

Collected charge, gain and jitter measurements of unirradiated LGADs from Teledyne e2v

39th RD50 Workshop, 18th November 2021

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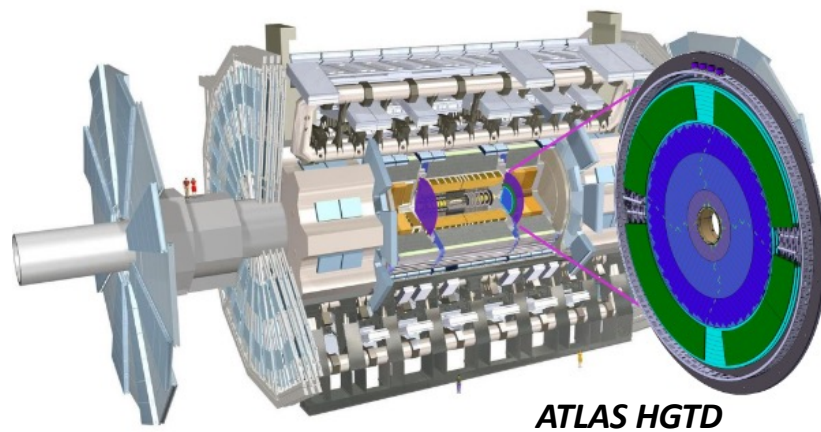


TELEDYNE e2v
Everywhereyoulook™

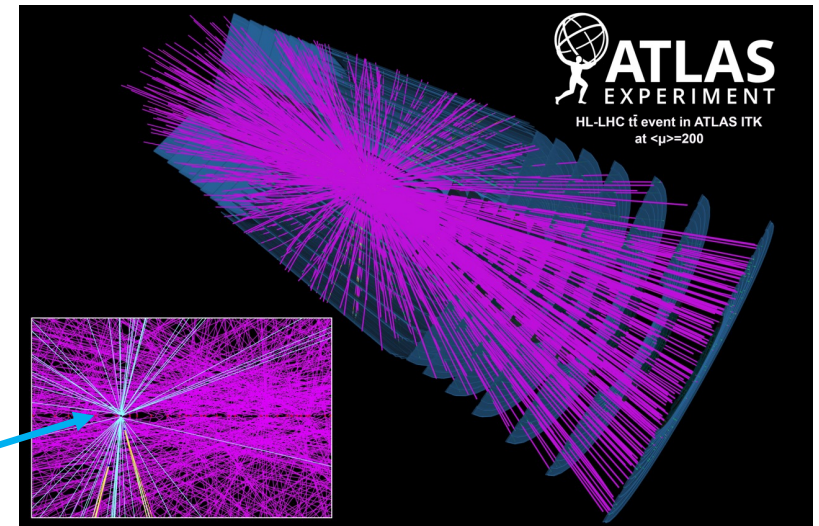
Outline

- Introduction: Ultra Fast Silicon Detectors
- Project overview: LGADs manufactured by Teledyne e2v
- Amplifier SPICE simulation
- Collected charge measurements
- Gain measurements
- Jitter measurements
- Future plans
- Summary

The need for Ultra Fast Silicon Detectors



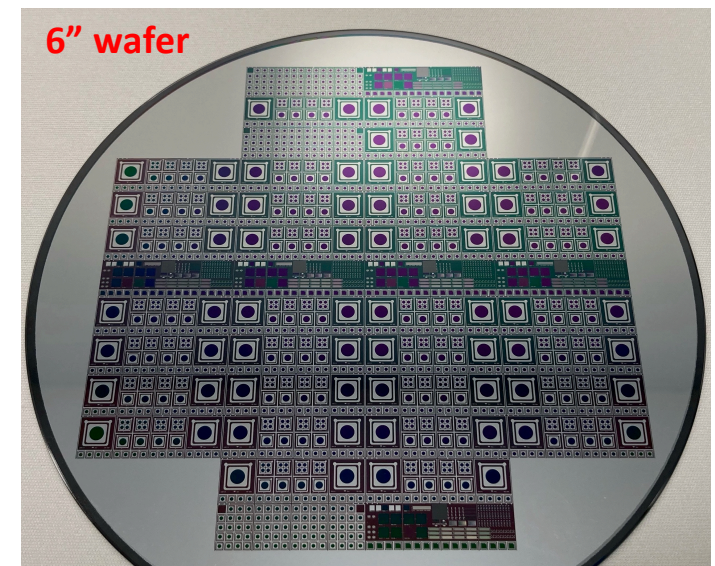
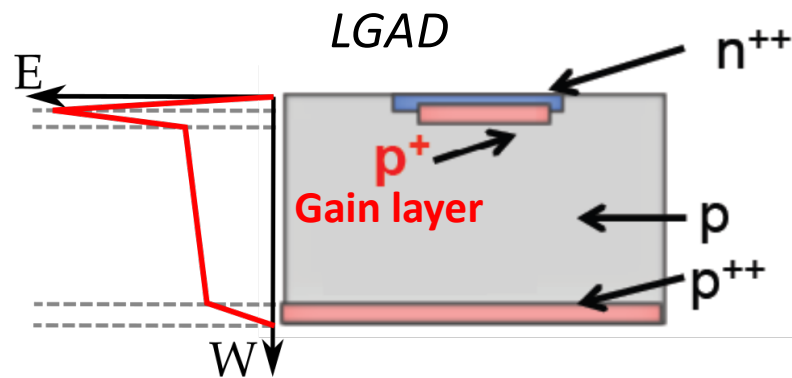
*1 pp interaction
amongst 200*



- Pile-up is one of the major challenges for tracking at the HL-LHC
- Timing information used to disentangle overlapping events
- ATLAS High-Granularity Timing Detector placed outside the ITk

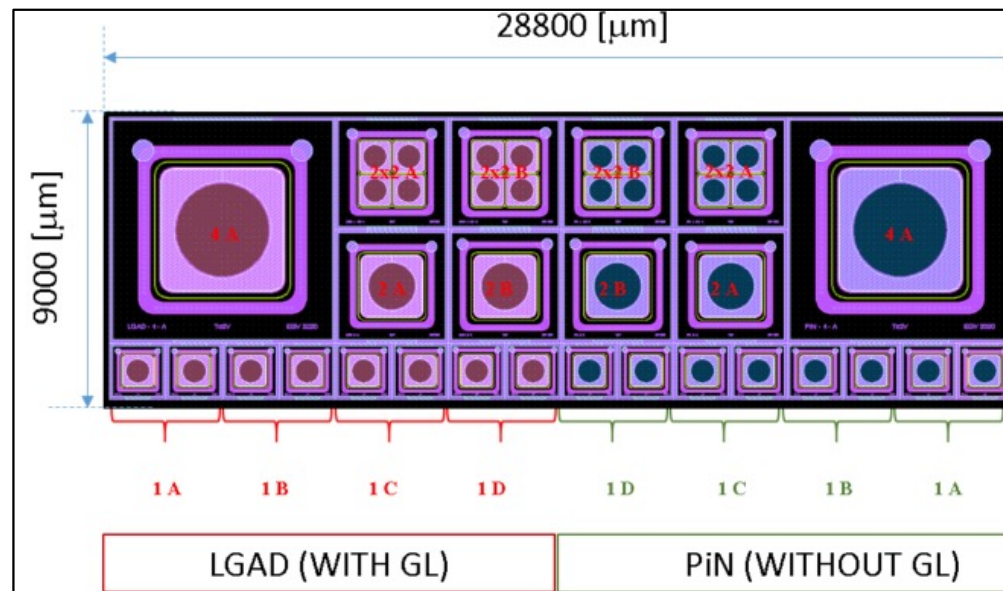
Teledyne e2v LGAD project

- LGAD: Low Gain Avalanche Detector
- Targeting track timing resolution of approx. 30-50 ps over detector lifetime
 - Time resolution benefits from high slew rate -> increased by introducing internal gain
 - Impact ionization in gain layer -> boron implantation (p^+)
- Pre-manufacture simulation done in TCAD
- University of Oxford, University of Birmingham, Open University, Rutherford Appleton Laboratory



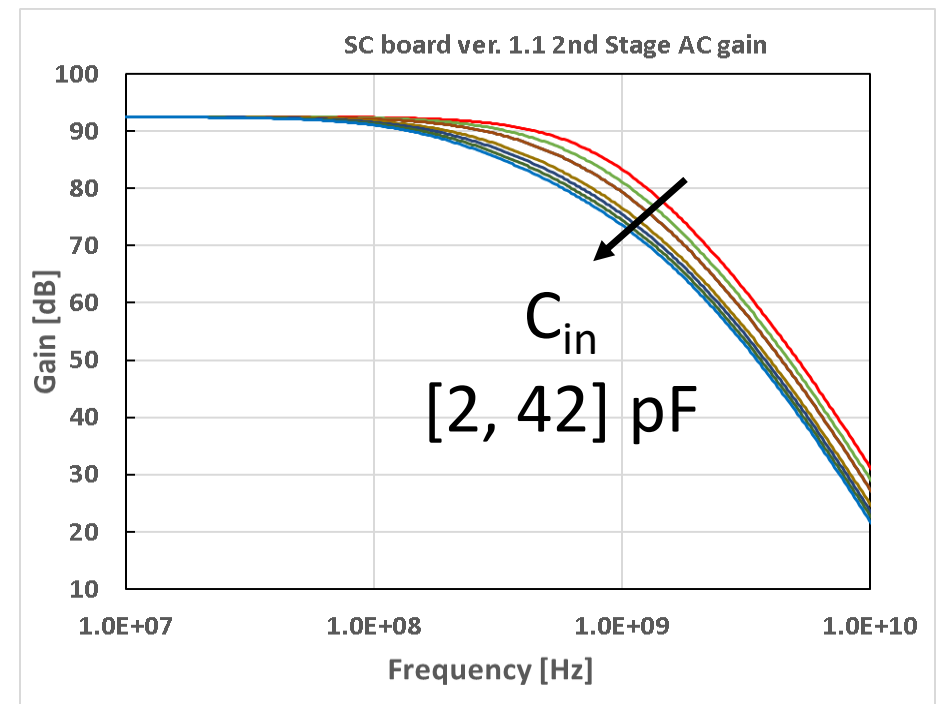
Teledyne e2v LGAD project

- Epitaxial layer: 50 μm thick, high resistivity
- 8 different combinations of manufacturing parameters (only 3 shown below)
- Each field contains LGADs and PiN diodes of the same layout (4 mm, 2 mm, 1 mm)



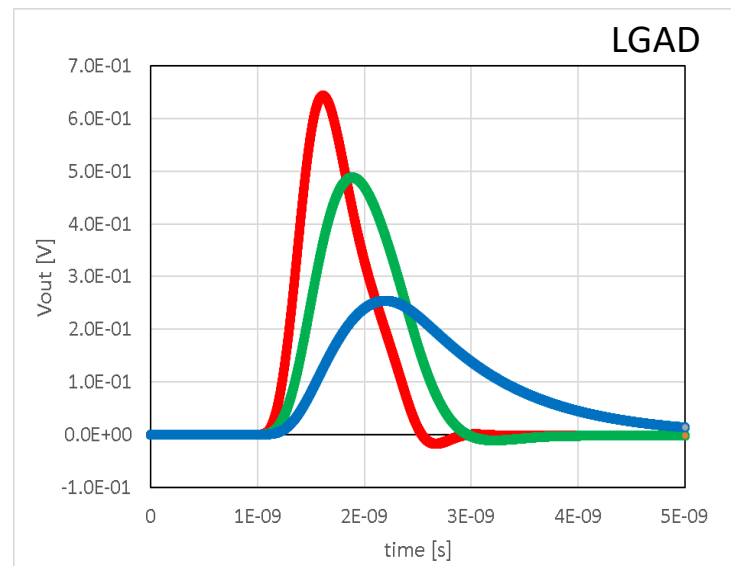
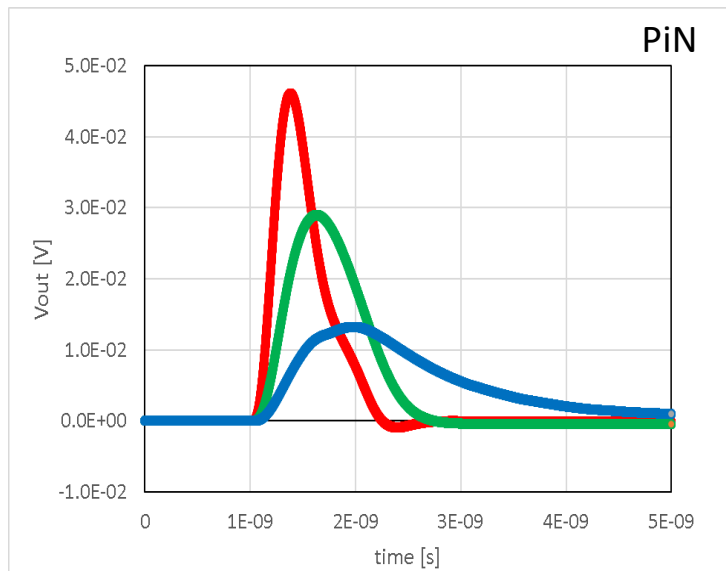
Charge gain measurement - amplification

- *First stage amplifier:*
Santa Cruz Readout v1.1
- *Second stage amplifier:*
FEMTO HSA-X-2-40, 40 dB – 2GHz
- Impedance matched to 50 Ohm
- The combined effect of the chain of amplifiers simulated in SPICE
 - Estimate the gain of the chain
 - Gain: 92.5 dB or 42,170 for 1mm devices with 2 pF capacitance
- Temperature is set to 25°C



SPICE – Transient current simulation of MIP signal

1st and 2nd stage amp. combined



Input capacitance:

1 mm \approx 2 pF

2 mm \approx 11 pF

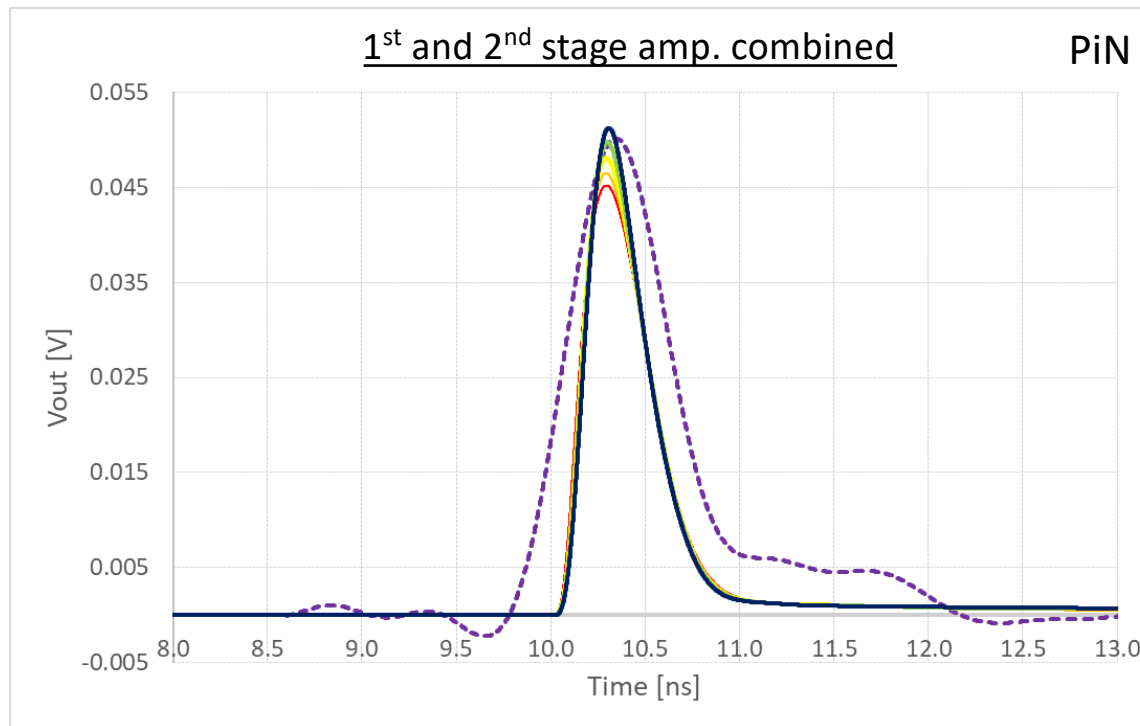
4 mm \approx 42 pF

PiN signal: assuming saturated carrier velocity, peak current 1.5 μ A
with e^- collection time 300 ps, h^+ collection time 1 ns

LGAD signal: peak current 15 μ A (10x of PIN signal)

SPICE – Transient current simulation

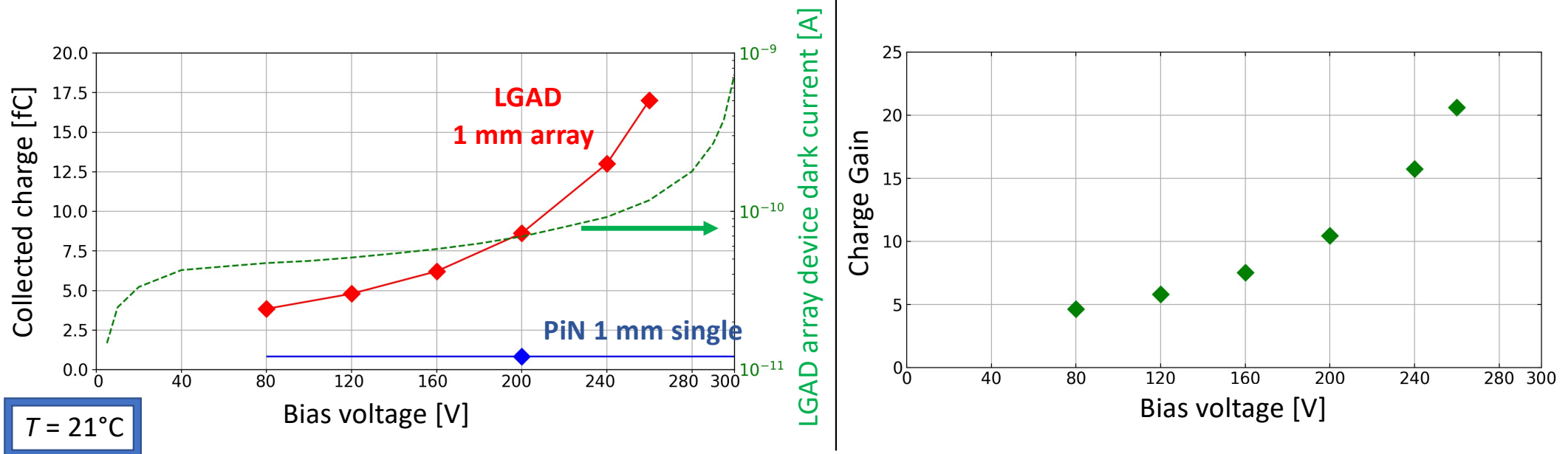
- PiN signal from TCAD simulation, input capacitance $C_{in} = 2 \text{ pF}$
- Calibration of the laser to inject MIP-like amount of charge



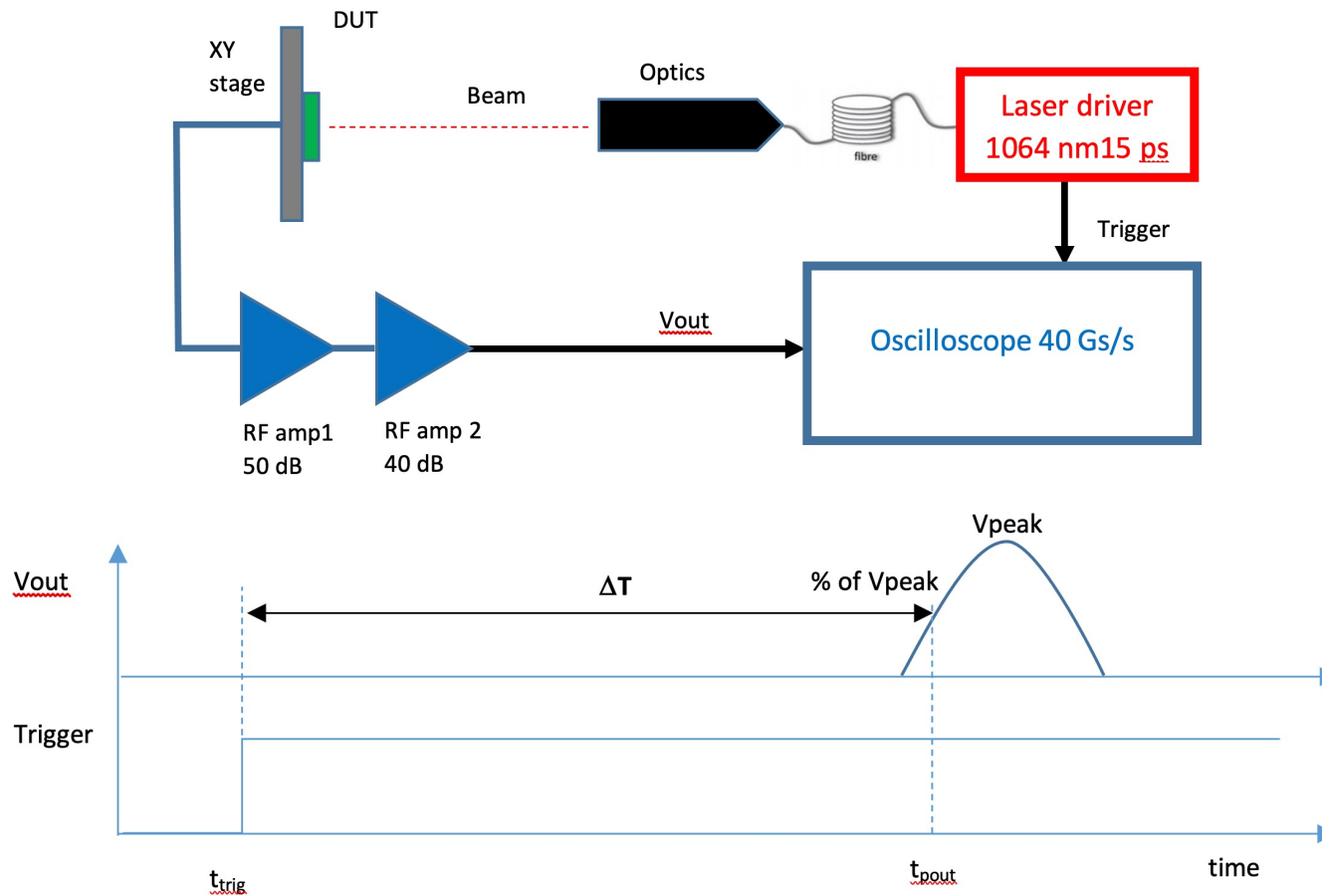
$T = 21^\circ\text{C}$

Charge collected and gain measurements – 1mm

- Conversion from the amplifier output to collected charge by estimating the gain of the chain of amplifiers from a SPICE simulation (92.5 dB or 42,170 for C_{in} of 2 pF – assumed constant up to 1.5 GHz)
- The charge gain - the ratio of the charge collected by LGAD and PiN

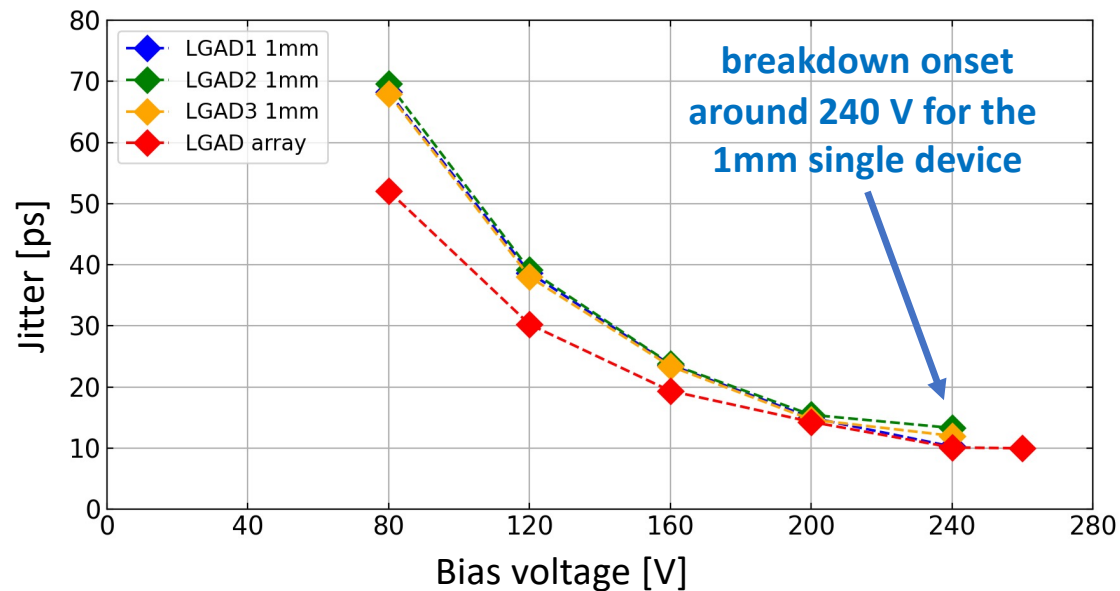


Jitter measurements - setup



Jitter measurements – 1mm LGAD (single and array)

- Jitter - the spread (standard deviation) of time delay between 50 % of trigger signal amplitude and 50 % of LGAD signal amplitude
- Low pass filter applied at 1 GHz – no substantial change to the signal
- Unirradiated device; no subtraction of other contributions



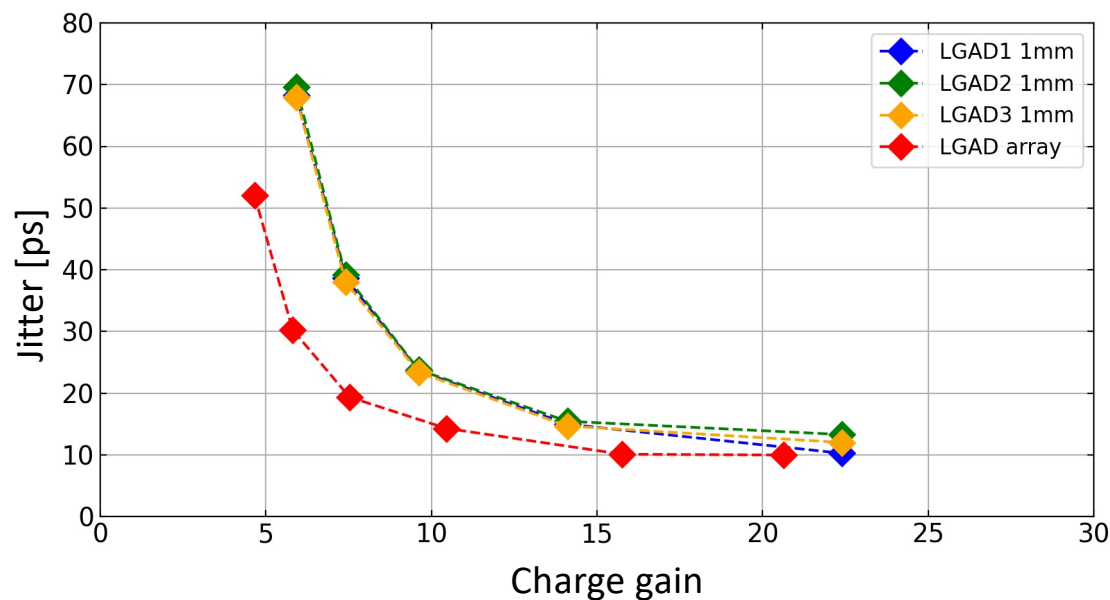
Other contribution
not subtracted (estimates)

Trigger jitter: $\sigma_{Trigger} \approx 1.5 \text{ ps}$
Laser pulse: $\sigma_{Laser} \approx 3.1 \text{ ps}$
SC amplifier: $\sigma_{Amp1} \approx 7.4 \text{ ps}$

$T = 21^\circ\text{C}$

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Timing Measurement uncertainties

$$\sigma_{\Delta t}^2 = \sigma_{trig}^2 + \sigma_{Laser}^2 + \sigma_{DUT}^2 + \underbrace{\sigma_{Amp1}^2 + \sigma_{Amp2}^2}_{\text{Jitter of the amplifiers}} + \sigma_{TW}^2 + \sigma_{TDC}^2$$

Jitter term of trigger output

Jitter term due to the laser pulse fluctuations

Intrinsic jitter of the DUT (+ distortion and Landau)

Jitter of the amplifiers

Time-walk term

Time quantization noise of the scope

Timing Measurement uncertainties

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Negligible according to the data sheet

Jitter term of trigger output

$\approx (1.5 \text{ ps})^2$

Jitter term due to the laser pulse fluctuations

$\approx (3.1 \text{ ps})^2$

Intrinsic jitter of the DUT (+ distortion and Landau)

Negligible

- Firing on the same spot
- Using a monochromatic laser

Jitter of the amplifiers

Time-walk term

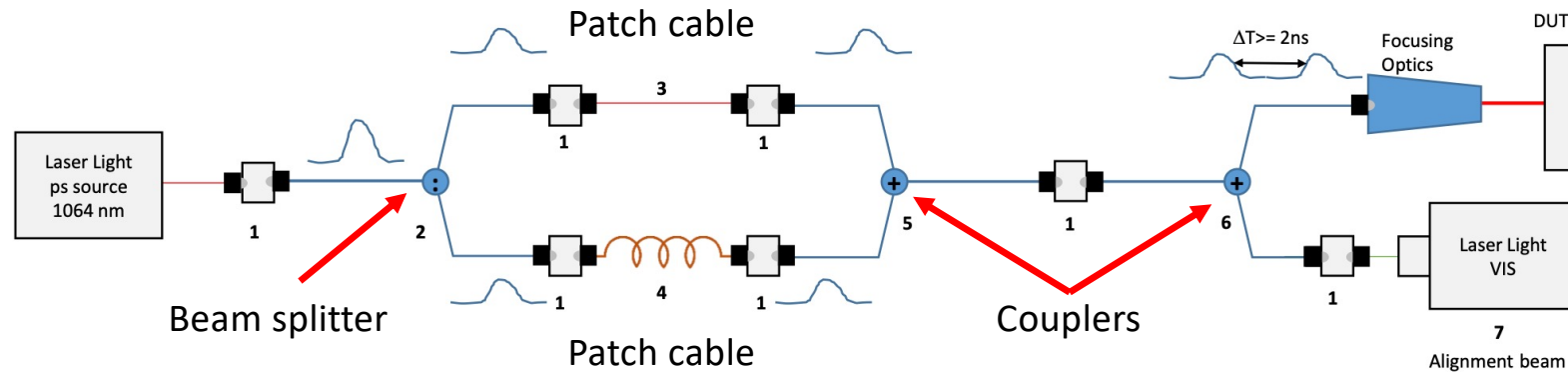
Time quantization noise of the scope

First stage $\approx (7.4 \text{ ps})^2$

Second stage negligible

Future tests

- Jitter measurements – elimination of the laser trigger component



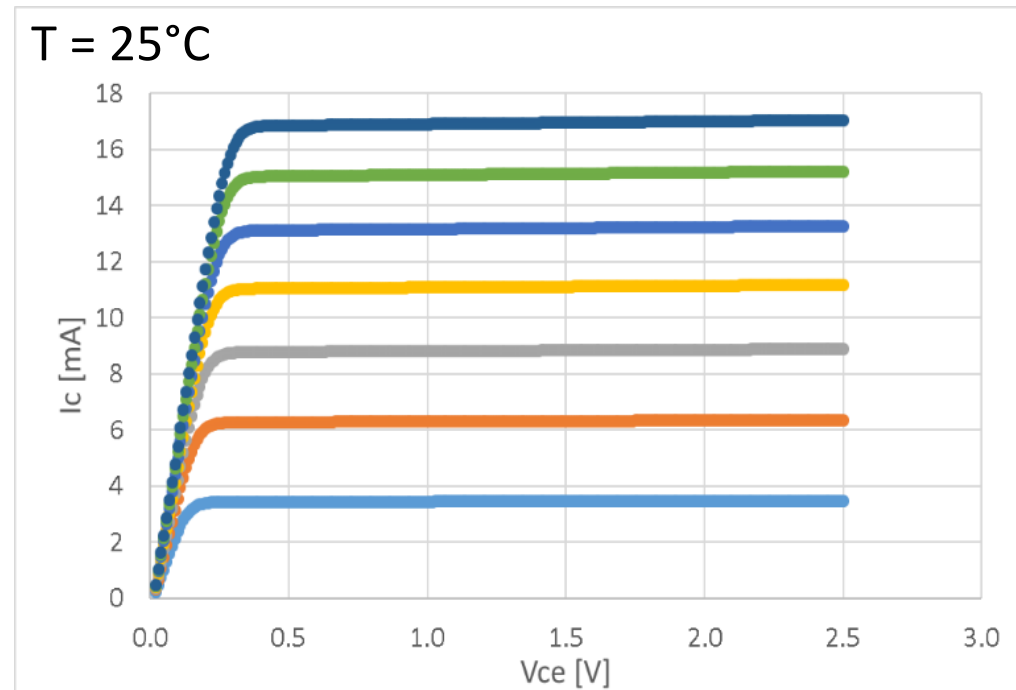
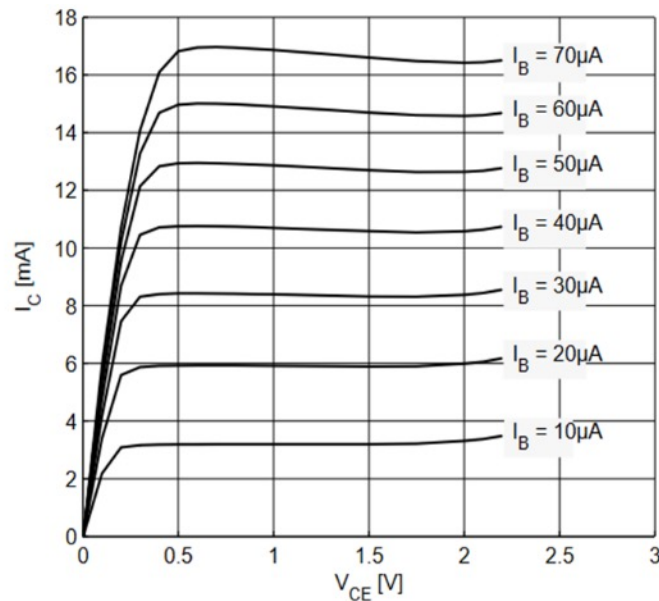
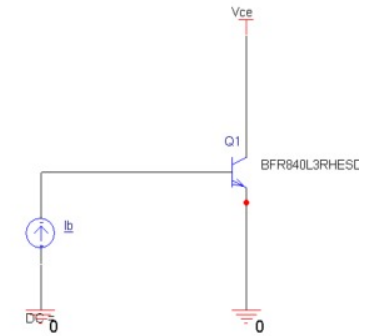
- Test with the other produced wafers – variation of implant dose and energy
- Irradiation of the devices

Summary

- Response of PiN and LGAD unirradiated devices simulated in SPICE
- Gain of the chain of amplifiers determined: 92.5 dB or 42,170
- Charge collection shows >15 fC charge collected for 1mm LGAD array device biased at >240 V (for unirradiated devices)
- 1mm LGAD array devices show jitter of <20 ps for bias >160 V
- Future improvements of laser optics setup should allow to refine jitter measurements – remove contributions from trigger and laser jitter

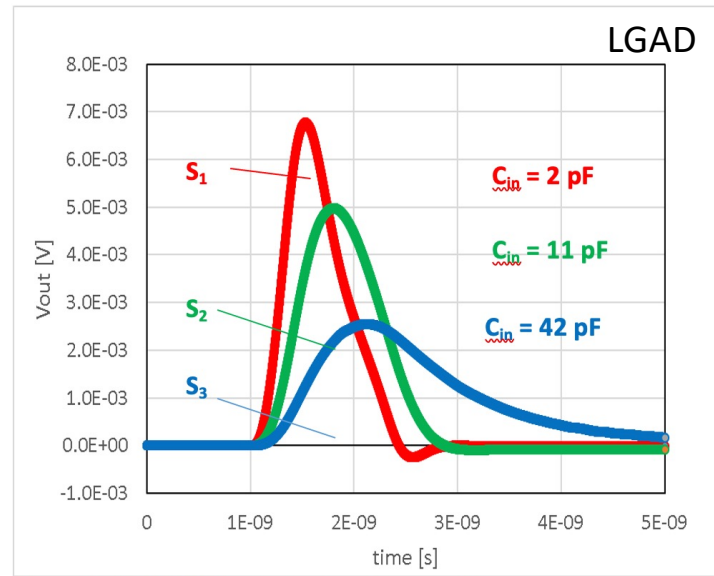
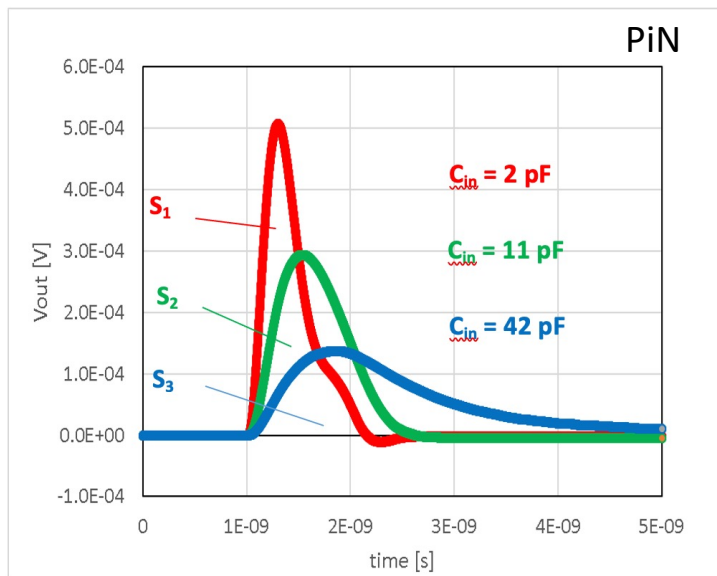
SPICE – DC Simulation of the SiGe NPN

- SiGe NPN BFR840L3RHESD (Infineon)
- Compare SPICE predictions with typical DC curves reported in the design sheet



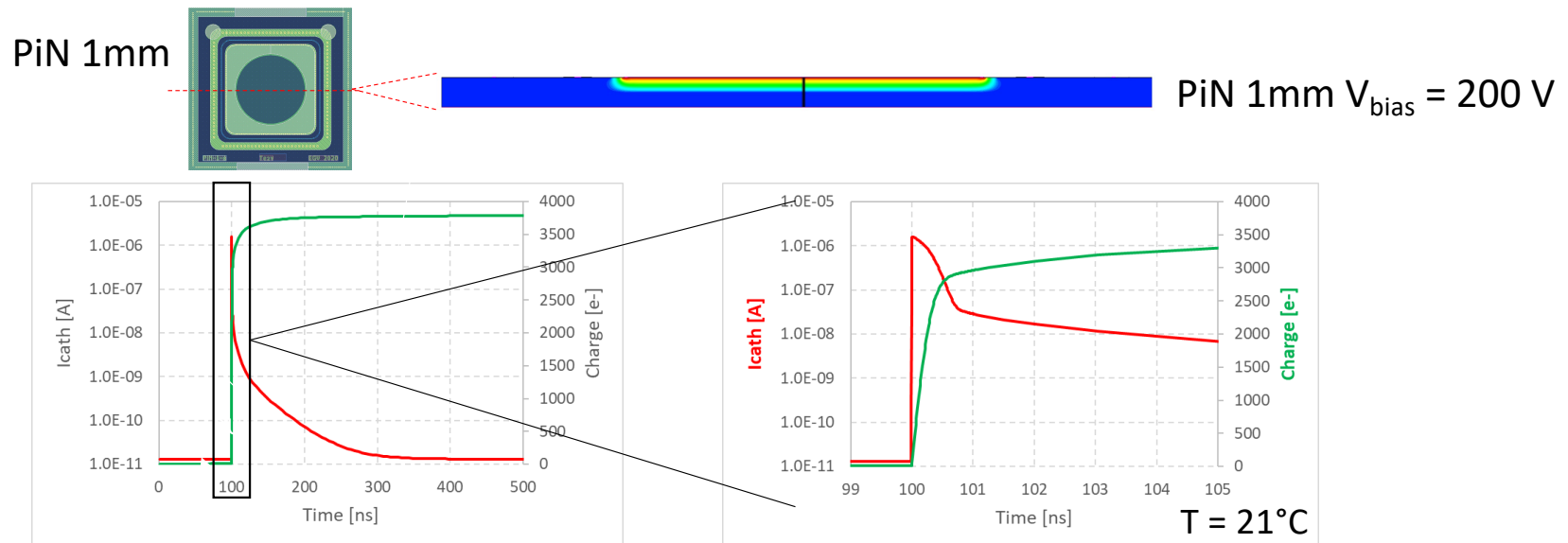
SPICE – Transient current simulation

1st stage only



1 mm \approx 2 pF
2 mm \approx 11 pF
4 mm \approx 42 pF

TCAD simulation for PiN(MIP)

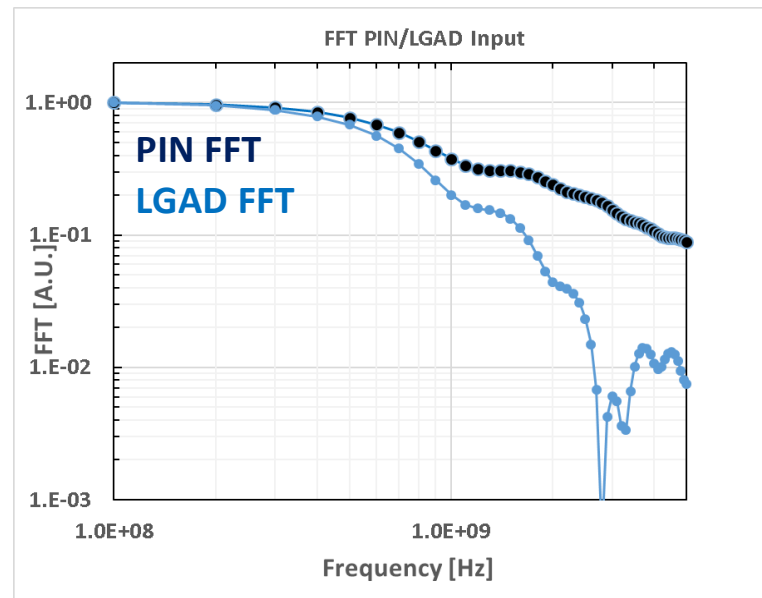


MIP transient current and collected charge for PiN diode at $V_{\text{bias}} = 200 \text{ V}$

- MIP : MPV [300 μm] $\sim 72 \text{ e/h pair}/\mu\text{m}$
- Central hit
- Time resolution [$t_0, t_0+1\text{ns}$] : 100 fs
- Implement the current waveform [$t_0, t_0 + 5 \text{ ns}$] into SPICE simulation of RF amplifier
- TCAD estimated collected charge at 5 ns = 3303 e^- (eqv. 0.53 [fC])

Normalized PiN and LGAD (MIP) FFT of current signal

- Comparison the FFT of the PiN and LGAD signals, normalized to their maximum magnitude



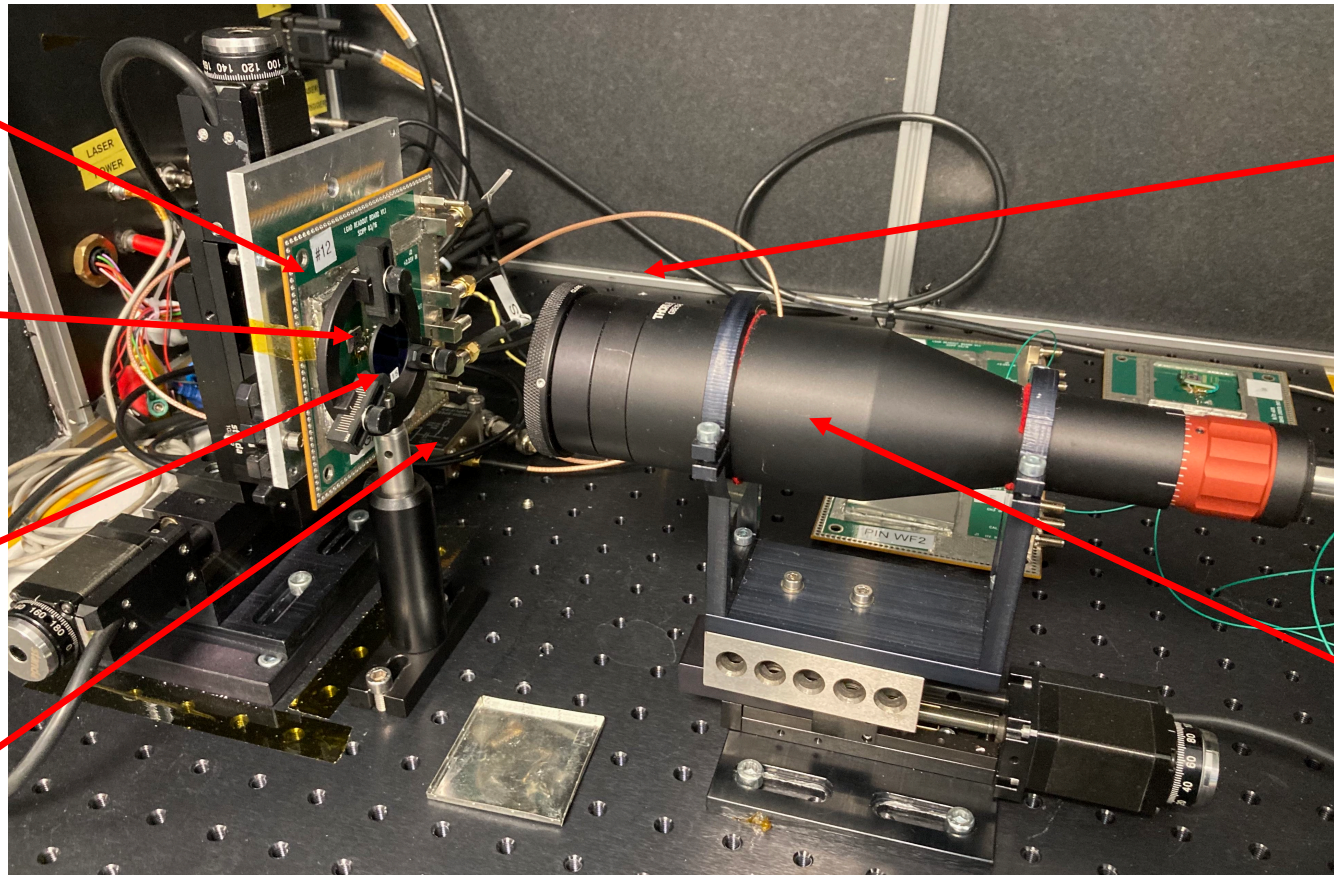
Charge collection and jitter - laser setup

Santa Cruz v1.1
(1st stage amp)

LGAD/PiN
device

ND filter

FEMTO 40dB
(2nd stage amp)



QD Laser
1064 nm
(behind)

Laser Optics

1mm LGAD array signal – 240 V bias

