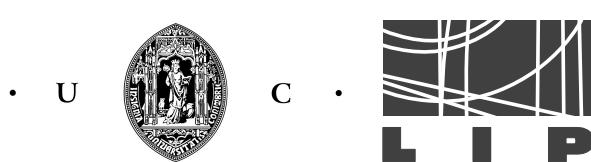
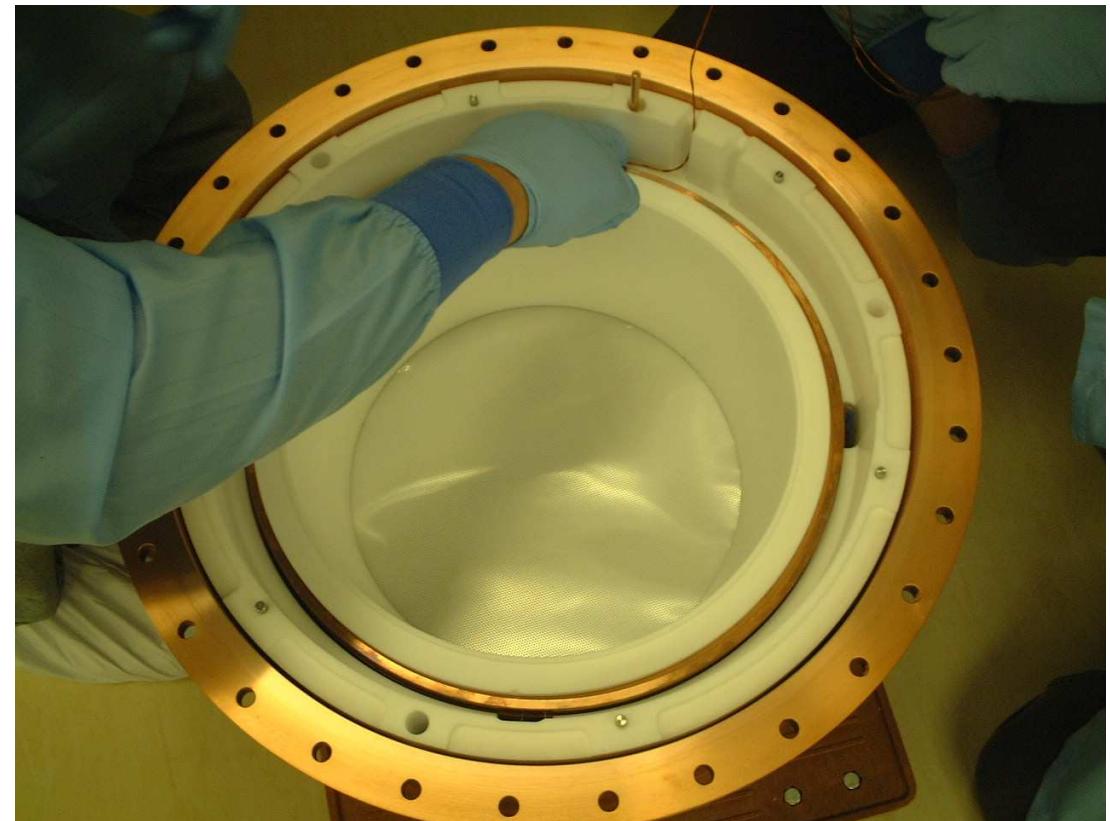


PTFE Reflectance Measurements, Modeling and Simulation for Xenon Detectors

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University of Coimbra
LIP Laboratory

Chicago, 11 June 2011



TIPP 2011

The PTFE in Xenon Detectors

PTFE (polytetrafluoroethylene) is a common choice for the inner walls of liquid/gaseous xenon experiments

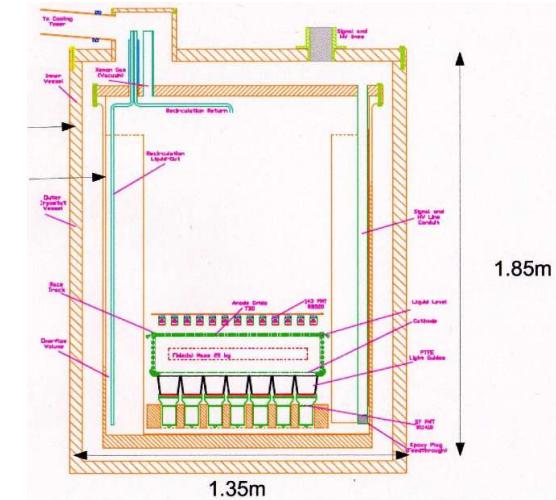
■ Dark Matter Detectors



LUX



XENON100

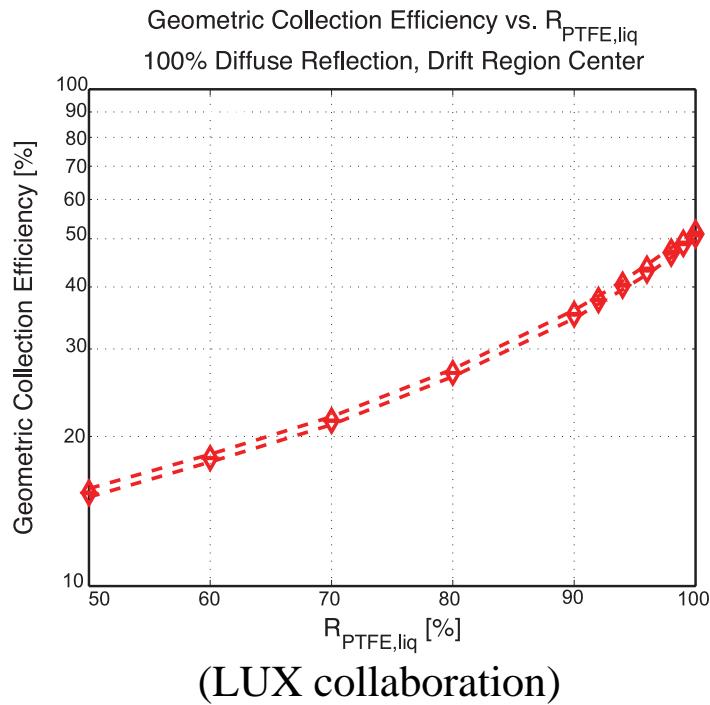


Panda-X

■ Double-beta decay

- ## ■ NEXT (gaseous xenon)

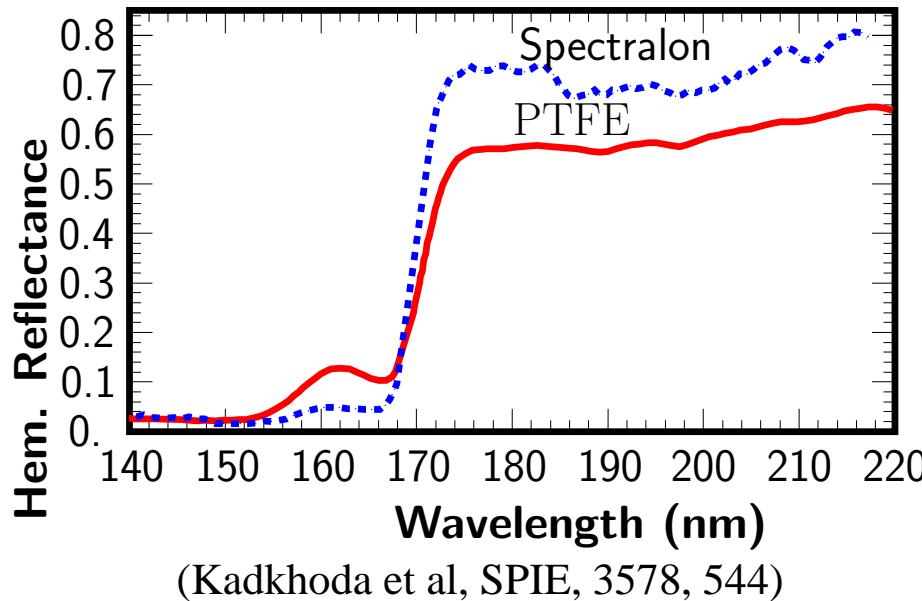
Why the use of PTFE



Xenon emits in the VUV region (175-178 nm).

Below 250 nm the reflectance of the PTFE is not well known.

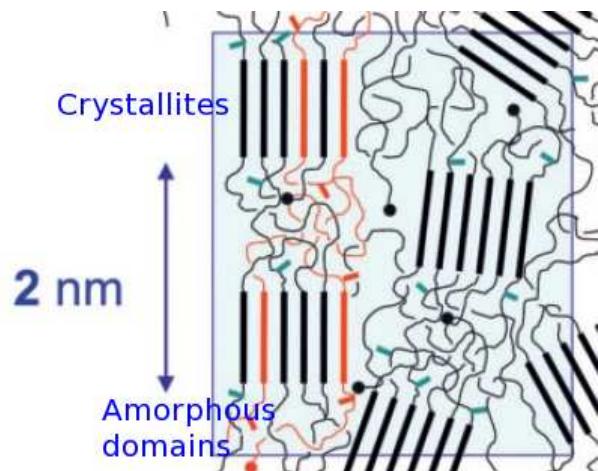
PTFE has a high reflectance in the visible spectra ($\approx 99\%$).
A large reflectance essential to optimize the light collection.



Objectives

- The measurement of the reflectance distributions of various fluoropolymers samples for the xenon scintillation light.
- The modeling of the processes involved and the application to Geant4 simulations.
- Prediction of the reflectance distribution for the liquid xenon/PTFE interface.

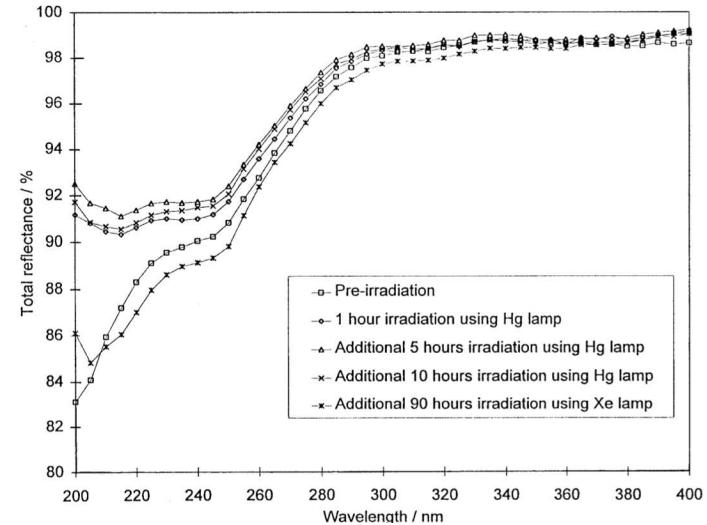
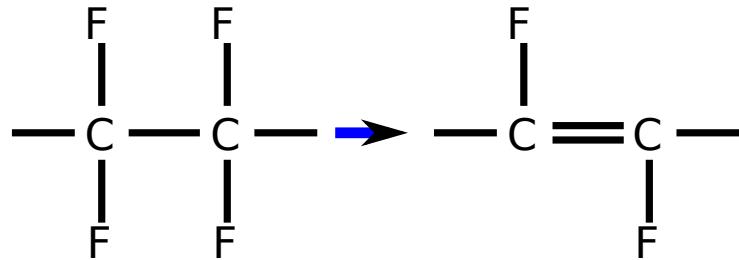
The PTFE/Teflon®



- The simplest fluoropolymer
 $(-\text{CF}_2)_n-$
- CF is the strongest bond in organic chemistry (good chemical resistance)
- High temperature resistance
-200 °C to 260 °C
- Helicoidal structure (temperature dependent)
- Composed by a crystalline and amorphous phase (usually with different optical properties)

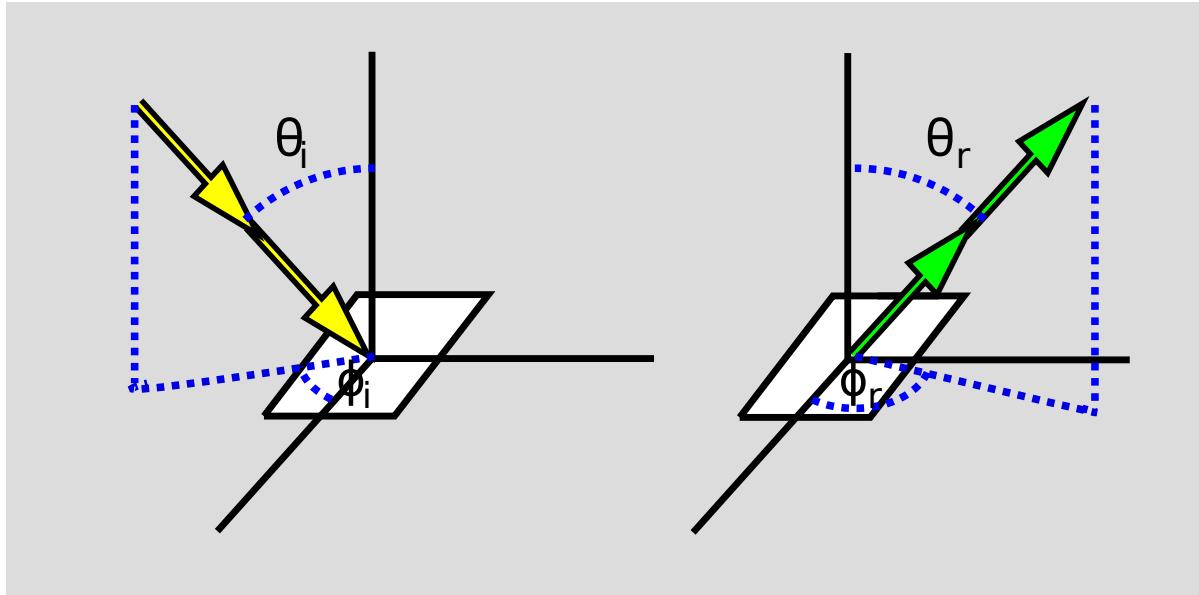
PTFE - What we should be careful

- PTFE degradation under intense VUV radiation



- PTFE absorbs contaminants (hydrocarbonets)
 - Vacuum-baking at about 90 °C for a period of about 48 h recommended
 - It should be left in a sealed container.
 - Plastic containers are not recommended.

What do We Mean by Reflection?

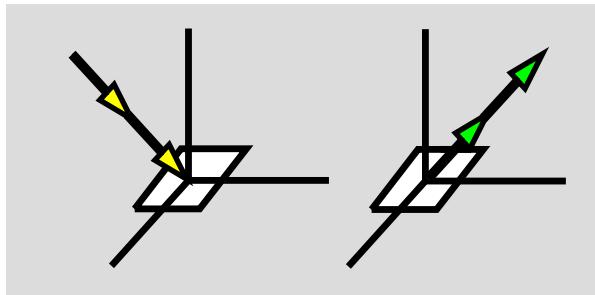


Bidirectional reflectance distribution function

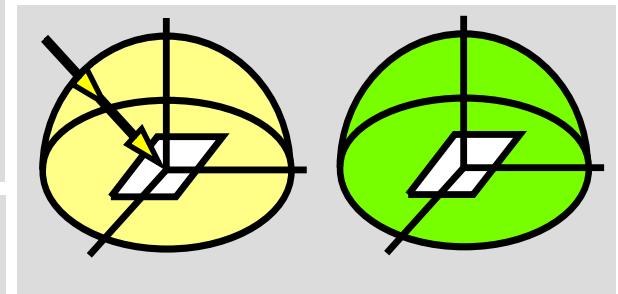
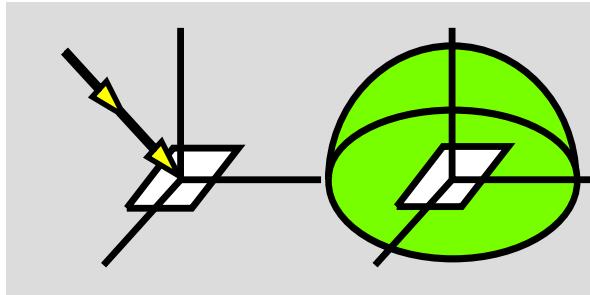
$$\rho(\theta_i, \phi_i; \theta_r, \phi_r) = \frac{dI_r(\theta_i, \phi_i, \theta_r, \phi_r)}{d\Phi_i(\theta_i, \phi_i)}$$

What do We Mean by Reflection?

Bidirectional

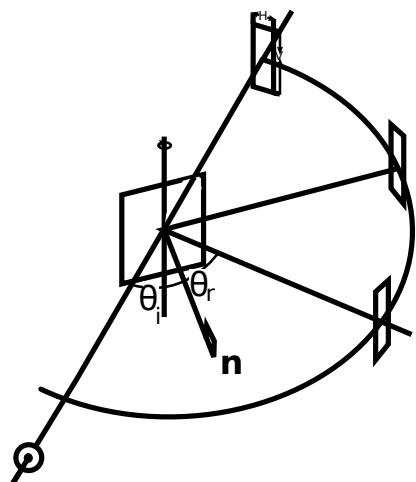


Directional-Hemispherical

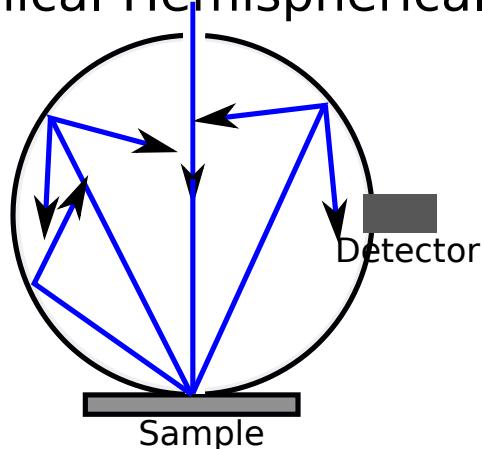


Bi-Hemispherical

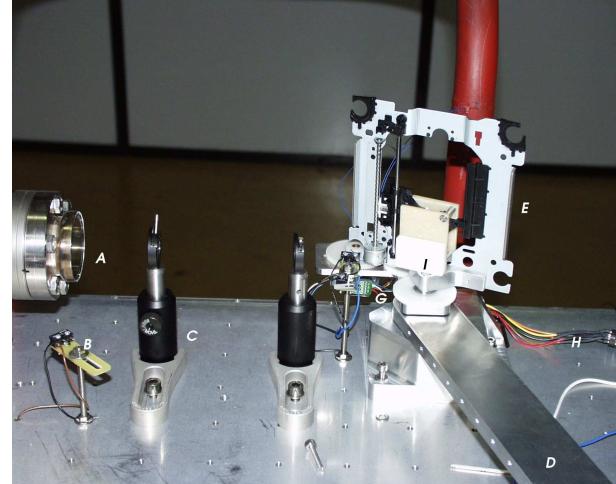
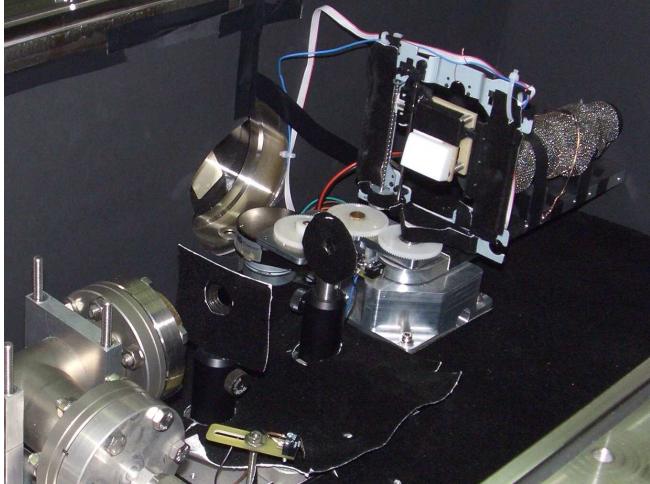
Biconical



Conical-Hemispherical

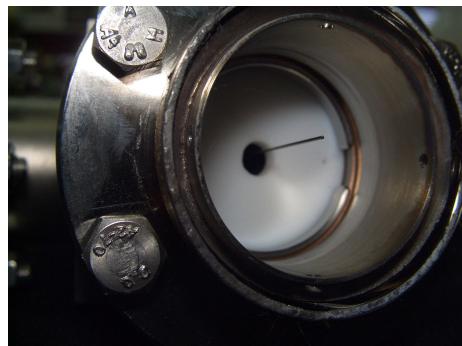
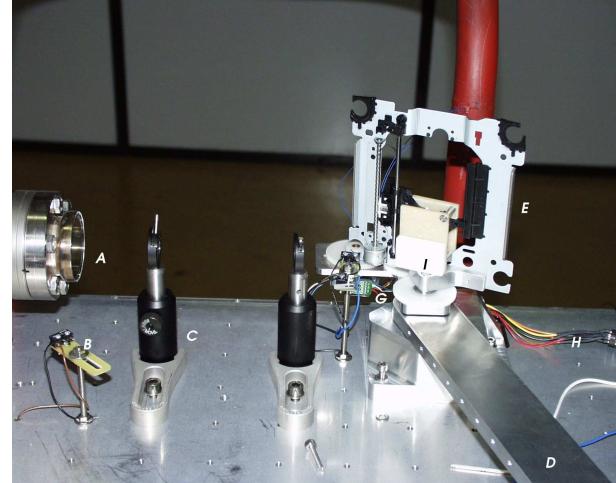
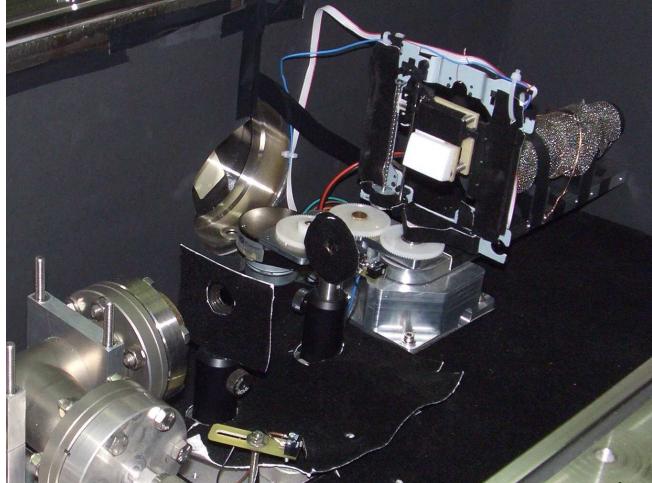


The Angle Resolution System

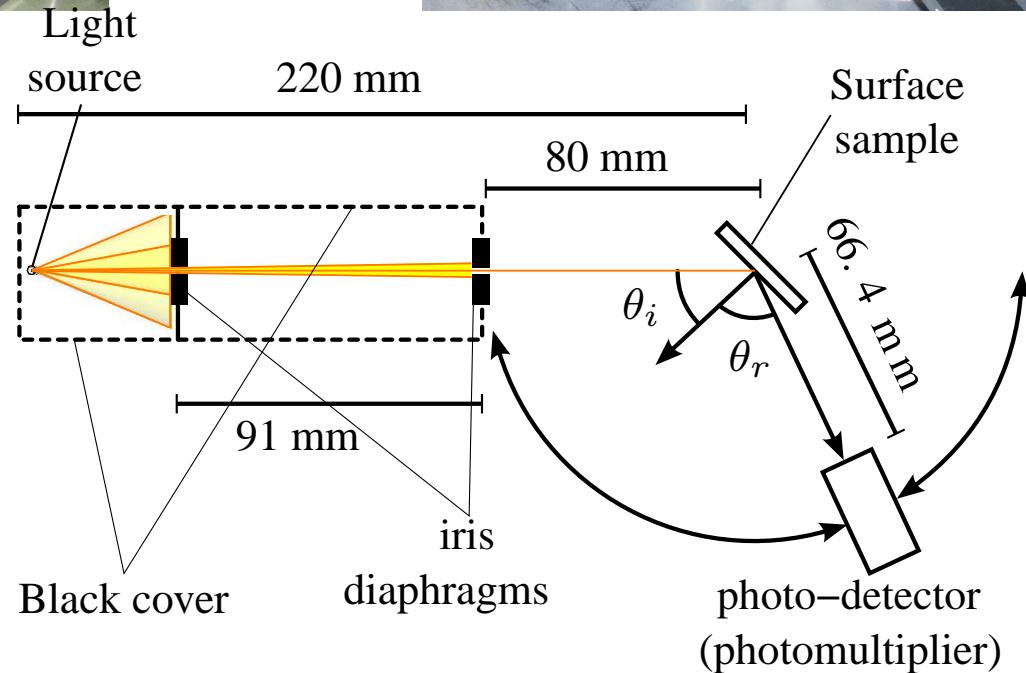


- The Angle Resolution System (ARS) is placed inside an air tight chamber.
- The light of 175 nm is emitted by a xenon proportional counter.

The Angle Resolution System

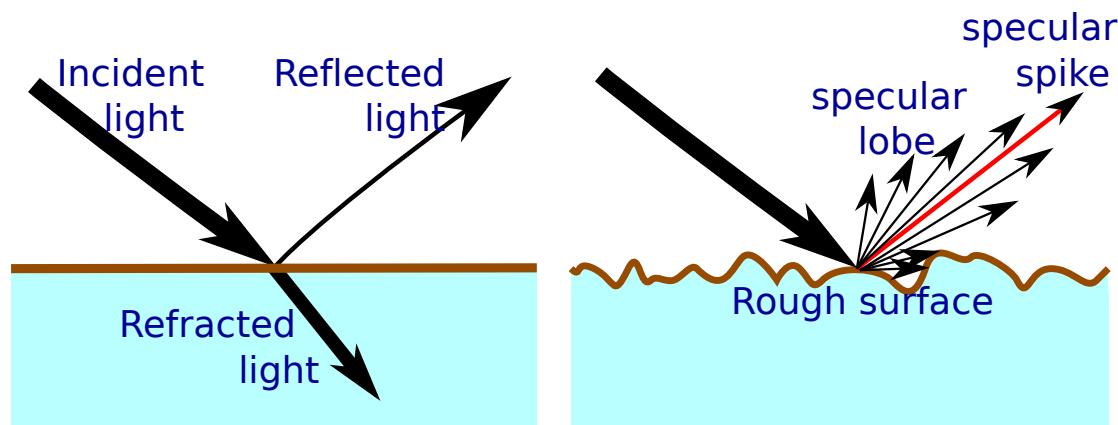


Xenon scintillation
light source

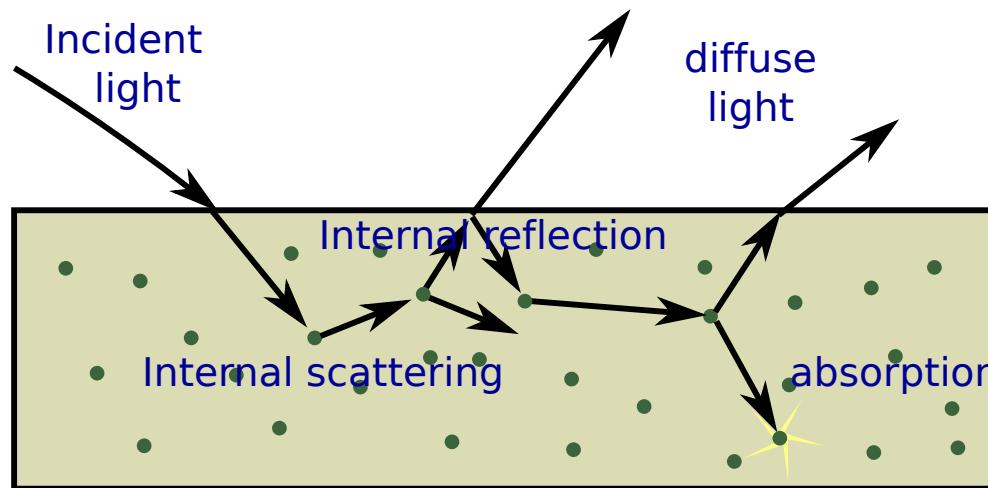


Reflectance Components

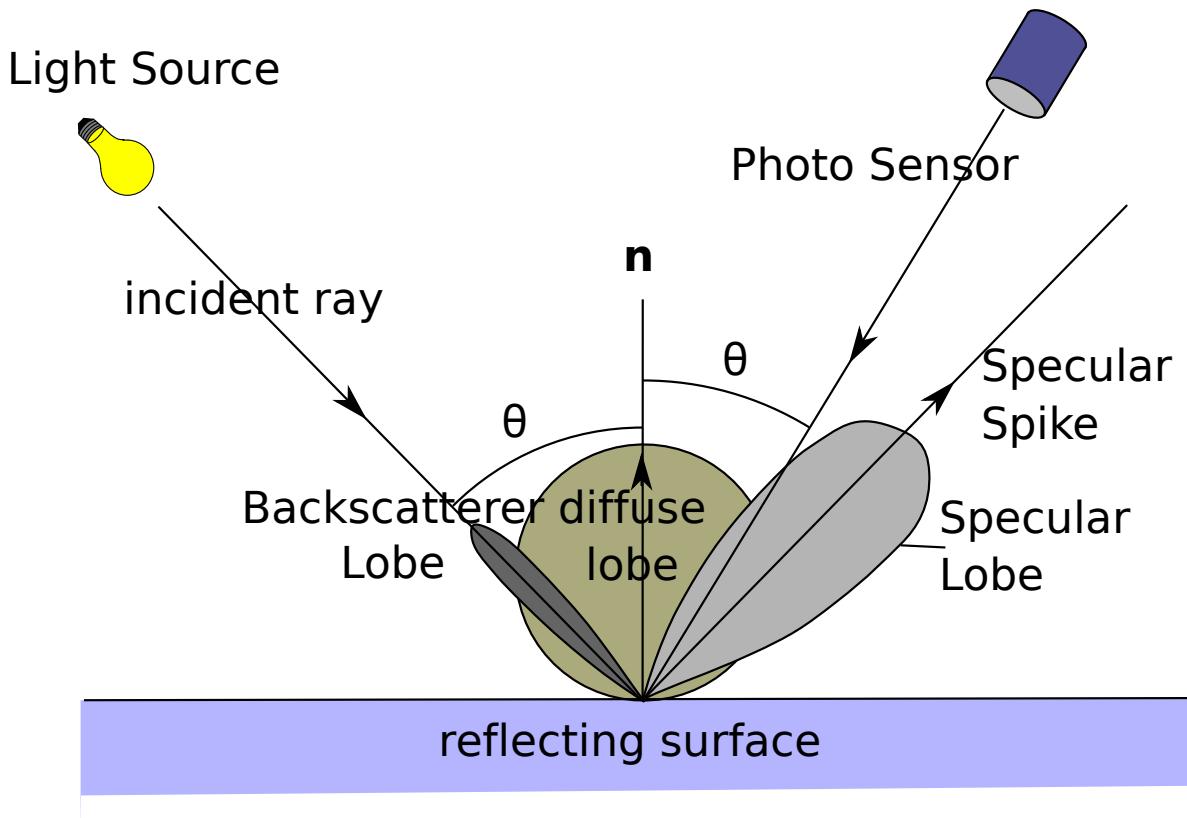
■ Specular:



■ Diffuse:



Reflectance Components



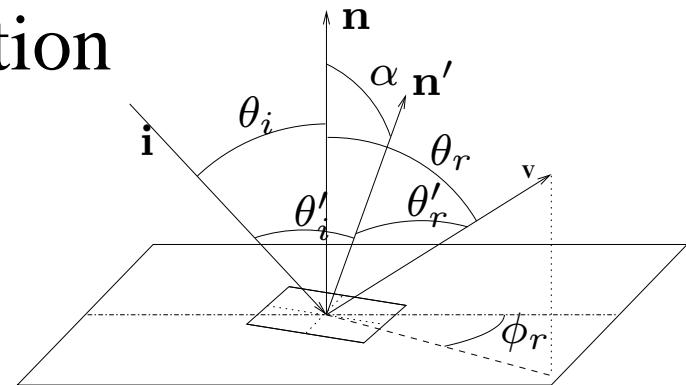
$$\rho = \rho_l + \rho_s + \rho_d + \rho_b$$

- $\rho_l \rightarrow$ specular lobe
- $\rho_s \rightarrow$ specular spike
- $\rho_d \rightarrow$ diffuse lobe
- $\rho_b \rightarrow$ backscatterer lobe

The Specular Reflection

$$\rho = F(\theta_i) \chi_1 \chi_1^* \delta(\mathbf{i} - \mathbf{r}) + (1 - \chi_1 \chi_1^*) F(\theta') \frac{P_\alpha(\alpha) G(\theta_i, \theta_r)}{4 \cos \theta_i}$$

- F - the Fresnel equations, dependent of n and κ
- χ_1 - the characteristic function of the probability distribution of heights $P_1(z)$
- $P_\alpha(\alpha)$ - the probability distribution of the slopes α
- $G(\theta_i, \theta_r)$ - shadowing-masking attenuation coefficient



The Specular Lobe

The following distributions P_α were considered

- Cook-Torrance - *Gaussian Like*

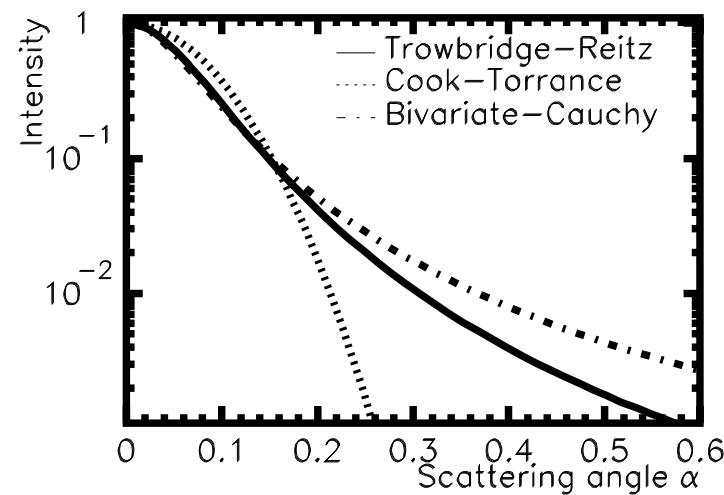
$$P_{CT}(\alpha, m) = \frac{1}{\pi m^2 \cos^4 \alpha} \exp\left(-\frac{\tan^2 \alpha}{m^2}\right)$$

- Trowbridge-Reitz

$$P_{TR}(\alpha, \gamma) = \frac{\gamma^2}{\pi (\gamma^2 \cos^2 \alpha + \sin^2 \alpha)^2}$$

- Bivariate-Cauchy

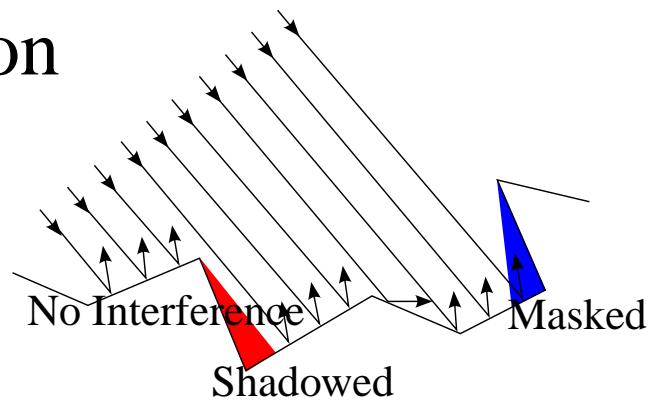
$$P_{BC}(\alpha, \gamma) = \frac{\gamma^2 + \gamma}{\pi (\gamma^2 \cos^2 \alpha + \sin^2 \alpha)^{\frac{3}{2}}}$$



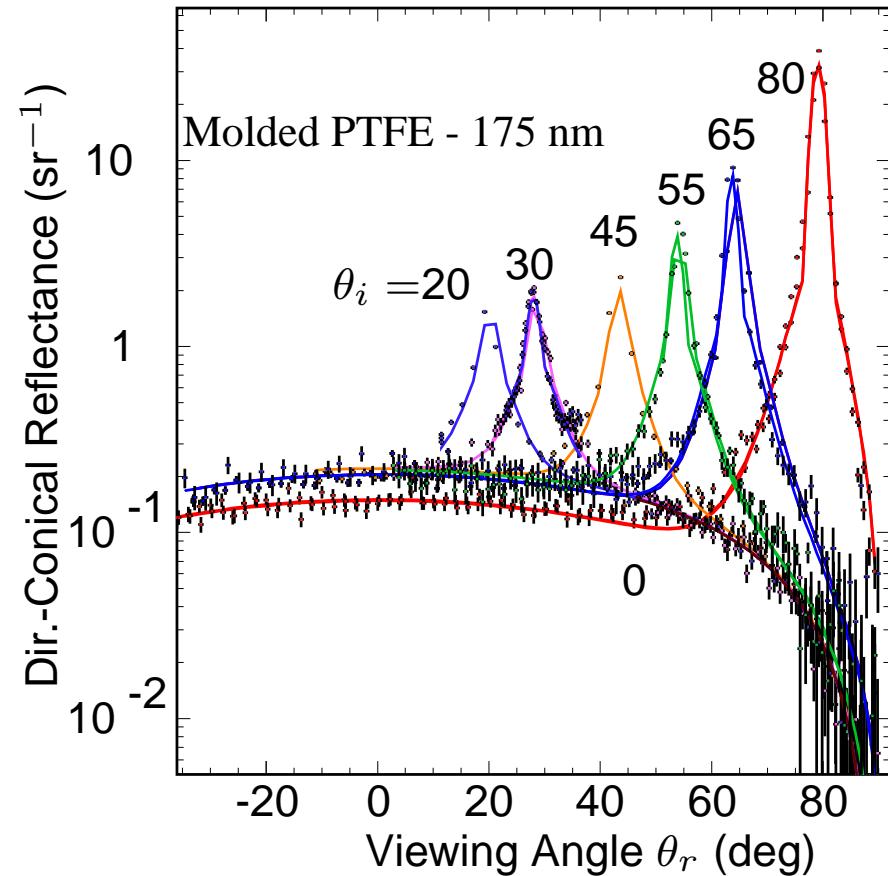
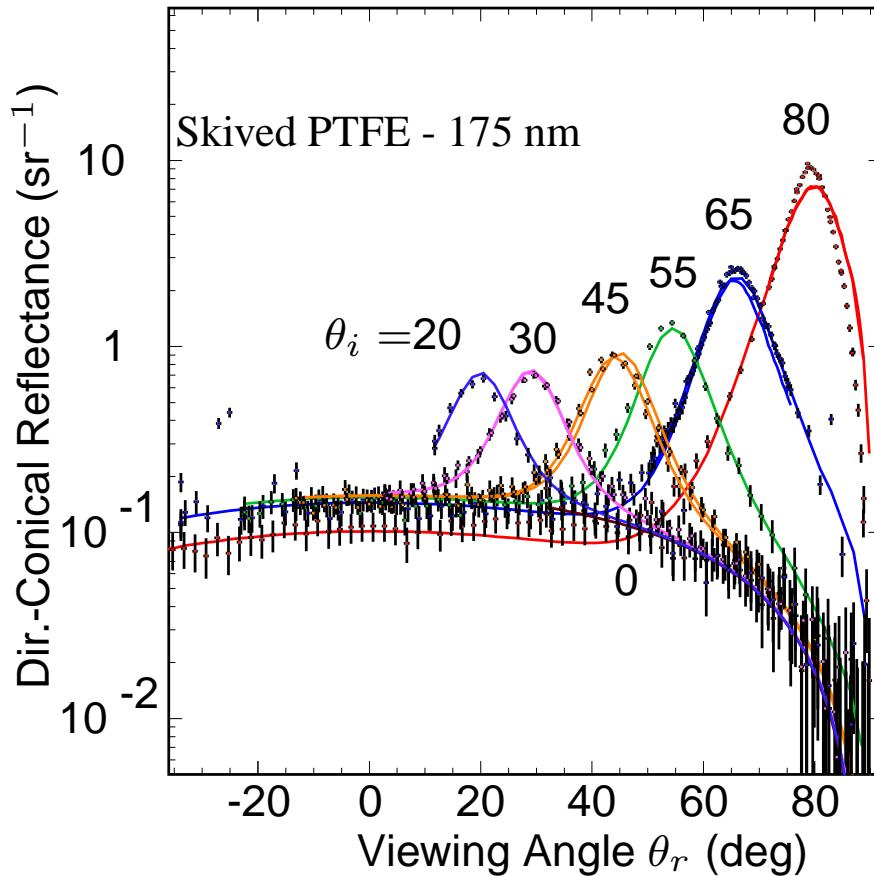
The Specular Reflection

$$\rho = F(\theta_i) \chi_1 \chi_1^* \delta(\mathbf{i} - \mathbf{r}) + (1 - \chi_1 \chi_1^*) F(\theta') \frac{P_\alpha(\alpha) G(\theta_i, \theta_r)}{4 \cos \theta_i}$$

- F - the Fresnel equations, dependent of n and κ
- χ_1 - the characteristic function of the probability distribution of heights $P_1(z)$
- $P_\alpha(\alpha)$ - the probability distribution of the slopes α
- $G(\theta_i, \theta_r)$ - shadowing-masking attenuation coefficient



PTFE Reflectance Distributions

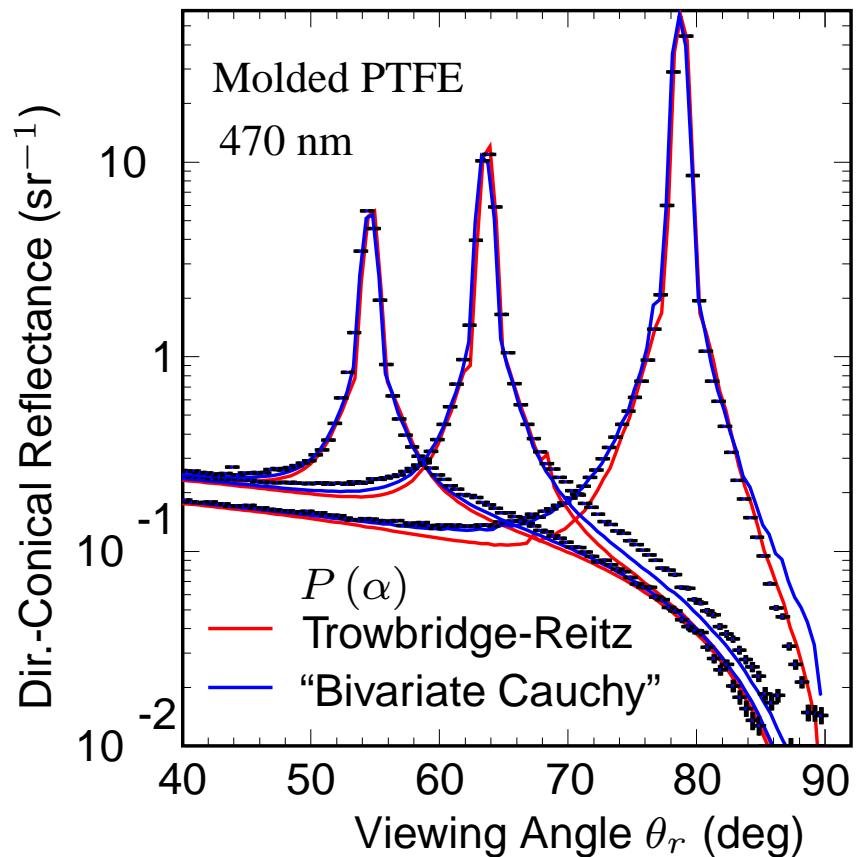
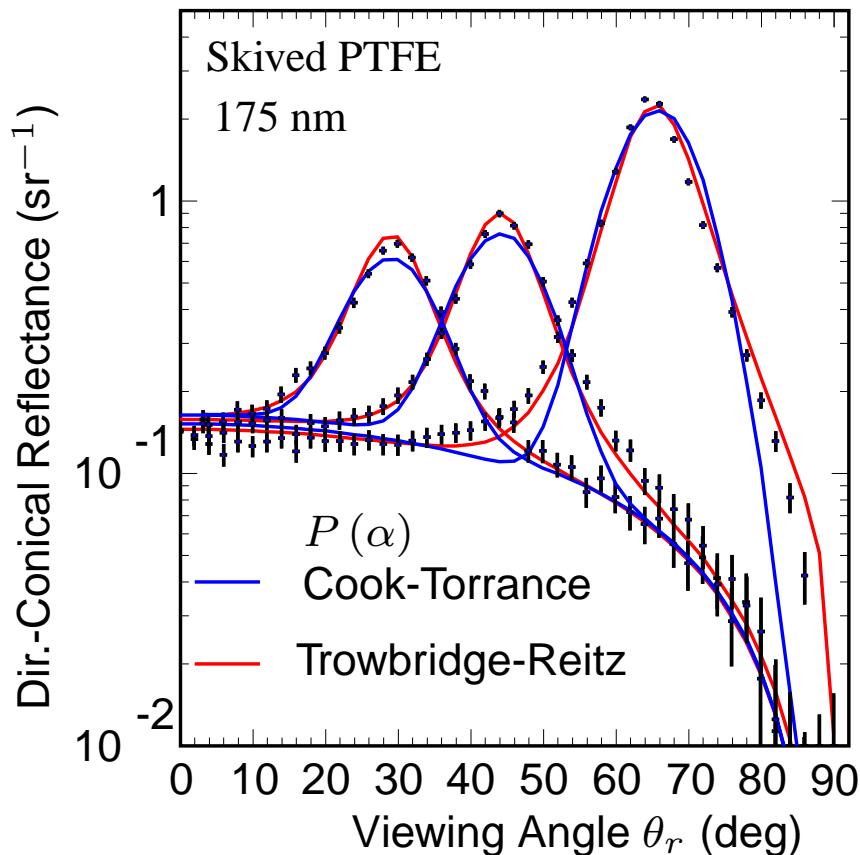


We observe three different components

- Diffuse Lobe
- Specular Lobe
- Specular Spike

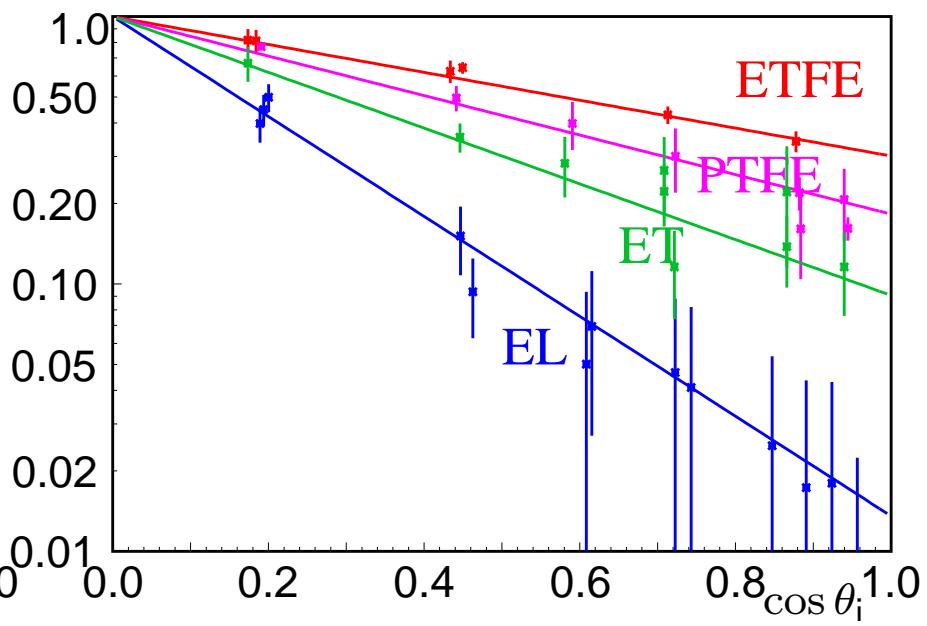
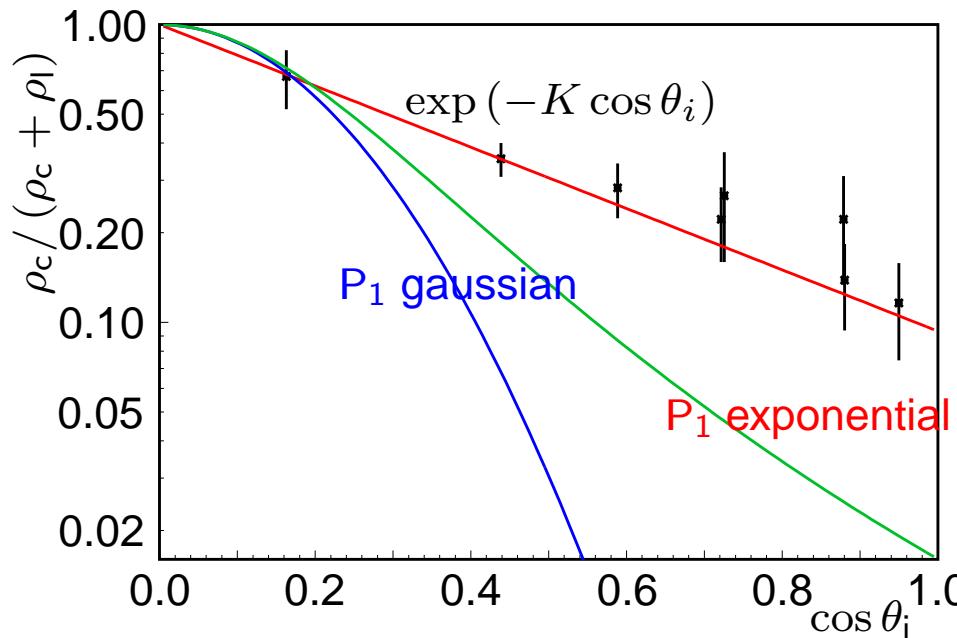
The Specular Lobe

- The “bivariate-cauchy” has the best description
- γ is constant with θ_i and decreases with λ .



The Specular Spike

The intensity of the specular spike ($\rho_c / (\rho_c + \rho_l)$) changes with the roughness, wavelength of the light and angle of incidence.



- The usual distributions p_1 do not describe the data.
 $\Lambda = \exp(-K \cos \theta_i)$ is an empirical function.

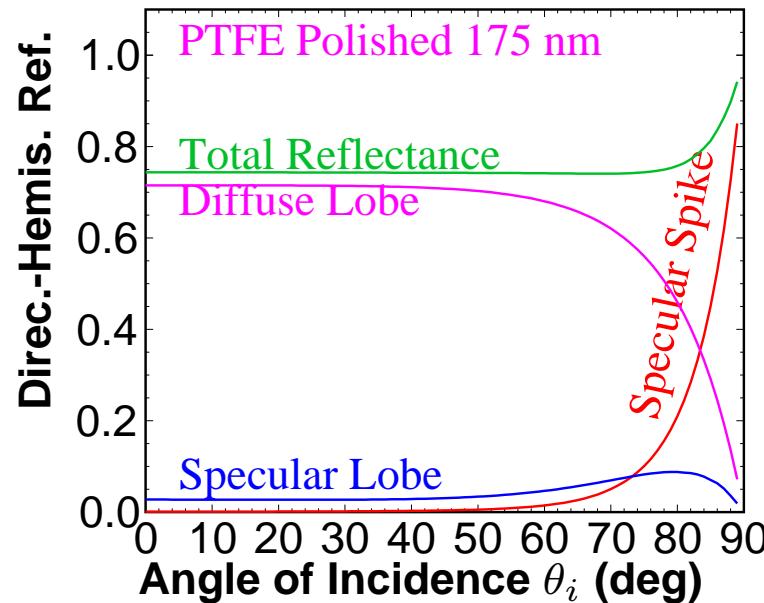
The Fits

A global fit is applied to results with **only three or four** parameters. For the different samples we obtain

| $\lambda = 175 \text{ nm}$ | n refractive index | a_d albedo | γ sp. lobe width | K spike intensity |
|-------------------------------|----------------------------|-----------------|-------------------------------|---------------------------|
| Skived PTFE | 1.49 ± 0.07 | 0.58 ± 0.02 | 0.064 ± 0.006 | - |
| PTFE (not polished) | 1.51 ± 0.07 | 0.52 ± 0.06 | 0.057 ± 0.008 | - |
| Extruded (\perp) PTFE | 1.50 ± 0.03 | 0.69 ± 0.07 | 0.055 ± 0.007 | 3.0 ± 0.3 |
| Extruded (\parallel) PTFE | 1.46 ± 0.04 | 0.63 ± 0.07 | 0.066 ± 0.008 | 4.3 ± 0.5 |
| Molded PTFE | 1.45 ± 0.04 | 0.74 ± 0.07 | 0.049 ± 0.015 | 1.7 ± 0.2 |

The Hemispherical Reflectances

■ Directional-Hemispherical



■ Bi-Hemispherical Reflectance

| | Diffuse. | S. Lobe | S. Spike | Total |
|-----------------|-------------------|-------------------|--------------------|-------------------|
| Skived PTFE | 0.488 ± 0.009 | - | 0.089 ± 0.008 | 0.577 ± 0.007 |
| Molded Polished | 0.625 ± 0.034 | 0.040 ± 0.004 | 0.0438 ± 0.024 | 0.71 ± 0.04 |

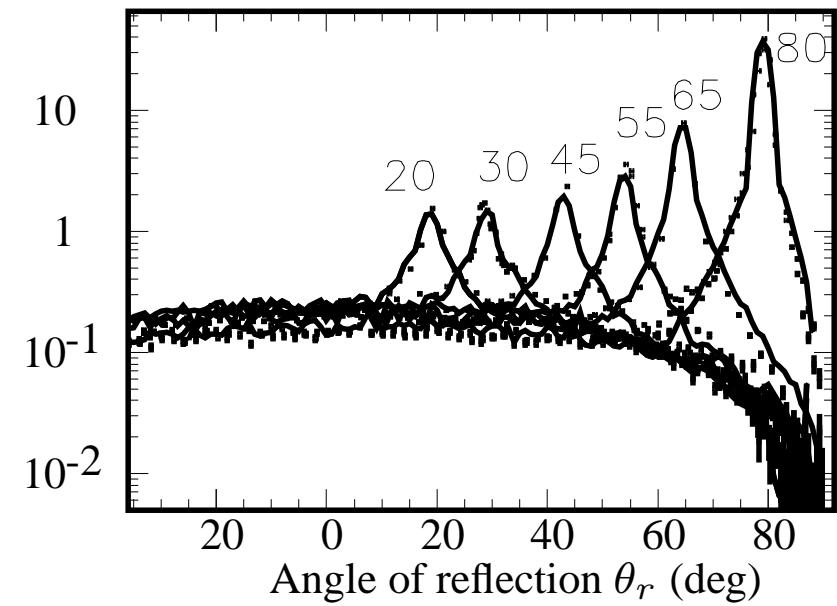
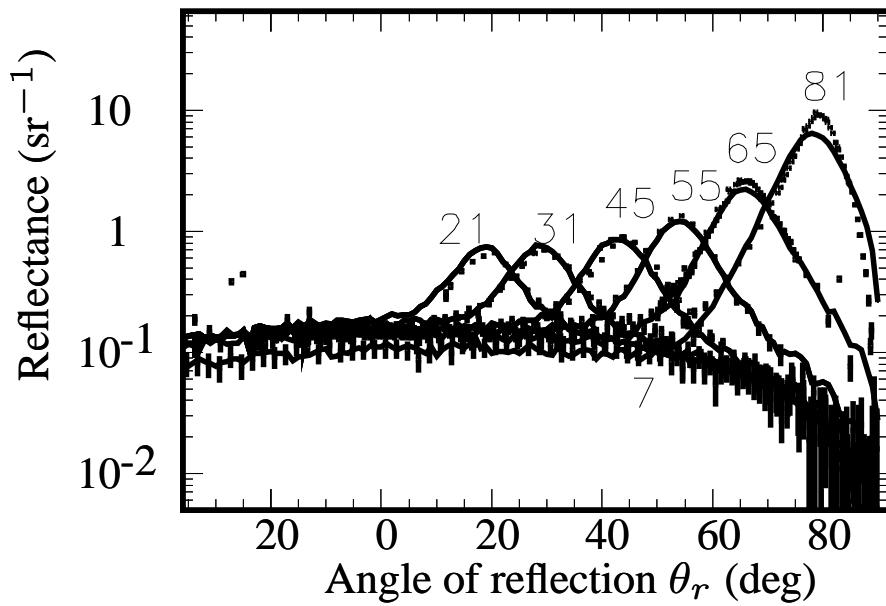
Geant 4 - Current

The current descriptions (Unified and Glisur) do not agree in many ways with our measurements

- Diffuse lobe proportional to the reflected light
- The intensity of the specular spike is independent of the angle of incidence
- It is restricted to gaussian statistics
- The shadowing and masking are not fully considered

Geant 4 - New

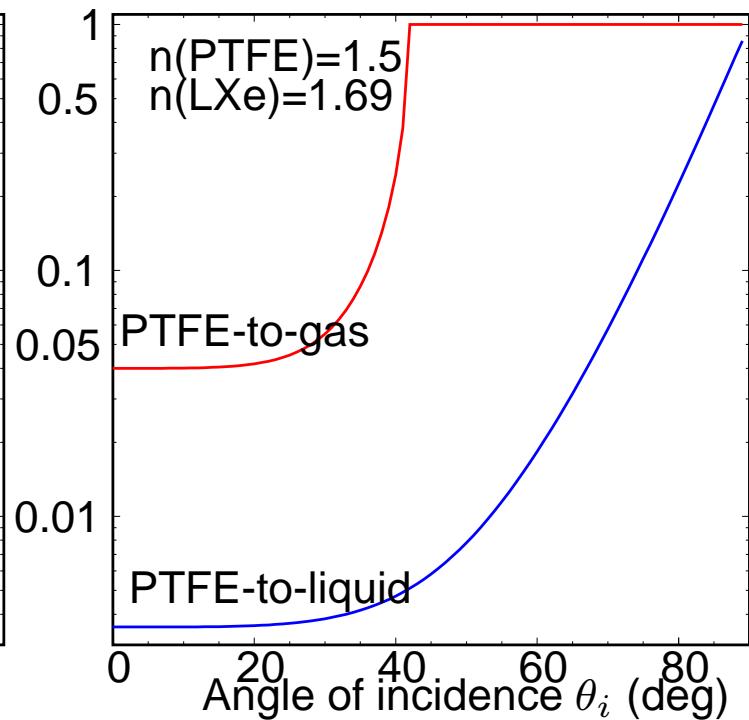
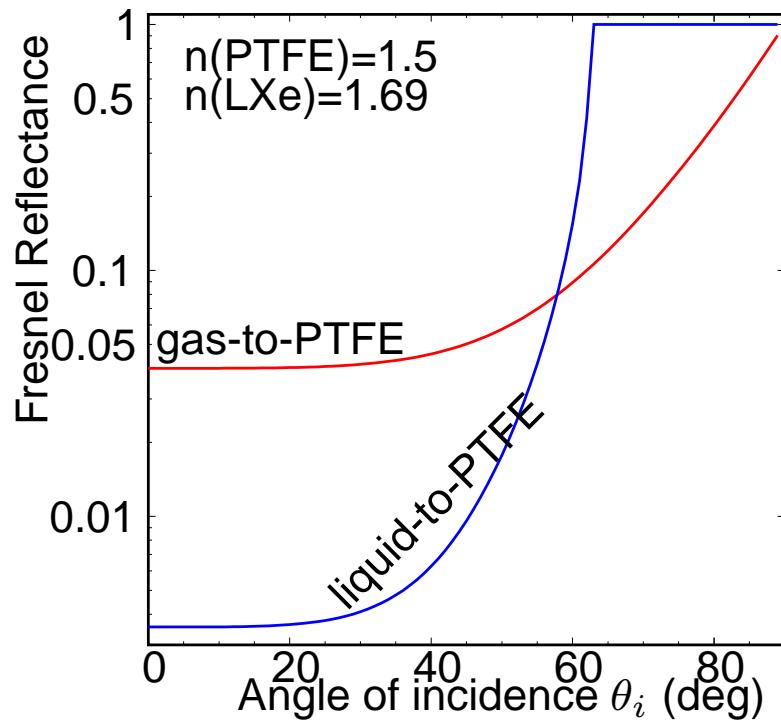
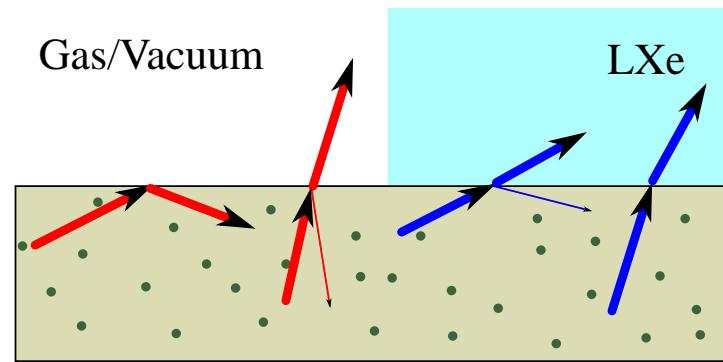
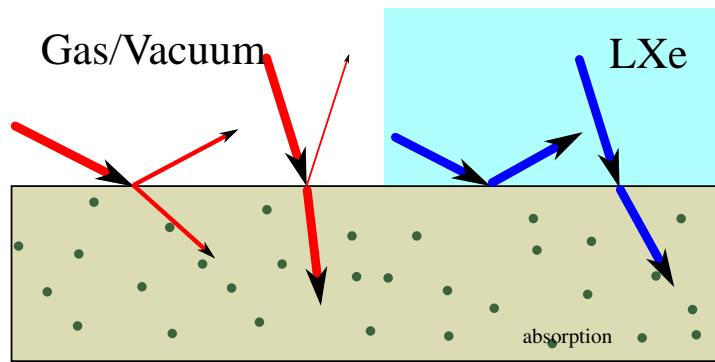
- This model of reflection was included in the Geant4 as new method of the class G4BoundaryProcess.
- Inverse cumulative functions are used to generate the direction of both the diffuse reflected and specularly reflected light.



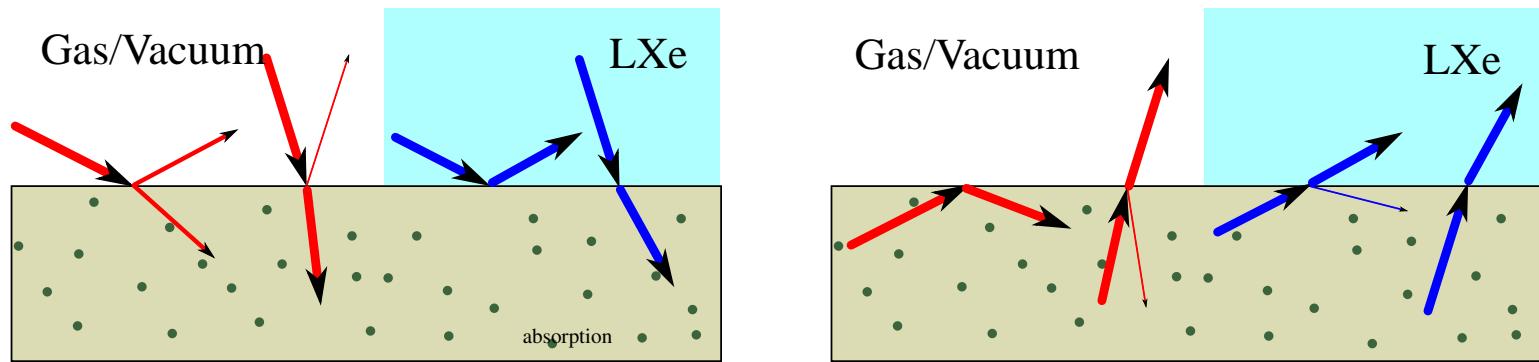
Reflection in a Liquid Interface

- The reflectance obtained in the gas/PTFE is between 60-80%. There are strong indications that the reflectance in the liquid xenon is much higher ($>80\%$).
- The liquid xenon has a higher index of refraction ($n \simeq 1.69$) comparatively to the air or vacuum

Reflection in a Liquid Interface



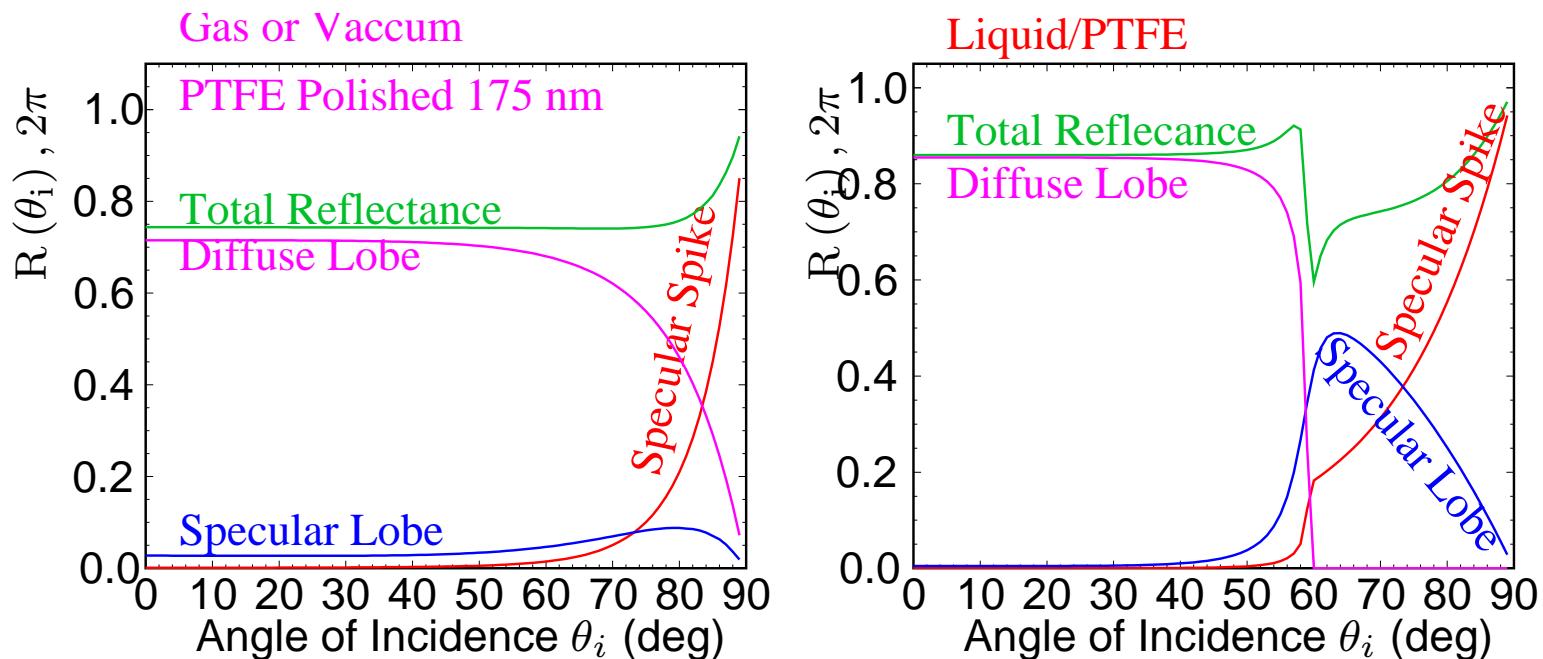
Reflection in a Liquid Interface



In the liquid:

- The internal reflection probability is smaller.
- Less light returns to the bulk to be internally scattered where it can be eventually absorbed.
- The multiple-diffuse albedo a_d will be larger.

Reflection in a Liquid Interface



| | Diffuse Lobe | | Specular Lobe | | Specular Spike | | Total Ref | |
|-------------|--------------|------|---------------|------|----------------|------|-------------|-------------|
| | Gas | Liq. | Gas | Liq. | Gas | Liq. | Gas | Liq. |
| Skived PTFE | 0.49 | 0.55 | 0.089 | 0.25 | 0.0 | 0.0 | 0.58 | 0.80 |
| Molded PTFE | 0.63 | 0.59 | 0.040 | 0.13 | 0.04 | 0.16 | 0.77 | 0.89 |

Conclusion

- We developed an angle resolution system to measure the reflectance distribution in vacuum.
- The reflectance distribution of the PTFE is composed by three contributions (diffuse lobe, specular lobe and specular spike).
- Four free parameters reproduces fairly well the details of the measured reflectance distributions.
- A new simulation of the reflectance processes was included in Geant-4
- The reflectance distributions were estimated to a Liquid-PTFE interface.

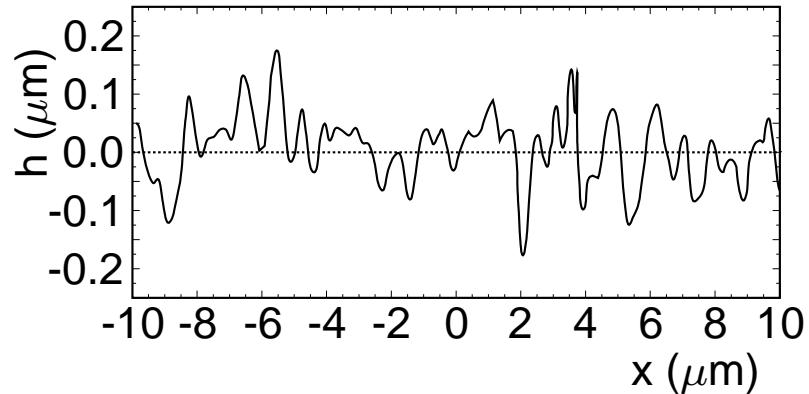


Thank you!

Surface Statistics

- $h(x, y)$ the height function

$$z = h(x, y) \quad \langle h(x, y) \rangle = 0$$



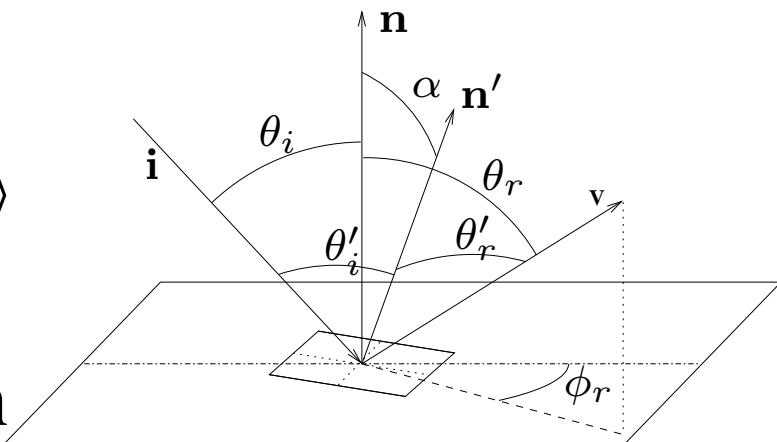
- $P_2(z, z')$, bivariate distribution of heights

$$P_2(z, z') = \frac{1}{\sqrt{2\pi[1-C(\tau, T)]}\sigma_h} \exp \left\{ -\frac{z^2 - 2C(\tau, T)zz' + z'^2}{2\sigma_h^2[1-C(\tau, T)]} \right\}$$

- $C(r, T)$ correlation function

$$C = \frac{1}{\sigma_h^2} \langle h(x_1, y_1), h(x_2, y_2) \rangle$$

- $P_\alpha(\alpha, \sigma_\alpha)$ - slope distribution



The Specular Reflection in a Rough Surface

- A complex diffraction problem

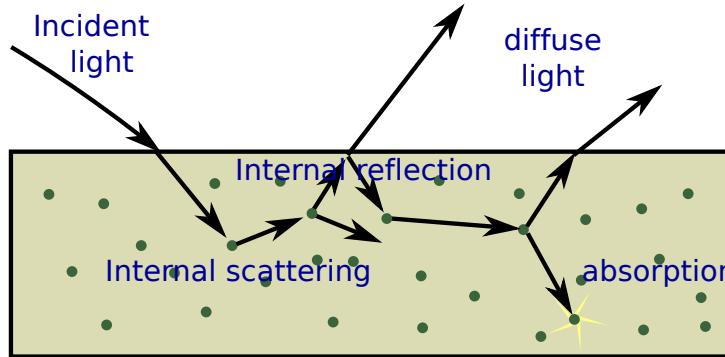
$$\rho = \frac{R^2 \cos^2 \theta'}{\cos \theta_i \lambda^2} \int_0^\infty \chi_2(\tau) J_0(k_z \tau) \tau d\tau$$

χ_2 is the characteristic function of P_2

- For a bivariate gaussian distribution

$$\begin{aligned} \rho = & \frac{E_0^2 R^2 \cos^2 \theta'}{\lambda^2} \chi_1 \chi_1^* \left\{ \int_0^\infty J_0(k_z \tau) \tau d\tau \right. \\ & \left. + \sum_{n=1}^{\infty} \frac{k_z^{2n} \sigma_h^{2n}}{n!} \int_0^\infty [C(\tau, T)]^n J_0(k_z \tau) \tau d\tau \right\} \end{aligned}$$

The Diffuse Component



$$\rho_d = \frac{a_d}{\pi} \cos \theta_r \Upsilon (\theta_i, \theta_r, \phi) [1 - F(\theta_i, \phi)] [1 - F(\theta_r)]$$

- The light is scattered isotropically in the bulk.
- The Fresnel factors account with the two refractions of the light, Air-to-PTFE and PTFE-to-Air.
- a_d is the multiple-diffuse albedo of the surface.
- **Oren-Nayar factor** Υ accounts for the roughness of the surface.