

# Capacitance measurements on AC-LGADs (FBK RSD1)

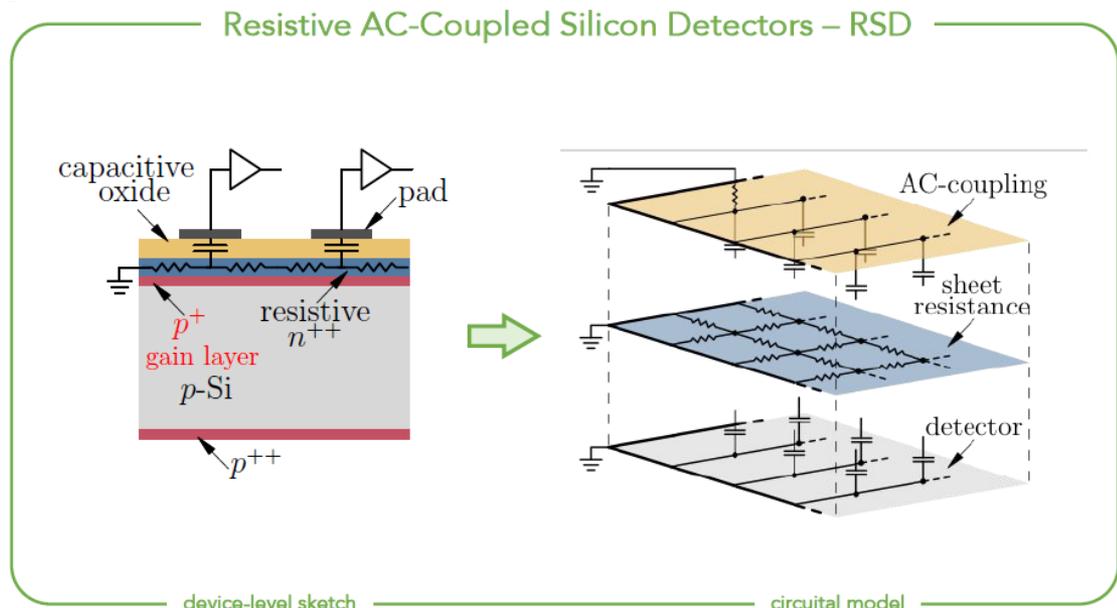
*Jennifer Ott,*

*A. Das, E. Gonzalez, S. Mazza, E. Potter, E. Ryan, H. Sadrozinski,  
B. Schumm, A. Seiden, A. Summerell, N. Tournebise, M. Wilder*

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# Background and motivation

- Low-gain avalanche diodes (LGADs) are studied for ultrafast timing applications and 4D tracking
- In AC-coupled LGADs, also referred to as Resistive Silicon Detectors (RSD), the multiplication layer and  $n^+$  contact are continuous, and only the metal layer is patterned:
  - the signal is read out from metal pads on top of a continuous layer of dielectric
  - the underlying resistive  $n^+$  implant is contacted only by a separate grounding contact





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  - the signal is read out from metal pads on top of a continuous layer of dielectric
  - the underlying resistive  $n^+$  implant is contacted only by a separate grounding contact
- C-V measurements can be used to probe various capacitances in such sensors:
  - Give an idea of the RC characteristics, interpad and dielectric capacitances etc
  - Also important for the design of readout electronics!



# FBK RSD1 production

wafer #	<i>n</i> -plus dose	<i>p</i> -gain dose	dielectric thickness	<i>p</i> -stop dose	substrate	V <sub>bd</sub>	Dose [a.u.]
3	A	0.92	L	B	Epi	460	0.05
4	A	0.94	H	B	Si-Si	440	
8	B	0.94	L	B	Si-Si	460	0.1
10	B	0.96	H	B	Si-Si	430	
13	C	0.94	L	B	Si-Si	465	0.2
15	C	0.96	H	C	Si-Si	445	

Information from the manufacturer is used to assign dose values in arbitrary units:

Dose B is ~ 1/10 of the usual LGAD doping,

Dose A is 50% of Dose B

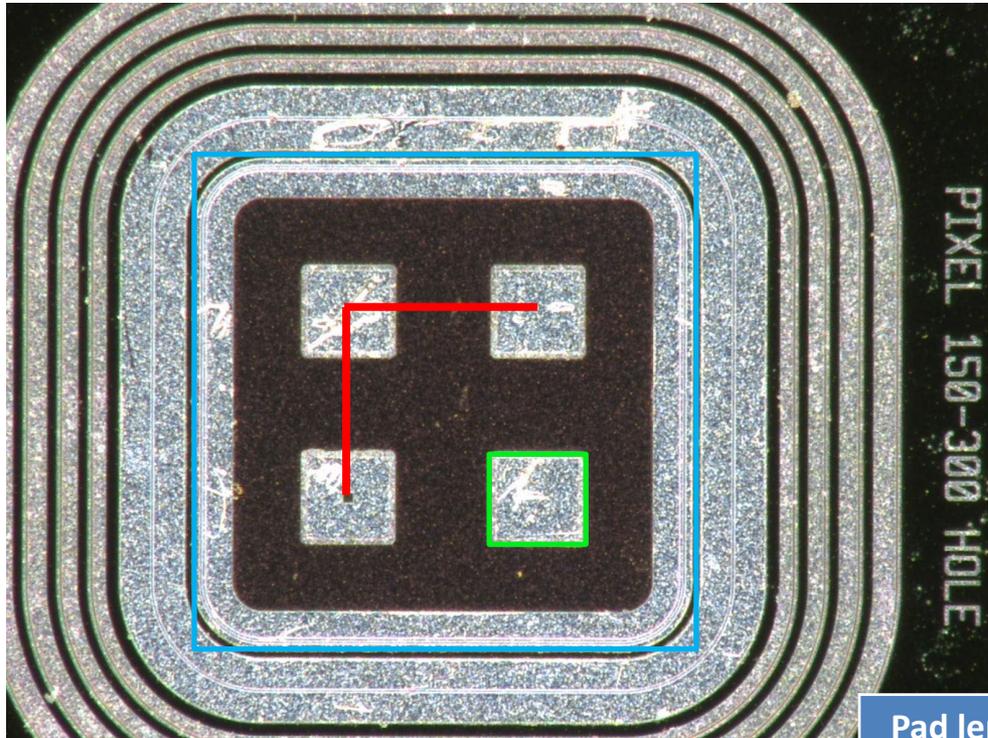
Dose C is 2x times Dose B

## Investigating:

- Dielectric thickness
- $n^+$  dose
  
- Measurement frequency
- Pad size
- Neighboring pads

# Sample geometry

2x2 arrays, each die with 3 different pad sizes (but same pitch)  
 → varying pad area and distance between pads



Area of the  $n^+$ :  
 ca.  $770 \times 770 \mu\text{m}^2$

Pitch:  $300 \mu\text{m}$

Pad length:  $150/200/290 \mu\text{m}$

Pad length, width ( $\mu\text{m}$ )	Area ( $\mu\text{m}^2$ )	Interpad distance ( $\mu\text{m}$ )
150	22 500	145
200	40 000	100
290	84 100	10

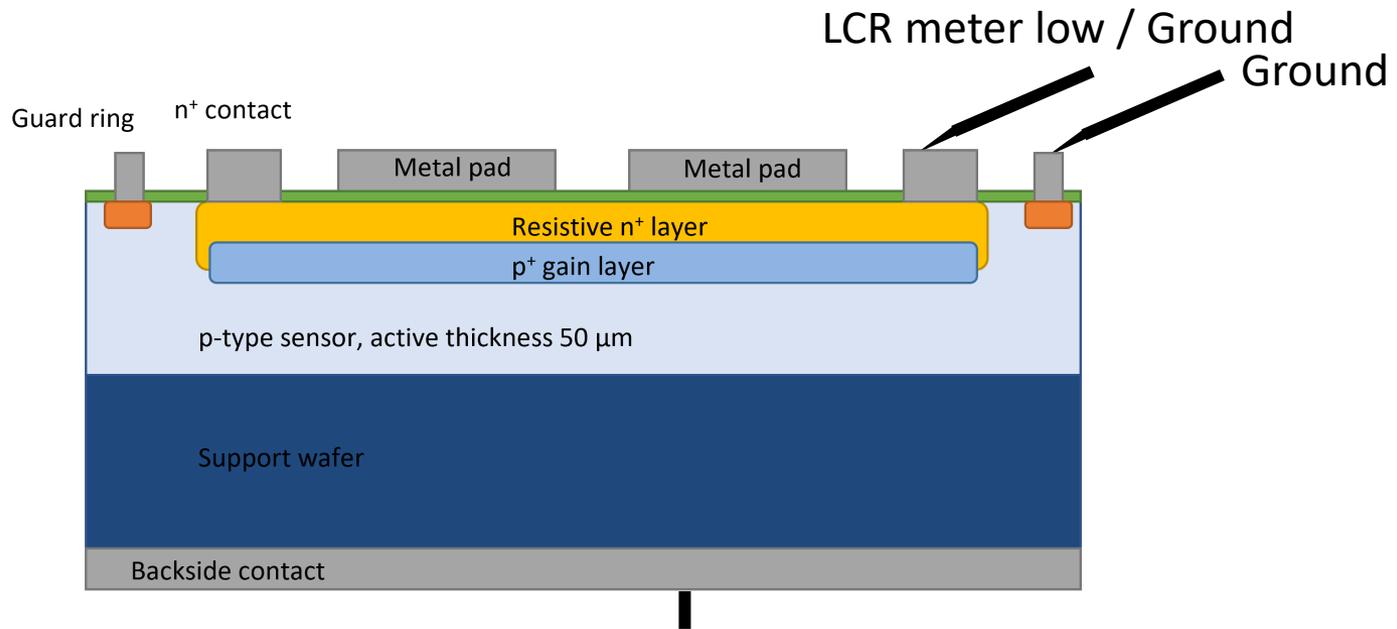


# Capacitance measurement configurations

$C_p$ - $R_p$  as LCR meter capacitance model

High voltage always from backplane, biasing ground to  $n^+$

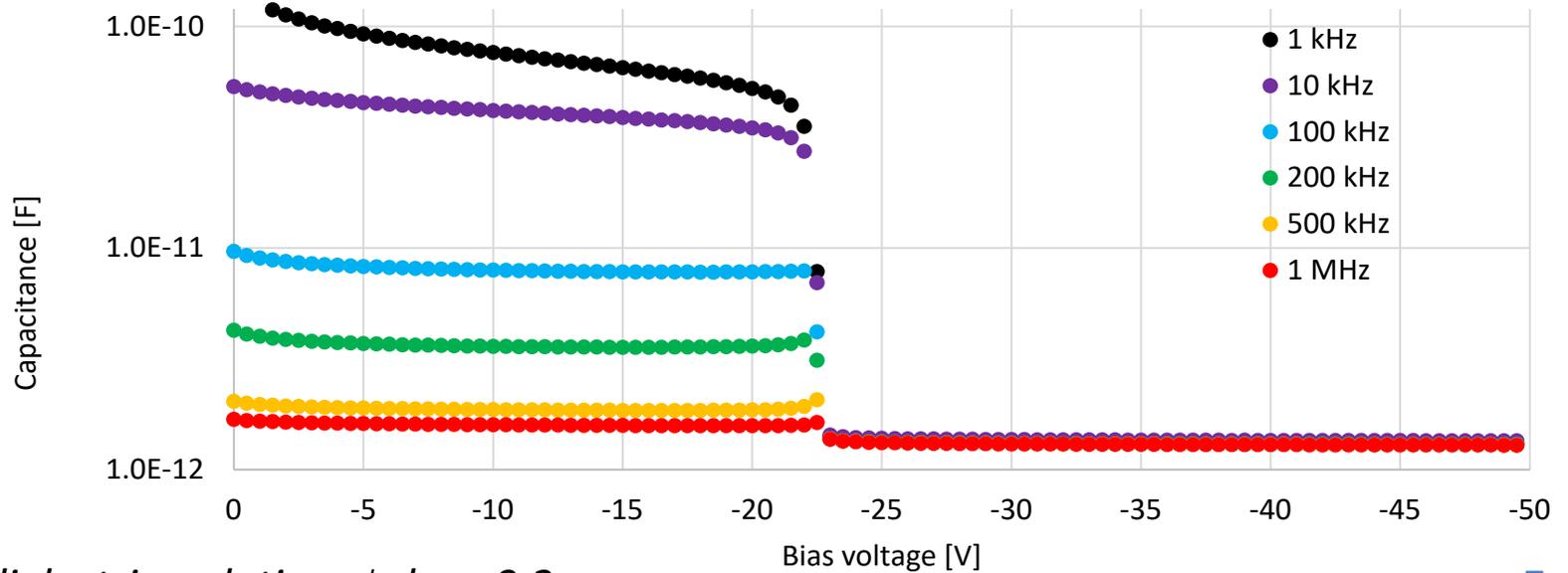
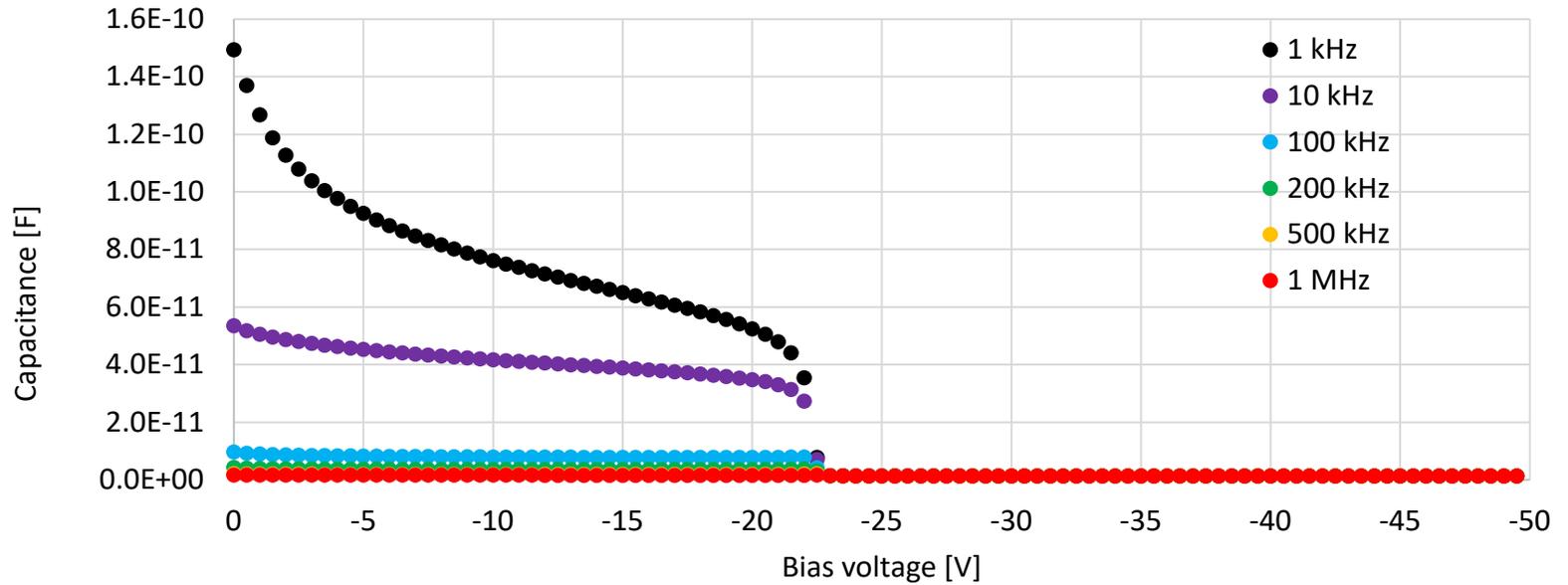
- **DC:** sensor backplane to front side  $n^+$
- **AC:** sensor backplane to metal pad
- **AC-AC / interpad:** between two metal pads
- **$n^+$  to metal pads:** between  $n^+$  and one metal pad





# DC configuration

J. Ott, RD50 workshop Nov 2021

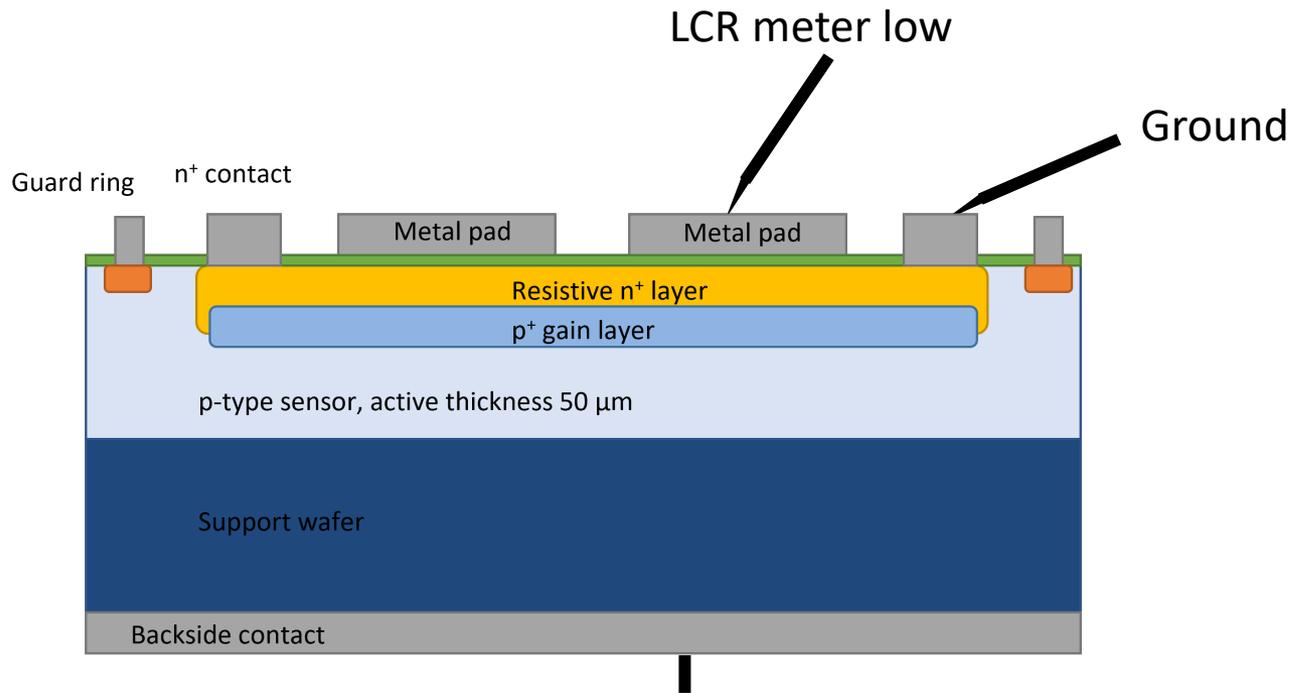


W13, thin dielectric, relative  $n^+$  dose 0.2



# Capacitance measurement configurations

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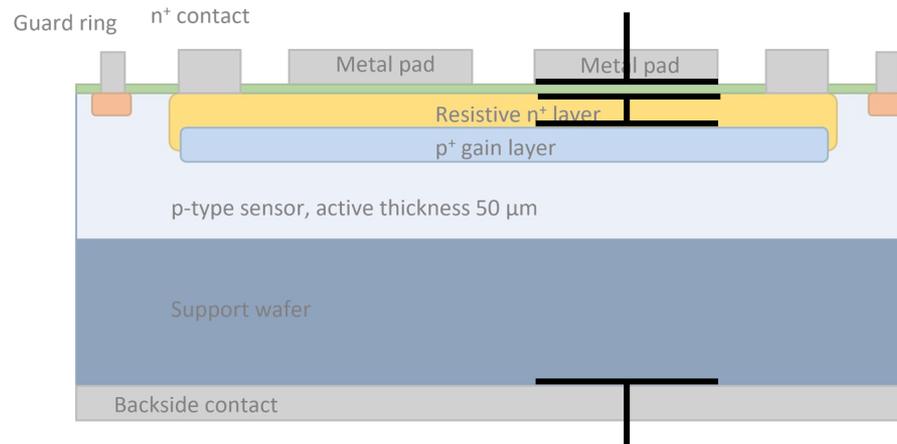


# Examining the 'AC configuration'

The capacitance of the dielectric layer is orders of magnitude larger than that of Si

$$\frac{1}{C_{tot}} = \frac{1}{C_{Si}} + \frac{1}{C_{dielectric}}$$

- *If silicon and dielectric capacitance are in series: silicon capacitance dominates!*
- Effective Si capacitance in measurement depends on bias voltage: for the not-depleted sensor, dielectric capacitance is significant - after full depletion, negligible difference

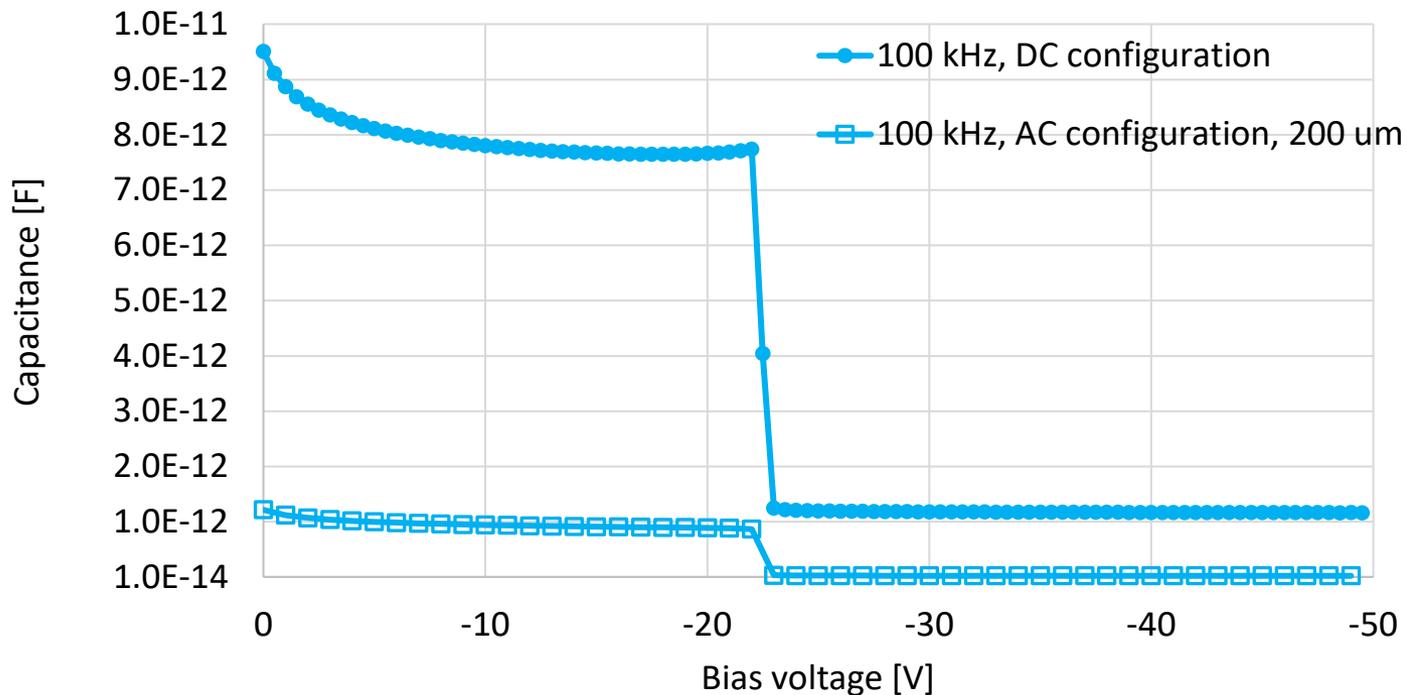




# DC and AC configuration

Notable differences in DC and AC configuration:

- Capacitance before depletion in AC configuration is affected by the dielectric capacitance
- Even with the large common n<sup>+</sup> layer, the pad capacitance is determined by the **size of the metal pad**

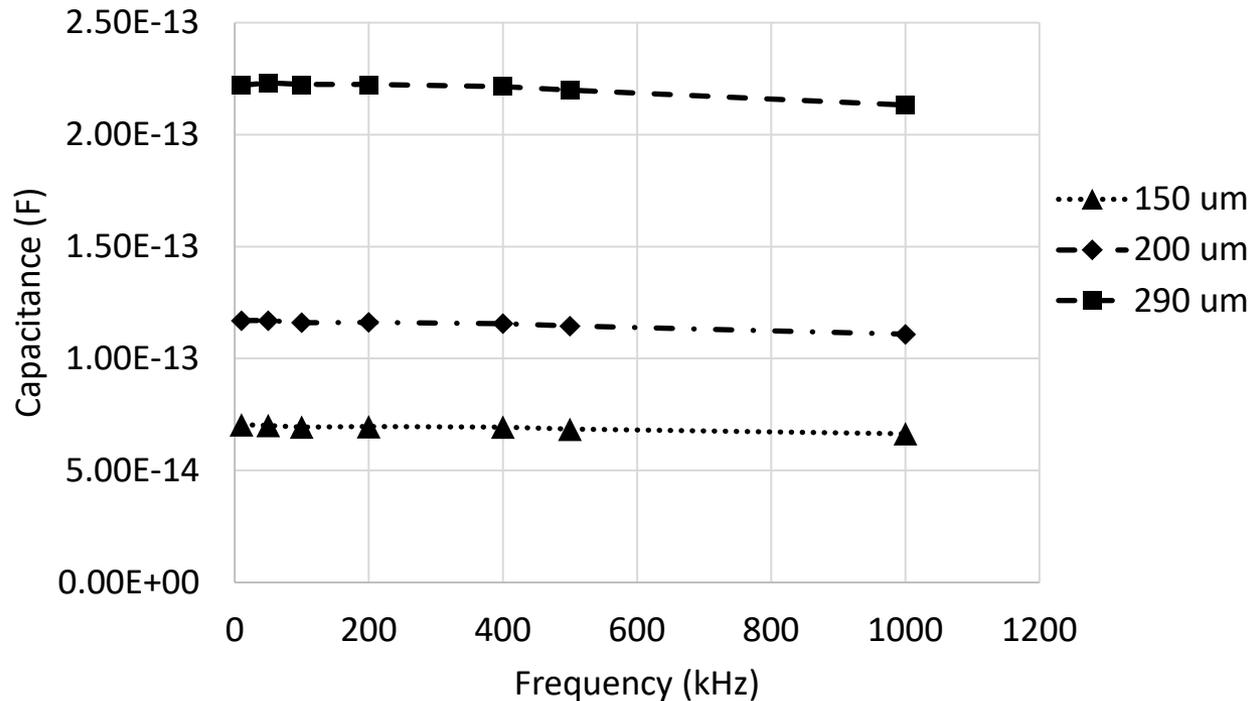




# AC configuration: pad size

Pad size affects the final capacitance values, since capacitance is directly proportional to the area

- Values after full depletion are relatively small compared to “regular” CV measurements: for 150  $\mu\text{m}$  pads,  $< 100$  fF



W4, thick dielectric, relative  $n^+$  dose 0.05



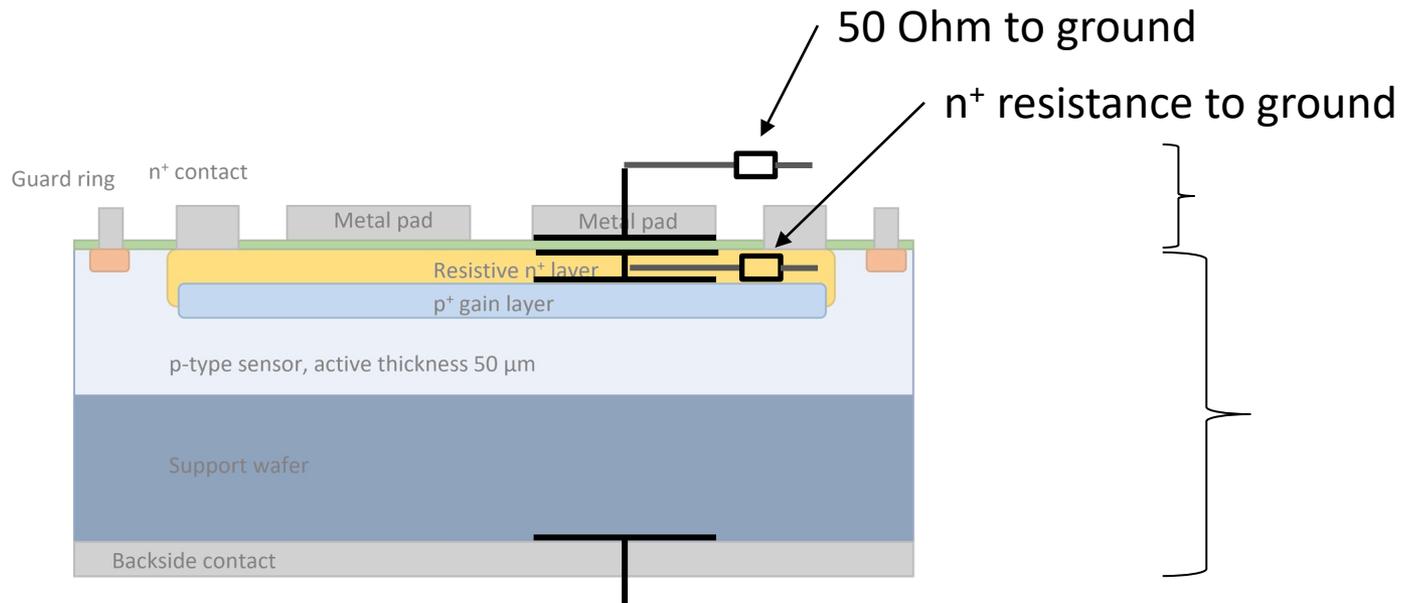
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Grounding and n<sup>+</sup> introduce resistances: two CR filters in series

- Frequency dependence

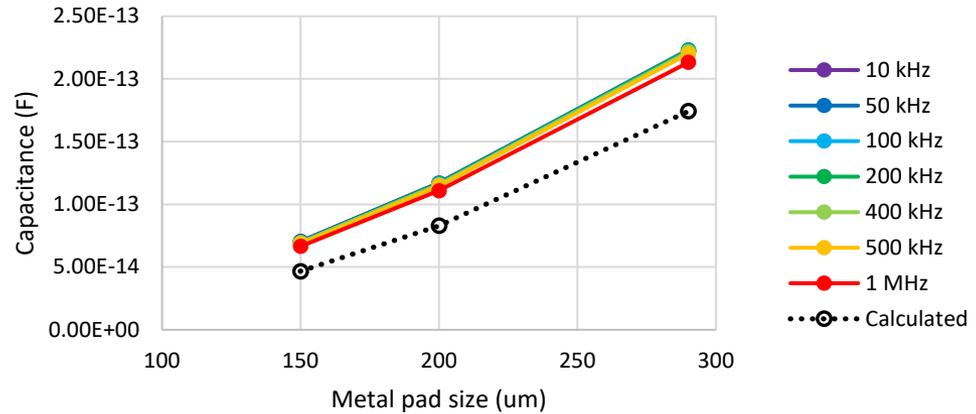




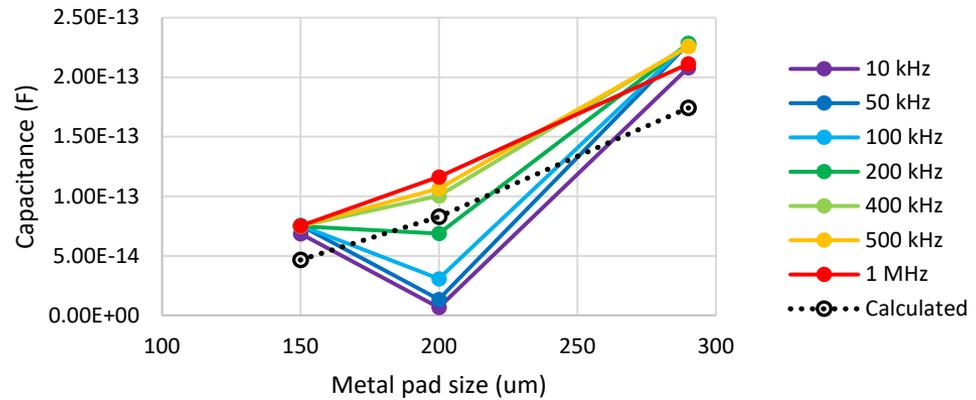
# AC configuration: n<sup>+</sup> splits (thick dielectric)

J. Ott, RD50 workshop Nov 2021

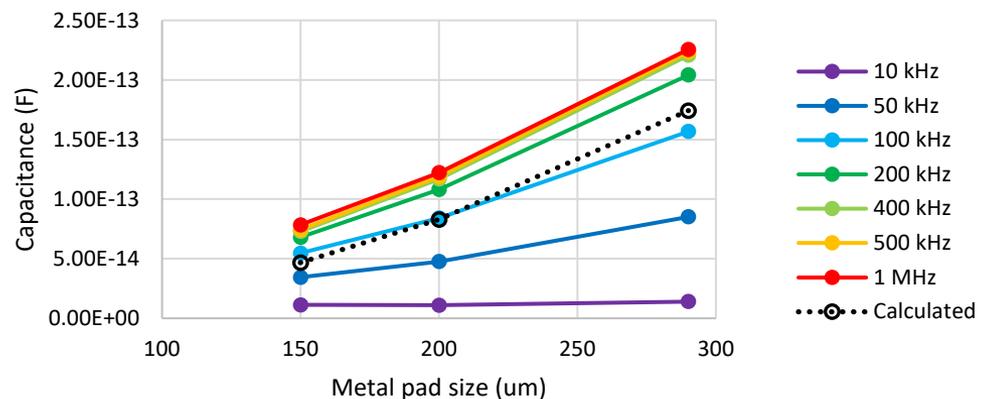
W4, relative n<sup>+</sup> dose 0.05



W10, relative n<sup>+</sup> dose 0.1



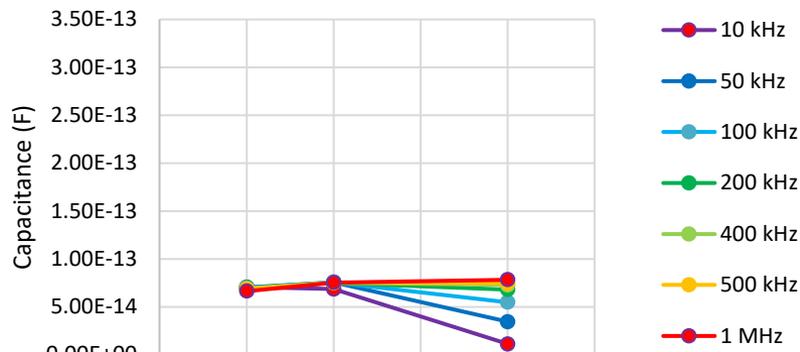
W15, relative n<sup>+</sup> dose 0.2



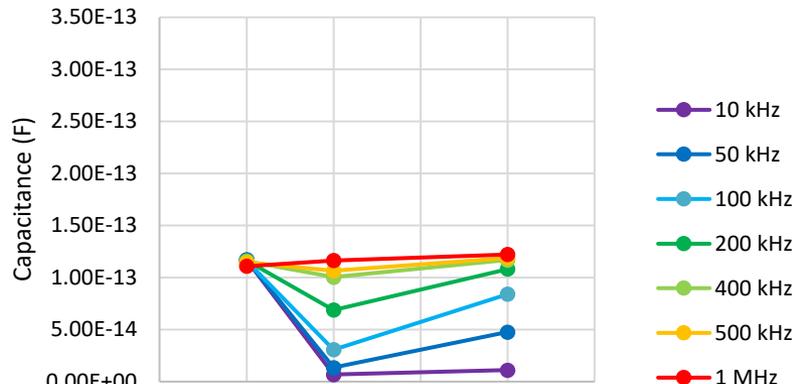


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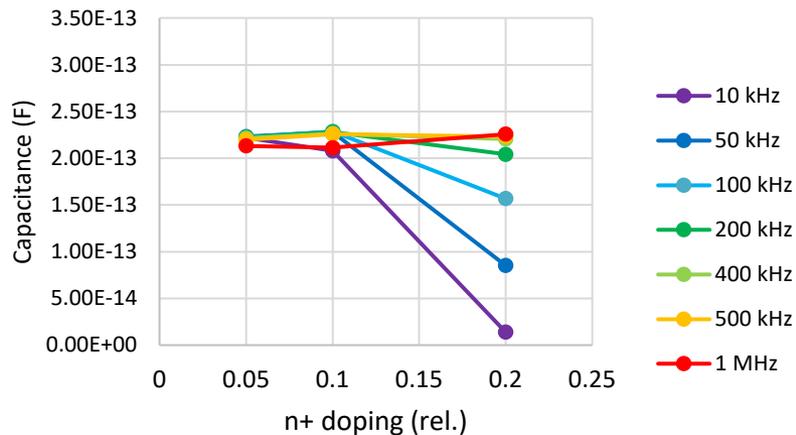
150 μm pad



200 μm pad



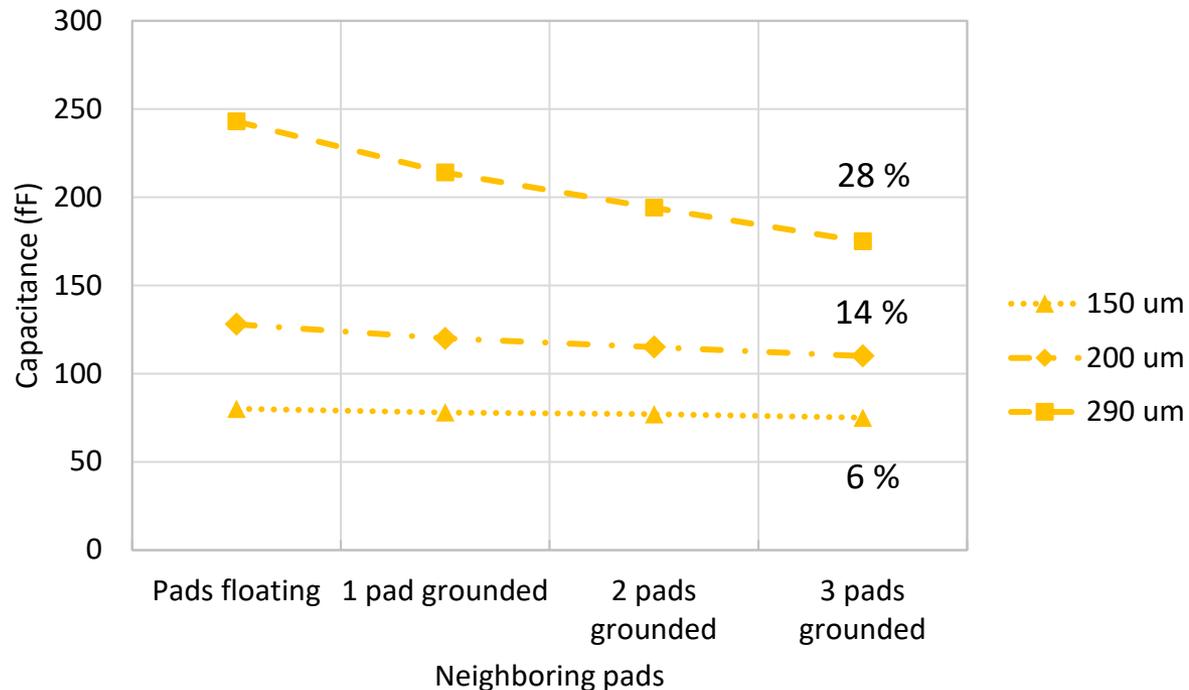
290 μm pad





# AC configuration: grounding of neighboring pads

Grounding of the 3 remaining pads impacts the final capacitance value more significantly for larger pads = smaller interpad gap

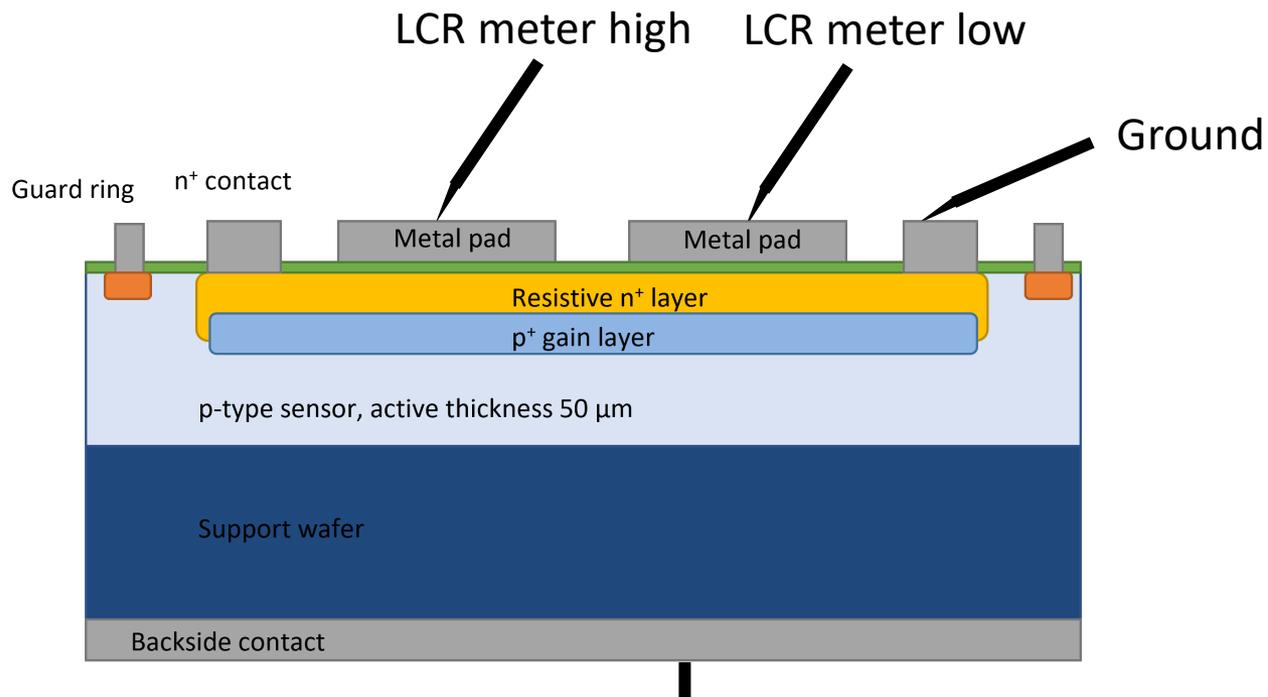


W4, thick dielectric, relative  $n^+$  dose 0.05. At 500 kHz



# Capacitance measurement configurations

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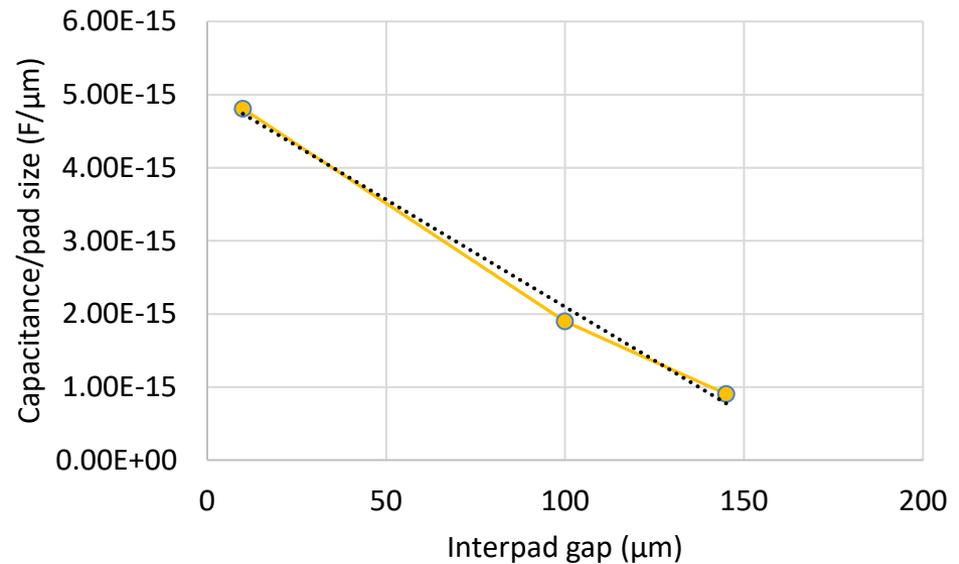
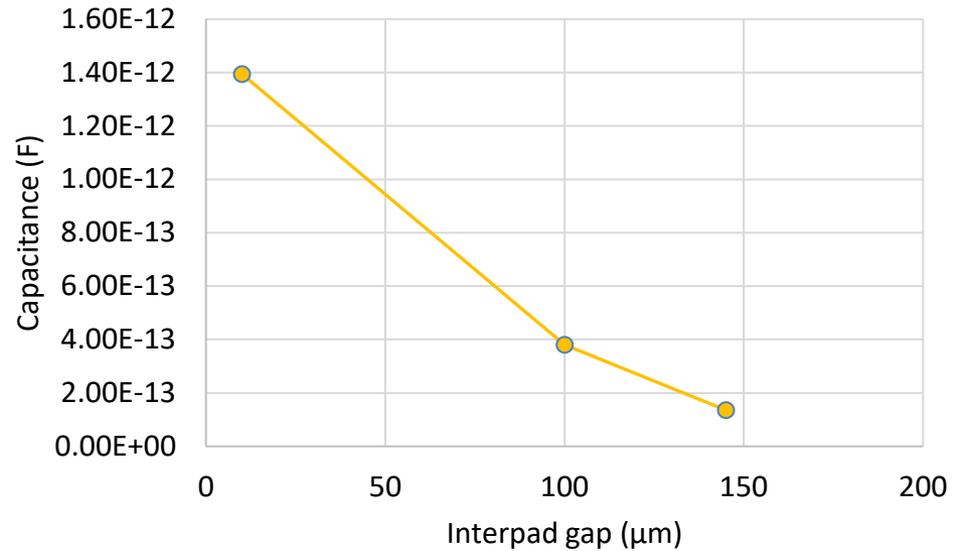




# Interpad capacitance

Interpad capacitance depends on distance between pads

Scaling by the pad size does not quite result in an inverse linear dependence – edge effects?

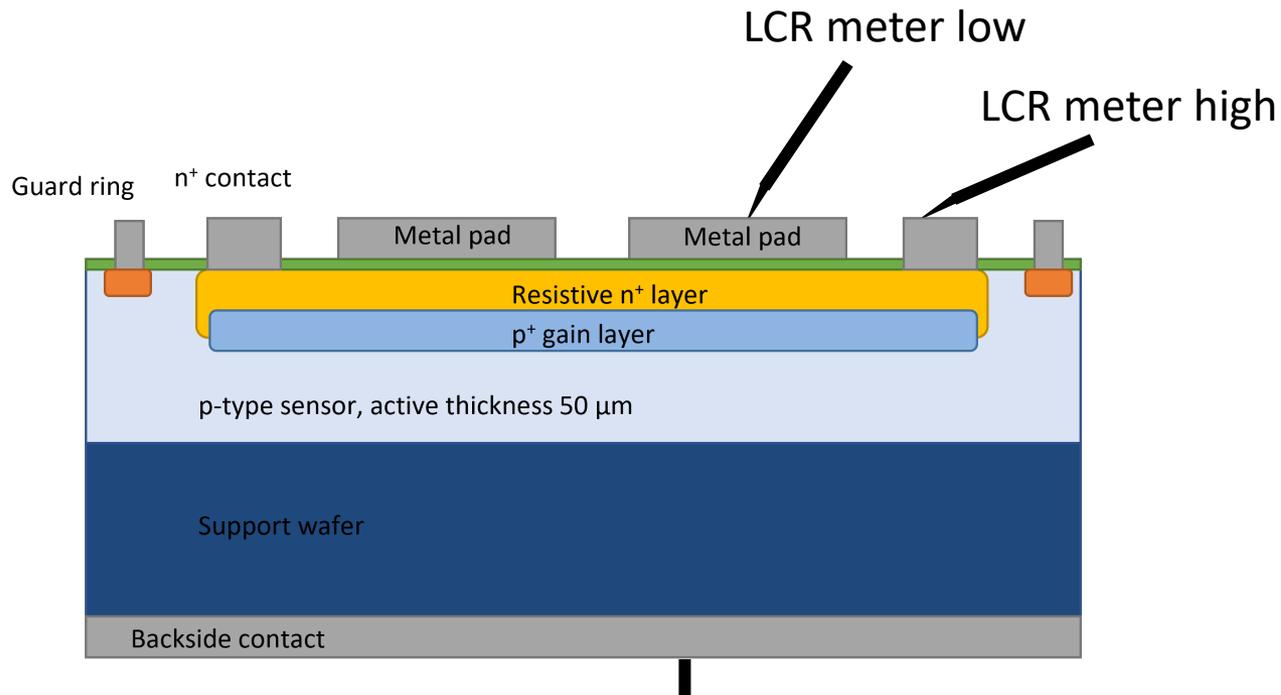


*W4, thick dielectric, relative  $n^+$  dose 0.05. At 500 kHz; other pads grounded*



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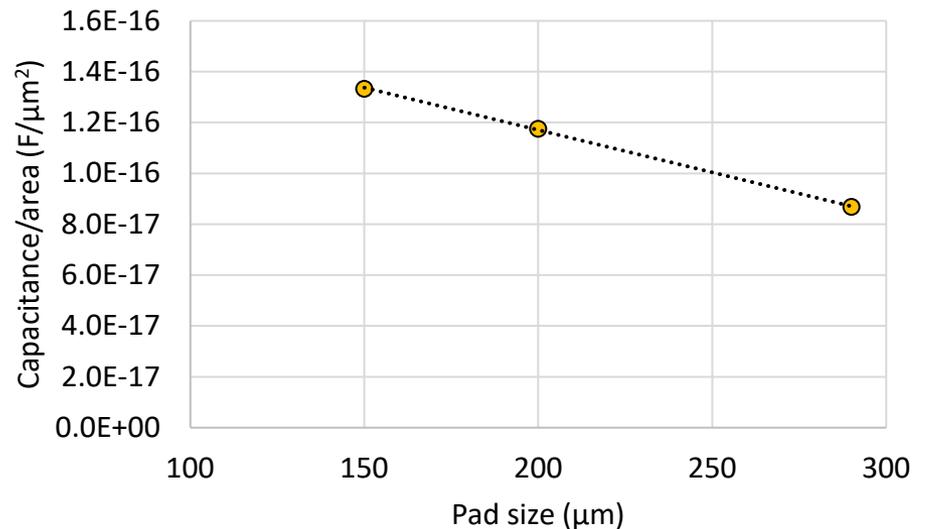
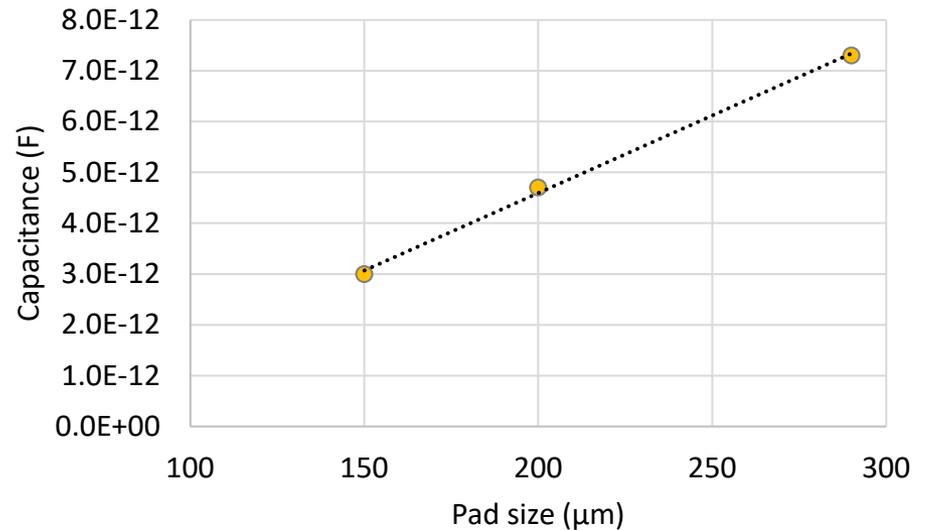




# Dielectric capacitance ( $n^+$ to metal pad)

Measured dielectric capacitance depends on pad size and area

Capacitance scaled by area still shows correlation with pad size – edge effects?  
Effective pad size different from geometric metal pad?



W4, thick dielectric, relative  $n^+$  dose 0.05. At 500 kHz; other pads grounded



# Summary

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- C-V measurements on AC-LGADs have been conducted in various configurations
- Results are an interplay of pad size, pitch, grounding of other pads, and measurement frequency
- Small pad sizes result in low capacitances
  - More challenging to measure in practice
  - Good news with respect to input capacitance for amplification stage in readout electronics
- Differences in wafer splits (dielectric and  $n^+$  layer) may manifest themselves as dependence on measurement frequency



# Next steps

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Further measurements on interpad and  $n^+$ /metal capacitances

- Aim to disentangle the effects of pad sizes and distances

Circuit simulations of frequency dependence

Conduct similar series of measurements on:

- Other array geometries in FBK RSD1: larger pitches and even smaller pad sizes...
- Recently arrived FBK RSD1 irradiated samples
- FBK RSD2
- AC-LGADs from BNL and HPK



Thank you!



# FBK RSD1 production

Split table (with breakdown voltage)

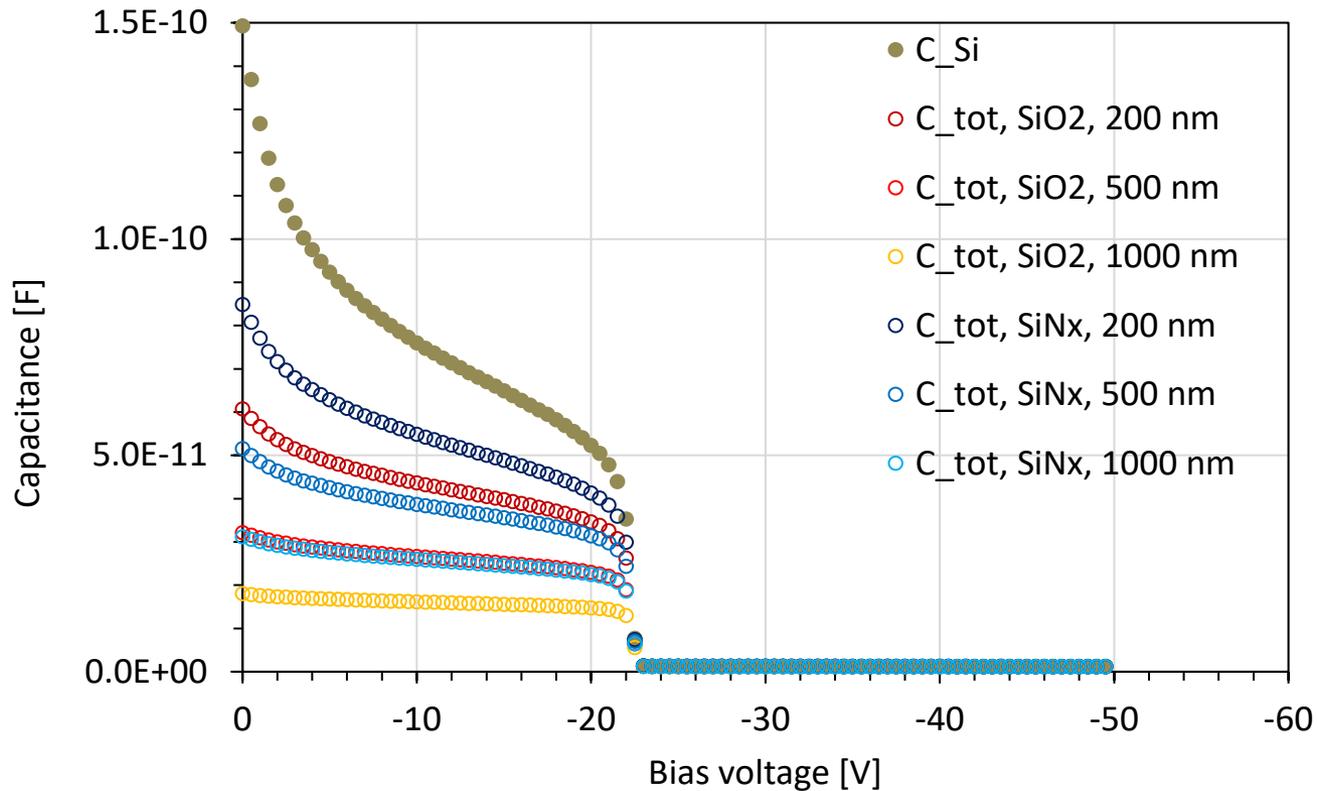
wafer	<i>n</i> -plus dose	<i>p</i> -gain dose	dielectric thickness	<i>p</i> -stop dose	substrate	Vbd
1	A	0.92	L	B	Si-Si	480
2	A	0.94	L	A	Si-Si	440
3	A	0.94	L	B	Epi	460
4	A	0.94	H	B	Si-Si	440
6	B	0.92	L	B	Epi	525
7	B	0.94	L	A	Si-Si	460
8	B	0.94	L	B	Si-Si	460
10	B	0.96	H	B	Si-Si	430
11	C	0.92	L	B	Si-Si	515
12	C	0.94	L	B	Epi	490
13	C	0.94	L	B	Si-Si	465
15	C	0.96	H	C	Si-Si	445



# Silicon and dielectric capacitance

Calculation of the total capacitance from the silicon capacitance and some potential thicknesses for two different materials:

- Dielectric capacitance is more significant before full depletion





# Z - $\theta$

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## DC configuration

$\theta$  ca.  $-89^\circ$  when the maximal value for a Cp-Rp model is  $-90^\circ$

## AC configuration

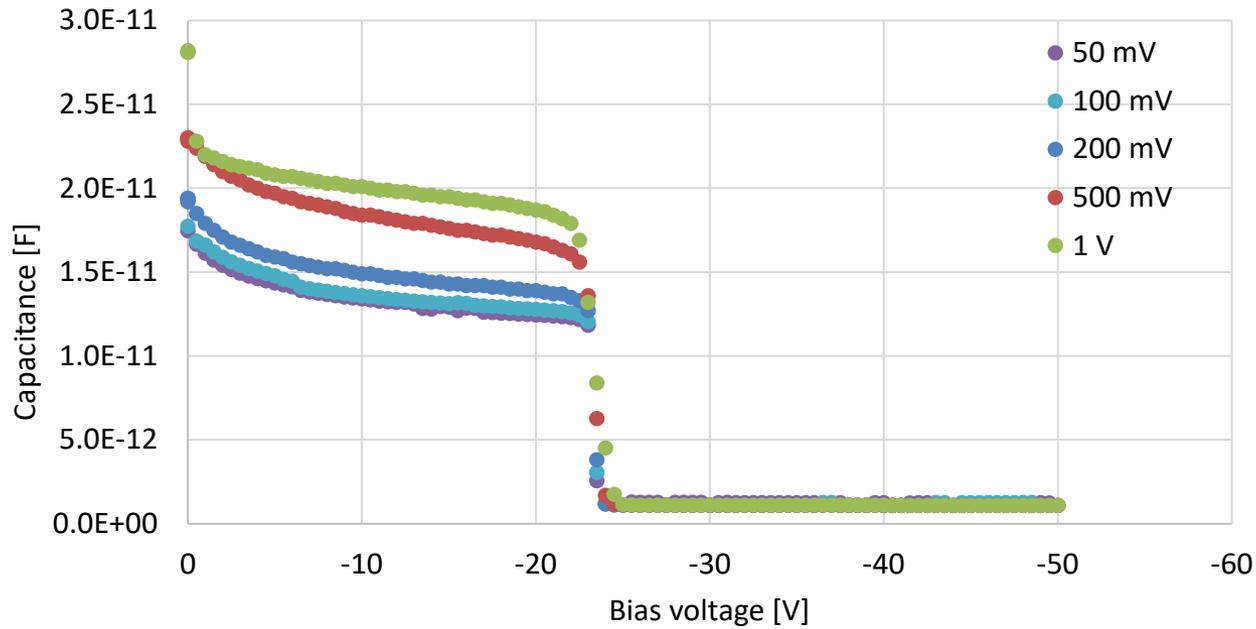
$\theta$  increases significantly with frequency:

$-92^\circ$  at 1 MHz,  $-103^\circ$  for 100 kHz,  $-160^\circ$  at 10 kHz

- this is seen as negative Rp
- Frequency dependence is clearly observed, although translation into Cp may not be a valid model



# LCR meter AC signal amplitude



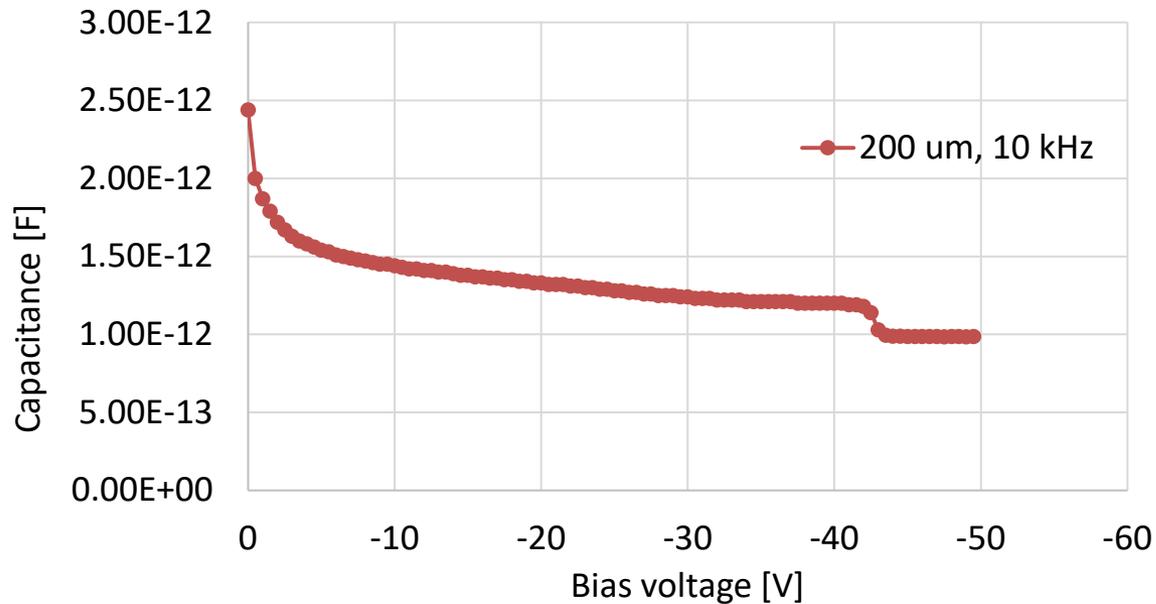
W3, thin dielectric, relative  $n^+$  dose 0.05. At 100 kHz



# Erroneous measurements

Relatively common observations in the AC measurement configuration, if contact to  $n^+$  is not good:

- Knee appears at  $> 40V$ , instead of ca. 23 V
- Final capacitance is closer to the value of the full  $n^+$  area than the metal pad



*W3, thin dielectric, relative  $n^+$  dose 0.05*

