

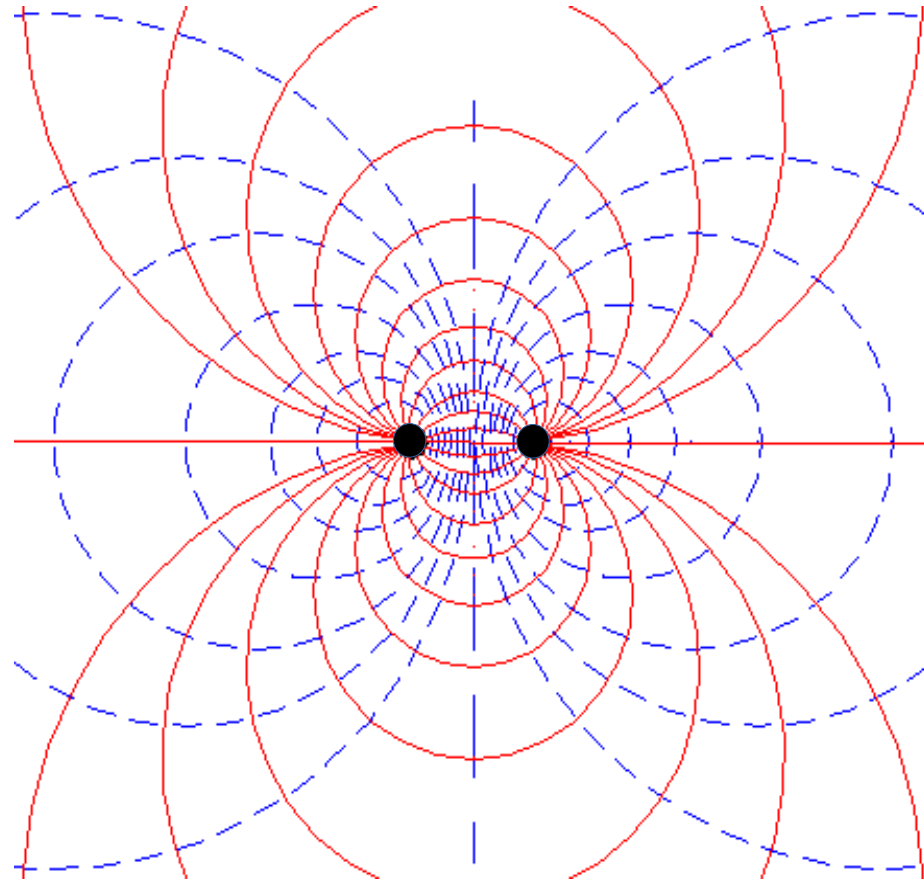
Everything you
need to know to
choose the right
cable assembly

RADIO FREQUENCY

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Geretsried, Germany
21 – 23 June 2021

Attenuation

To connect a signal from A to B two wire will work.



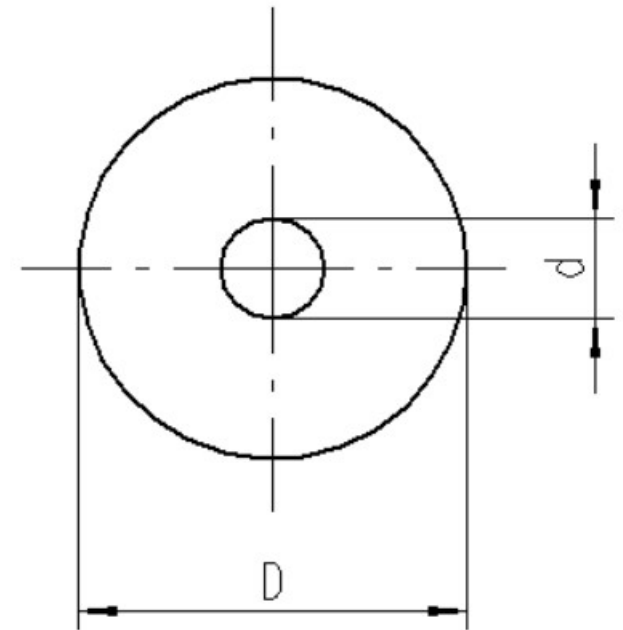
Coaxial Cable

$$Z_L = \frac{Z_0}{2 \cdot \pi \cdot \sqrt{\epsilon_r}} \cdot \ln \frac{D}{d} \quad (1)$$

$$Z_0 = \sqrt{\frac{\mu_0}{\epsilon_0}} \quad (2)$$

$$\epsilon_0 = \frac{1}{\mu_0 \cdot c^2} \quad (3)$$

$$Z_L = \frac{\mu_0 \cdot c}{2 \cdot \pi} \cdot \frac{1}{\sqrt{\epsilon_r}} \cdot \ln \frac{D}{d} \quad (4)$$



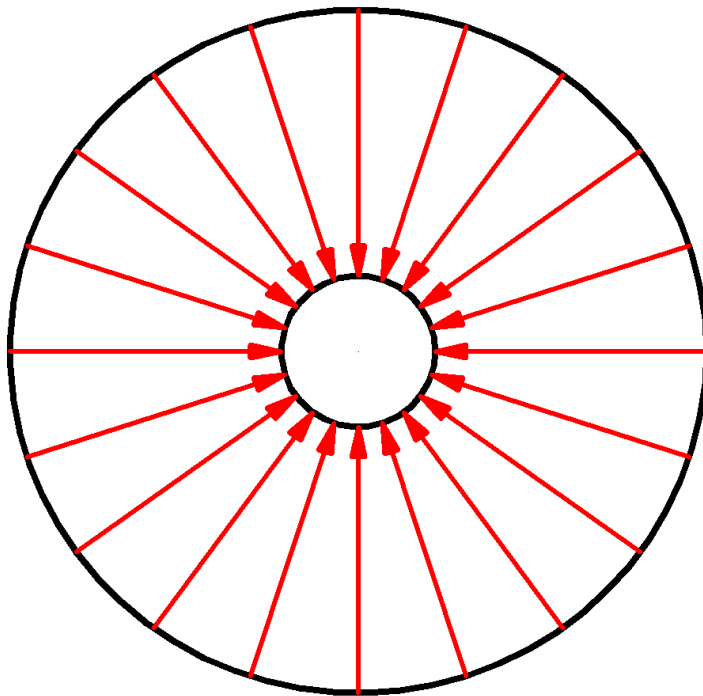
Approximate Equation

$$Z_L \approx \frac{60\Omega}{\sqrt{\epsilon_r}} \cdot \ln \frac{D}{d} \quad (5)$$

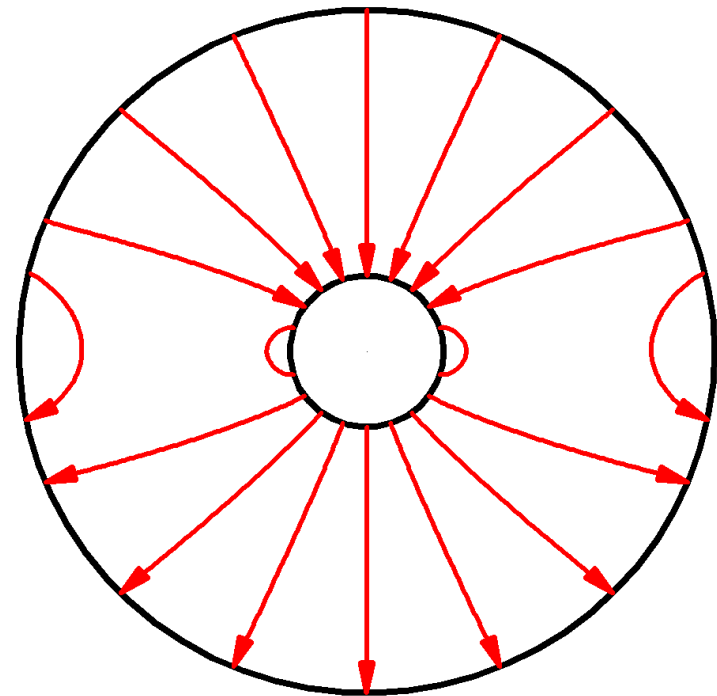
- Z_L : Impedance
- μ_0 : Vacuum permeability $4 \cdot \pi \cdot 10^{-7} \frac{N}{A^2}$
- c_0 : Speed of light $299\,792\,458 \frac{m}{s}$
- ϵ_r : Permittivity of dielectric
- D : Shield diameter
- d : Inner Conductor diameter

Coax Mode

The coax-cable can be use for DC signal
Does it has a maximum frequency?



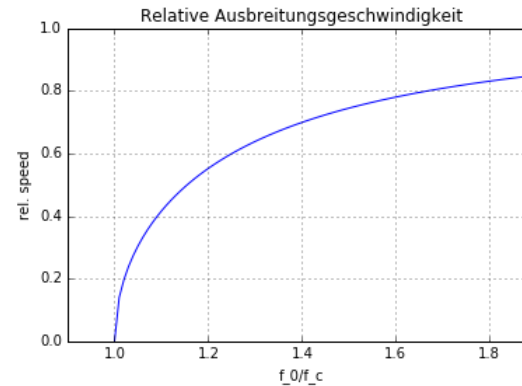
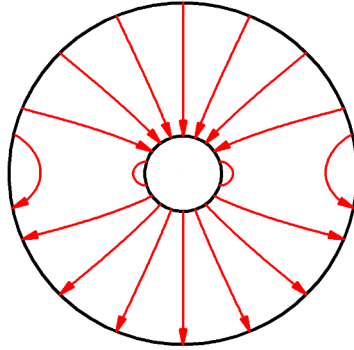
TEM-Mode



TE11-Mode

Coax Mode

The coax-cable can be use for DC signal
Does it has a maximum frequency?



$$\left(J_0(x \cdot A) - J_2(x \cdot A) \right) \cdot \left(Y_0(x) - Y_2(x) \right) - \left(Y_0(x \cdot A) - Y_2(x \cdot A) \right) \cdot \left(J_0(x) - J_2(x) \right) = 0 \quad (6)$$

$$A = \frac{R}{r} \quad (7)$$

$$f_c = \frac{x \cdot c_0 \cdot (A + 1)}{(R + r) \cdot 2 \cdot \pi \cdot \sqrt{\epsilon_r}} \quad (8)$$

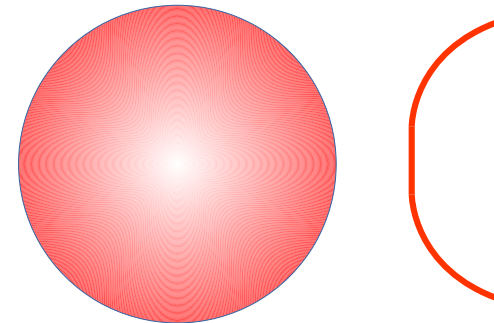
J_n : Bessel function first kind
 Y_n : Bessel function second kind
 R : Shield radius
 r : Inner conductor radius

Skin Depth

With increasing the frequency the current is distributed in the wire such that the current density is largest near the surface.

To keep the equation simple we consider $\mu_r = 1$.

Skin Depth $\zeta = \frac{1}{\sqrt{\pi \cdot f \cdot \mu_0 \cdot \mu_r \cdot \sigma}}$

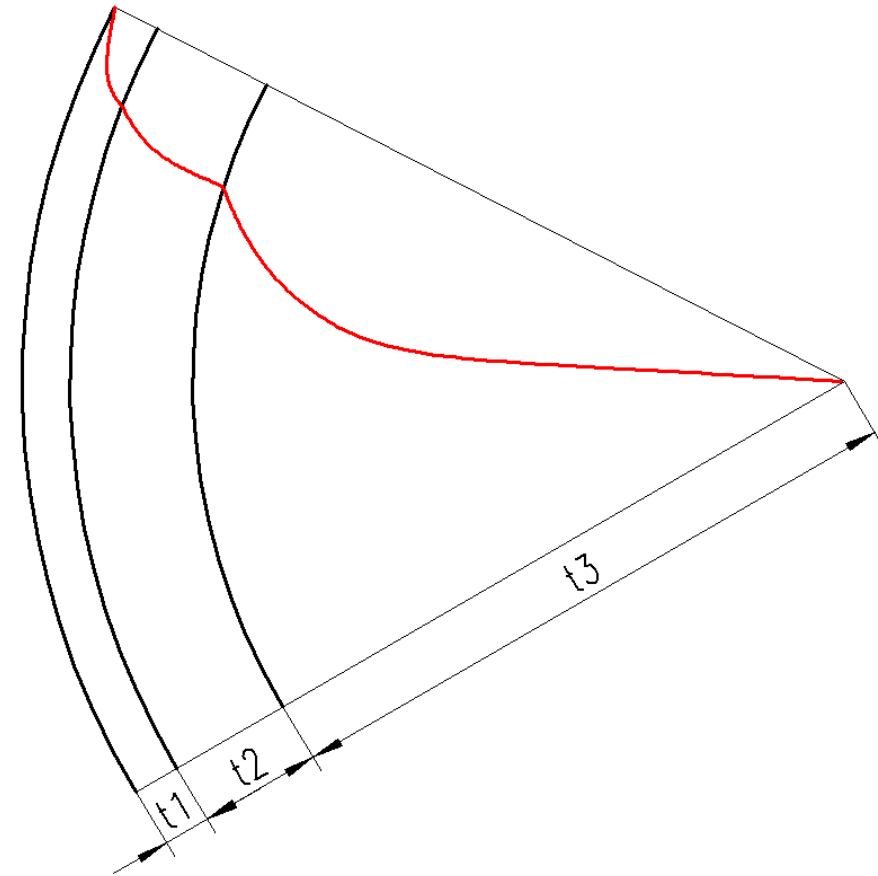
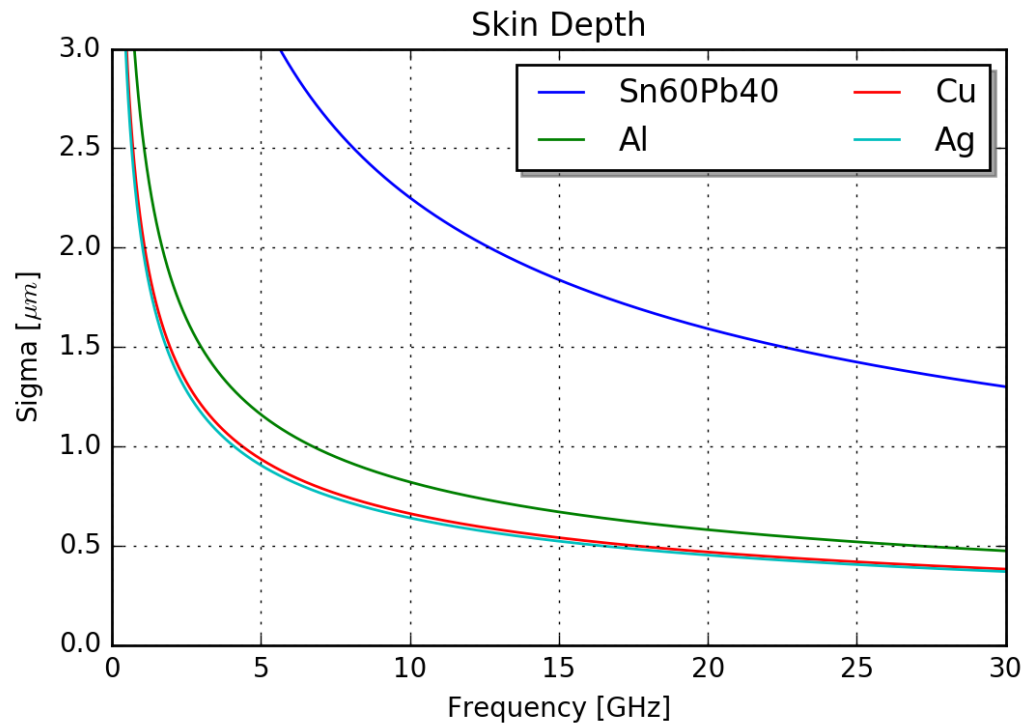


Example

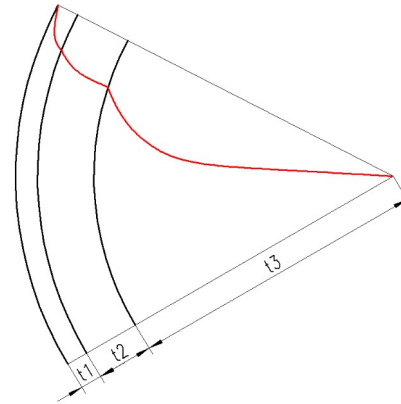
A 1mm diameter Copper wire at $F = 1$ MHz
Skin Depth = 65 μm

\Rightarrow At a distance of 0.325 mm from the surface isn't any current!

Skin Effect



Skin Effect



$$\zeta(i) = \frac{1}{\sqrt{\pi \cdot f \cdot \mu_0 \cdot \sigma(i)}}$$

$$B(1) = 0 \quad B(i+1) = \frac{t(i)}{\zeta(i)}$$

$$G_{tot} = 2 \cdot \pi \cdot \sum_{i=1}^n \zeta(i) \cdot \sigma(i) \cdot \left(e^{-B(i)} - e^{-B(i+1)} \right)$$

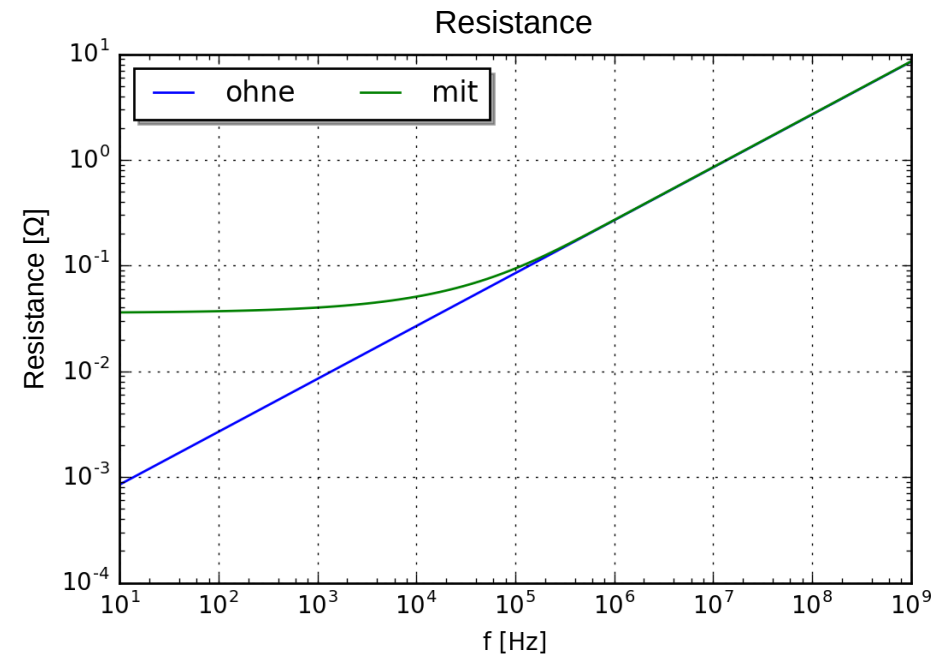
$$a_R = \frac{20}{\ln(10)} \cdot \frac{1}{G_{tot} \cdot 2 \cdot Z_L} \left[\frac{dB}{m} \right]$$

(19)

(20)

(21)

(22)



Resistive Loss

$$R_S = \sqrt{\frac{\pi \cdot f \cdot \mu_0 \cdot \mu_r}{\sigma}} \quad (11)$$

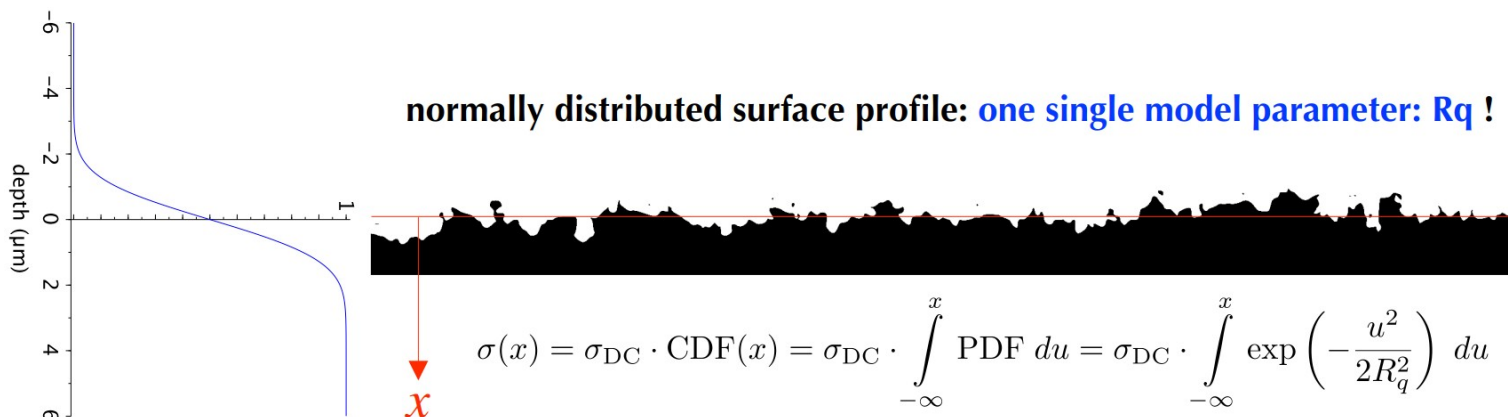
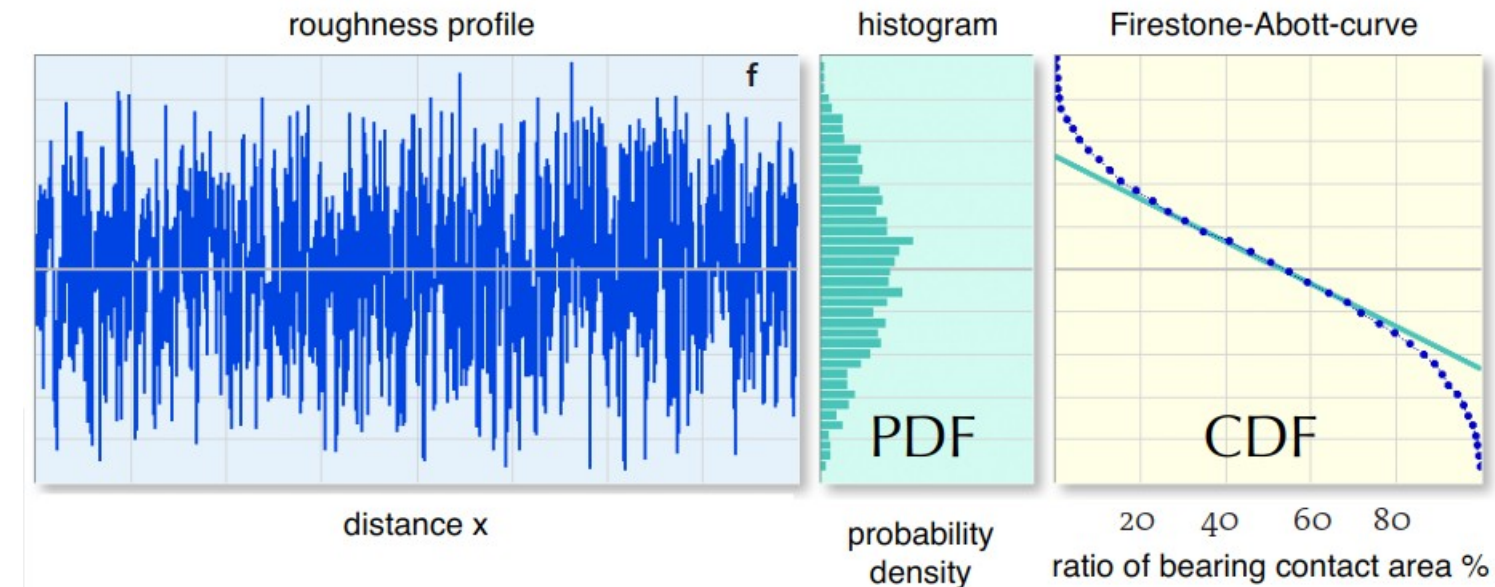
$$R_i = \frac{R_{Si}}{\pi \cdot d} \quad (12)$$

$$R_o = \frac{R_{So}}{\pi \cdot D} \quad (13)$$

$$\alpha = \frac{R}{2 \cdot Z_L} \left[\frac{Np}{m} \right] \quad (14)$$

$$\alpha = \frac{20}{\ln(10)} \cdot \frac{\sqrt{\pi \cdot f \cdot \epsilon_0 \cdot \epsilon_r}}{\ln\left(\frac{D}{d}\right)} \cdot \left(\frac{1}{d \cdot \sqrt{\sigma_i}} + \frac{1}{D \cdot \sqrt{\sigma_o}} \right) \quad (15)$$

Rough Surface



Dr.-Ing. G. Gold, Institute of Microwave and Photonics, FAU Erlangen-Nürnberg, EUC 2016

Rough Surface

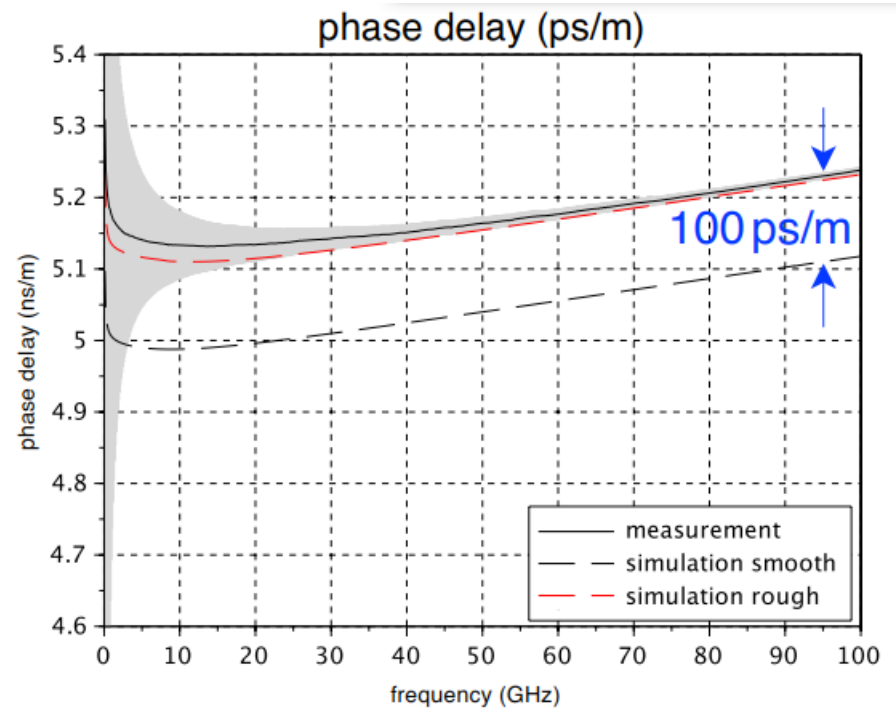
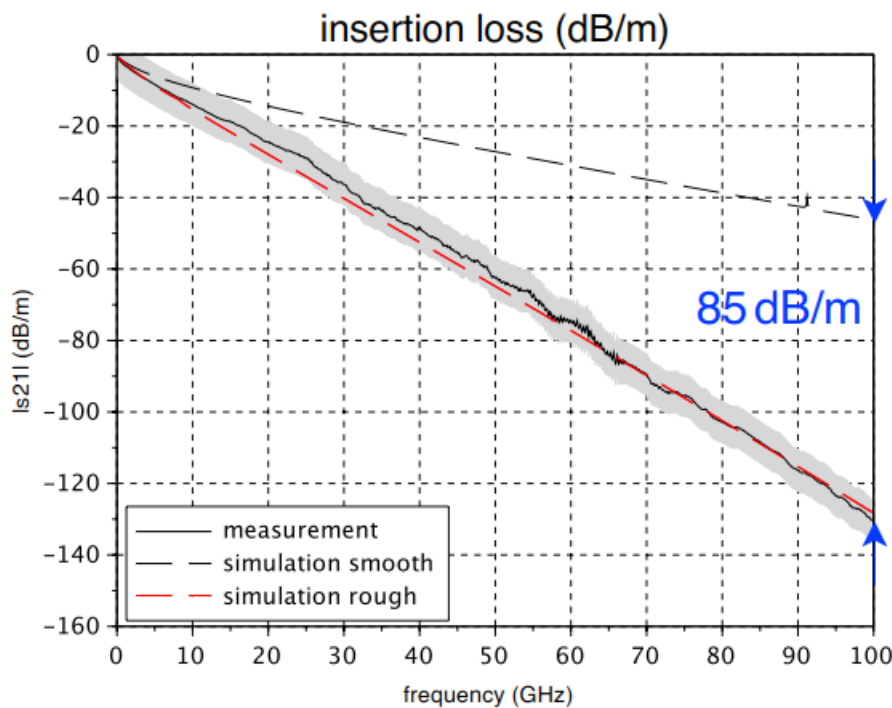
Surface Impedance

$$Z_{\square} = R_{\square} + j\omega L_{\square} = -\mu_0 \frac{E_z}{B_y}$$



$$Z_{\square, \text{rough}} = -j\omega \frac{\int_{\sigma > 0} B_y dx}{\int_{\sigma > 0} J_z dx}$$

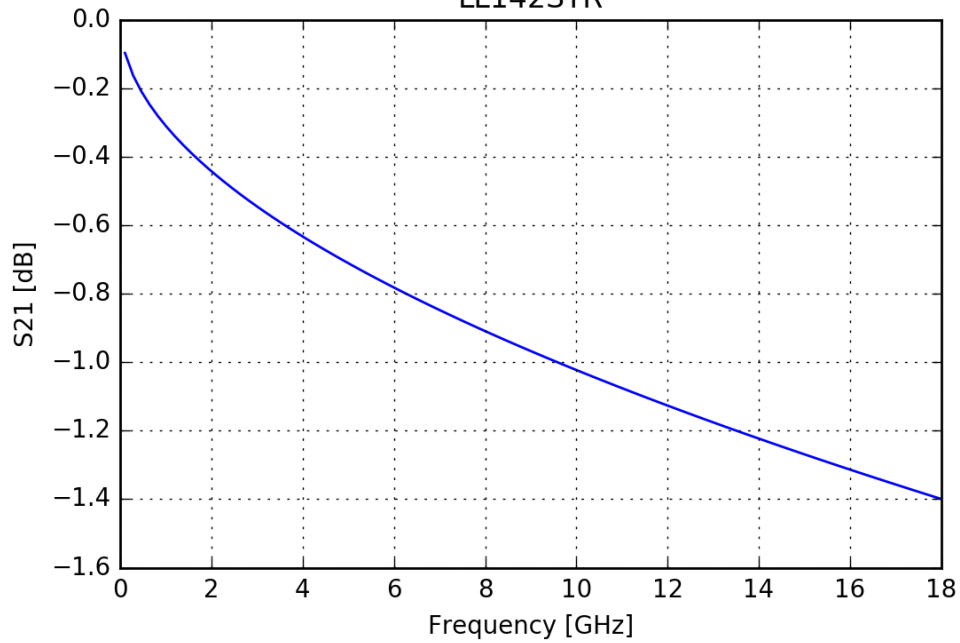
Example of a Microstrip Line



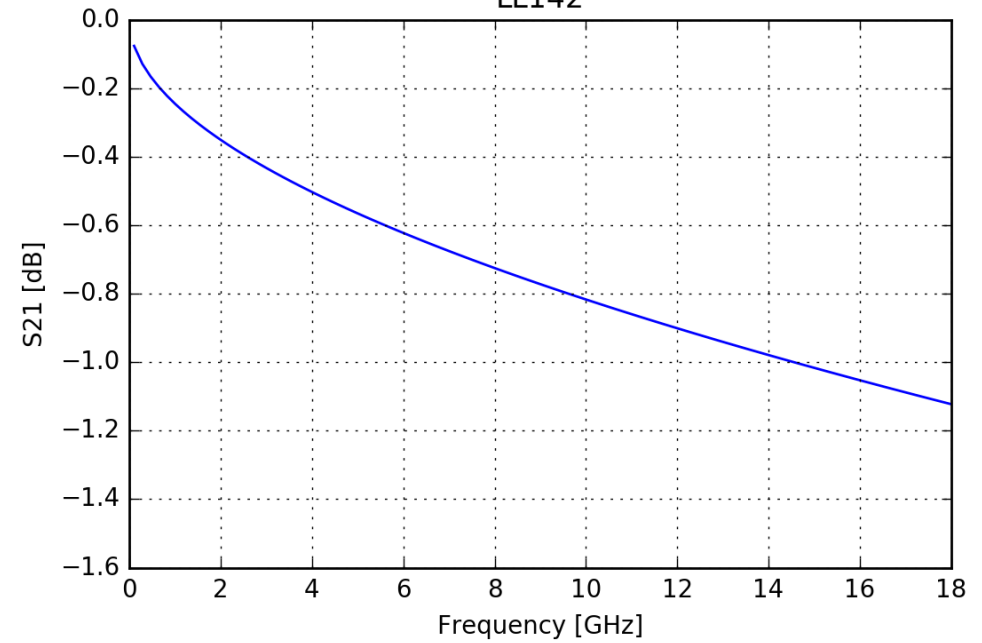
Rough Surface



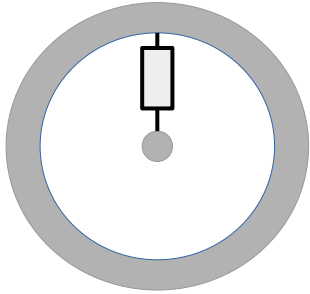
LL142STR



LL142

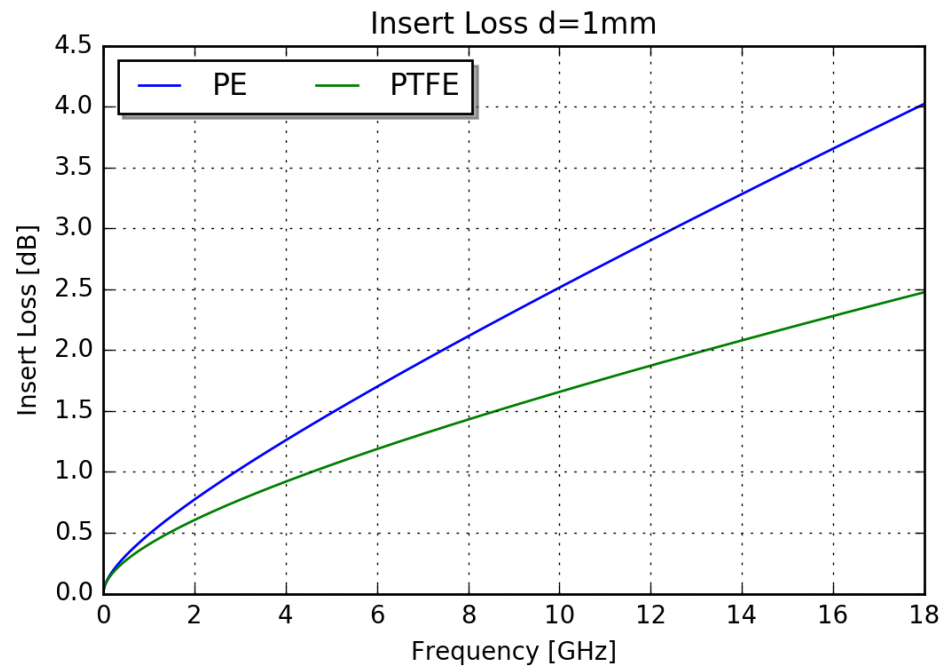


Dielectric Loss

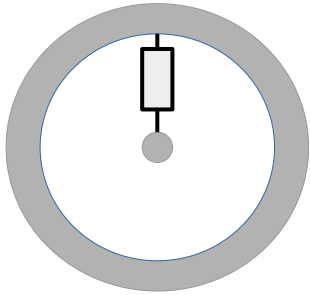


$$\alpha_D = \frac{20}{\ln(10)} \cdot \frac{\pi \cdot f \cdot \tan(\delta) \cdot \sqrt{\epsilon_r \cdot \mu_r}}{c_0} \quad (16)$$

Typical insulators are Polyethylene (PE) and Polytetrafluoroethylene (PTFE)

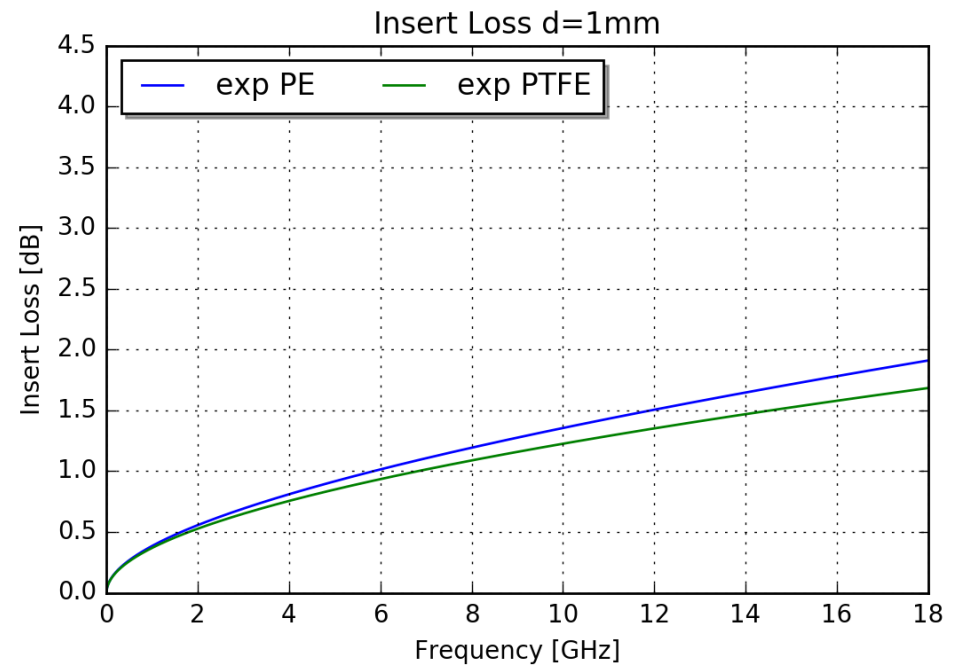
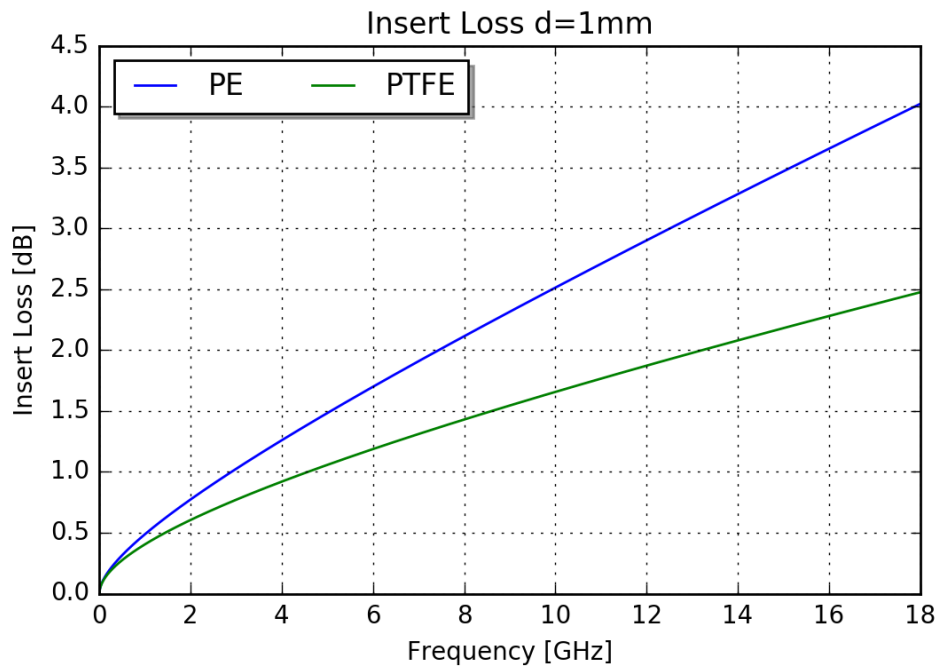


Dielectric Loss



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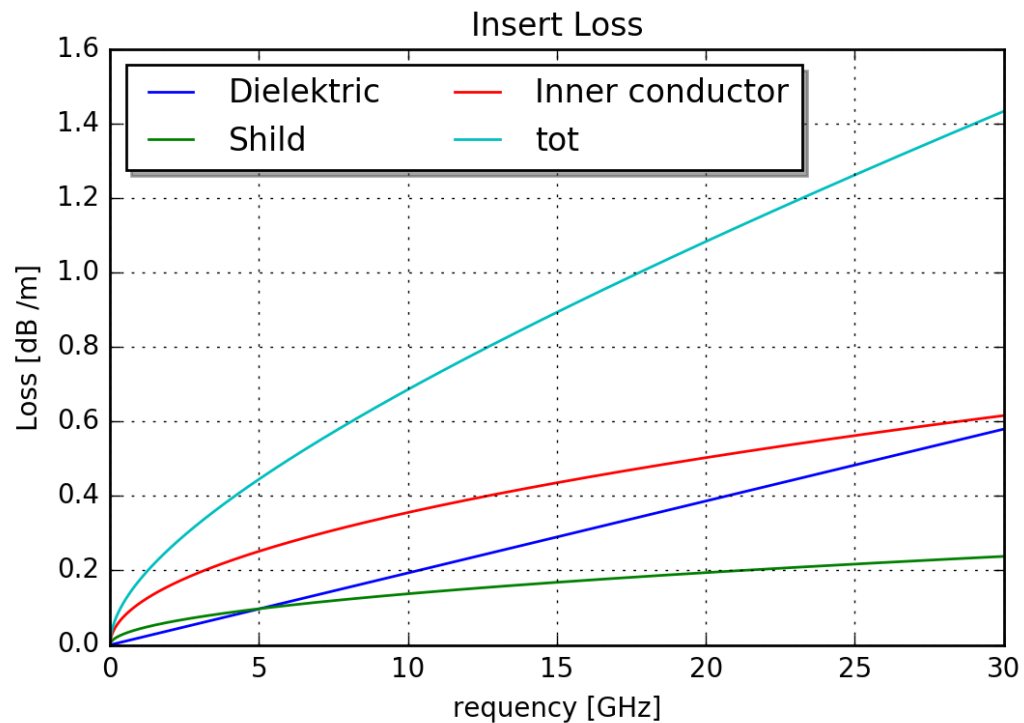


Coax-Cable Loss

$$\alpha = \frac{20}{\ln(10)} \cdot \frac{\sqrt{\pi \cdot f \cdot \epsilon_0 \cdot \epsilon_r}}{\ln\left(\frac{D}{d}\right)} \cdot \left(\frac{1}{d \cdot \sqrt{\sigma_i}} + \frac{1}{D \cdot \sqrt{\sigma_o}} \right)$$

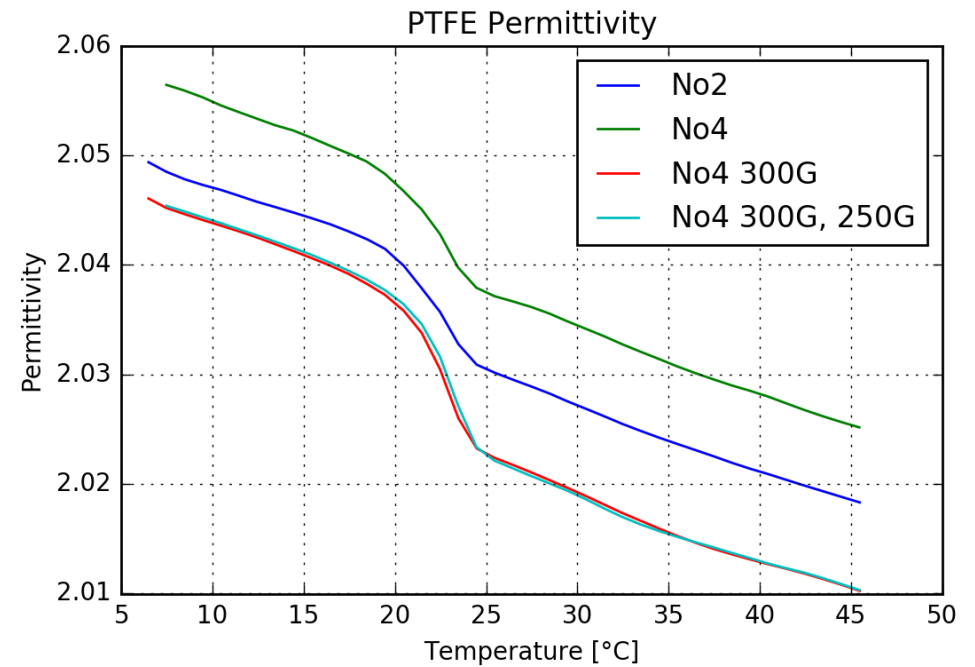
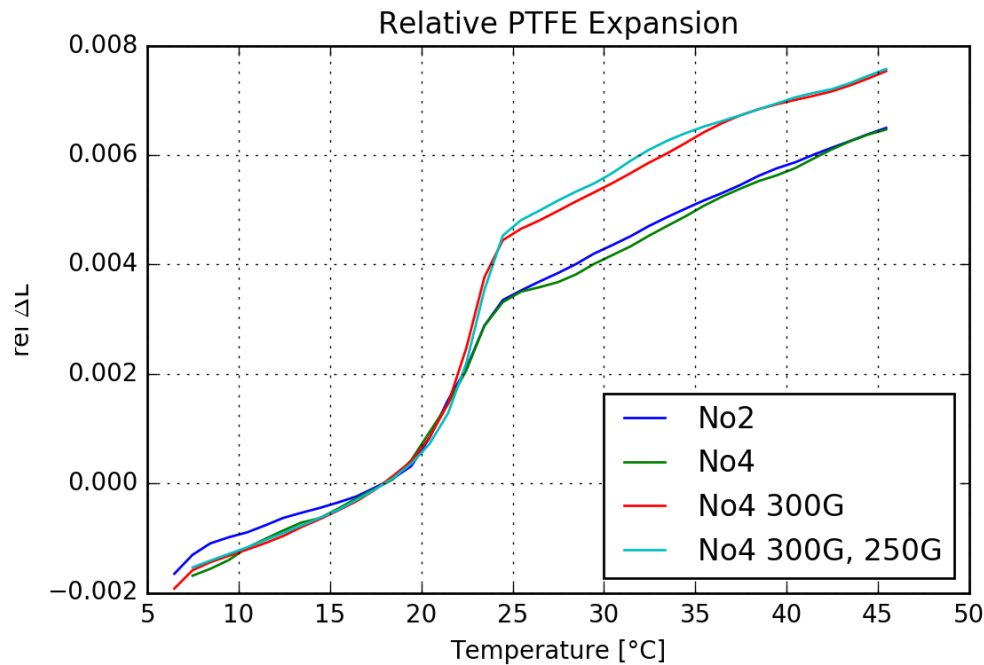
$$\alpha_D = \frac{20}{\ln(10)} \cdot \frac{\pi \cdot f \cdot \tan(\delta) \cdot \sqrt{\epsilon_r \cdot \mu_r}}{c_0}$$

$$IL = l \cdot (K1 \cdot \sqrt{f} + K2 \cdot f)$$



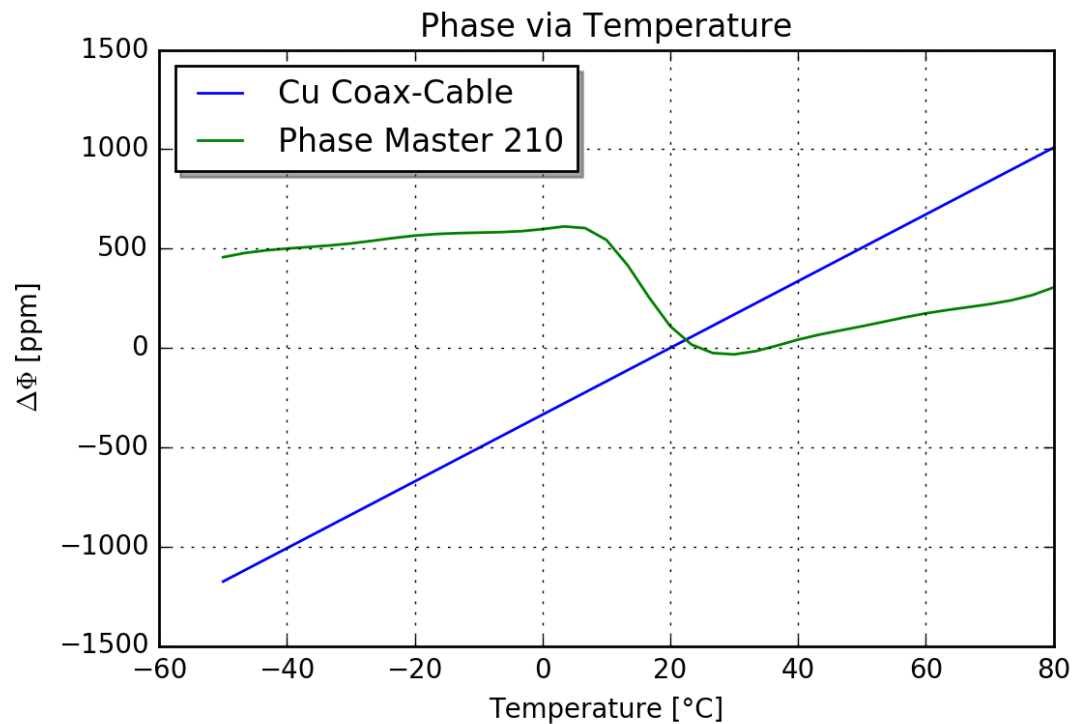
Velocity

$$v = \frac{c_0}{\sqrt{\epsilon_r(T, f)}}$$



Phase Stability via Temperature

Trough the material expansion when the temperature increase the coax-cable will be longer. This result in a phase change compare to room temperature.



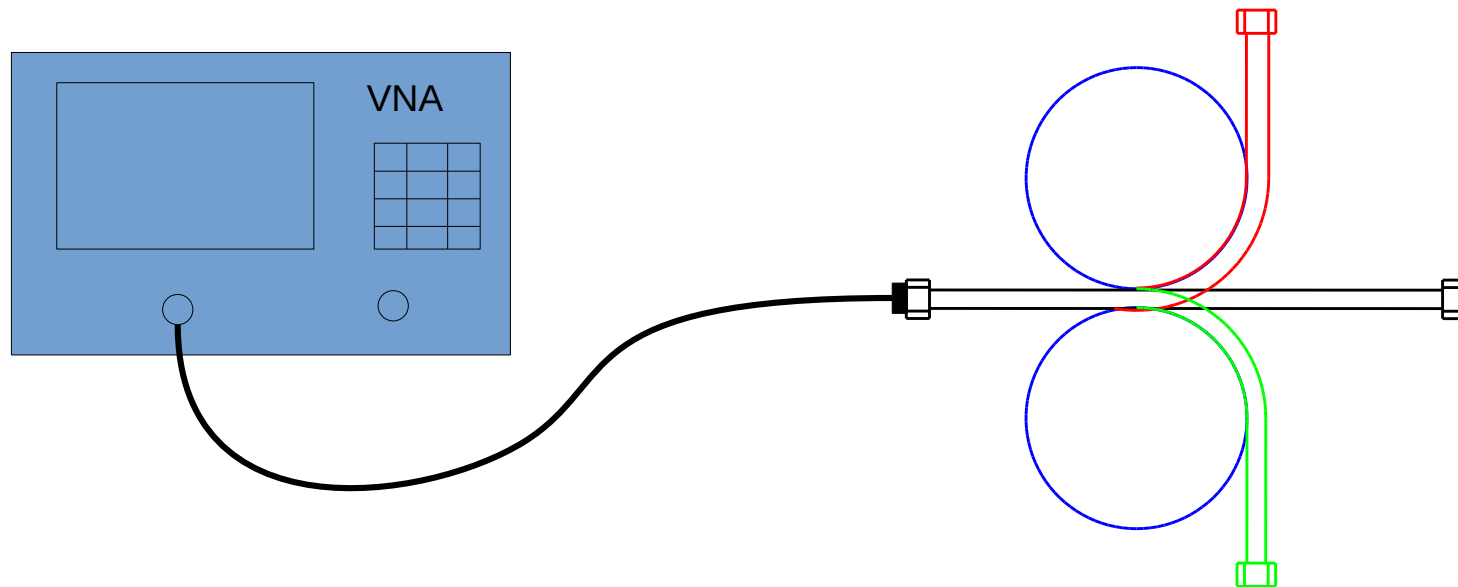
$$\Phi = \frac{l}{\lambda} \cdot \sqrt{\epsilon_r} \cdot 360^\circ \quad (17)$$

$$\Delta\Phi = \frac{\Delta\varphi}{\Phi} \cdot 10^6 [ppm] \quad (18)$$

Phase Stability via Bending

If you bend a coax-cable the pressure on the dielectric increase and the diameter will deform This results in a phase change.

There is no standard test.
Different companies perform different test.

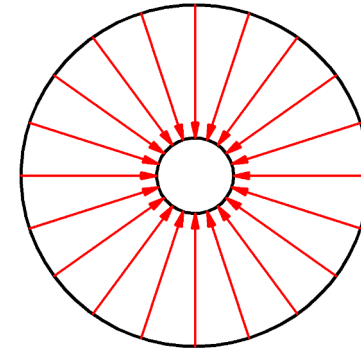


Peak Power

The restriction for peak power is the arcing which will damage the cable.

$$E_d = \frac{V_{peak}}{r \cdot \ln\left(\frac{R}{r}\right)}$$

E_d : Electric field
 V_{peak} : Peak voltage
 R : Dielectric radii
 r : Inner wire radii



$$V_{peak} = E_d \cdot r \cdot \ln\left(\frac{R}{r}\right)$$

$$P_{peak} = \frac{E_d^2 \cdot r^2 \cdot \ln\left(\frac{R}{r}\right) \cdot \sqrt{\epsilon_r}}{120 \Omega}$$

Dielectric strength PTFE \approx 100MV/m
 Air \approx 1MV/m



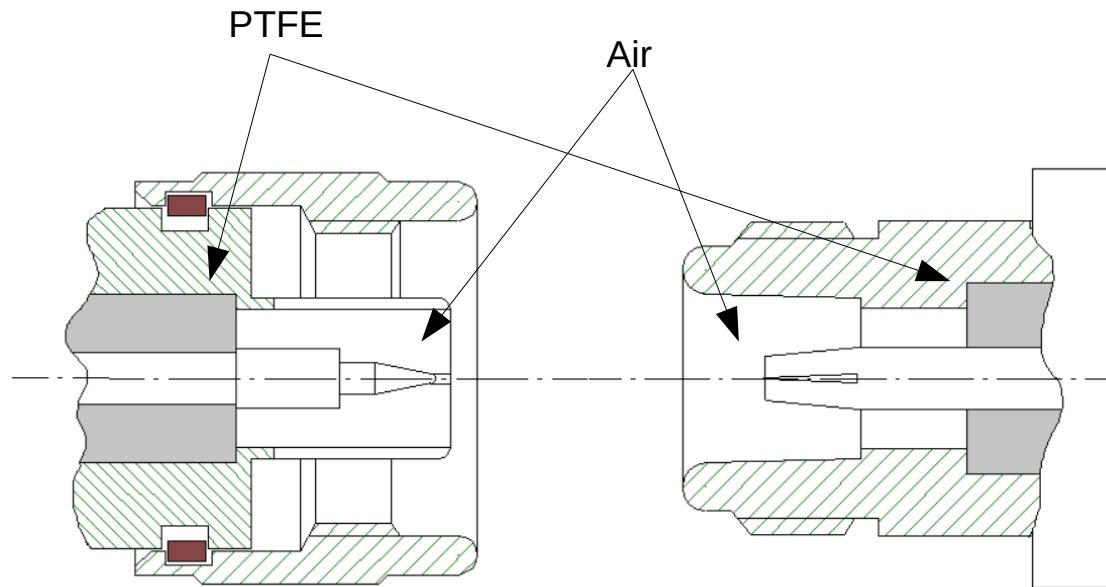
50Ω coax-cable with $r = 3\text{mm}$

Air $P_{peak} = 64.2 \text{ kW}$
 PTFE $P_{peak} = 1.35 \text{ GW}$

13.5 MW
 With margin

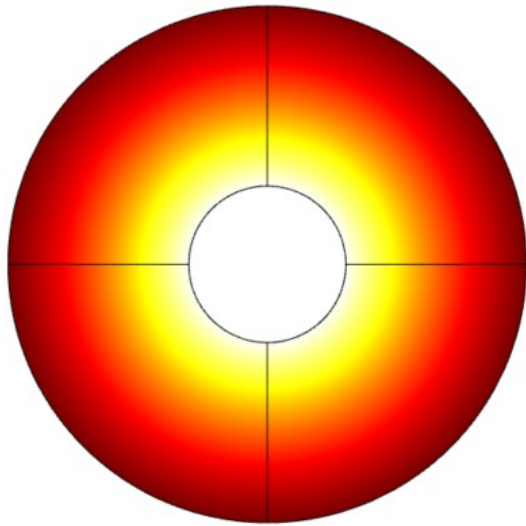
Peak Power

Weakest part is in the connectors

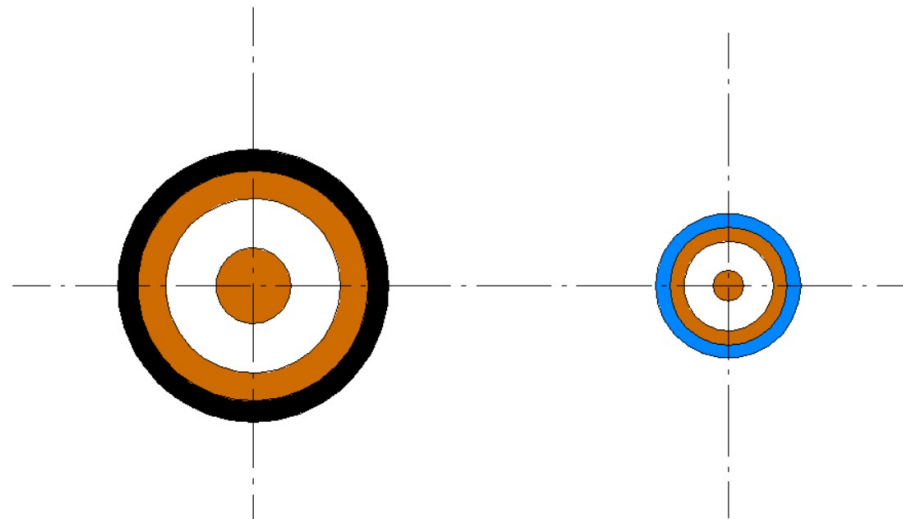


N-connector

Average Power



- Highest loss at surface of inner contact
- Continues serving temperature of insulator
 - PTFE 250°C
 - PE 80°C
 - TF4™ 150°C



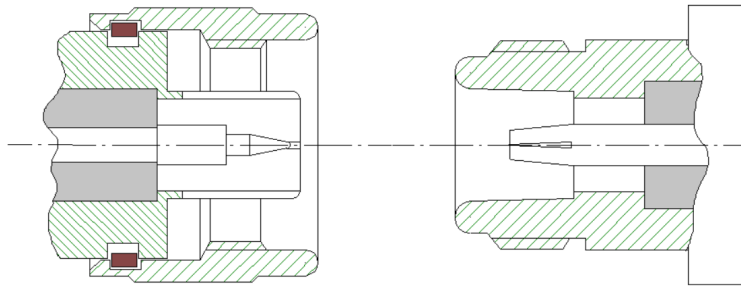
3/8" Flexwell ePE

640 W @ 1 GHz

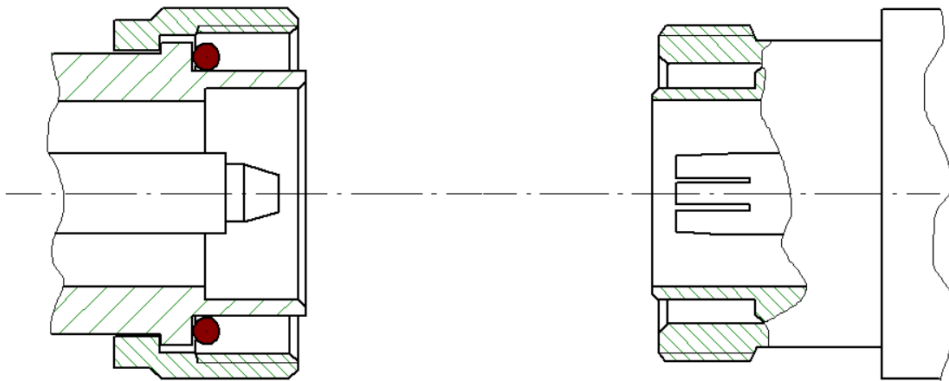
LL142 ePTFE

720 W @ 1 GHz

Average Power



N-connector 1100W @ 1GHz
 $f_{\max} = 11 \text{ GHz}$



7/16-connector 2300W @ 1GHz
 $f_{\max} = 8.3 \text{ GHz}$

At sea level !

Power via Pressure

Paschen's law

$$V_B = \frac{B}{\ln(A \cdot p \cdot d) - \ln(\ln(1 + \gamma^{-1}))} \cdot p \cdot d$$

Air

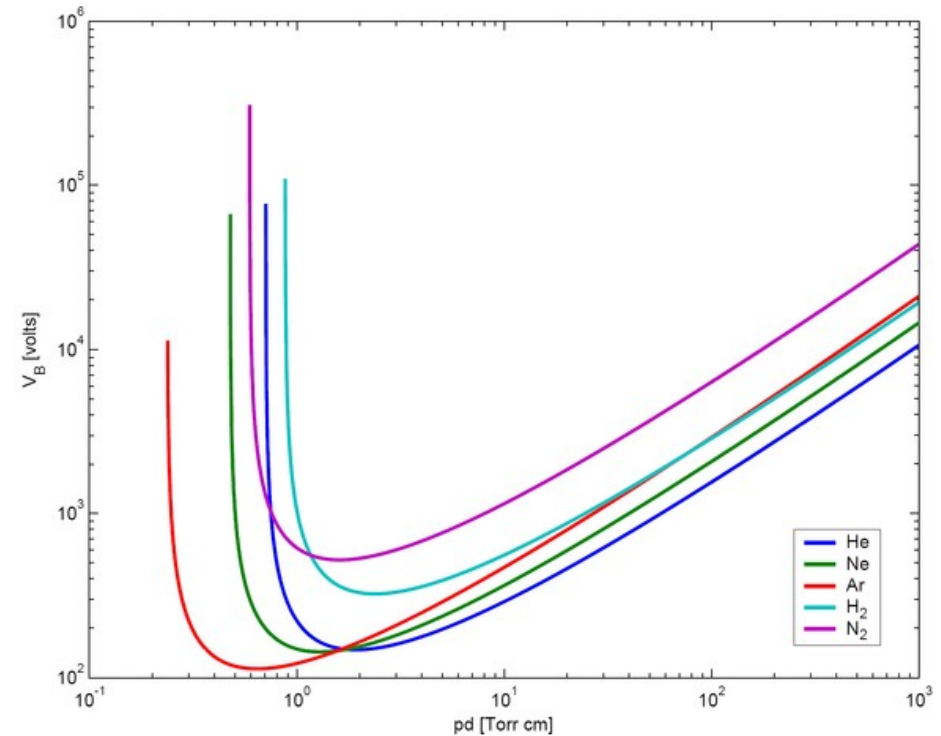
$$A = 10.95 \text{ (Pa} \cdot \text{m)}^{-1} \quad B = 273.8 \text{ V} \cdot \text{(Pa} \cdot \text{m)}^{-1}$$

$$V_B \approx 47 \text{ V} \Rightarrow P_B \approx 44 \text{ W}$$

Helium

$$A = 2.25 \text{ (Pa} \cdot \text{m)}^{-1} \quad B = 25.5 \text{ V} \cdot \text{(Pa} \cdot \text{m)}^{-1}$$

$$V_B \approx 21 \text{ V} \Rightarrow P_B \approx 8.8 \text{ W}$$



Von Paschen.jpg: Wikigianderivative work: Harlock81 (talk) - Paschen.jpg, CC BY-SA 3.0, <https://commons.wikimedia.org/w/index.php?curid=7231129>

Shielding



A single braid shield has an overlapping of 80% to 97%

→ Shielding effectiveness up to 40 dB @ 1GHz



Two braid shield

→ Shielding effectiveness up to 80 dB @ 6 GHz

Shielding



Best shielding for flexible cable is with a foil and braid

→ Shielding effectiveness up to 110 dB @ 26.5GHz



Best shield is a pipe!

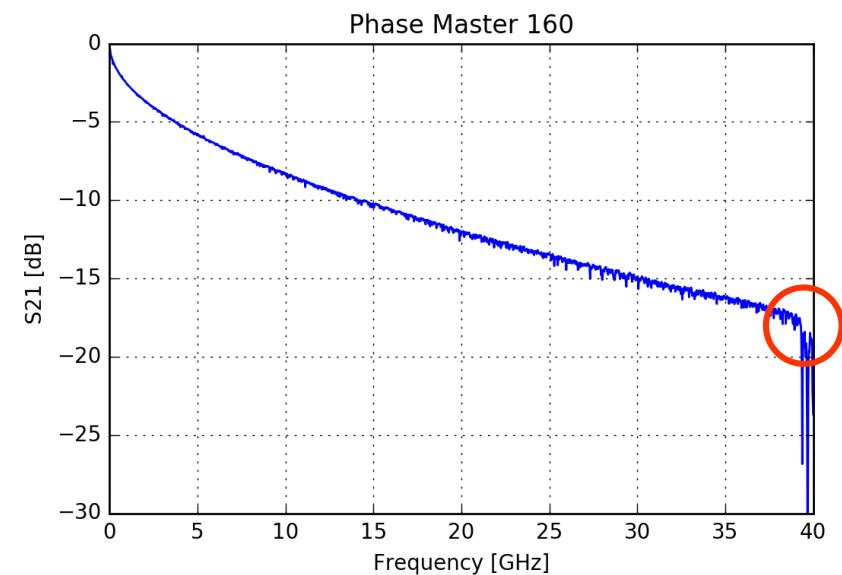
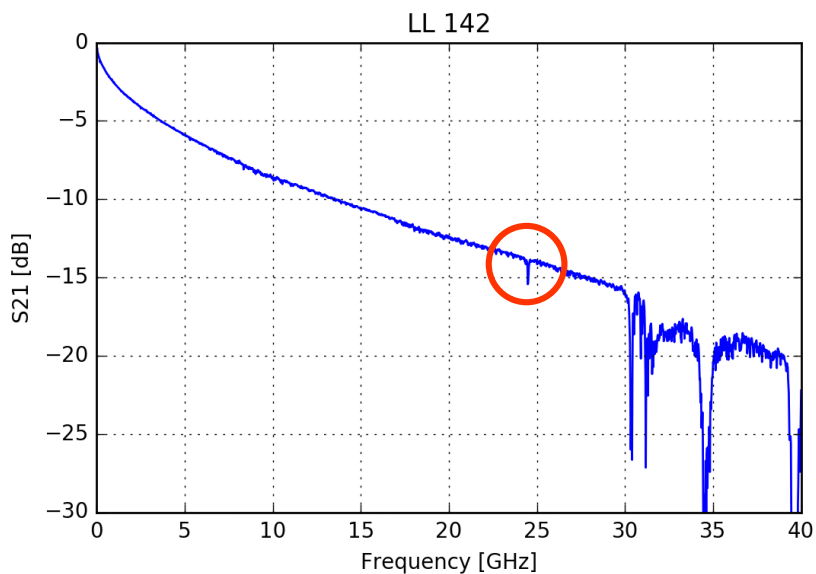
Measurement of more than 120 dB is difficult and if you get an result it could be from leakage of the connectors.

→ Shielding effectiveness more than 120 dB @ 26.5GHz

Periodic Structures

At higher frequency periodic structures of the shielding and stranded inner wire can be the reason for unexpected behaviour.

	LL 142	PM 160
Centre conductor diameter	1.30 mm	1.11 mm
Dielectric diameter	3.68 mm	2.89 mm
Permittivity	1.54	1.32
TE11 cut-off frequency	31.69 GHz	42.54 GHz



Kink Protection

The most sensitive part on the cable is where the coax-cabel is assembled with the connector.

The strain should be minimised with a prober kink protection.

1 Good kink protection

2 Simple kink protection

3 No kink protection



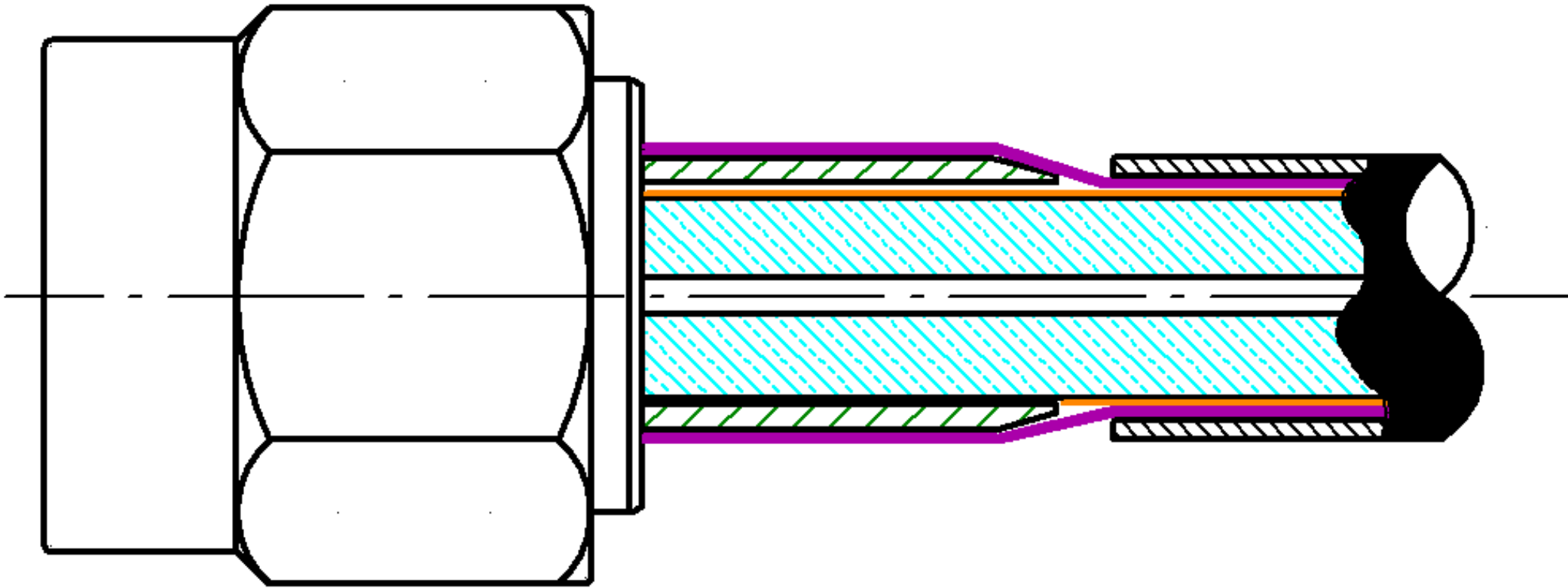
Bend Radius

Coax-cable don't like to be bend with a small radius except of exceptions.
In no case torsion!

SPECIFICATIONS	160
Cable Designator	84
Diameter (in/mm)	0.160/4.06
Operating Frequency (Max, GHz)	40
Attenuation–Max @ 2 GHz (dB/ft)	0.150
Attenuation–Max @ 10 GHz (dB/ft)	0.347
Attenuation–Max @ 18 GHz (dB/ft)	0.474
Attenuation–Max @ 26.5 GHz (dB/ft)	0.585
Attenuation–Max @ 32 GHz (dB/ft)	0.648
Attenuation–Max @ 40 GHz (dB/ft)	0.732
Power Handling – Avg Power in Watts @ 1 GHz	527
Phase Stability vs. Flexure† (@ 18 GHz, nom)	±3.5°
Shielding Effectiveness–Min‡ (dB @ 1 GHz)	> -90
Typical VSWR (2 straight connectors)	1.28 to 40 GHz
Min Bend Radius (in/mm)	Static
	Dynamic
Connector Retention to 18 GHz, pull (lbs/kg)	20/9.07
Velocity of Propagation (%)	87.0
Weight (grams/ft & /m)	12.12/39.76
Operating Temperature Range (°C)	-55 to +125

141
920
0.160/4.06
26.5
0.60
0.76
–
–90 or better
Available (except Express)
0.320/8.13
40/18.14
15/6.80
13.4/43.95
–54 to +125

Crimp Connector



Humidity

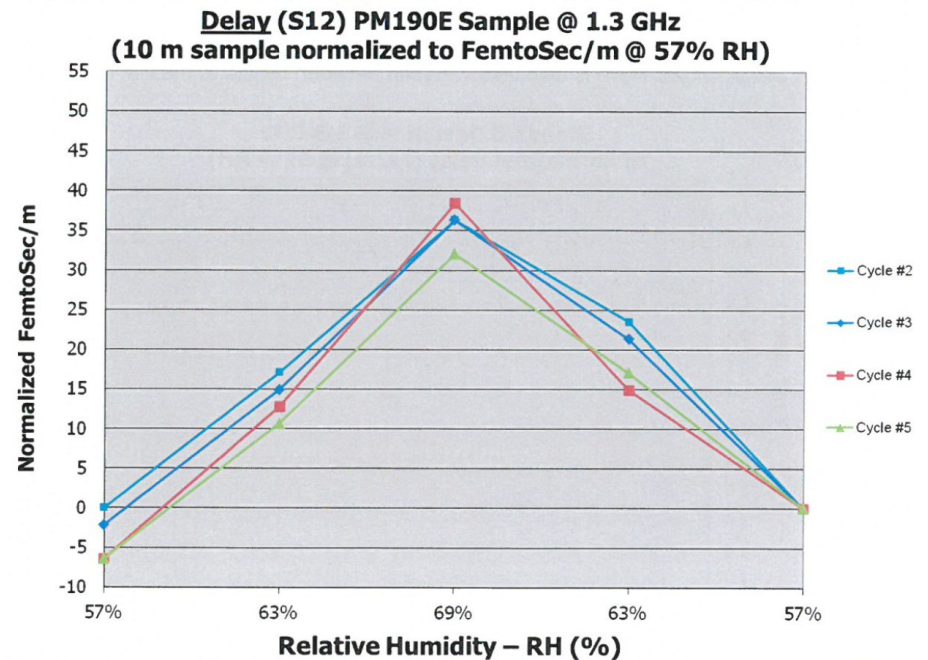
$$a = \frac{\left(\frac{c}{v}\right)^2 - \epsilon_{r_PTFE}}{\epsilon_{r_Air} - \epsilon_{r_PTFE}} \quad (19)$$

$$\epsilon_r = a \cdot \epsilon_{r_Air} + b \cdot \epsilon_{r_PTFE} \quad (20)$$

$$\Delta t = \frac{l}{c} \cdot (\sqrt{\epsilon_{r_1}} - \sqrt{\epsilon_{r_2}}) \quad (21)$$

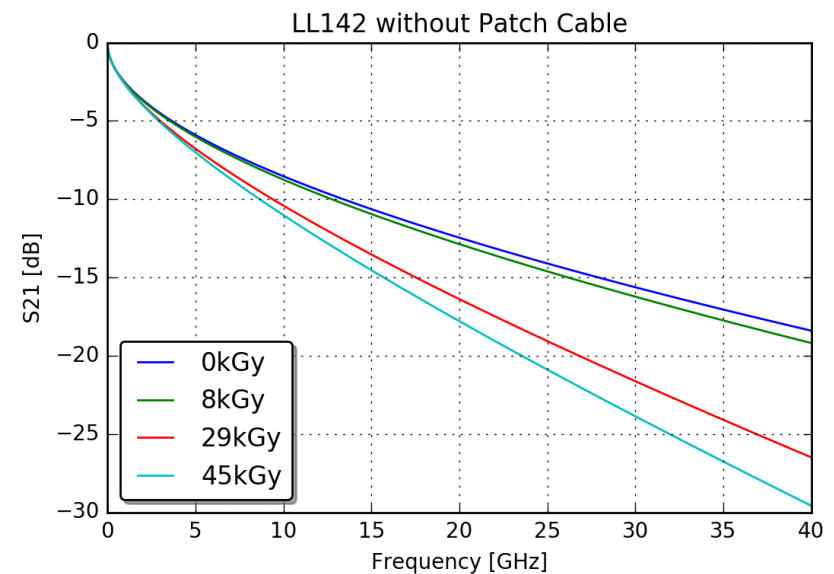
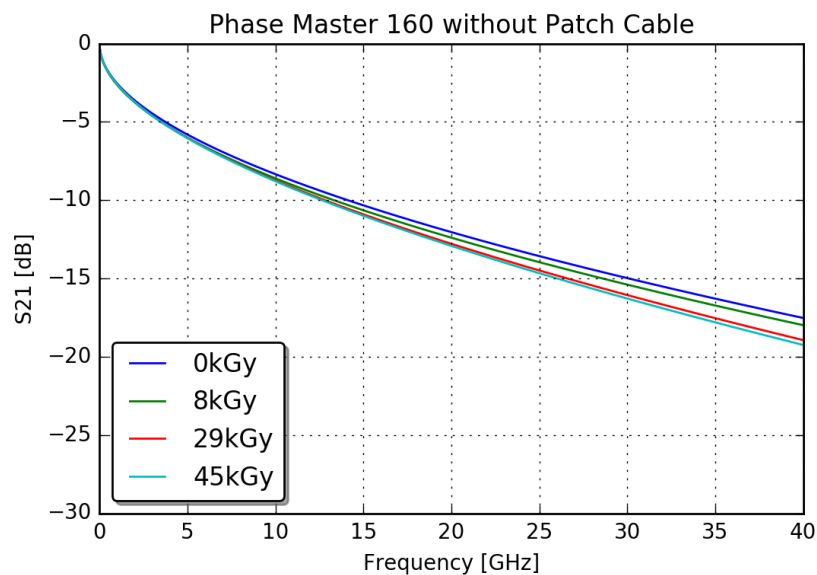
- a : Air amount
- $\frac{v}{c_0}$: Velocity of propagation 86%
- ϵ_{r_PTFE} : Permittivity of PTFE
- ϵ_{r_Air} : Permittivity of air

Humidity	$\epsilon_r - 1$	Δt [fs/m]
0%	$5.287 \cdot 10^{-4}$	97.4
36%	$6.019 \cdot 10^{-4}$	27.3
50%	$6.304 \cdot 10^{-4}$	0
70%	$6.710 \cdot 10^{-4}$	-38.9
100%	$7.320 \cdot 10^{-4}$	-97.3

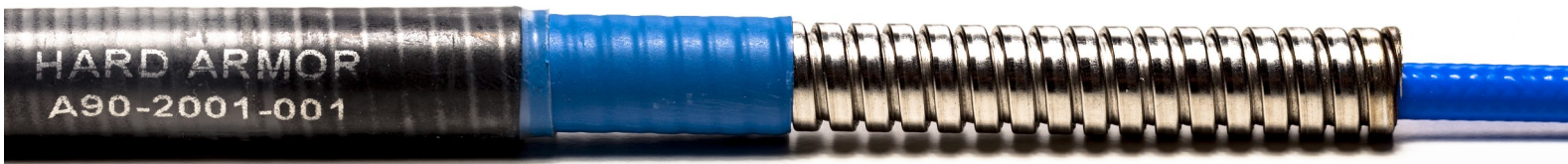
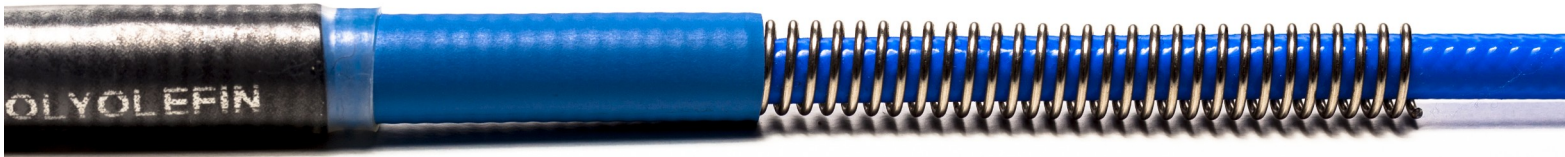


Ionising Radiation

Ionising radiation break the long molecules of the PTFE polymer. If nearby another break new connection will happen, cross-links.
This change the material properties.

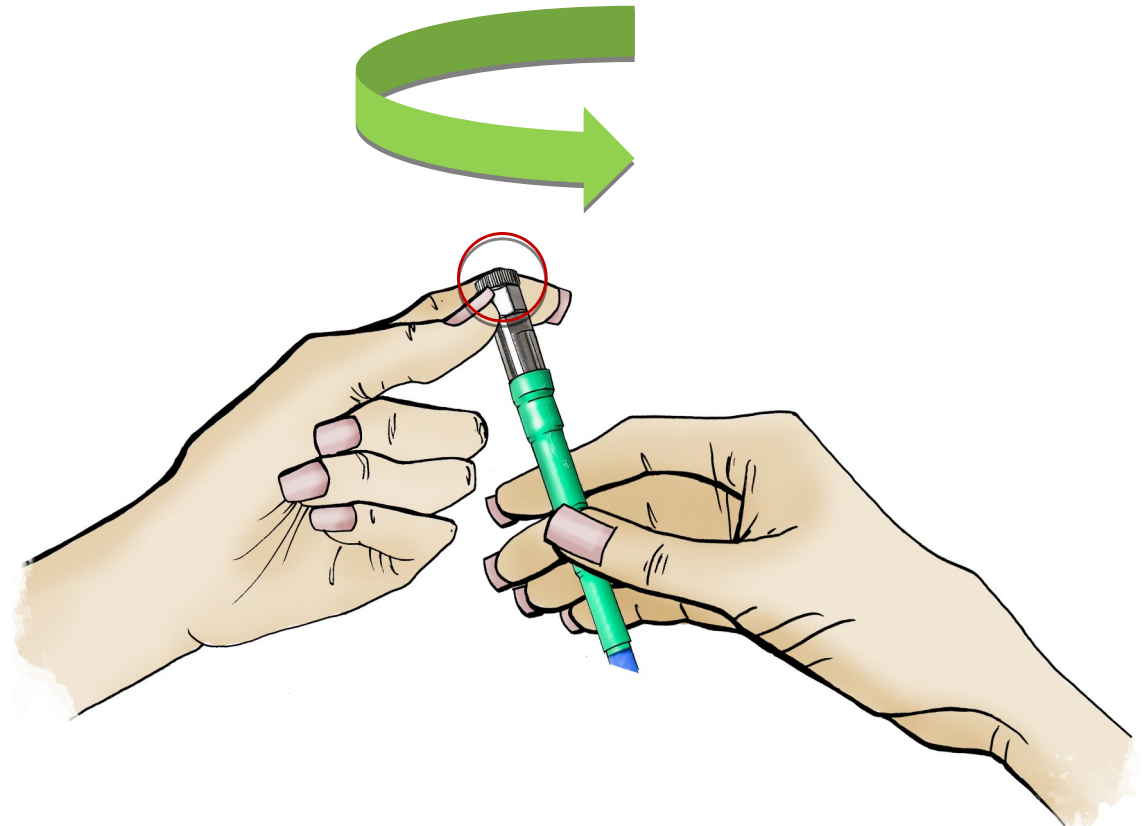
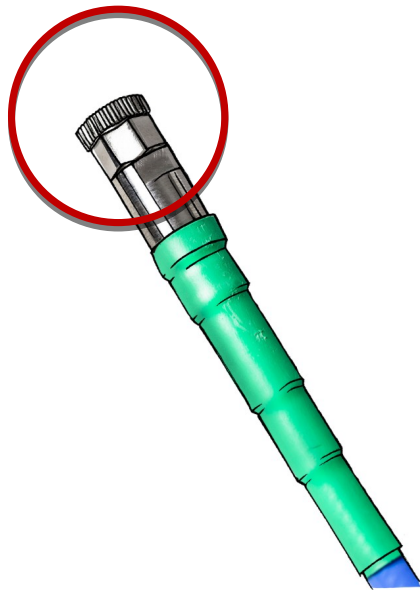


Cable protection



Protection against light compression to running over with a car.

Secure connection

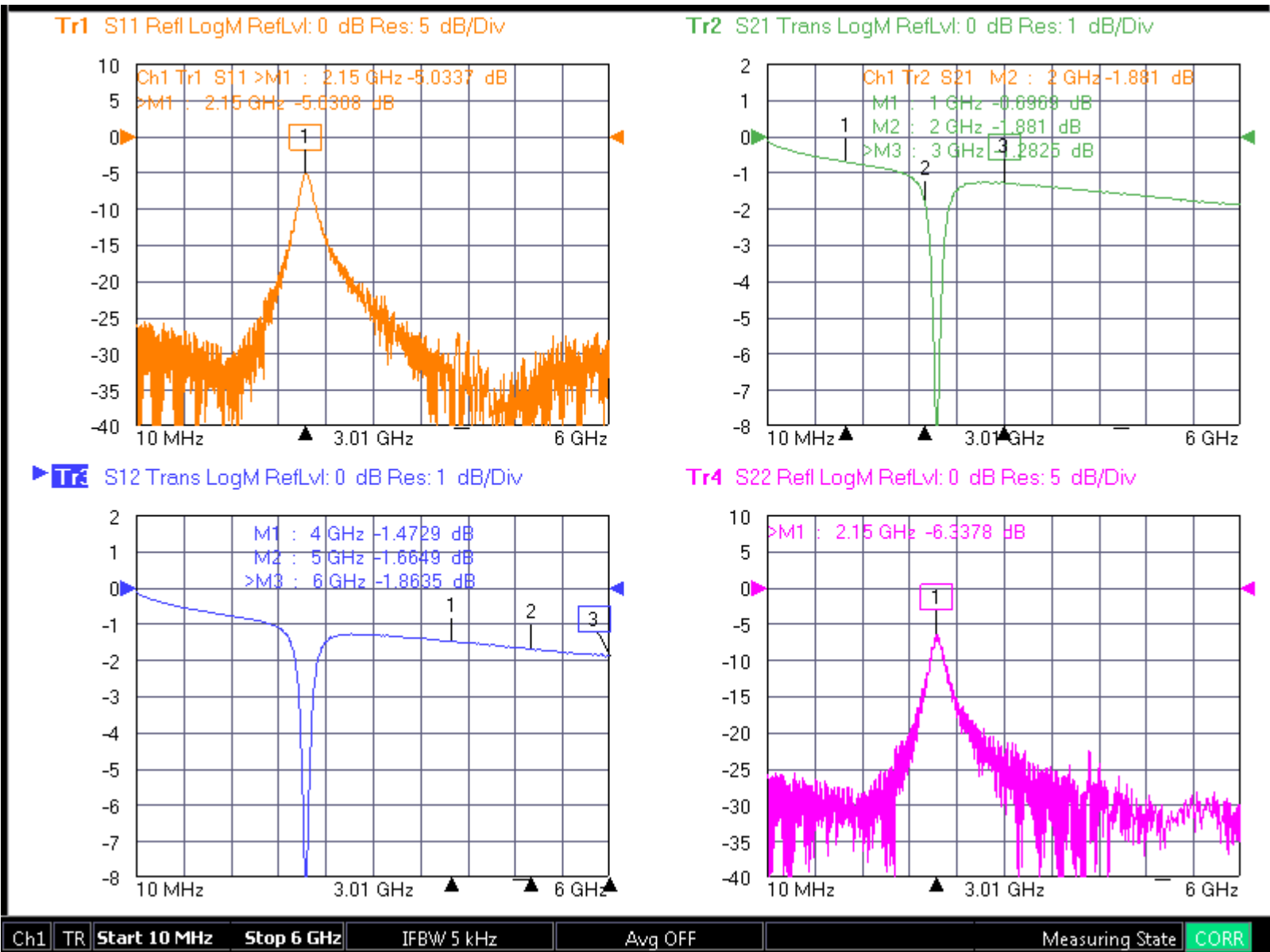


Secure connection



Use the right torque spanner to fasten it.

Secure connection



Thank you for your attention!

Stefan Burger

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