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ProteCCT

(Protection of Canted-Cosine-Theta-type Magnets)

2nd STEAM Workshop 13th of October 2021

Matthias Mentink



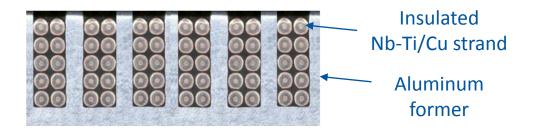
2nd STEAM Workshop – CERN, Geneva, CH – 13th of October 2021

Overview

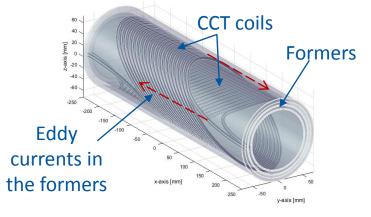
- Motivation
- Thermal aspects
- Internal circuit / Co-simulation
- User interface
- Complexities + correction factors:
 - Oversimplified model of eddy currents in the formers → Correction factor fLoopFactor
 - Additional helium present between the (non-bonded) formers and outer cylinder → Correction factor addedHeCpFrac
- Simulation vs. experimental observations
- Running the model
- Demonstration
- Summary



Motivation



Canted-Cosine-Theta (CCT) magnets: superconducting strand inside slots in conductive former [1]



Eddy currents in formers surrounding CCT coils during discharge (Field, courtesy J. van Nugteren)

[1] G. Kirby et al. IEEE Trans. on Appl. Supercond. 28, p. 4002205 (2018)



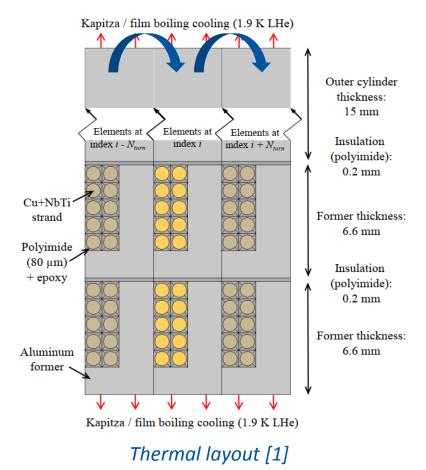
Why STEAM-ProteCCT?

- Canted Cosine Theta Magnets: Concentric superconducting coils held in place by conductive aluminum formers
- Quench protection of MCBRD Twin Aperture Orbit Correctors for HL-LHC upgrade and other future CCT-type magnets
 - Magnet is discharged over energy extractor
 - Eddy currents in the conductive formers → Heating in formers → Fast development of normal zone throughout superconducting coils (Quench-back)
 - Complex three-dimensional geometry

→ Quench simulation with STEAM-ProteCCT

Thermal aspects

Turn-to-turn periodic boundary condition



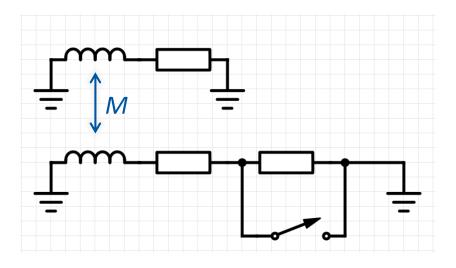
Three-dimensional thermal propagation in simplified geometry [2]

- Longitudinal heat propagation along length of strands, insulation, and formers
- Transverse heat propagation
 - Individual thermal elements for strands, insulation, formers, former insulation
 - Heat flow to the bath: 1.9 K: Kapitza + film boiling cooling, 4.5 K: Nucleate + film boiling
 - Periodic boundary conditions: Simulation of single turn per former to simulate entire magnet
- Non-linear magnetic-field- and temperature-dependent properties taken from STEAM library and LEDET material database

[2] M. Mentink et al. IEEE Trans. on Appl. Supercond. 28, p. 4004806 (2018)



Internal circuit / Co-simulation



Formers + outer cylinder: Inductively coupled

to main circuit (typically: 4x4 matrix)

Main circuit with CCT coils: Inductance, internal resistance, crowbar and dump resistor

Representation of internal circuit

- Circuit types:
 - Internal circuit: Inductance of CCT coils, internal resistance, crowbar, dump resistor + switch
 - External circuit: ProteCCT takes external current waveform (co-simulation)
 - Both cases: Main circuit (CCT coils) inductively coupled to formers and outer cylinder
- Adaptive time-stepping (constraints on maximum dT/dt, maximum dl/dt in formers, user-specified dt)



User interface

A	B	0	D	t	G H I J K L M I	0 P Q	B :	5 T	U
ProteCCT +1.0									
magnetIdentifier	"MCBRDp1_1430hm				Magnet identifier. Here "should be placed in front of the name.				
Magnet properties									
totalConductorLength	4480				Total strand length in [m], for both inner and outer former.				
numTurnsPerStrandTotal	365				Total number of windings on a single former.				
CuFraction	0.661016343				Copper fraction of the Nb-Ti/Cu conductor.				
RRRStrand	230				RRR of the copper. Note that the considered reference temperature is 2	5 K. The literature reference curv	e is MIST, which	includes temp	rotero-
BMazAtNominal	3,1				Peak field on conductor at nominal current in [7].				
BMinAtNominal	1.86				Lowest field on conductor at nominal current in [7].				
Nominal	400				Nominal current in [A], used as reference for calculating magnetic field pr	47			
fieldPeriodicity	400					the over the conductor.			
heldPeriodicity magneticl eagth	1.32				Field periodicity (2 for a dipole, 4 for a quadrupole, etc).				
					Magnotic Longth in [m].				
thFormeringul	3.50E-04				hsubtion thickness between formers in [m]. This insulation is considered	mixture of polyimide and epoxy	, and the ratio b	ofmoon the fir	o is give
wStrandSlot	1.00E-03				Size of the strand slot in [m]				
DStrand	8.25E-04				Strand diamotor in [m]				
numRowStrands	2				The number of rows of strands				
numColumeStrands	5				The number of columns of strands				
IcFactor	1.00				ic multiplier, to allow for heat-treatment-induced degradation of ic				
polyinideToEpoxyRatio	0.5				Ratio of polyimide to G10 in insulution. For thermal purposes, the two m	and the second se			
windingOrder	[6 16 1 11 7 17 2 12 8 18 3 13								
windingurder	Te le Li Li Li 5 15 8 18 2 13	0 10 4 14 10 20 0 10]			Gives the electrical ordering of the turns. Note that the indexing in the sin	ration taxes (as the bottom-feld	or the inner for	mer, 2 as the S	occom-ri
-									
Former related properties									
M	5.05E-01	5.62E-04	5.93E-04	5.17E-04	Inductance matrix in units of [H/m]. Must have dimensions (Numformers+	Numformers+2)			
	5.62E-04	7.17E-07	6.53E-07	5.41E-07					
	5.93E-04	6.53E-07	7.17E-07	5.33E-07					
	5.17E-04	5.41E-07	5.99E-07	6.76E-07					
	5.112-04	0.412 01		0.106.01					
innerRadiusFormers	5.50E-02	6.20E-02							
		6.20E-02			hner radius of the formers in [m]				
formerThicknessUnderneathCoil	1.60E-03				Thickness of the former underneath the slot holding the strands in [m]				
innerRadiusOuterCylinder	6.30E-02				hner radius of the outer cylinder in [m]				
thicknessOuterCylinder	1.50E-02				thickness of the outer cylinder in [m]				
RRRFormer	8.0				RRR of the former, assuming aluminum. Note that the considered referen	: temperature is 295 K.			
RRRDuterCylinder	8.0				RRR of the outer cylinder, assuming aluminum. Note that the considered	Second temperature is 295 K			
					· · · · · · · · · · · · · · · · · · ·				
Extra stuff									
coolingToHeliumBath					Determines whether inner surface of inner former and outer surface of ou				
cooling1 offeliumDath						r support cynhaer are in contact	e with the heavth	0.060	
tMaxStopCondition	10				Maximum evoluation time in [s] after which simulation is stopped				
tempMaxStopCondition	350				Maximum allowed hotspot temperature in JKJ after which simulation is st				
IOpFractionStopCondition	0.01				Once the operating current drops below IOpFractionStopCondition *the	nitial current, the simulation is st	topped		
Sweepable parameters (this mea	ans that you may put mor	e than one value and the sim	ulation will run for thes	e multiple values)					
fLoopLength	2.0			, ,	The simulation model assumes cos-theta current distribution in the forme	but the reality is more complie	ated with calcul	ha current 78	is canalair
TOp	1.3				Both temperature in /K/			,	
Dohitisl	400				hitial operating current in [A]				
RCrowbar	400 5.50E-02								
					Crowbar resistance in Olim				
RDunpPreconstant	1.428				Constants describing the dump resistance. R(I):RdumpPreconstant Jab.				
RDunpPower	0				Constants describing the dump resistance. R(I)=RdumpPreconstant Yab:				
addedHeCpFrac	0.006				Extra holium host capacity that is added to the formers. This number is th	fraction of the former volume th	at is assigned to	be helium, as	running a s
addedHeCoolingFrac	0				Fraction of regular cooling to the helium bath that the other formers best				· · ·
tSwitchDelay	1.00E-02				Time required to open the switch after protection triggering in [s]				
coolingToHeliumBath	1				For (0), cooling to the both is not considered. For (1), the inner surface of	the inner former and the outer of	intace of the nut	er support rm	ledor are
Solver configuration options									
sorrer configuration options	0.025				All shares all the second and the description of the second		A matter almost 1		
fracCurrentChangeMax					Maximum dill for a given iteration (applies to both the coil and the forme				
resultsAtTimeStep	2.00E-03				The simulation time stop in [s] at which the simulation notifies the user of				me step.
deltaTMaxAllowed	0.1				Maximum change in temperature in JKJ between subsequent solver iterati	is. This parameter is used for ad	hptive time-step	iping	
minTimeStep	1.00E-06				Absolute minimum time step size in [s]				
	50				Amount of elements for given turn.				
turnLengthElements					If withPlots is set to 1 then for every timeStep, the voltage-to-ground dis	inution is plotted			
turnLengthElements Graphics options					if withPlots is set to 1 then ror every timestip, the voltage-to-ground dis if withPlots is set to 1 then some pause time is needed to render the grap		4		
turnLengthElements Graphics options withPlots					a anamous is set to 1, then some pause time is needed to render the grap	s. r enumermore, ror convenience,	, one user might i	nuu more	
turnLengthElements Graphics options withPlots	1								
turnlangthEloments Graphics options withPlots plotPauseTime	1								
turnLengthElements Graphics options withPlots plotPauseTime postProcessing	1								
turnLengthElements Graphics options withPlots plotPouseTime postProcessing withVoltageEralustion	1				If this option is set to { then for selected turns {see voltageToGroundOn			ı is calculated	and inclu
turnLengthElements Graphics options withPlots plotPouseTime postProcessing withVoltageEralustion	1 (6 10 14 20)				If this option is set to 1, then for solected turns (see voltageTeGroundDi Solected turns for voltage-to-ground-evolution (see above option). He			r is calculated	and inclu
turnLengthElements Graphics options withPlots plotPouseTime postProcessing withVoltageEralustion	1							ı is cəlculəted	und inche
ternlangtkÉlements Graphics options withPlots plotPauseTime postProcessing withYoltsgeEraluation voltsgeToGroundDatputSelection	1							n is calculated	and inclu
tendangtkÉlemants Graphics options withPlats plotPauscTime postProcessing withValsagEvaluation voltageTariandOtputSelection Options read for co-simulation	1 [6 10 14 20]				Selected turns for voltage-to-ground-evaluation (see above option). Her	the indexes consider the winding		n is calculated	and inclu
ternlangtkÉlamants Graphics options withPlate plotPauseTime postProcessing withVottageTaviasion voltageToGroundDutputSelection Options used for co-simulations externalWaveform	[6 10 14 20] 0				Saloctod turns for voltage-to-ground-evaluation (see above option), Her Option to use other internal circuit (0) or externally supplied current wav	the indexes consider the winding form [1]	g order.	n is calculated	and inclu
terrilongtiklioments Graphics options withPlats plotPaceTime portProcessing withVoltogEsubution voltogeTrainsubor potpose secondoutputSelection Options secondoutputSelection Options for Corrisolations externat/Vaveform saveStateAtEnd	1 [6 10 14 20] 0 0				Selected turns for voltage-to-ground-walvation (see above option). Her Option to use either internal circuit (0) or externally supplied current wav Stree the workspace at the and of the simulation, 0 = no save, 1 = save to	the indexes consider the winding form [1] workspace, 10 = Mast time interv	g order. volk.mot'	n is calculated	and inclus
ternlangtkÉlamants Graphics options withPlate plotPauseTime postProcessing withVottageTaviasion voltageToGroundDutputSelection Options used for co-simulations externalWaveform	[6 10 14 20] 0				Saloctod turns for voltage-to-ground-evaluation (see above option), Her Option to use other internal circuit (0) or externally supplied current wav	the indexes consider the winding form [1] workspace, 10 = Mast time interv	g order. volk.mot'	n is calculated	and inclu

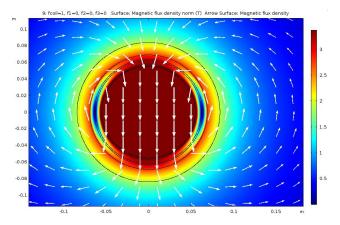
Model input: Excel file

- ProteCCT user manual [3]
- All user input is taken from a single Excel file (inspired by LEDET user interface)
- Co-simulation: Tool exchanges information through text-files
- For the most part, easy-to-understand parameters (Conductor RRR, Operating current, etc.)

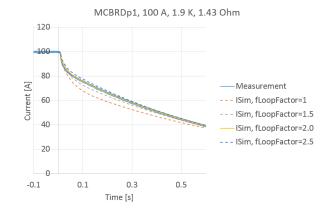
[3] M. Mentink, "STEAM-ProteCCT User manual", EDMS nr. 2160020, (2019)



Complexity & correction factor #1: fLoopFactor



Coupling-matrix calculated in Comsol, assuming simplified 2D geometry with cos-θ current distribution



Determination of fLoopFactor by matching to experimentally observed low-current discharge (no quench-back)

- Coupling matrix: Calculated in Comsol, assuming simplified 2D geometry with cos-θ current distribution in the coils, formers, and outer cylinder [3]
- Assumption: Eddy current flows axially through formers
- Reality: Eddy current model is oversimplified (and uncertainty in former material parameters)

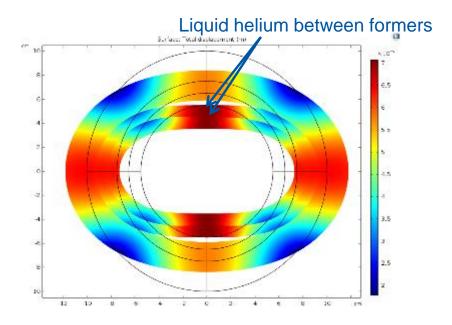
 \rightarrow Empirical correction factor *fLoopFactor* (= 2.0), to modify eddy current path length, determined by matching simulations to experimental observations

[3] M. Mentink, "STEAM-ProteCCT User manual", EDMS nr. 2160020, (2019)



Complexity & correction factor #2: addedHeCpFrac

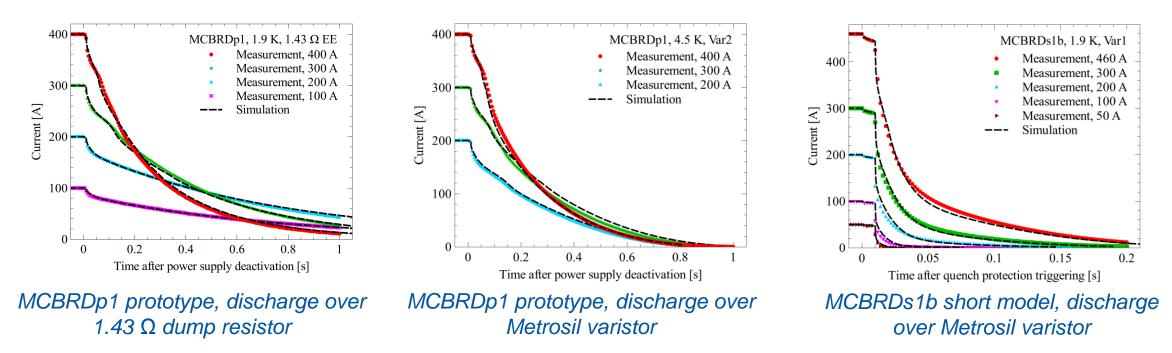
- CCT magnets: Formers are sliding with respect to each-other when powered → Gaps are present, which fill with liquid helium
- Heat capacity of liquid helium has to be overcome before quench back can occur
- To account for liquid helium: Global correction factor addedHeCpFrac → Additional heat capacity in formers (~0.6% of volume)
- Determination of correction factor by matching quench back onset t_{QB} at I₀ = 400 A, 1.9 K, 1.43 Ω
 → Used as a global parameter



Sliding and deformation of formers during powering (Courtesy Martin Novak)



Simulation vs. Experimental observation

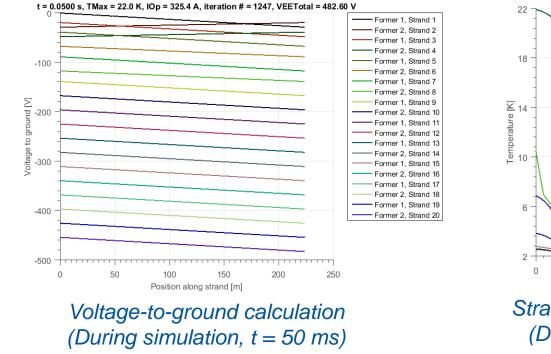


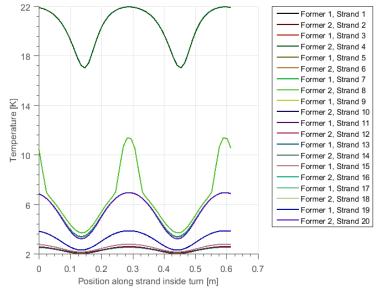
Comparison between simulation and experimental (MCBRD prototype apertures and short models):

- High degree of consistency between simulations and experimental observations
- Checked for: Different magnetic lengths, former material types, operating temperatures, varying dump resistors + Metrosil varistors, operating currents
- Two fixed global correction parameters *fLoopFactor* and *addedHeCpFrac* for all cases
- Measurement data: Courtesy F. Mangiarotti



Running the simulation





Strand temperature development (During simulation, t = 50 ms)

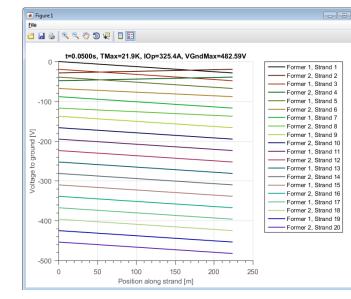
- Fast: Typically no more than few minutes to run
- Free-to-use standalone executable, no license required (Does require MCR installation)
- During simulation: Optional plotting of voltage-to-ground and strand temperature for each time-step
- Simulation output written to excel file: Time-dependent Current, hot-spot temperature, voltage-toground of selected turns, etc



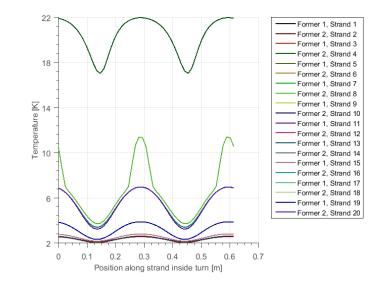
Demo: MCBRDp1

Í	ID:\Dropbox\TE-MPE-PE\tools\ProteCCT, 11-6-19\ProteCCT.exe
I	ProteCCT v1.0, developed at CERN TE-MPE-PE by Matthias Mentink (mmentink@cern.ch ,
), 7-5/19 MCBRDp1_1.430hm, TOp = 1.9, IOpInitial = 400, RCrowbar = 0.06, RDumpPreconstant = 1.43.
I	RDumpPower = 0.000, addedHeCpFrac = 0.006, addedHeCoolingFrac = 0.000, tSwitchDe
	lay = 0.010 t, TMax, IOp, UGndMax, UEETotal, UInductive, RStrandsSum, tCalc, iter #
	0.0000s, 1.9K, 400.000, 22.0U, 22.0U, -22.0U, -0.000hm, 12s, 1 0.0020s, 1.9K, 399.290, 22.0U, 22.0U, -22.0U, -0.000hm, 20s, 175 0.0040s, 1.9K, 399.070, 21.9U, 21.9U, -21.9U, -0.000hm, 25s, 197 0.0060s, 1.9K, 390.9070, 21.9U, 21.9U, -21.9U, -0.000hm, 25s, 219 0.01008s, 1.9K, 390.730, 21.9U, 21.9U, -21.9U, -0.000hm, 32s, 219 0.01008s, 2.9K, 31.700, 56.03U, 566.3U, -566.3U, -0.000hm, 32s, 219 0.01008s, 2.9K, 31.700, 56.3U, 558.2U, -558.2U, -0.000hm, 36s, 389 0.01108s, 2.9K, 374, 21.9U, 21.9U, -21.9U, -0.000hm, 36s, 412 0.01008s, 3.3K, 367.970, 545.8U, 545.8U, -545.8U, -0.000hm, 52s, 402 0.0120s, 3.8K, 364.3110, 540.3U, 545.8U, -545.8U, -0.000hm, 52s, 402 0.0120s, 3.8K, 364.3110, 540.3U, 540.3U, -540.3U, -0.000hm, 68s, 411 0.0220s, 4.2K, 366.890, 535.6U, 535.6U, 535.6U, -0.000hm, 68s, 421 0.0220s, 5.5K, 351.870, 522.2U, 522.2U, -522.2U, -0.000hm, 67s, 434 0.0220s, 5.5K, 351.870, 522.2U, 526.2U, -526.2U, -0.000hm, 75s, 448 0.0320s, 5.5K, 344.720, 518.1U, 518.1U, -518.1U, -0.000hm, 75s, 448 0.0320s, 6.2K, 346.720, 514.1U, 518.1U, -518.1U, -0.000hm, 75s, 463 0.0320s, 6.2K, 346.720, 514.1U, 518.1U, 518.1U, -6100hm, 98s, 457 0.0320s, 6.2K, 346.720, 514.1U, 518.1U, 518.1U, -0.000hm, 98s, 453 0.0320s, 6.2K, 346.720, 514.2U, 551.2U, 557.0U, -0.000hm, 98s, 457 0.0320s, 6.2K, 346.720, 514.2U, 518.1U, 518.1U, -618.1U, -0.000hm, 98s, 453 0.0320s, 6.2K, 346.720, 514.2U, 551.2U, 557.0U, -0.000hm, 98s, 453 0.0320s, 6.2K, 346.720, 514.2U, 551.2U, 557.8U, 0.000hm, 98s, 481 0.0330s, 6.2K, 340.350.41.2U, 501.2U, 501.0U, -500, 000hm, 98s, 481 0.0330s, 6.K, 337.930, 504.4U, 504.4U, -504.4U, -0.000hm, 98s, 481 0.0330s, 6.K, 337.930, 504.4U, 504.4U, -504.4U, -0.000hm, 98s, 481 0.0400s, 15.2K, 335.330, 497.3U, 497.3U, -577.8U, 0.090hm, 198s, 485 0.0440s, 15.2K, 335.330, 497.3U, 497.3U, 557.8U, 0.170hm, 138s, 697 0.0440s, 17.8K, 332.840, 490.1U, 490.1U, -545.5U, 0.170hm, 118s, 697 0.0440s, 19.5K, 330.450, 490.1U, 490.1U, -545.5U, 0.170hm, 118s, 697 0.0440s, 21.9K, 325.380, 402.6U, 482.6U, -575.0U, 0.280hm, 122s
	Elapsed time is 122.617033 seconds.
L	

Command prompt output



Voltage distribution in magnet during simulation, t = 50 ms



Strand temperature development during simulation, t = 50 ms

ProteCCT is found on STEAM website: cern.ch/steam

- Manual: EDMS Nr. 216002 (link of STEAM website)
- Simulation tool available of steam website
- Running requires installation of Matlab runtime (see Matlab runtime.txt)



Summary

ProteCCT

- Simulation tool for evaluating discharge of CCT-type magnets (With quench-back from conductive formers)
- Very fast, standalone executable
- User-interface: Input from Excel, output to Excel (plus optional plotting during execution)
- Available on STEAM website (cern.ch/steam)
- Compatible with co-simulation, which allows for more exotic circuits
- Free to use, but please reference to ProteCCT manual when used for publications / presentations

