

# **The DUNE Vertical Drift HV System: Overview & Requirements**



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# **HVS Scope for the FD-VD**

- Vertical Drift HV concept largely derived from previous DP design. HV system designed to maximize active volume:
	- Readout units close to LAr surface and cryostat floor: 2 times 6.5 m drift distance
	- Cathode at middle height: LAr hydrostatic pressure allows improved HV stability minimizing the distance of Field cage from the cryostat walls (~60 cm)
	- Single modular field cage surrounding active volume hanging independently from the roof
- Present reference layout (with lessons learned from NP04/NP02 incorporated):
	- Cathode planes:
		- 80 modules (3x3.4m2) with resistive surfaces
		- suspension features to the super CRPs
		- integration of X-Arapucas Photon Detectors (14% coverage) including networking of PoF/SoF
	- **Field cages** 
		- 192 field cage modules (3x3.3m2) including aluminum profiles and RDB'as in HD and DP
		- 70% transparency (close to anodes) matching PD's position on cryostat membrane
	- **HV** delivery
		- HVPS, PS monitoring system, HV cable, ripple filters, HVFT, and HV extender

#### **Cathode Plane (***details in Fabien talk***)**

- Each cathode module is constructed from a 3m x 3.4m x 0.05m FRP I-beam frame with 16 openings. Modules are suspended to the super CRP structure above the top anode plane using insulating ropes (Dyneema).
- Double sided X-arapuca PD modules are installed in 4 of the openings (PDS scope), encased by highly transparent (~80%) metal wire mesh panels on both sides.
- 12 pairs of perforated resistive panels are mounted on the top and bottom faces of the frame, reinforced by light-weight rib structures. These and the wire mesh panels are electrically interconnected to form two highly resistive surfaces with sufficiently slow discharge RC time constant to reduce harmful charge injection to the FEE connected to the anodes. The porosity of the resistive panels is to be determined by CFD.

The electrical characteristics of this cathode is very similar to that of the FD1 cathode planes.

Choices of resistive perforation:

- Resistive Kapton laminated FR4 sheet (FD1 CPA)
- Resistive bulk conducting FR4 sheet
- 3D printed carbon fiber + PEEK grid.

#### *Charge Question #4*

#### **Field Cage (***details in Jae's talk***)**

- Design based on experiences gained from both NP04 and NP02 installation/operations.
- Arrays of FC modules (~3x3.3m2) surrounding the LAr volume between top and bottom anode planes, 13m double drift depth covered by columns of 4 modules. Two columns supported by a common stainless steel I-beam to form a super FC module, suspended from two roof penetrations
- Aluminum profiles mounted on the outer flanges of FRP Ibeams, terminated by UHMWPE caps to prevent the exposure of high E field to the bulk liquid argon. Own resistor divider chain eliminates need for lateral electrical interconnect.
- Along vertical edges, profiles bent at 90° to provide smooth conductive surfaces and reduce field enhancement.
- Minimum distance from ground shield  $\sim$  600 mm (scaled from NP04 experience)
- Key assembly/installation features demonstrated in NP02.
- 70% transparency near the anodes, to match the location of the PD's on the membrane, ensured with thinner profiles: slightly higher local E field but within the maximum E field requirement.





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#### **High Voltage Delivery System (***details in Sarah's talk***)**

It comprises: HVPS, HV cable, ripple filters, HV feedthrough, and the HV extender inside the cryostat to deliver the voltage to the cathode and field cage at the mid height of the TPC. Proposed reference design:

- Heinzinger PNChp 300kV power supply to power bias the cathode at ~293kV: successfully deployed in the ProtoDUNEs with good performance.
- Inline ripple filter based on the successful design for NP04 (moderate voltage drop to allow a higher voltage at the cathode).
- The HVFTs with improved (UCLA) design wrt the ones in used in ProtoDUNEs. The HVFT in NP04 worked well for more than 2 years. Both HVFTs developed ice buildup at the HV cable connection on the air side: a shortcoming in the FT design. An existing HVFT free from cold connection, built by UCLA for the 35ton TPC being evaluated at CERN for 300kV operations.
- A new HV extender (simplified version of the one of NP02); critical elements under tested at Iceberg (FNAL). A full-size extender to be assembled at CERN and tested (with HVFT) in NP02 in the fall.



#### **High Level Requirements (EB/TB held)**

- Most requirements for FD1-HD are also valid for FD1-VD
- Higher Cathode voltage and different HV distribution (extender) included
- Consortium held requirements and specifications under development.



### **R&D on 350-360 kV HV-PS**

- Investigations are ongoing to develop a 350-360kV power supply:
	- Heinzinger, FuG Elektronik.
- FuG was very responsive and willing to collaborate on a joint R&D program:
	- detailed discussions on technical aspects on HV scaling and tooling required to achieve it, while maintaining the specs on stability, ripple and longevity.
	- Scaling reachable with present technology
	- $\sim$  one year to develop a working prototype
	- BUT: very expensive R&D (650 kEuro including prototype) due to development of infrastructures and tooling and very limited commercial market
	- High cost of the final HV-PS (~240 kEuro)
	- Alternative solutions also surveyed with the help of French colleagues (ILL 380 kV PS built by Heinzinger with dedicated oil bath design)
		- Similar cost (> 400-500 kEuro) as for the FuG solution and additional R&D required to adapt to the DUNE underground environment.
- Other alternatives under study as well





#### **Motivations for HV-PS delivering more than 300 kV?**

- In present VD layout, the total resistance of the field cage is 2.81 GOhm (96 RDV in parallel, 270 GOhm each; schematics successfully tested in NP04/02).
- A  $\sim$  50 MOhm resistance for the warm RC ripple filters should be included (as demonstrated by NP04)
- With these conditions, to reach the nominal drift field of 500 V/cm, the HV-PS should deliver 330 kV.
- With a 300 kV HV-PS, a drift field of 450 V/cm could be reached.
- Variation of the most relevant LAr-TPC parameters, going from 500 V/cm to 450 V/cm, (<https://lar.bnl.gov/properties/#basic-prop>) are sublinear:
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- Free electron drift velocity  $= 1.601$  mm/us  $\rightarrow$  1.517 (-5.25%)
	- $\text{Max drift time } (6.5\text{m})$  = 4063 us  $\rightarrow$  4285 us (+5.25%)
	- $E1$ -ion recombination  $= 0.595 \rightarrow 0.5814 (-2.3\%)$
	- $-$  Scintillation yield  $= 0.4395 0.4473 (+ 1.8%)$
	- Longitudinal diffusion coef.  $= 6.627 \text{ cm}^2/\text{s} \rightarrow 6.589 (-0.6\%)$
	- Transverse diffusion coef.  $= 13.24 \text{ cm}^2/\text{s} \rightarrow 12.62 (-4.6\%)$
	- $\lambda = 8 \text{ mm/s} \rightarrow 7.2 \text{ } (\sim -10\%)$
- DUNE physics analysis group involved to evaluate the performance of the VD TPC at a drift field of  $\sim$  450V/cm, compared to 500 V/cm.

#### **Extender as single point failure?**

- *Based on the experience from NP02, the new extender has been designed to overcome single-point-failure risks.*
- *If the validity of this design is confirmed in 2021 tests (CERN/FNAL), the identified failure points are:*
	- *Connection from the Extender to the FC/Cathode. This will be not accessible, but it is be easily mitigated with the already assumed multiple flexible-wired connections.*
	- *Connection from the Extender to the HVFT. This is fully accessible as the HVFT can be extracted and replaced. Note that this operation has been successfully performed several times in several different LArTPC based detectors.*
	- *Failure of the Extender hanging structure. In this case the effects will not be minimal or with high impact for the detector operation, depending on the failure degree (the extender could fall down or change position). Mitigation (implemented) is to use multiple hanging rods.*
	- *Occasional HV instabilities due to hopefully rare discharges to the cryostat walls or the FC. HV current limitation and resistive filtering stages along the warm cable will slow down the discharge thus limiting the effect of the stored energy release.*
- *In all these scenarios, a second extender would not mitigate these issues but rather increase the possibility of failures, being the additional extender at the same HV as the one connected to the HVFT.*
- *For this reason, we do not consider a second extender as a way to mitigate the HV single-point-failure risks.*

#### **Key Interfaces (***details in Bo's talk***)**



#### **Ongoing and Planned Technology Development**



*Details on HVS components validation program in Filippo's and Sarah's talks*



#### **Risks**

- Evaluation started (discussed at the recent Risk Workshop)
- Mostly derived from HD and former DP
- To be refined also according to the HV validation with demonstrators



## **HVS consortium Organization**





# **HVS consortium Institutional commitments**





# **HVS funding model for Vertical Drift**



- The cathode and its suspension system is a deliverable that will be fully funded by France/IN2P3
- The scope of the rest of the HV system for the DUNE FD2 is shared between DUNE-US and CERN
- DUNE-US is responsible for the design prototyping, production of the FD and the project management and installation at SURF.
- CERN contributes with design, prototyping (ProtoDUNE and HV), procurement of all FC profiles, HV power supplies and HV power distribution system.
- CERN will contribute with some FTEs during the FD assembly and installation period

#### **Summary**

- The conceptual design of the HV system components have been developed, with some detailed parameters and material choices under evaluation.
- Most of the operating principles and design features are evolved from the FD FD-HD counterparts, and have been validated by the ProtoDUNEs operation, with further improvements.
- We recognize a number of new challenges, such as the HV extender, and have planned a series of development activities and small to large scale tests to validate the designs and mitigate the risks.
- A 70% transparent field cage design is taking shape. It appears that we have the flexibility of mixing the more transparent FC configuration with the conventional design to accommodate the wall-mount PDs while minimizing HV risks.
- The FD-VD HVS is expected to meet the same high level requirements from FD-HD. We are performing cost and benefit analysis to see if we need to set the drift field goal to 450V/cm.
- The FD-VD HVS has a distinctively different set of interfaces with other subsystems compared to FD FD-HD. The interface with PDS is very complex and must be closely coordinated.
- The first draft of the CDR HVS chapter released to CET on June 10th. The content is presented in this review. HVS prototyping sections also released.



