X-band novel open cavity for SLED-type rf pulse compressors

Xiaowei Wu (wuxw@zjlab.ac.cn), Shanghai Synchrotron Radiation Facility (SSRF) Alexej Grudiev, CERN

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Outline

- 1. Overview of existing pulse compressors
- 2. Introduction to bowl-shape open cavity
- 3. Correction cavity design
- 4. Storage cavity design
- 5. Conclusion and future work

Overview of X-band passive pulse compressors

SLED-type pulse compressors with resonant cavities



SLEDII type pulse compressor with delay lines



SLEDII type pulse compressors in my eyes

SLED-type pulse compressors with resonant cavities



SLEDII type pulse compressor with delay lines





Flat-top in the compressed pulse

Very long delay lines for long compressed pulse width

SLED-type pulse compressors in my eyes



Spherical cavity



1. 2014 (M)
 2. 2014

Very compact (\checkmark) Relatively easy fabrication

Relatively low Q \otimes Dense mode spectrum



Compact (\checkmark)

High magnetic field at coupling iris (\mathbf{X}) Many pieces for assembling

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Novel bowl-shape open cavity

SLED-type resonant cavity working at $TE_{1,2,i}$ rotating quasi-spherical mode

index i depends on the radius of the cavity (R_{cav})

High quality factor with compact size

 $Q_0 \sim 240000$ in $TE_{1,2,13}$ mode with R_{cav} =16.5 cm

Open boundary at the top the cavity

low field at the top area, connect to stainless steel flange (open boundary) and used for vacuum pumping

suppress many parasitic modes

Bowl shape symmetric geometry

machining by lathe with high accuracy and low cost no brazing needed for the cavity fabrication





Requirement from CLIC rf pulse compression system

Firstly studied for CLIC rf pulse compression system [1] Can also be applied to other pulse compression systems



		Correction cavity	Storage cavity	
Required Q_0 60000 240000	Required Q_0	60000	240000	

6 correction cavities + 1 storage cavity



Requirement from CLIC rf pulse compression system

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	Correction cavity	Storage cavity
Required Q_0	60000	240000
Mode selection	TE _{1,2,4}	TE _{1,2,13}
Mode Q ₀	~74000	~240000



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Mode spectrum of correction cavity



Chose *R*_{arc}=300 mm

large frequency (>200 MHz) separation from parasitic modes

high Q for working mode





Coupling iris design for correction cavity

Optimize R_{iris} and DZ_{iris}

43000.00

42000.00

41000.00

 ${\overset{40000.00}{\overset{-}{5}}}_{39000.00}$

38000.00

37000.00

36000.00 | 0.40

0.60

0.80

get required Q_{ext} and minimize the loss in stainless steel ensure the open boundary

Curve Info

Q(1) 1mode : LastAdaptive

1.60

1.80

Q_{ext}



1.00 1.20 \$DZiris [mm] 1.40

Correction cavity design

TE_{1,2,4} rotating mode



Correction cavity with E-rotator



E-rotator converts $TE_{1,0}$ rectangular waveguide mode to $TE_{1,1}$ circular waveguide mode and excites $TE_{1,2,4}$ rotating mode in the open cavity



E-field in logarithmic scale

Limitation study

Coupling iris could be a critical area with high field

Check the rf parameters at 50 MW, 2.25 µs input power in steady-state

Results shows low field due to detuning





Tolerance study

Key dimensions are checked for tolerance study

Frequency shifts of work mode and parasitic mode are relatively small (0.01 mm $R_{cav} \rightarrow 2.38$ MHz)

Coupling factor and more dimension study will be carried out in future





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Mode spectrum of storage cavity

Work at $TE_{1,2,13}$ mode

Chose *R*_{arc}=460 mm

- denser spectrum than correction cavity
- relatively large frequency (~40 MHz) separation from parasitic modes
- high Q for working mode





Storage cavity design

Work at $TE_{1,2,13}$ mode DZ_{cav} =170 mm, R_{arc} =460 mm

	Work mode	Parasitic Mode1	Parasitic Mode2	Parasitic Mode3	Parasitic Mode4
Frequency [GHz]	12.0000	11.9636	11.9651	12.0454	12.0556
Q ₀	249658	30716.8	47116.8	62083.3	120104





Storage cavity design



 S_{11} sweep of TE_{1,2,13}

m2

Name

m1

m2

m3

0.00

-2.00

-4.00

-6.00

-8.00

-10.00

11.95

m1

 S_{11} [dB]







11.9635 -6.0737

11.9940 -2.8403

12.0399 -6.0009

<mark>ф</mark>З

Storage cavity with E-rotator

E-rotator converts $TE_{1,0}$ rectangular waveguide mode to $TE_{1,1}$ circular waveguide mode and excites $TE_{1,2,13}$ rotating mode in the open cavity



Phase = 0deg

Pulse shape check

The influence to the pulse shape of the parasitic modes are checked



Limitation study

Check the rf parameters at 50 MW, 2.25 µs input power in steady-state

High magnetic field is seen at the coupling iris (Max T rise around 94 K)

[1] reports stable operation of similar coupling iris at T rise of 658 K

High power test is needed to verify the performance



 Frequency [GHz]
 11.994

 Max E [MV/m]
 97.79

 Max H [kA/m]
 577.0

 S_c [MW/mm²]
 2.46



[1] Y. Jiang, H. Zha, J. Shi, M. Peng, X. Lin and H. Chen, "A Compact X-Band Microwave Pulse Compressor Using a Corrugated Cylindrical Cavity," in *IEEE Transactions on Microwave Theory and Techniques*, vol. 69, no. 3, pp. 1586-1593, March 2021, doi: 10.1109/TMTT.2021.3053913.

Tolerance study

Key dimensions are checked for tolerance study

Frequency shifts of work mode and parasitic mode are very small (0.01 mm $R_{cav} \rightarrow 0.07$ MHz)

Coupling factor and more dimension study will be carried **/** out in future





Dimension	$\Delta f / \Delta x \ [MHz/mm]$			
Dimension	Work mode	Parasitic mode1	Parasitic mode2	
R _{cav}	-72.66	-24.41	-34.07	
DZ _{cav}	<±1.00	-45.50	-37.64	
R _{arc}	<±1.00	<±1.00	<±1.00	
R _{iris}	<±1.00	-2.44	<±1.00	

5/19/2022

Preliminary mechanical design of the storage cavity

First design from the workshop



Cooling system





Static structure analysis

Apply 0.1 MPa from outside atmospheric pressure Apply 0.3 MPa water pressure between cavity and the cooling jacket between bottom and spiral cooling slot



Static structure analysis

Maximum deformation of 0.004 mm when bottom thickness is 17 mm



Further study on mechanical design is ongoing

Working on adopting BOC mechanical design Iris shape optimization Copper thickness optimization







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A bowl-shape open cavity working at $TE_{1,2,i}$ rotating mode is proposed

TE_{1,2,4} mode with Q~74000 has been studied for CLIC correction cavity

TE_{1,2,13} mode with Q~240000 has been studied for CLIC storage cavity

Tolerance study shows promising results for fabrication

Mechanical design has been started

More details...

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Novel open cavity design for rotating mode rf pulse compressors

Xiaowei Wu[®]^{*} and Alexej Grudiev

European Organization for Nuclear Research (CERN), 1211 Geneva 23, Switzerland

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A new X-band high-power rotating mode SLAC energy doubler (SLED)-type rf pulse compressor is proposed. It is based on a novel cavity type, a single open bowl-shaped energy storage cavity with highquality factor and compact size, which is coupled to the waveguide using a compact rotating mode launcher. The novel cavity type is applied to the rf pulse compression system of the main linac rf module of the klystron-based option of the Compact Linear Collider. Quasispherical rotating modes of $TE_{1,2,4}$ and $TE_{1,2,13}$ are proposed for the correction cavity and storage cavity of the rf pulse compression system, respectively. The storage cavity working at $TE_{1,2,13}$ has a quality factor above 240 000 and a diameter less than 33 cm. The design of the pulse compressor and in particular of the high-Q cavity will be presented in detail.

DOI: 10.1103/PhysRevAccelBeams.24.112001

https://journals.aps.org/prab/abstract/10.1103/PhysRevAccelBeams.24.112001

SLED-type pulse compressors in my eyes







Corrugated cavity



 (\checkmark) Compact

High magnetic field at coupling iris (\mathbf{X}) Many pieces for assembling

Future work

X-band bowl-shape open cavity design

Parasitic modes suppression for storage cavity (absorption material?)

□ Coupling iris optimization to reduce surface field/pulse heating/...

X-band bowl-shape open cavity development for CLIC

- □ Finalize the mechanical design and fabrication
- Lower-power rf measurement and high-power test of the bowl-shape open cavity

C-band bowl-shape open cavity design is undergoing

Bowl-shape open cavity

Outpu

RF source



34

Future work

X-band bowl-shape open cavity design

in a to forward to fruitif

C-band bowl-shape open cavity design is undergoing

Bowl-shape open cavity





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