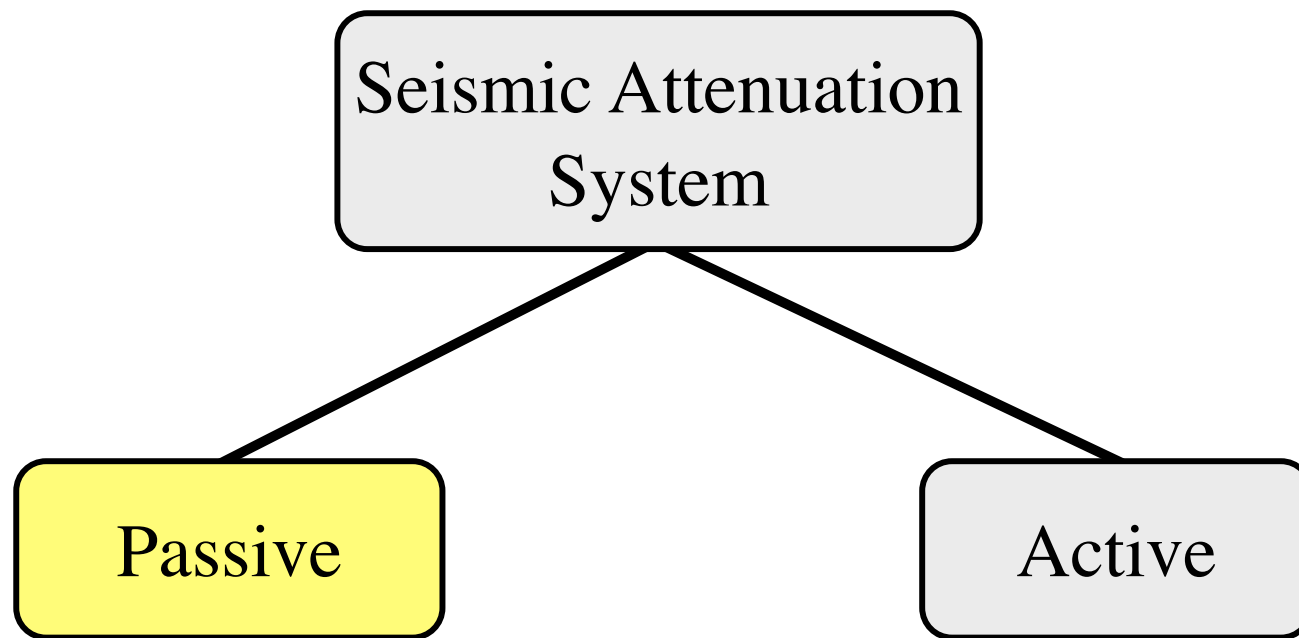
tion region.

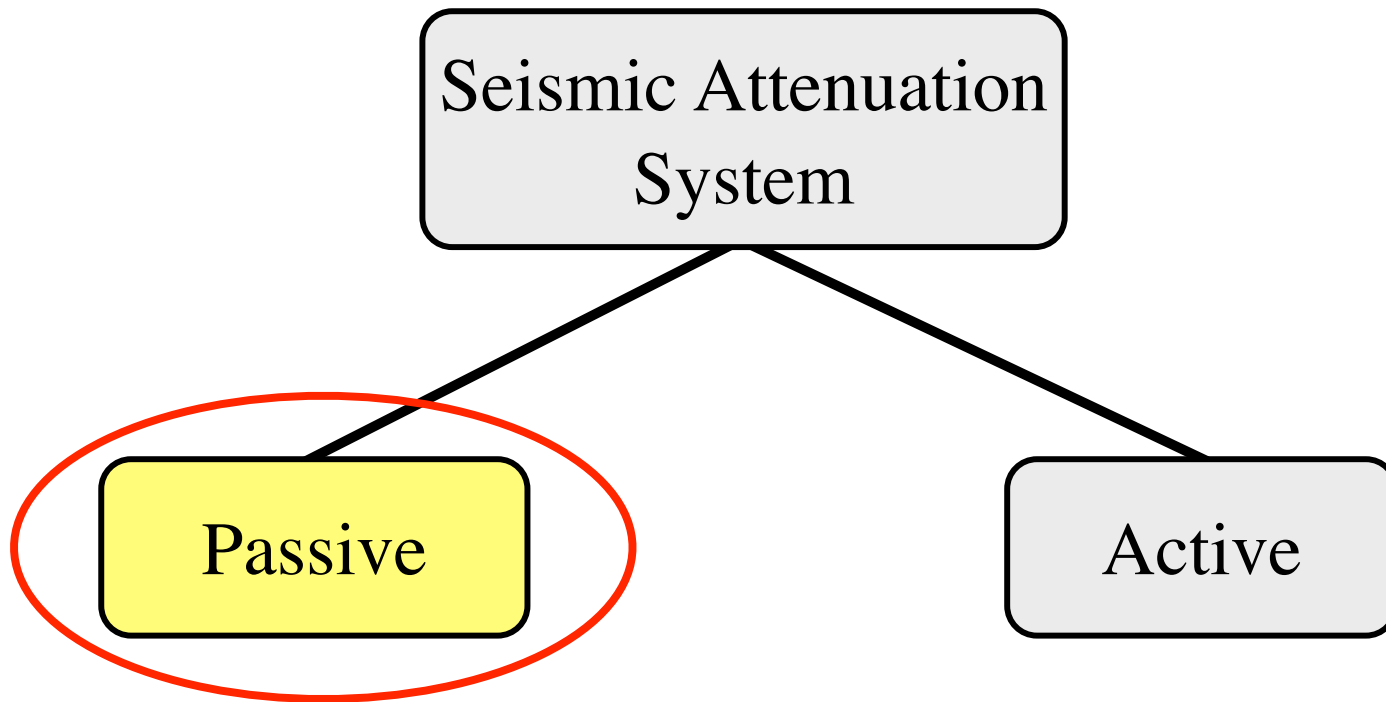
Seismic isolation systems also needed for future high-energy experiments

- Linear Colliders CLIC / ILC
 - *Sub nano-meter interaction points*
 - *Quadrupole movement (ATL law)*
- Synchrotrons
 - *ESRF e-beam and X-ray vibration stability*
- Free electron lasers
 - *DESY*
 - *FLASH Groningen*



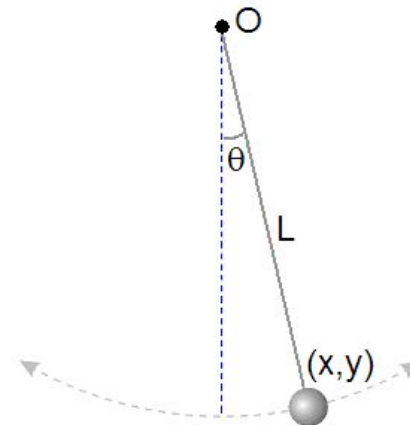
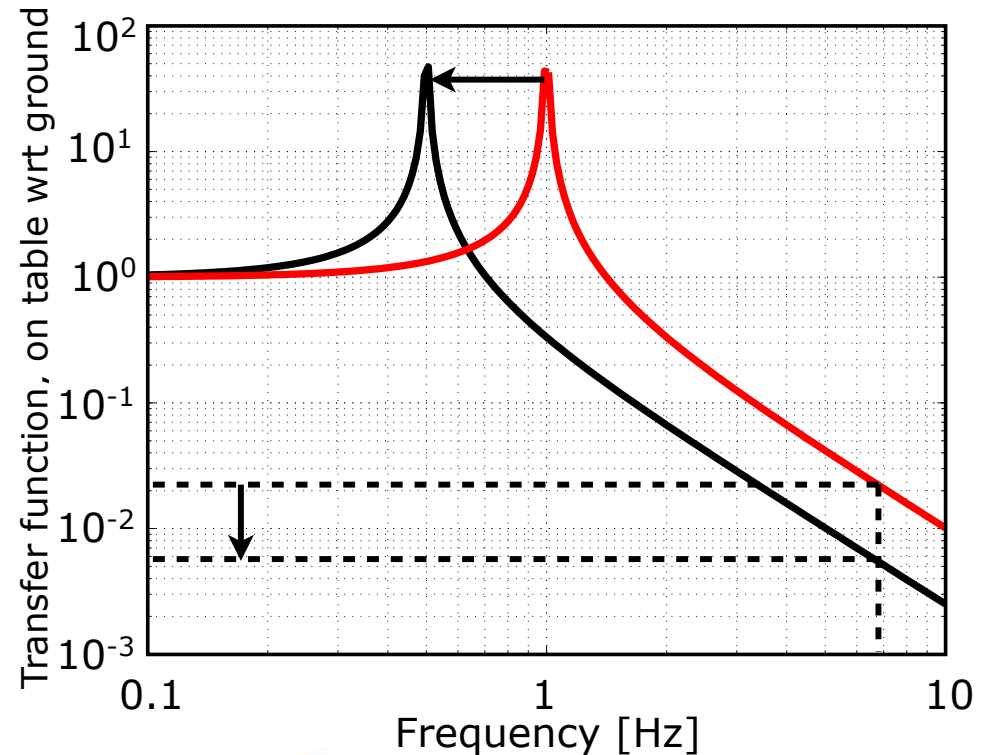
tion region.





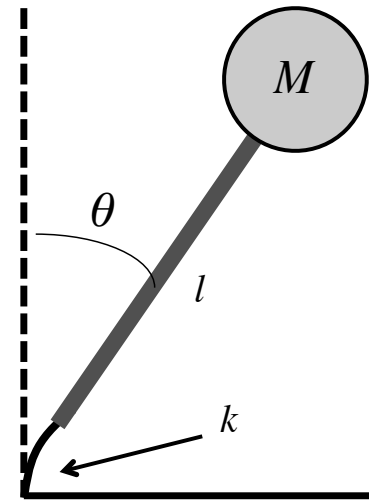
A passive isolation system utilizes the transfer function of harmonic oscillators

- Harmonic oscillator is a 2nd order low pass filter
- Transfer function:
 - $=1$ @ low frequencies
 - > 1 @ $\omega_0 = \sqrt{\frac{g}{l}}$ / $\omega_0 = \sqrt{\frac{k}{M}}$.
 - $\sim 1/f^2$ above resonance frequency
- Virgo/LIGO measure from 10 Hz
 - Want 40 dB suppression $>$ a few Hz
 - Need $f_0 \approx 0.3$ Hz $\Rightarrow l \approx 3$ m
 - Long pendulum / low stiffness and high mass
 - **Or**, use short *inverted pendulum* and *geometric anti-springs*

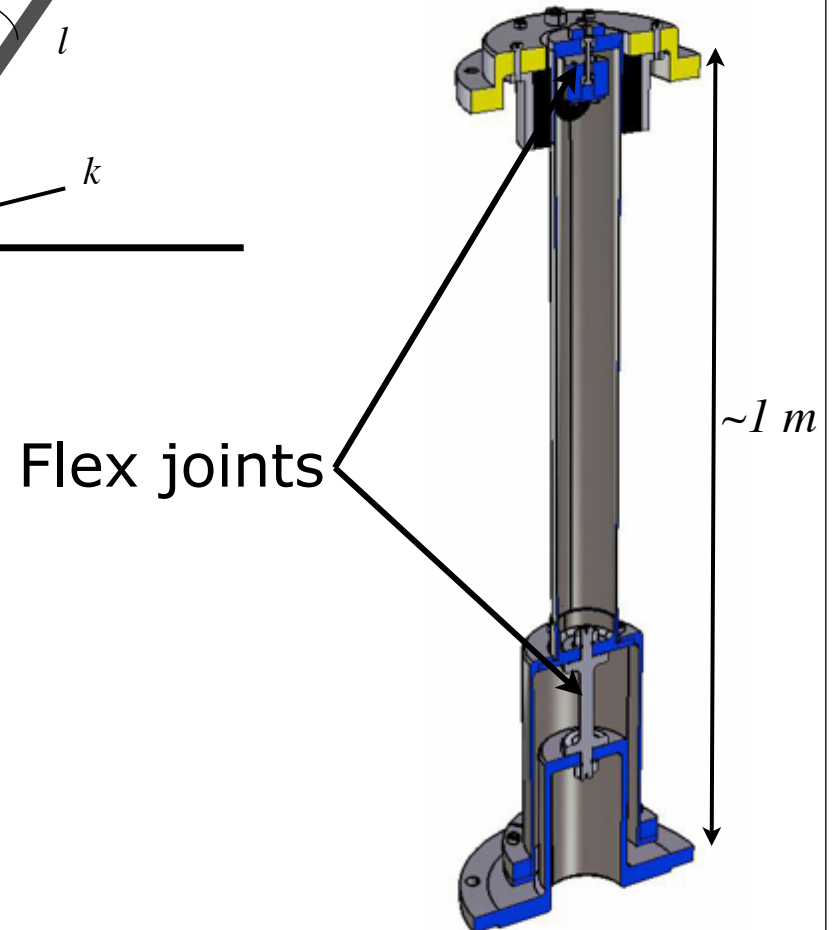
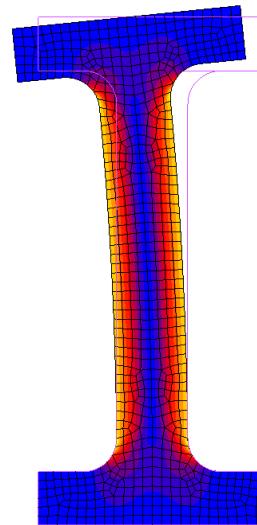
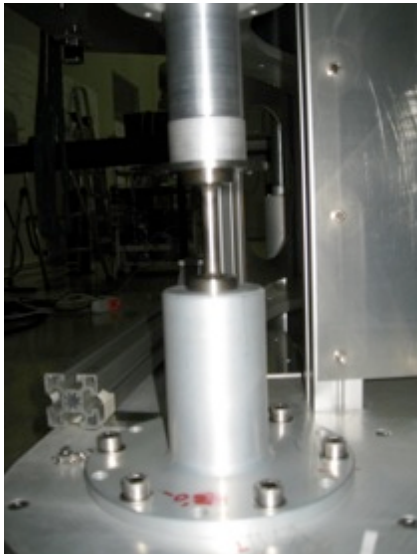


Inverted pendulum are used for the horizontal attenuation stage

- Gravity acts as an anti-spring
- Maraging steel flex joints provide stiffness, k
- Tunable in eigenfrequency by adjusting the supported mass
- Counter weights can be tuned to adjust center of percussion

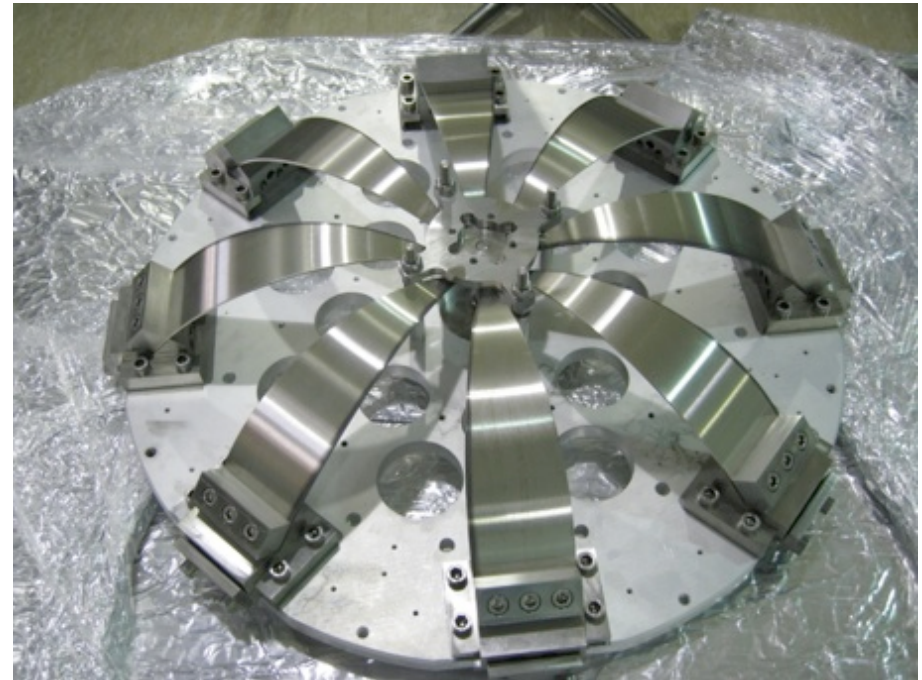
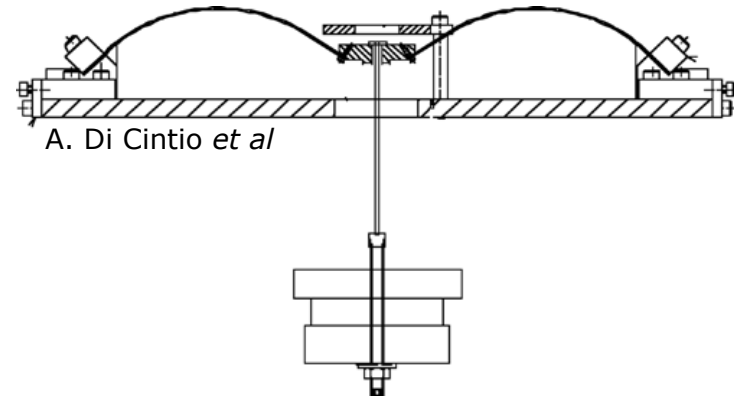


$$\omega_0 = \sqrt{\frac{k}{M} - \frac{g}{l}}$$



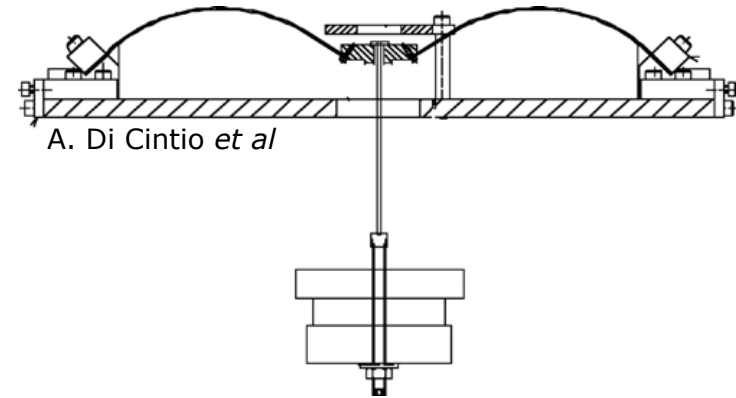
Geometrical anti-springs are used to provide vertical attenuation

- 8 maraging steel blades in pairs
- Opposite blades push against each other
 - *High pressure in radial direction*
 - *Low **vertical stiffness** in equilibrium position*
 - *Low eigenfrequency (~ 300 mHz)*
 - *Still capable of supporting high masses (~ 320 kg)*
 - *Strong filtering (>40 dB @ 10 Hz)*

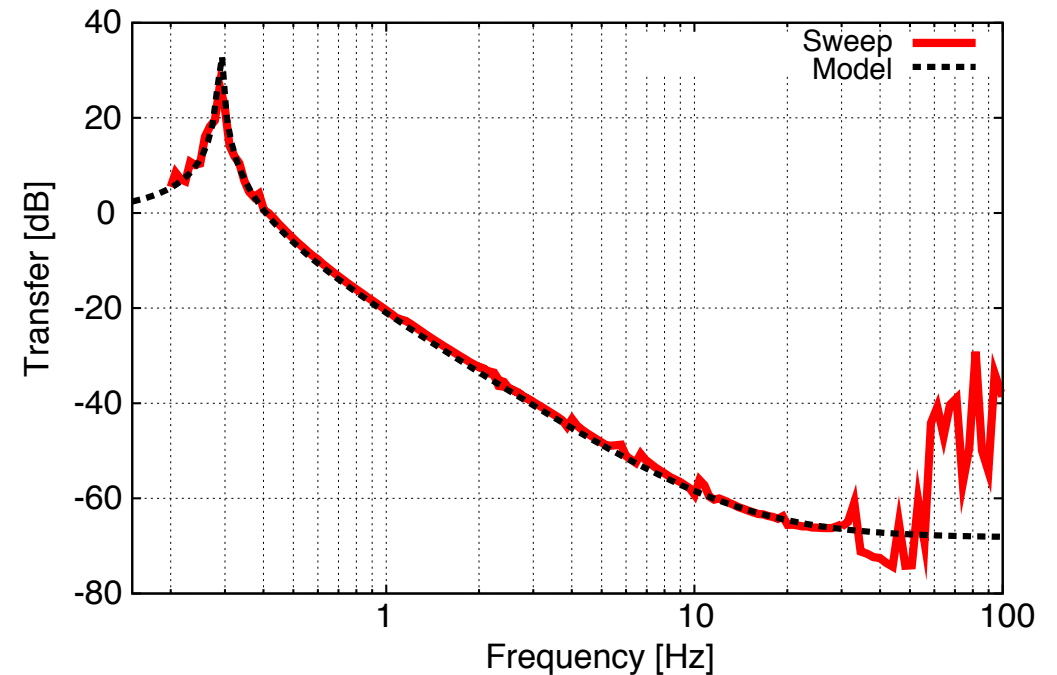


Geometrical anti-springs are used to provide vertical attenuation

- 8 maraging steel blades in pairs
- Opposite blades push against each other
 - *High pressure in radial direction*
 - *Low **vertical stiffness** in equilibrium position*
 - *Low eigenfrequency (~ 300 mHz)*
 - *Still capable of supporting high masses (~ 320 kg)*
 - *Strong filtering (>40 dB @ 10 Hz)*



Transfer function GAS 1

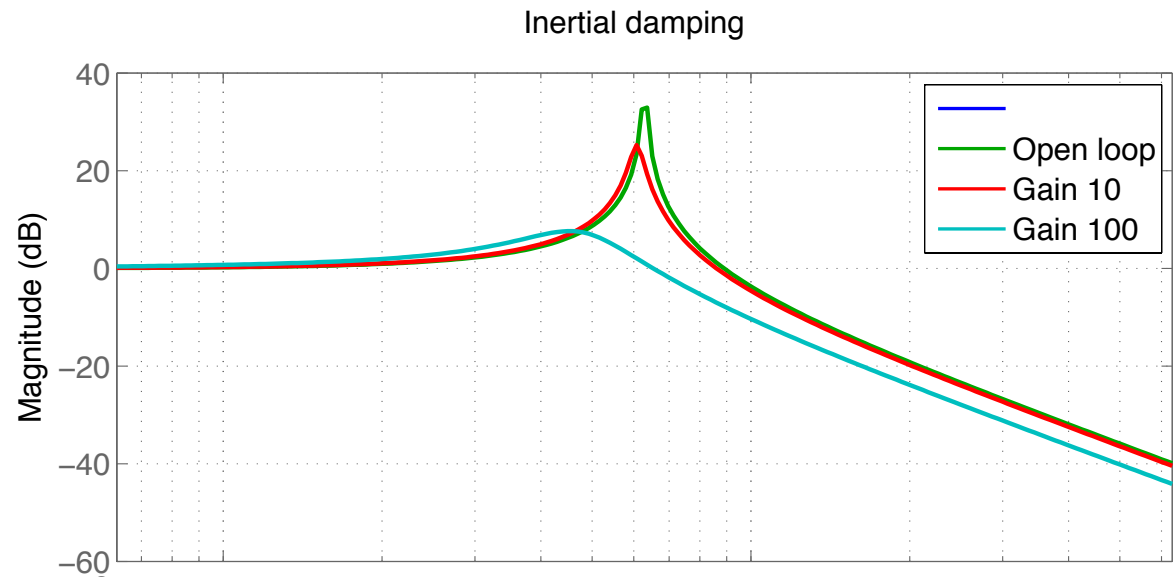
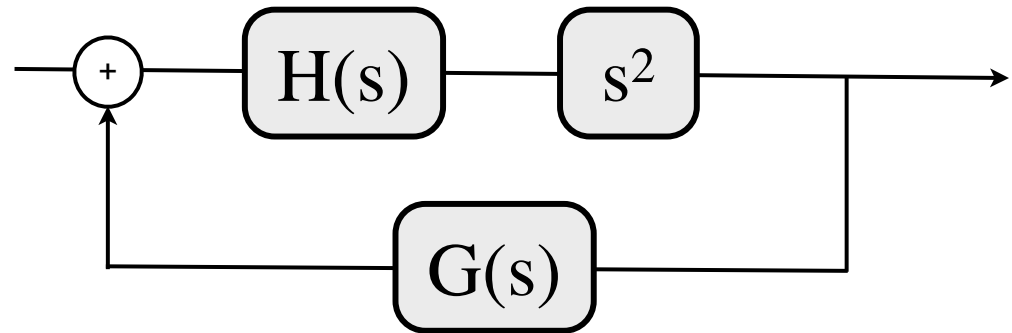


Movie GAS resonance



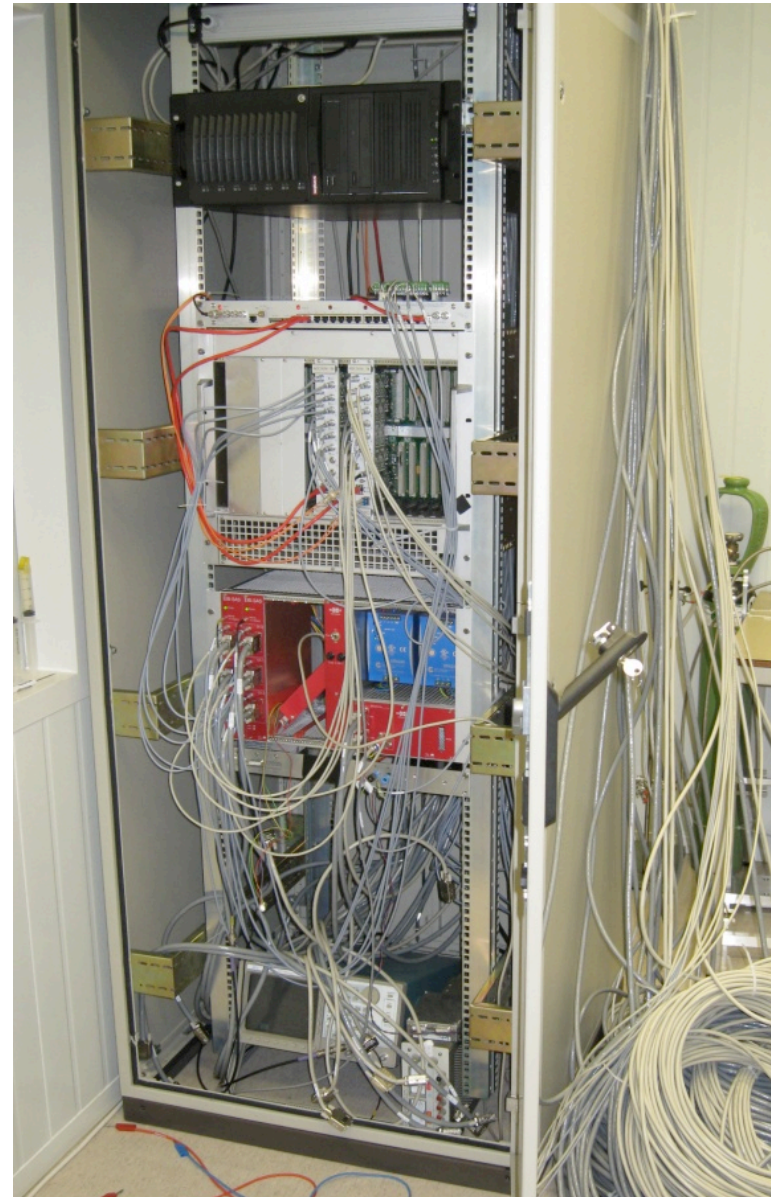
Feed-back control system used to actively damp resonant frequencies

- Order of magnitude damping of resonant frequencies required
- Calculations performed on Linux PC
- Feed-back done with electromagnetic actuators
- Sensing relies on displacement sensors and accelerometers



Feed-back control system used to actively damp resonant frequencies

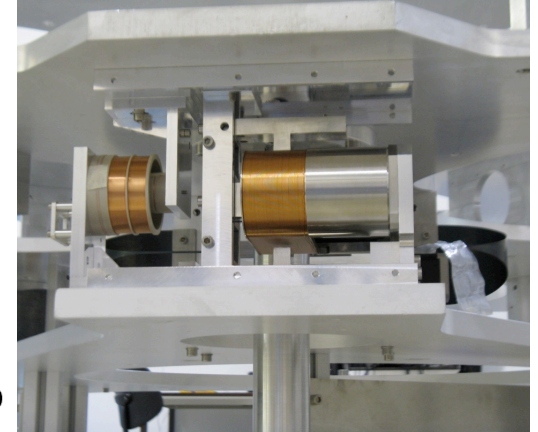
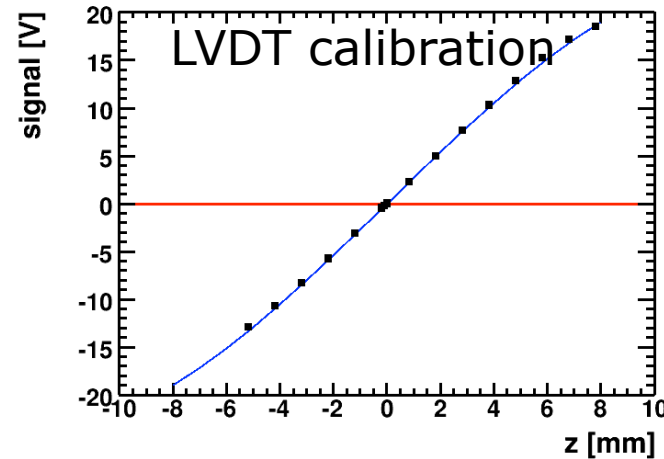
- Order of magnitude damping of resonant frequencies required
- Calculations performed on Linux PC
- Feed-back done with electromagnetic actuators
- Sensing relies on displacement sensors and accelerometers



Sensing of bench motion for resonance damping

- Linear Voltage Displacement Transducers (LVDT)

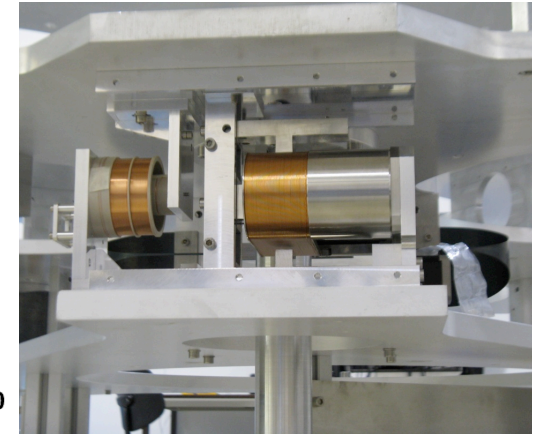
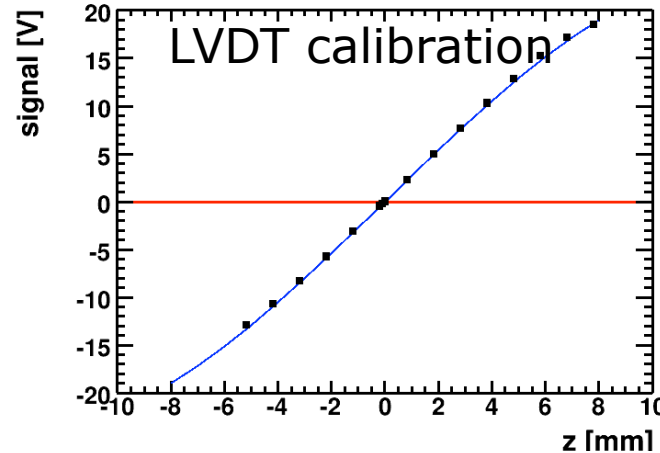
- *DC -> a few Hz*
- *~ 1 nm sensitivity*



Sensing of bench motion for resonance damping

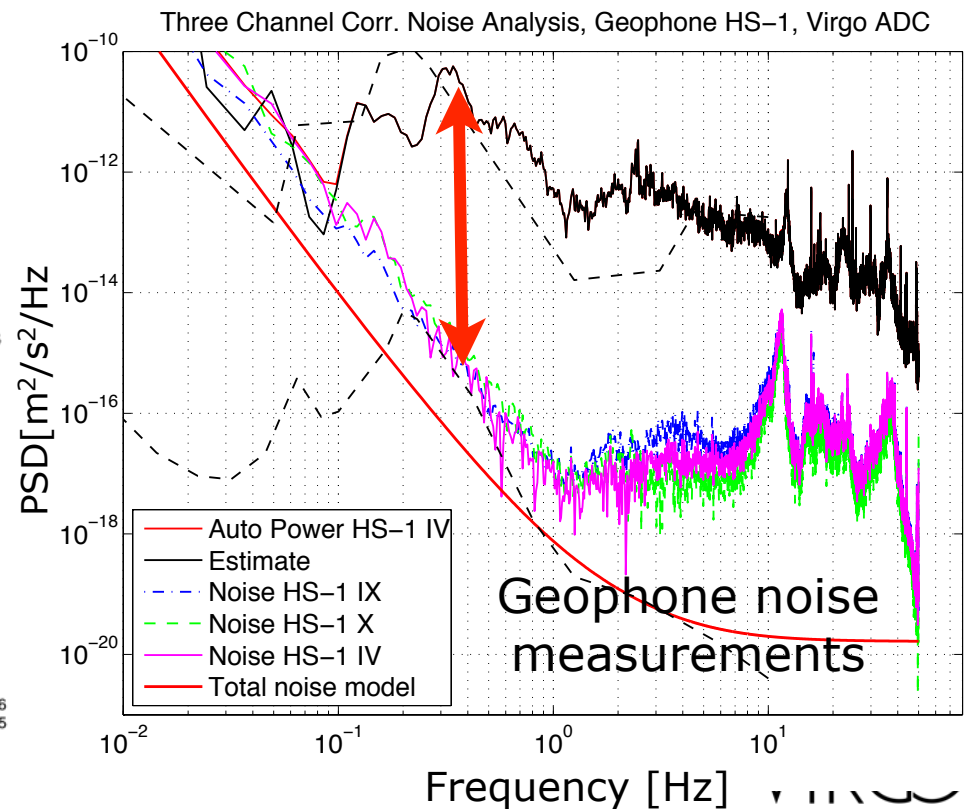
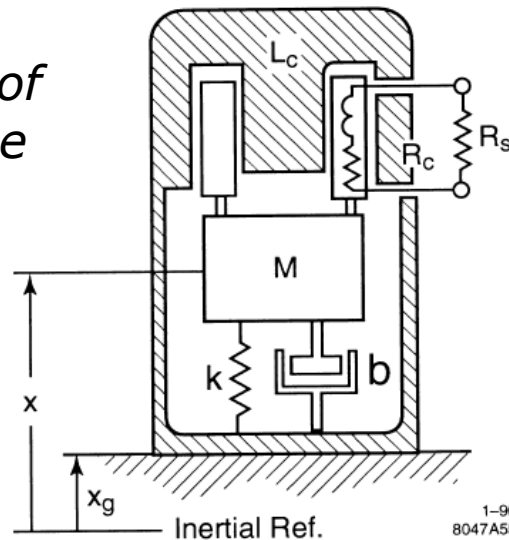
- Linear Voltage Displacement Transducers (LVDT)

- *DC -> a few Hz*
- *~ 1 nm sensitivity*

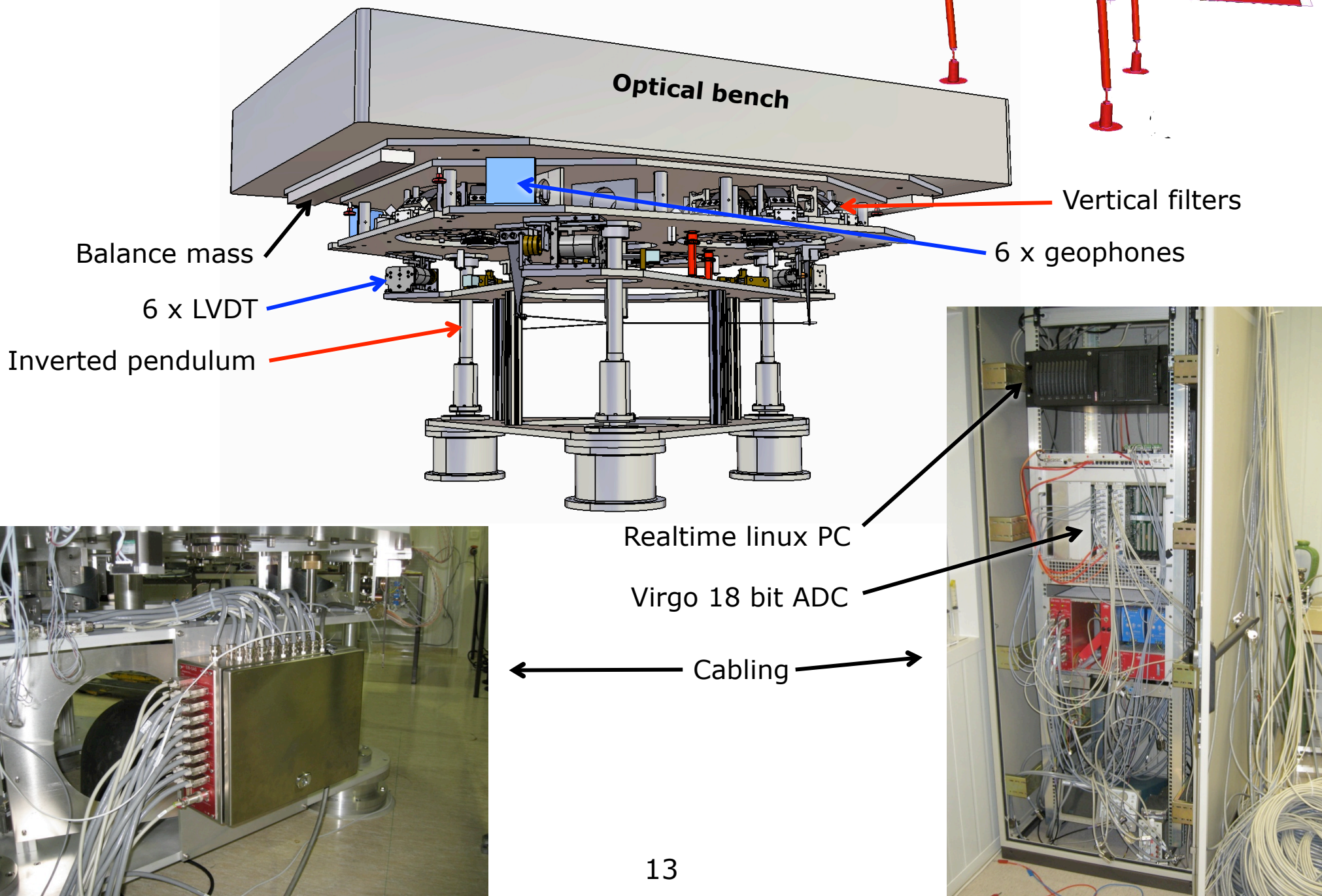


- Accelerometers (Geophones)

- *Eigenfrequency ~ 1 Hz*
- *0.1 -> 100 Hz*
- *Motion 4 orders of mag. above noise level*

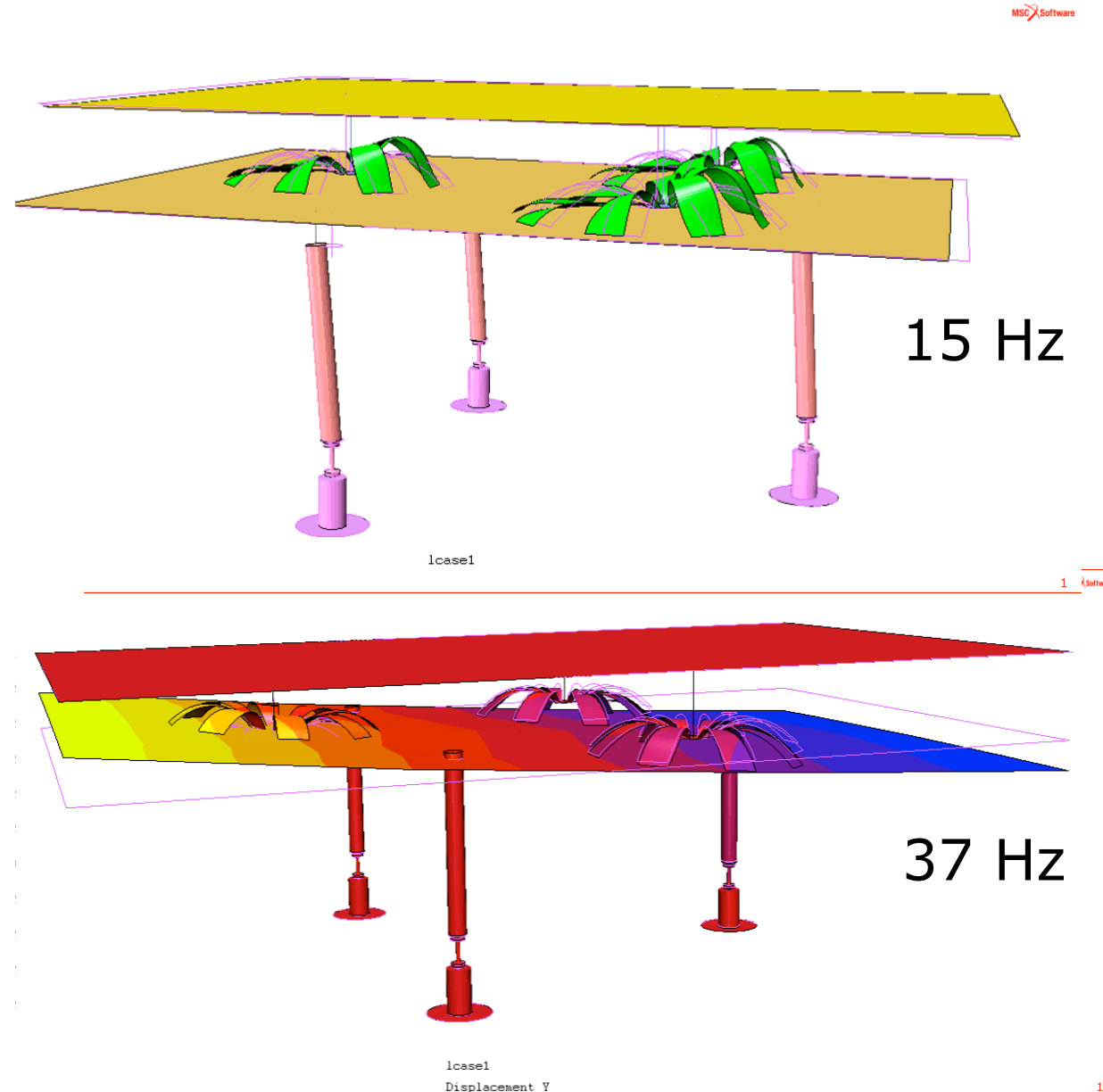
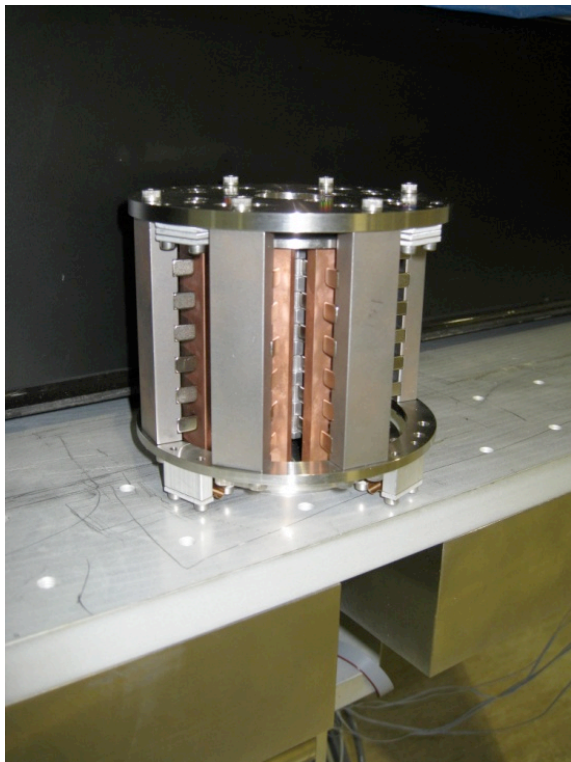


Putting it all together...

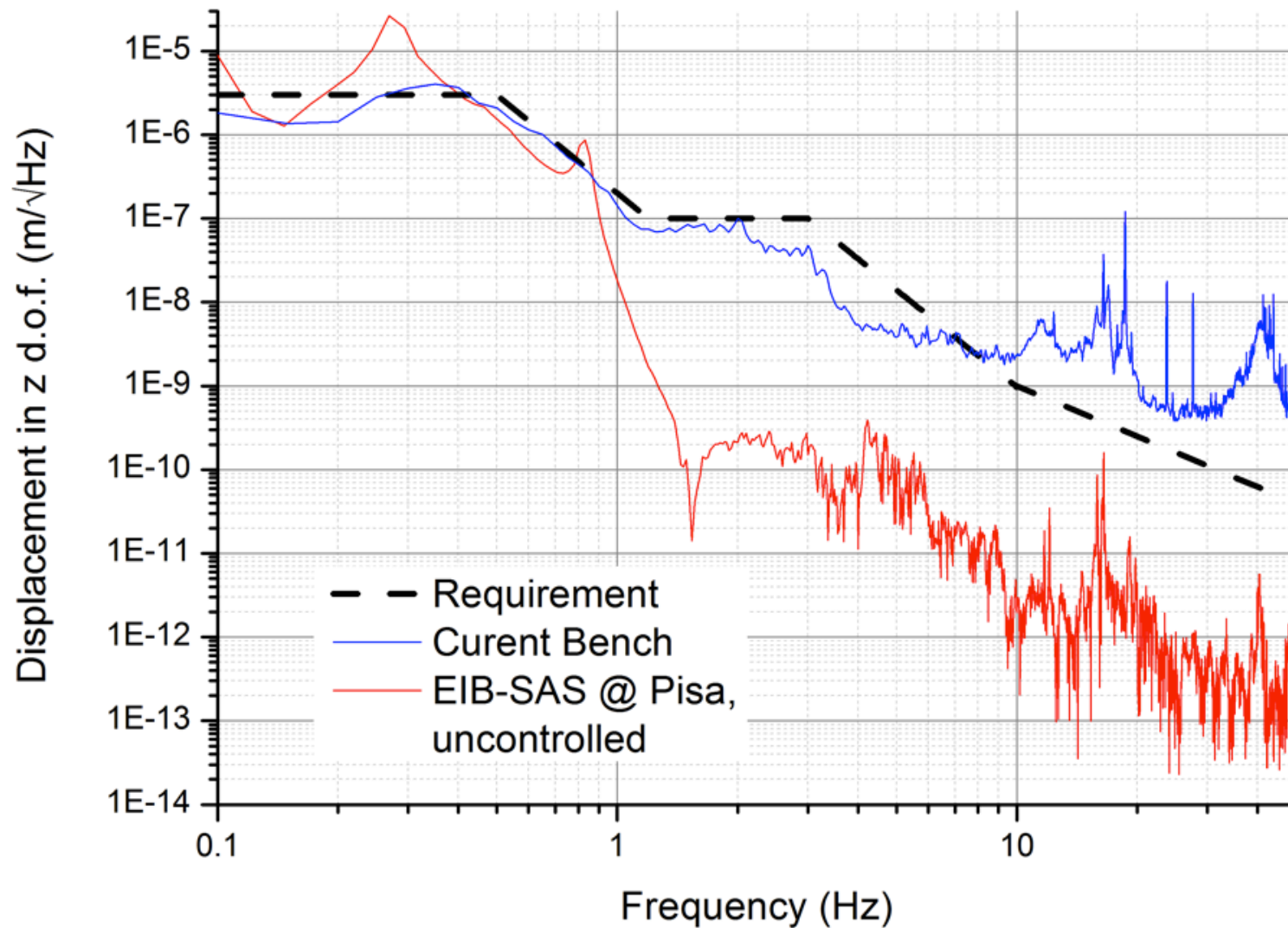


Peaks at higher frequencies are understood internal modes that can be damped

- Eddy-current dampers
- Horizontal and vertical dampers tunable to mode frequencies

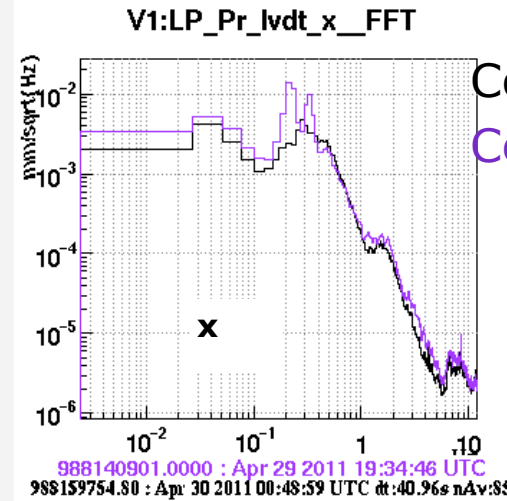
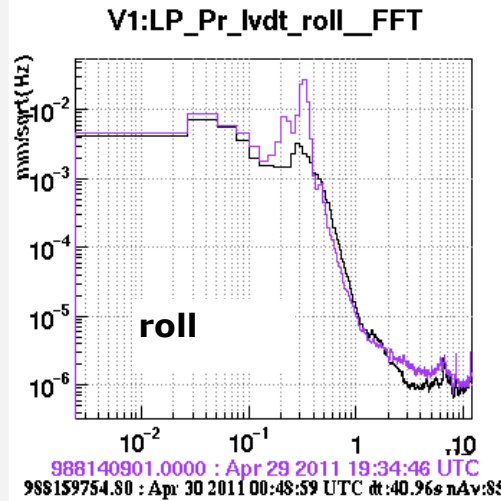
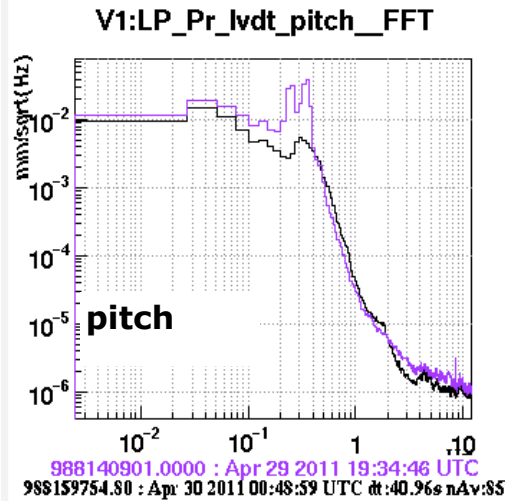


Eddy-current dampers reduce internal mode vibrations below requirements

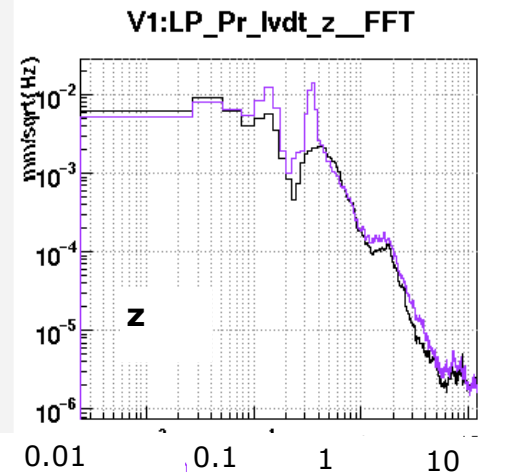
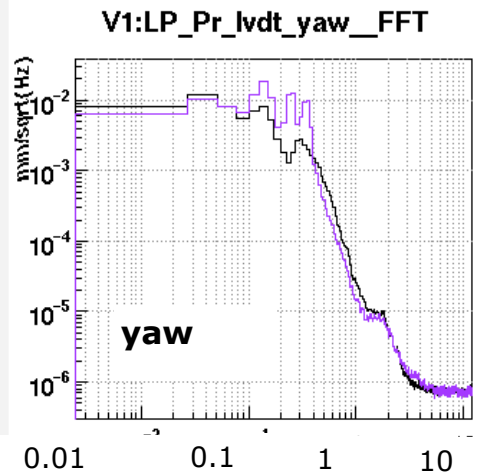
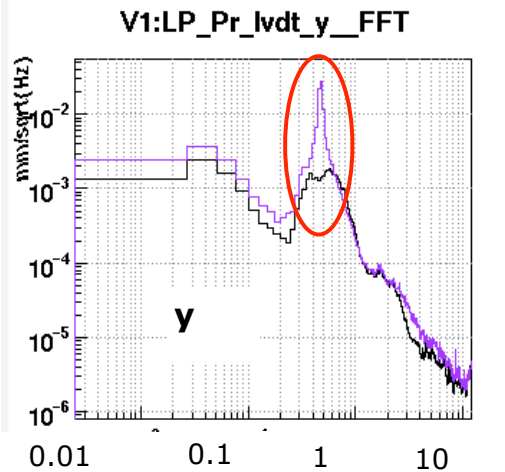


Active control system can damp resonant frequencies by an order of magnitude

FFT - Damping with LVDTs



Controls on
Controls off



Frequency (Hz)

Summary

- Seismic motion
 - *Induces noise in gravitational waves detectors*
 - *Seismic noise also an issue in (future) high-energy experiments*
- Optical bench - Seismic attenuation system
 - *Passive*
 - *Based on harmonic oscillator transfer functions*
 - *Inverted pendulum and anti-springs used at low f_0*
 - *Attenuation of 40 dB available above 10 Hz*
 - *Resonant frequencies damped by active feedback system*
 - *Internal modes removed by tunable eddy-current dampers*

Summary

- Seismic motion
 - *Induces noise in gravitational waves detectors*
 - *Seismic noise also an issue in (future) high-energy experiments*
- Optical bench - Seismic attenuation system
 - *Passive*
 - *Based on harmonic oscillator transfer functions*
 - *Inverted pendulum and anti-springs used at low f_0*
 - *Attenuation of 40 dB available above 10 Hz*
 - *Resonant frequencies damped by active feedback system*
 - *Internal modes removed by tunable eddy-current dampers*

Installation in Virgo \Rightarrow September 2011