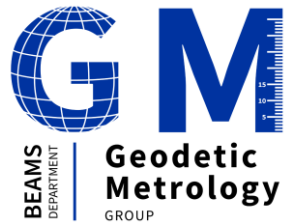




Frequency Scanning Interferometry for absolute measurements and its applications

M. Sosin, H. Mainaud-Durand, V. Rude, J. Rutkowski

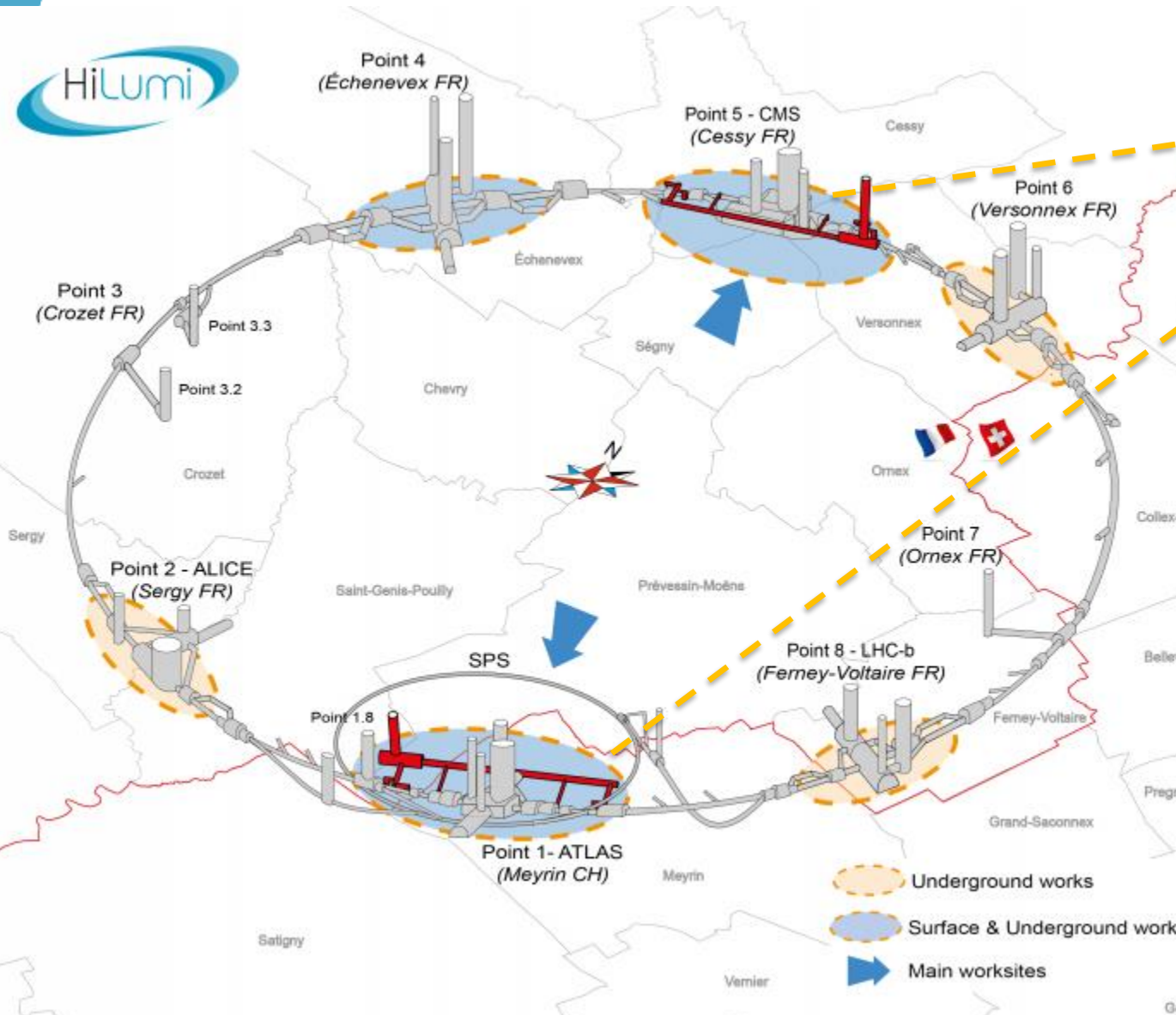


2nd PBC Technology Mini Workshop: Laser & Optics
10 December 2021

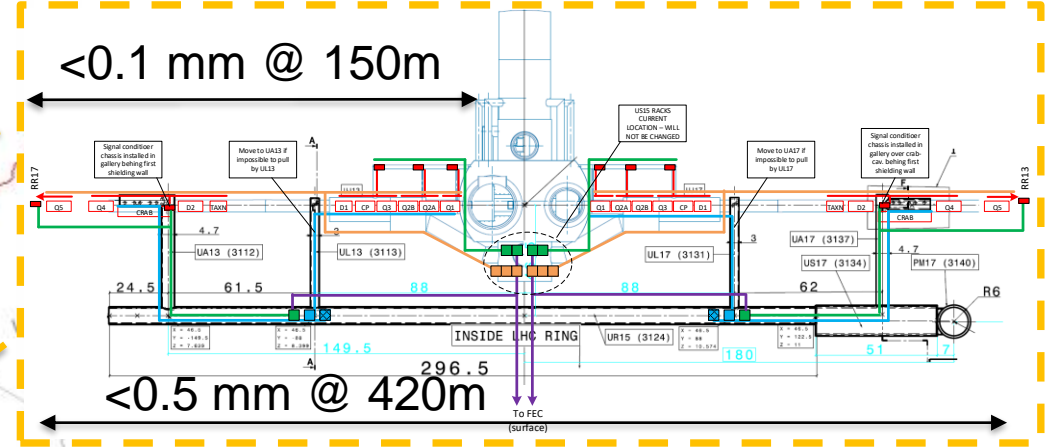
Outline

- High-Luminosity LHC (HL-LHC) and alignment systems
- Frequency Sweeping Interferometry (FSI) – classical approach
- First HL-LHC FSI applications
- Multi-target FSI (MT-FSI) as an alternative for robust measurements
- MT-FSI instrumentation examples
- Conclusions

CERN HL-LHC Upgrade and Alignment Monitoring Systems



P1 (ATLAS) & P5 (CMS) Long Straight Sections



Alignment of LSS components

- Vertical levelling of components (w.r.t. water surface)
- Radial alignment (stretched wire)
- Roll angle monitoring (inclinometers)
- Magnets longitudinal position monitoring
- Position monitoring of cold (nominal 2 .. 4 K) objects inside cryostats

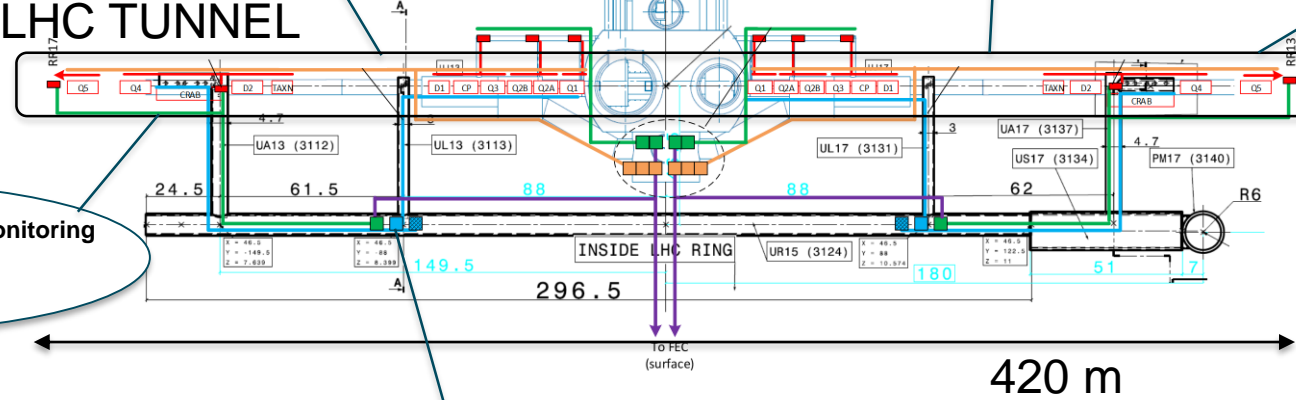
HL-LHC alignment monitoring and FSI

Internal monitoring cold components
(crab-cavities, inner triplets)
Nominal Temp.: 2 .. 4 K
320 x

Wire Position Sensor (X-Y position
measurement w.r.t. stretched,
conductive wire)
140 x

Hydrostatic levelling sensor
(humidity close to 100%)
120 x

TID ~1MGy
T=20..25 °C



Magnets longitudinal position monitoring
48 x

Inclinometer
70 x

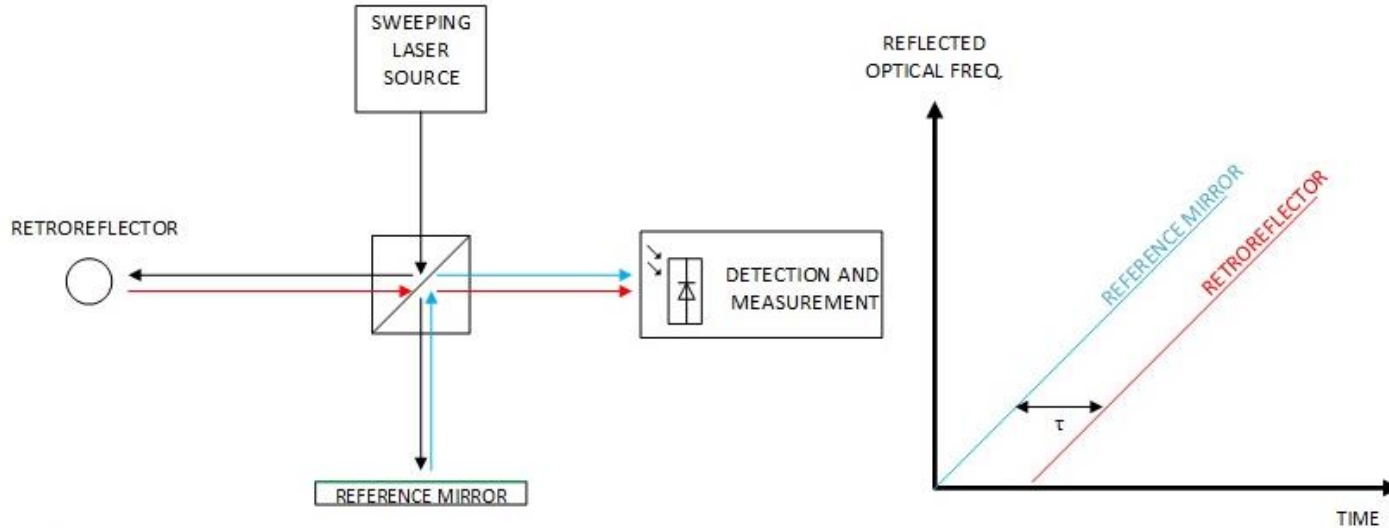
Interferometer
(radiation safe
location)

Why Frequency Sweeping Interferometry?

- Absolute distance measurement needed
- Measurement uncertainty (per ch) better than 10 μm / 10 μrad required
- Capacitive sensors very sensitive to dust and EM noise (replaced to optical ones where possible)
- Cabling and sensors cost need to be decreased
 - Big amount of channels, Large installation
- Simple and maintenance free systems needed (difficult access due to high radiation levels)



Introduction - Frequency Sweeping Interferometry



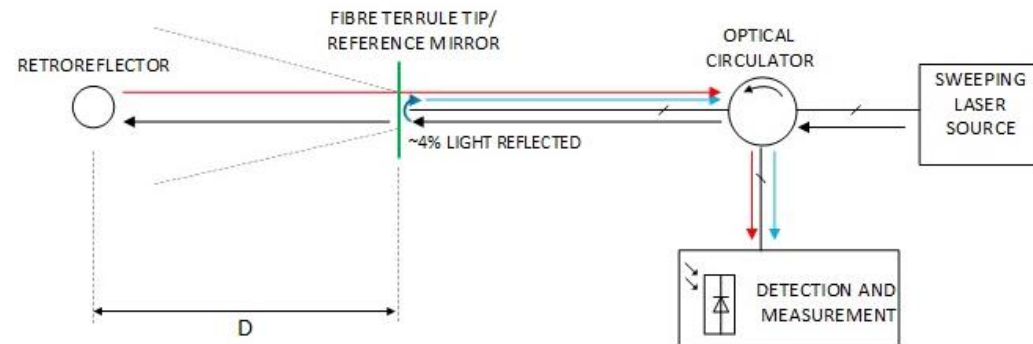
$$I(t, \tau) = A \cdot \cos[2\pi(\alpha \tau t + f_0 \tau)]$$

A – magnitude of the signal;

τ - is the time delay between the signals from the reflecting target and reference mirror arrival to photodetector;

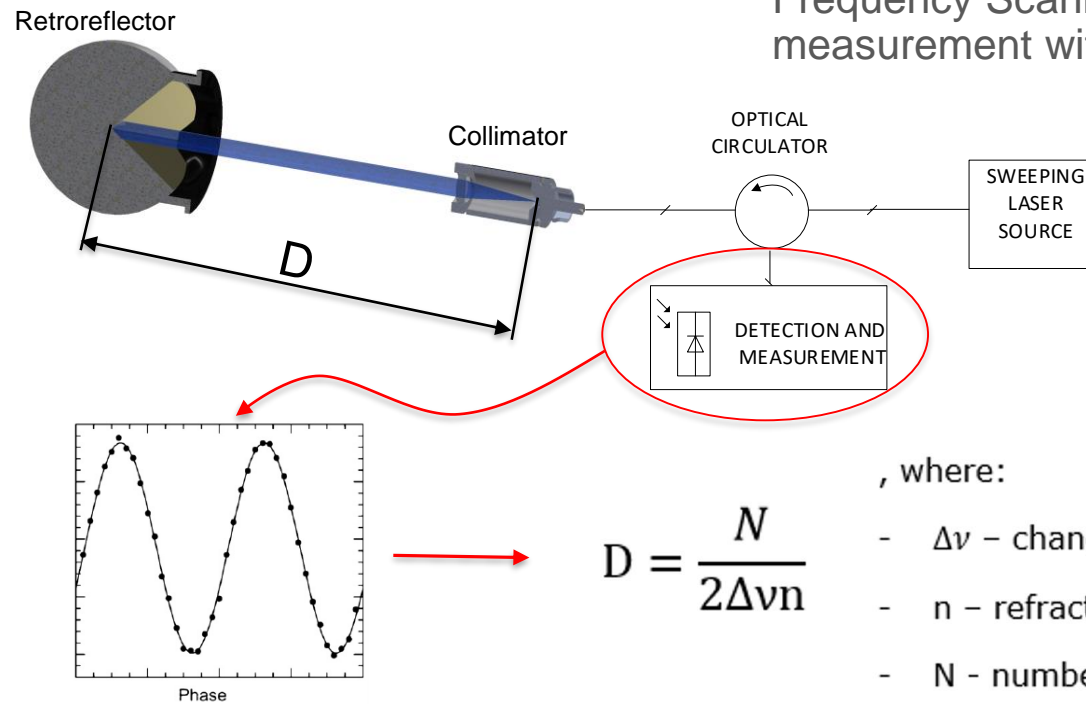
α – is a sweep rate of the laser ($\alpha = \frac{dv}{dt}$ - laser frequency change in time);

f_0 – is an optical frequency of the laser at the time t_0 .



Classical FSI

Frequency Scanning Interferometry allows for **absolute** distance measurement with μm uncertainty

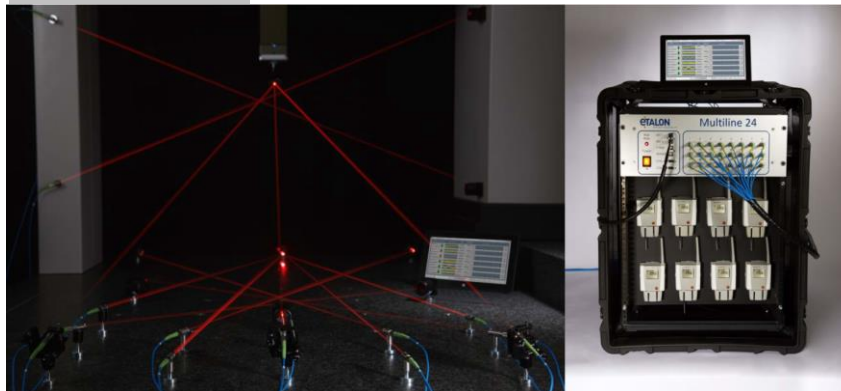


, where:

- $\Delta\nu$ – change of the laser frequency during sweep;
- n – refractive index of light transmission medium;
- N - number of cycles of signal measured during laser sweep;

$$D = \frac{N}{2\Delta\nu n}$$

ETALON[®]

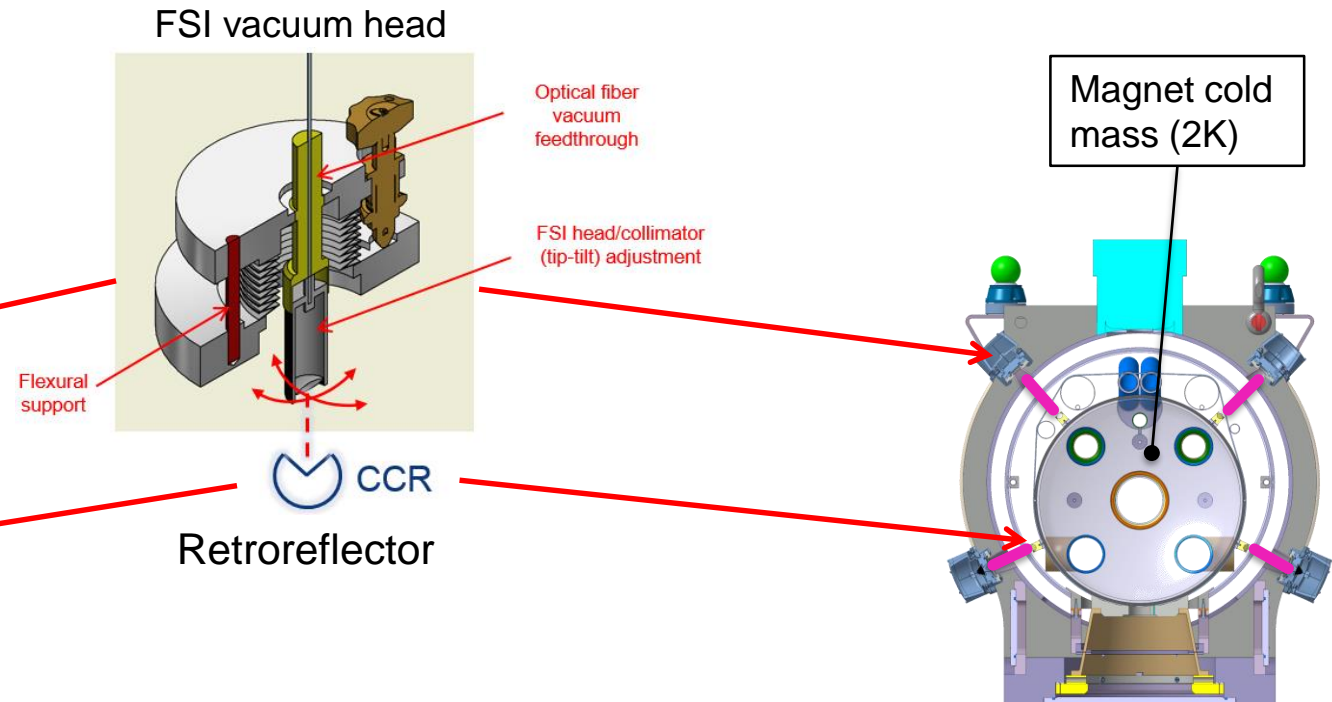
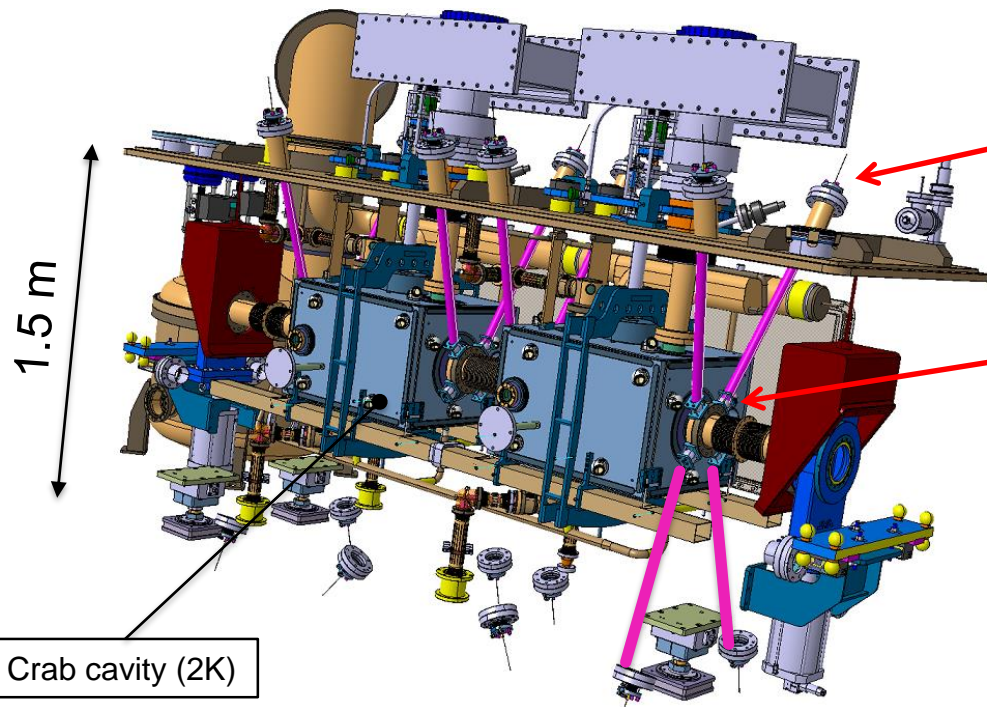


- Uncertainty (95%) = 0.5 $\mu\text{m}/\text{m}$
- Measurement distance: 0.2 – 20 m
- Double sweep laser – dynamic FSI
- Gas cell traceability

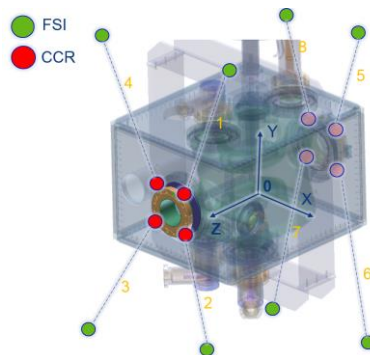
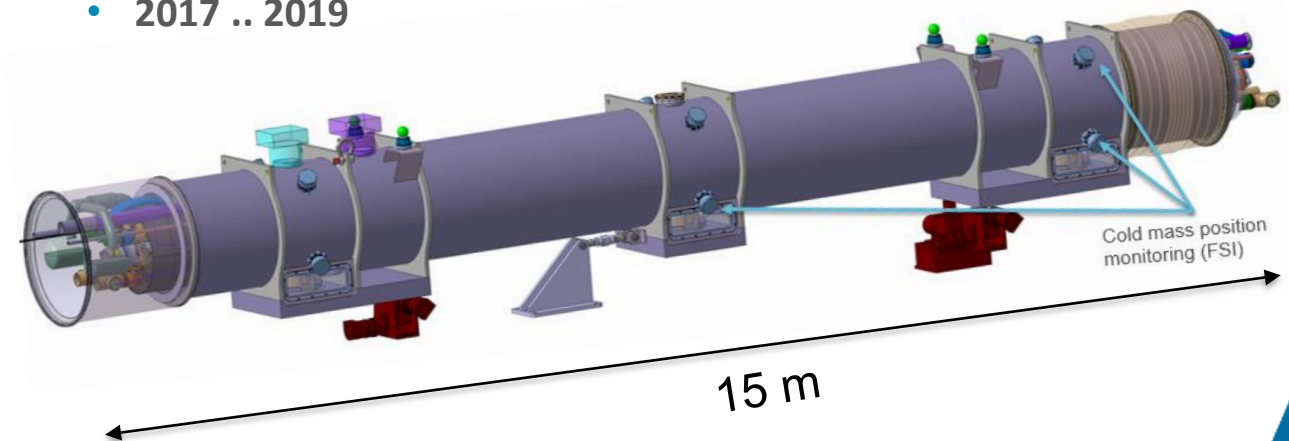
(www.etalon-gmbh.com)

FSI for internal monitoring of cold objects inside cryostats

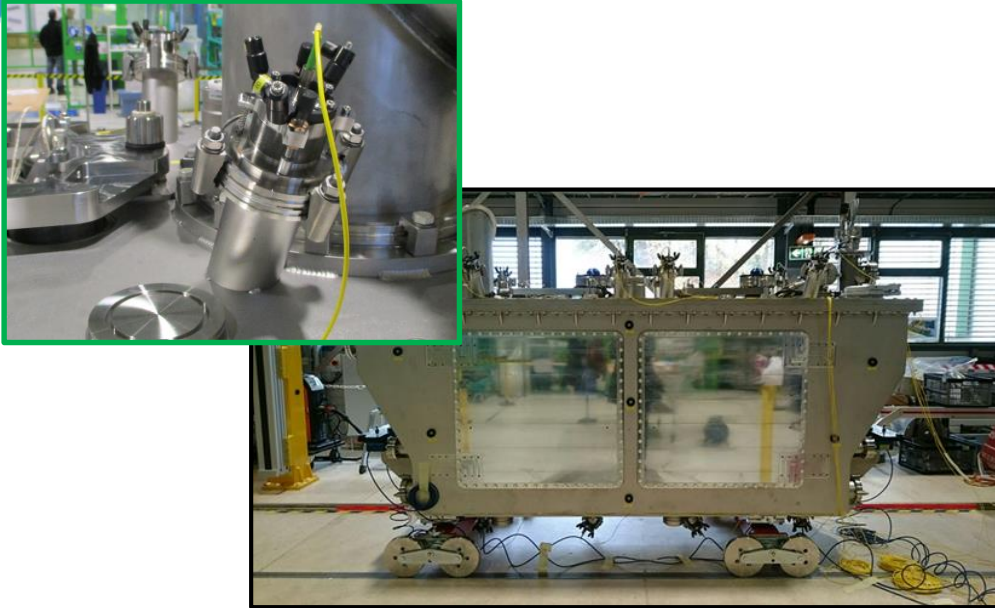
- First FSI application – crab cavity position monitoring
- 2016 .. 2018



- Second FSI application – inner triplet cold mass position monitoring
- 2017 .. 2019



Internal monitoring (classical FSI) – first conclusions



INNER TRIPLET:

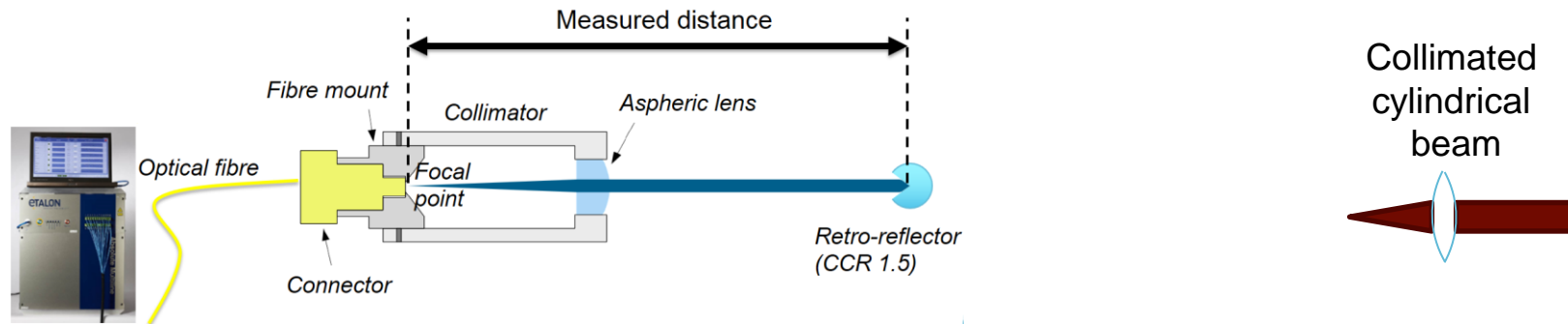
- Big lateral shifts of reflector caused by thermal contraction not allow to follow full cool-down cycle of the magnet
 - Tip-tilt adjustment of optical head needed
- Cryocondensation is an issue for reflector visibility
 - Solved by special design of reflector support
- Micrometric resolution of objects movements achieved

CRAB CAVITY:

- System allows to follow the cooled crab cavity position/orientation
- Micrometric resolution of objects movements achieved
- Continuous measurement by over 6 months
- However! 2 targets visibility lost during measurements (Cryocondensation? Lateral target displacement?)

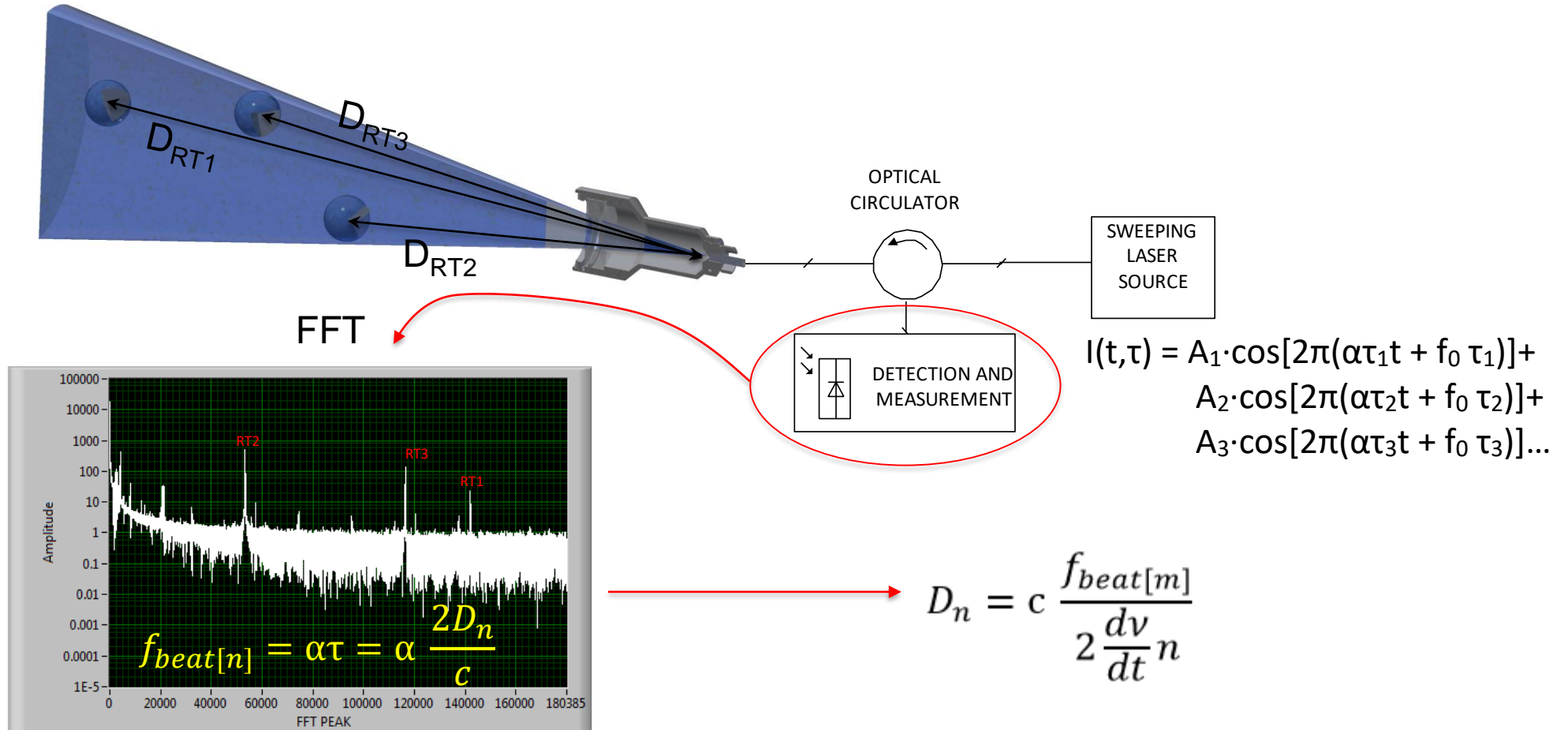


Classical FSI – summary



- **System is sensitive to return signal intensity level (beam alignment important)**
 - Reflectors lateral position or dust on the reflectors have big impact on measurement performance
- Beam diameter defines transversal movement range of the target
- Optical feedthroughs needs to include tip-tilt adjustment functionality for initial beam position targeting into retroreflector (higher cost of feedthrough, need of adjustment after cool down)
- Only collimated beams and observation of single target

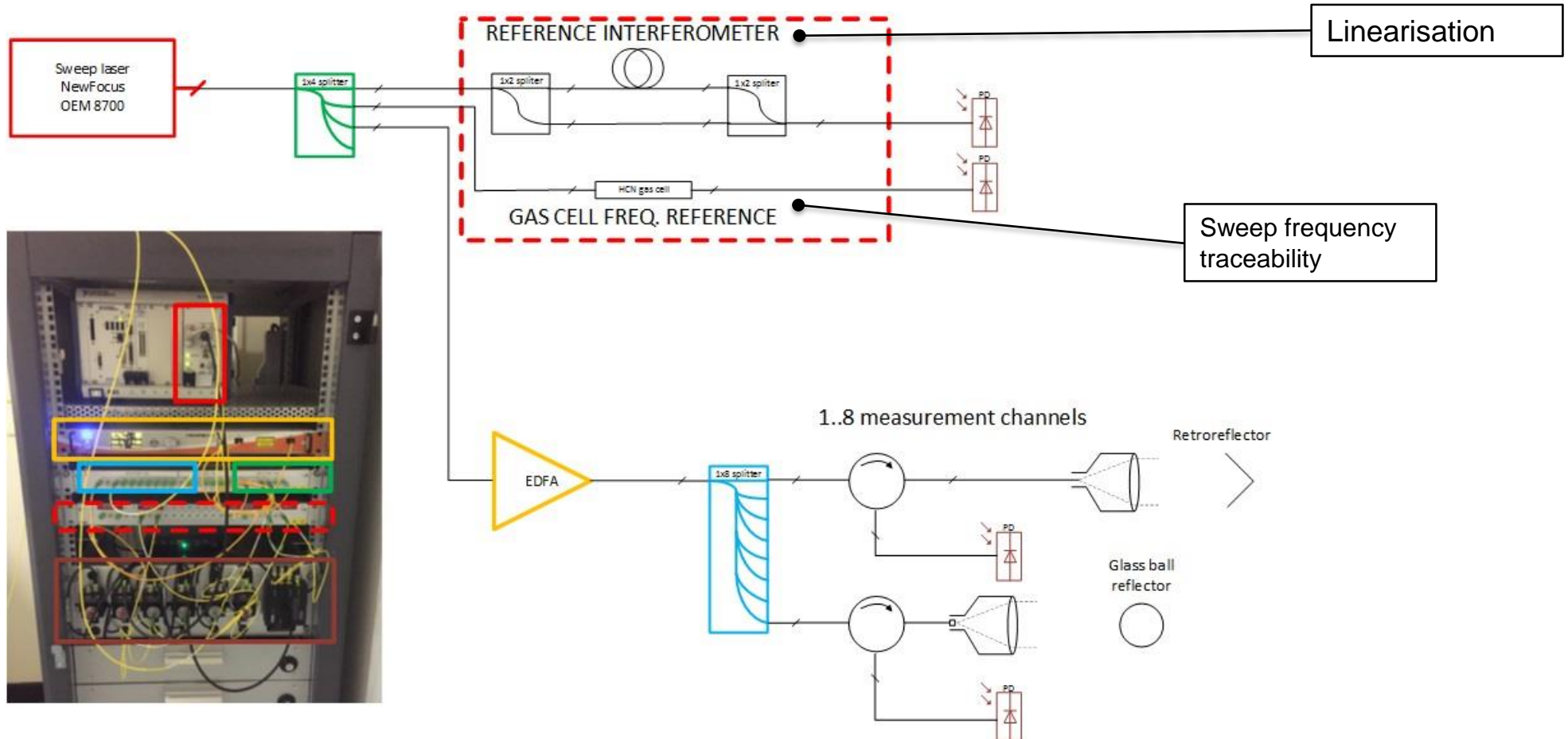
Multi-target FSI (Fourier analysis based)



α – is a sweep rate of the laser ($\alpha = \frac{dv}{dt}$ - laser frequency change in time);
 c – speed of light; n – refractive index of light transmission medium;
 τ – time of flight of laser to the target

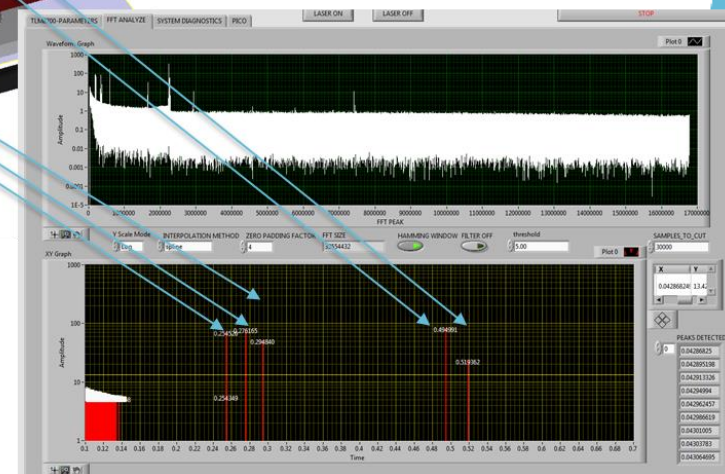
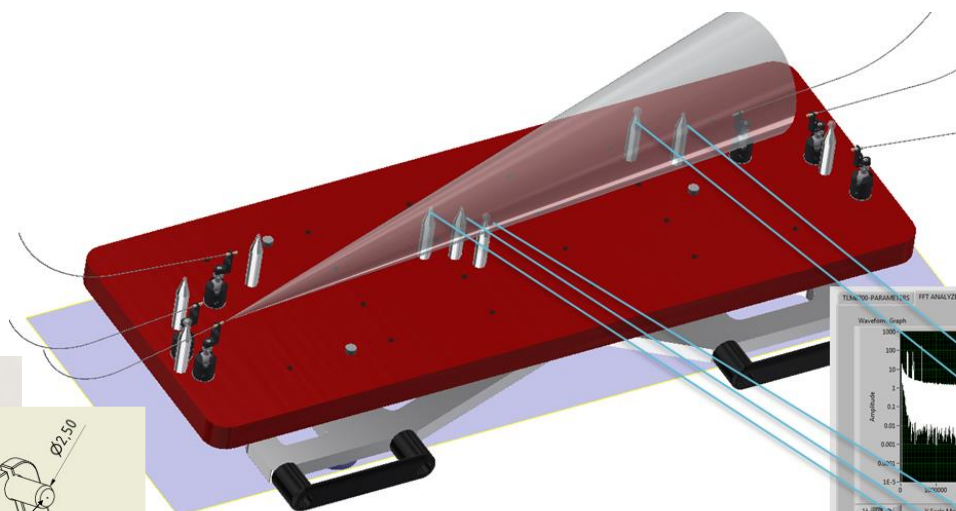
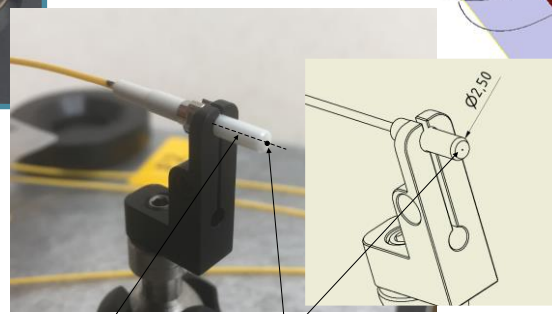
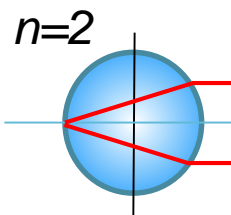
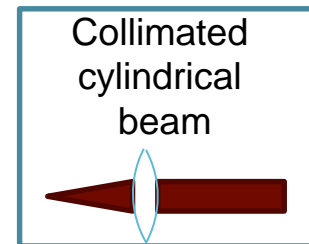
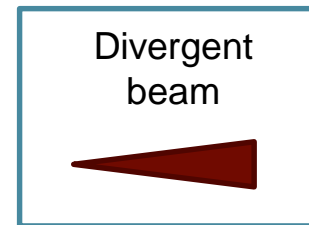
Multi-Target FSI – simple measurement setup

- Allows for flexible optical connections and scalability of the interferometer channels number
- Single laser (simple, but vibration sensitive) or „dynamic” - dual laser/sweep – FSI (complex, more expensive)



Multi-target FSI – advantages

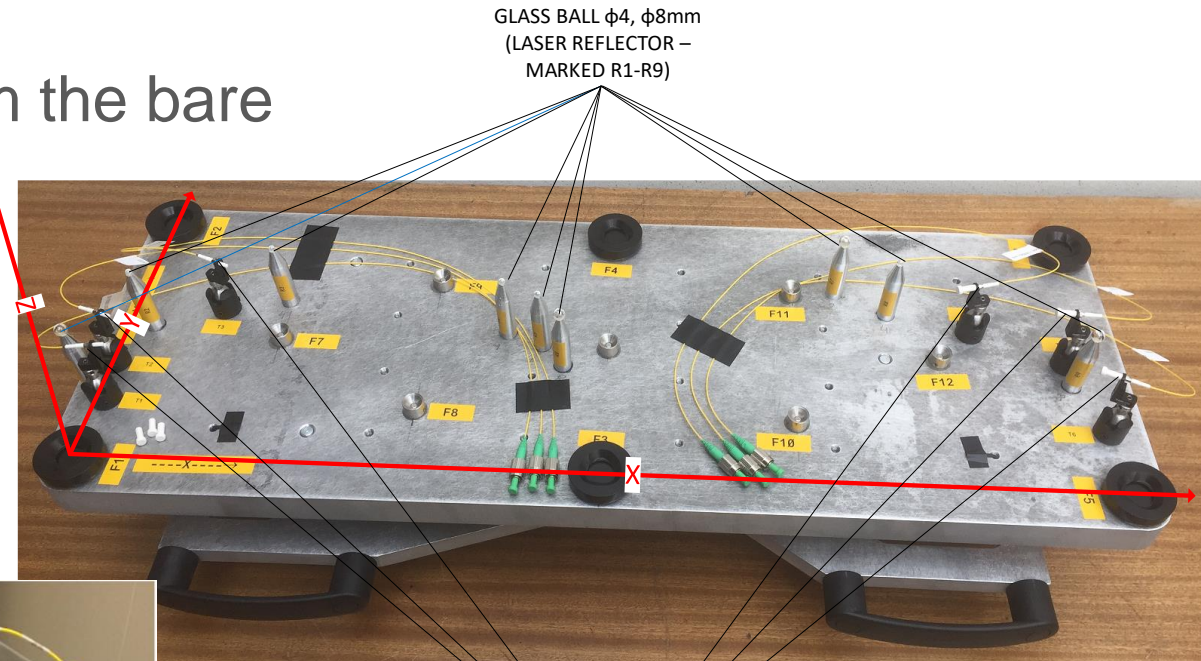
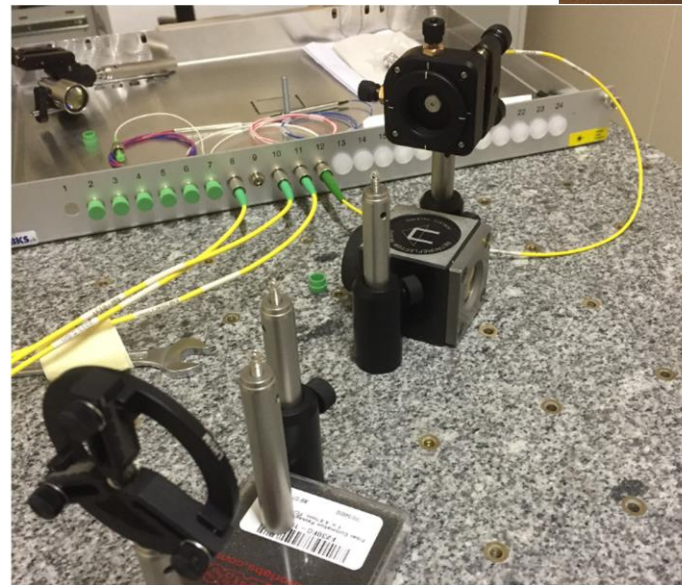
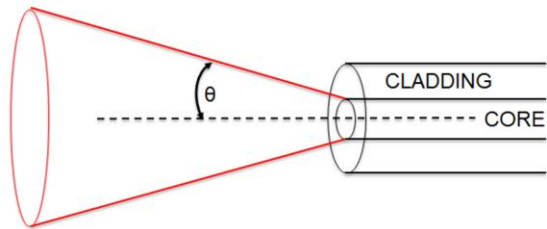
- **Very robust measurement method – almost insensitive to the light intensity (high and very small power reflections visible over the noise background)**
 - Possible to use cheap glass balls as a reflectors
 - Possible to measure reflection from various surfaces
- Measurement uncertainty $<5 \mu\text{m}$ (single laser configuration, no vibrations)
- Possible to measure multiple targets within single laser scan
- Possible to use with the collimated and divergent beams
- Simple beam delivery optics



Multi-target FSI – applications

Launch of the divergent beam directly from the bare fibre ferrules as most optimized solution

- Divergence angle defined by NA
- Sufficient to measure distances up to 0.7m
- Easy to measure „interference origin” (ferrule tip axis using CMM)



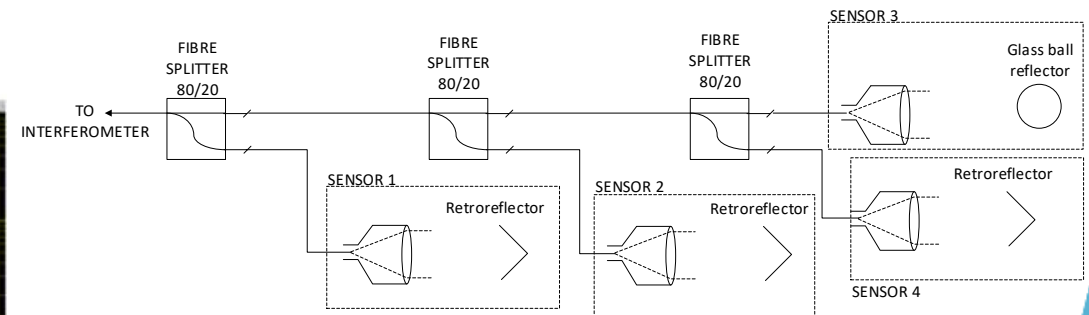
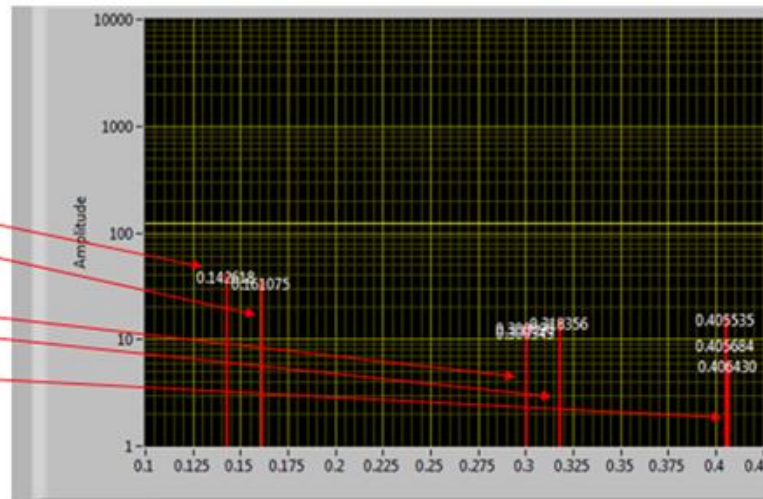
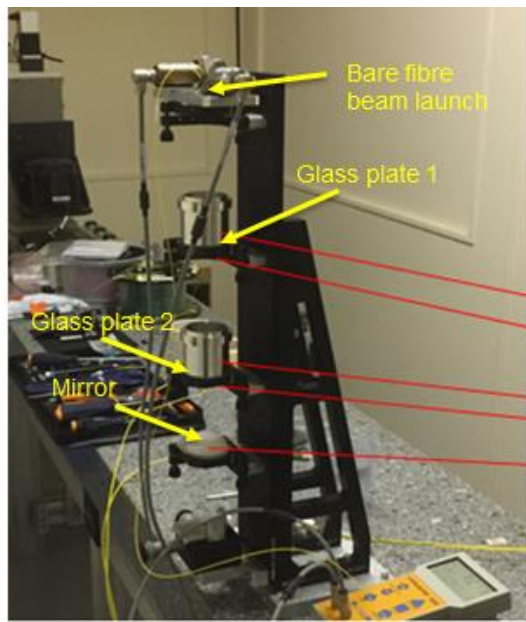
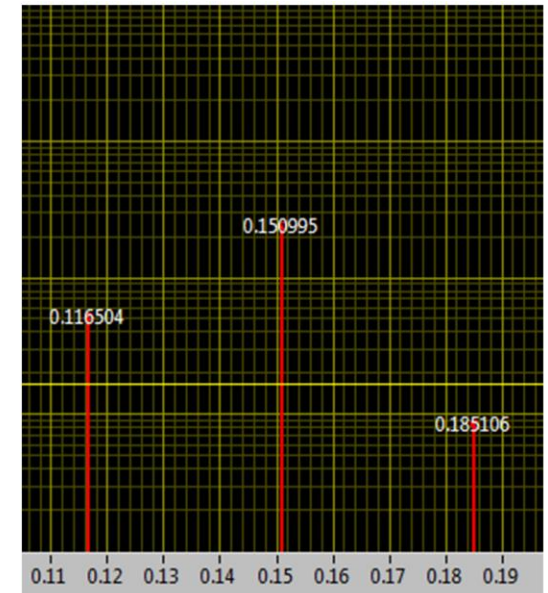
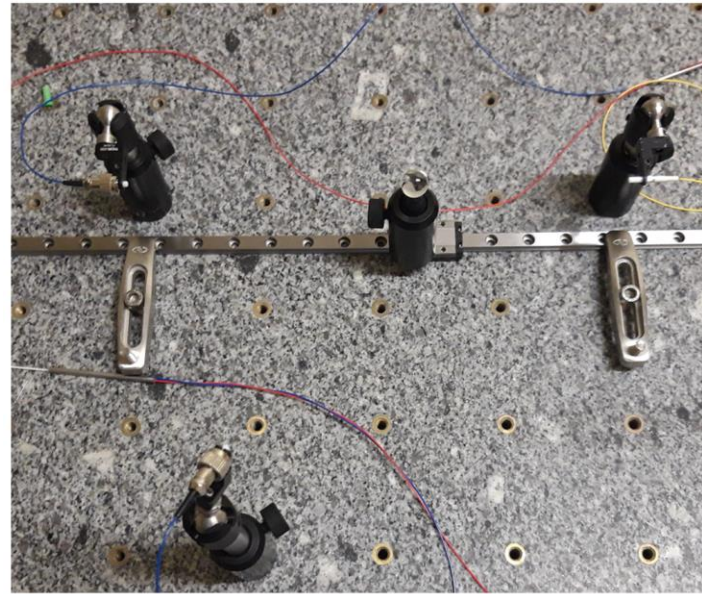
GLASS BALL $\phi 4$, $\phi 8$ mm
(LASER REFLECTOR –
MARKED R1-R9)

BARE FIBRE FERRULES
(LASER TRANSMITTER –
MARKED T1-T6)

Multi-target FSI – applications

Multiple reflection applications

- Multi-reflection sensors
- Multi-sensor solutions (serial connection of sensors)
 - Different physical quantities measurement through measurement of length of cavities created within the fibre

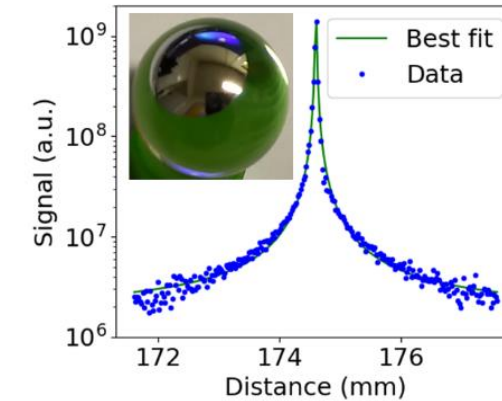
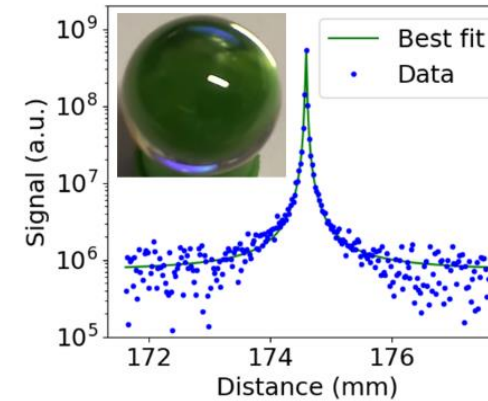
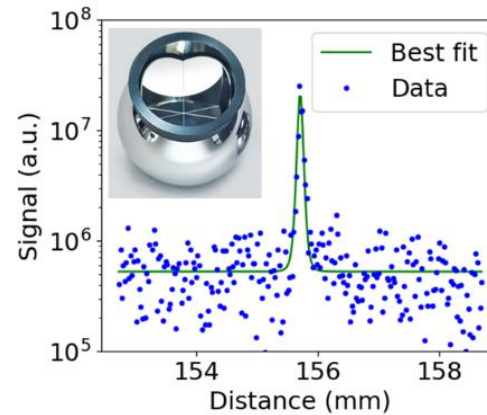


Multi-target FSI – drawbacks

Frequency spectrum will show all the reflections including also the unwanted ones

- Internal parasitic reflections (e.g. circulators)
- Fibres Rayleigh scattering increase noise ratio
- Sensitive to parasitic reflections from shiny surfaces surrounding the measured reflectors/surfaces
- Multi-surface or multi-sensor – beat frequency peaks can not overlap

MT-FSI Instrumentation – glass ball reflectors



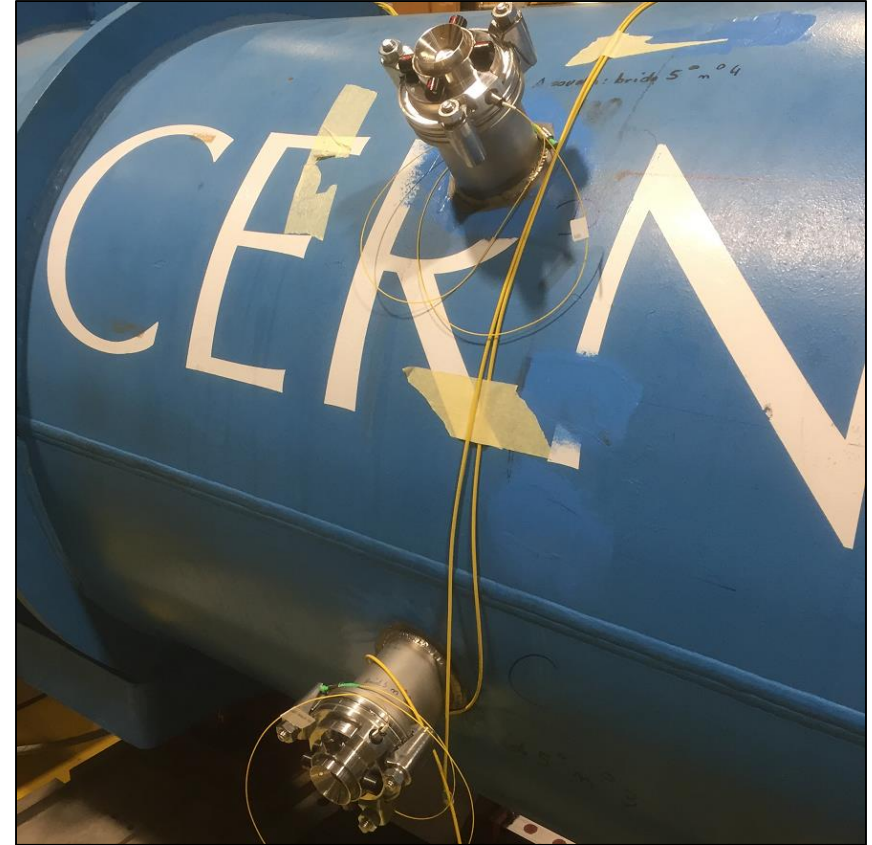
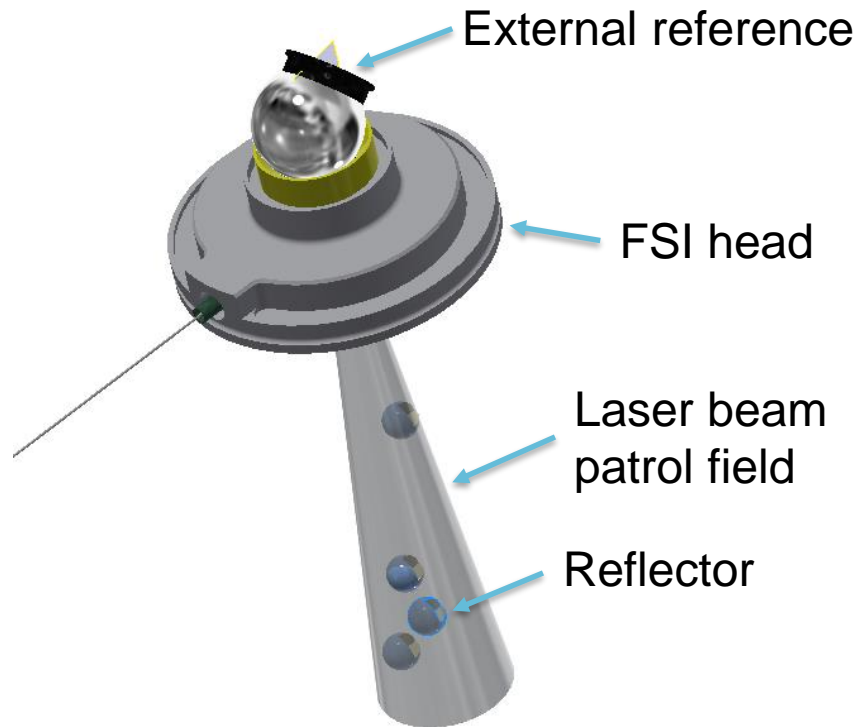
- Refractive index ≈ 2 glass ball used as an alternative to hollow retroreflectors or BMRs **(big reduction of installation cost!)**
 - 0.5” uncoated and coated reflectors manufactured and tested
- TAFD 55 and S-LAH79 ball reflectors radiation hard 5MGy, 10MGy samples under tests
- Coated glass ball reflector measurable by laser trackers



MT-FSI Instrumentation – vacuum heads

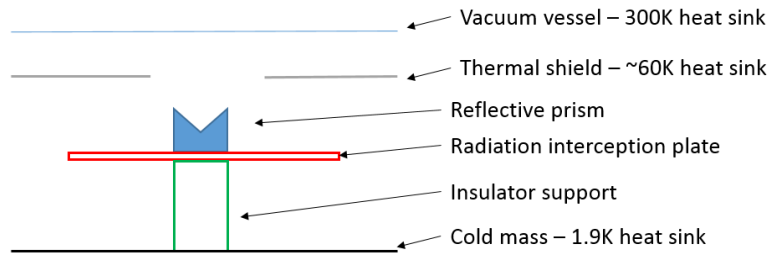
Simple vacuum FSI head for HL-LHC internal monitoring

- No moving parts, cheap, single steel body design
- Wide patrol field – big lateral reflector movement range
- Low cost (bare fibre ferrule beam launch)

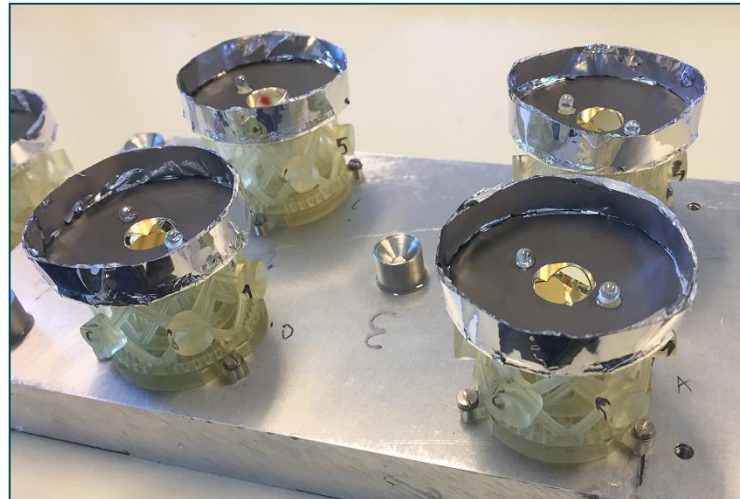
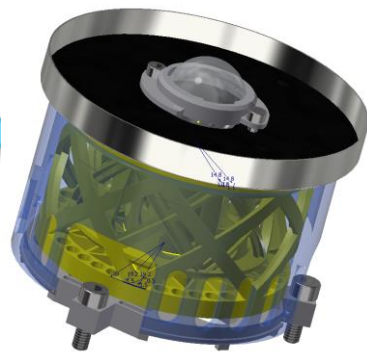
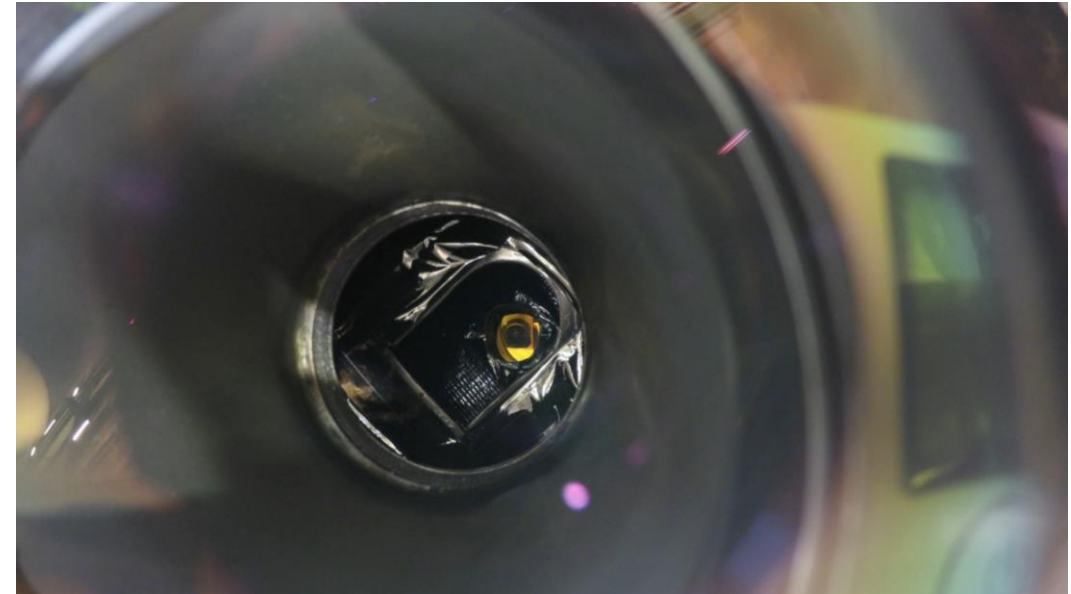


MT-FSI instrumentation - cryo-compatible reflector supports

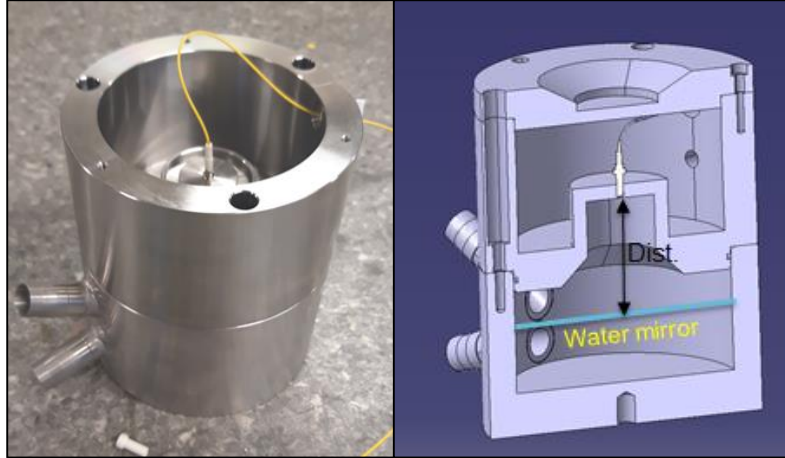
- „Passive”, SIMPLE design to suppress cryo-condensation effect
 - 3D printed targets to provide complex insulator shape
 - Graphite coated, heat interception plate
 - MLI film to minimize heat radiation towards cold mass of magnet



F. Micolon

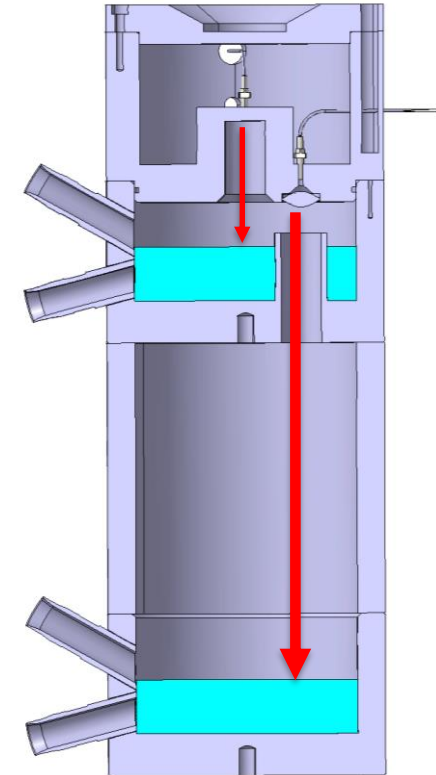
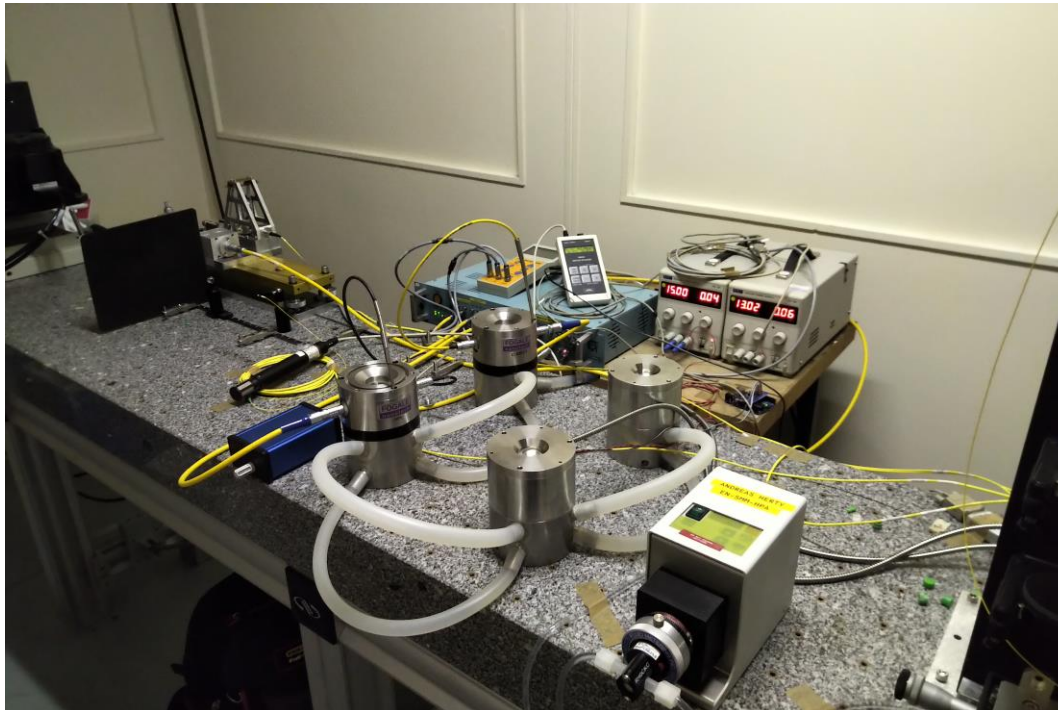


MT-FSI Instrumentation – interferometric Hydrostatic Levelling Sensor (iHLS)

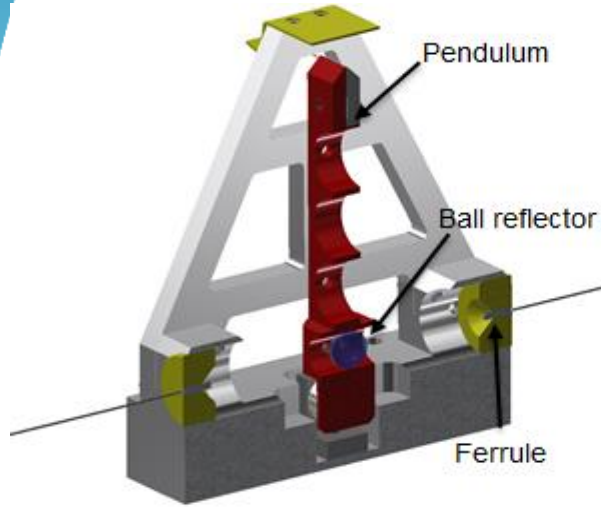


Cost optimized, divergent beam FSI HLS sensor for HL-LHC

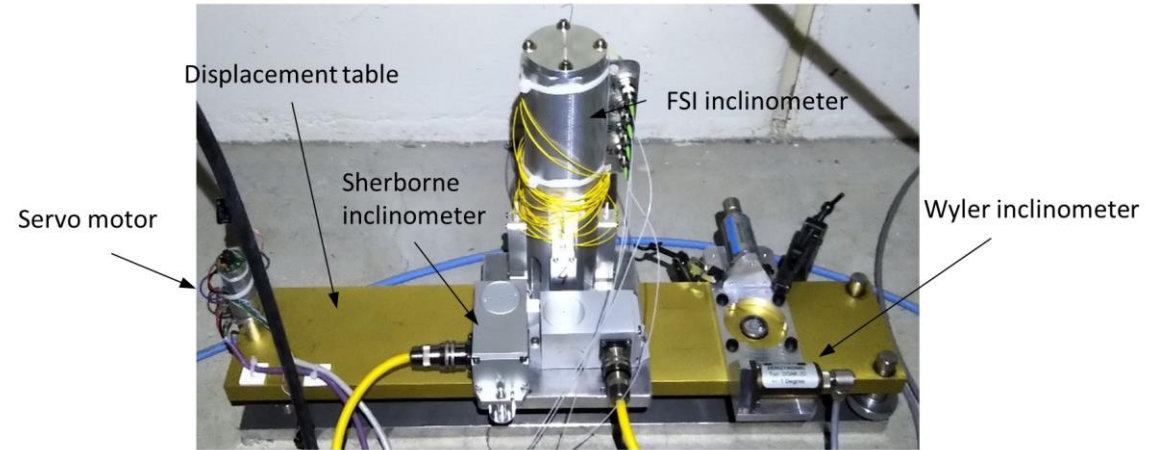
- Single metal body chassis, no movable parts, minimum amount of optical components
- Measurement uncertainty $< 5\mu\text{m}$, precision $\sim 1\mu\text{m}$
- Multiple level sensor under design



MT-FSI Instrumentation – optical inclinometer



1-st prototype (1-axis)

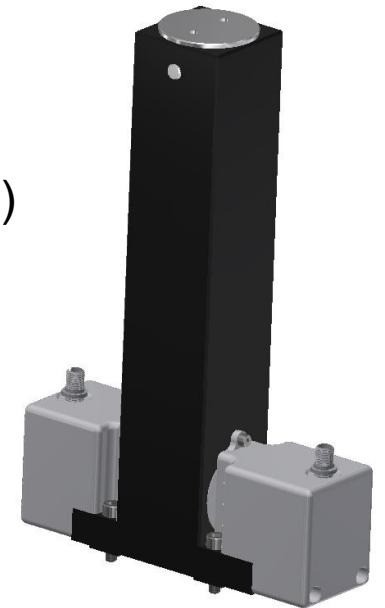


2-nd prototype (2-axis)

Optical inclinometer for HL-LHC

- Resolution $< 10 \mu\text{rad}$
- Differential pendulum measurement to anticipate thermal expansion effects
- Two generations of prototypes tested, allowed for final approach selection
- 3-rd – final generation of inclinometer under tests

3-rd (final) prototype (1-axis)



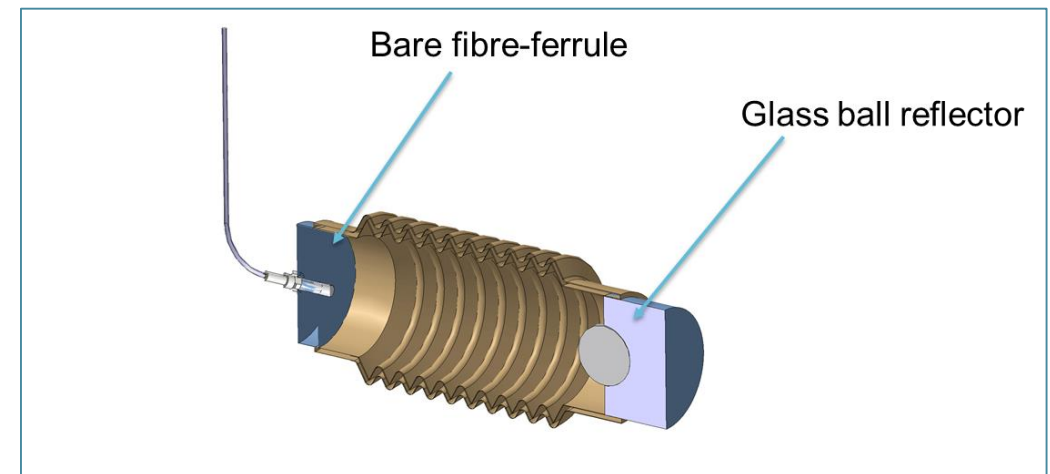
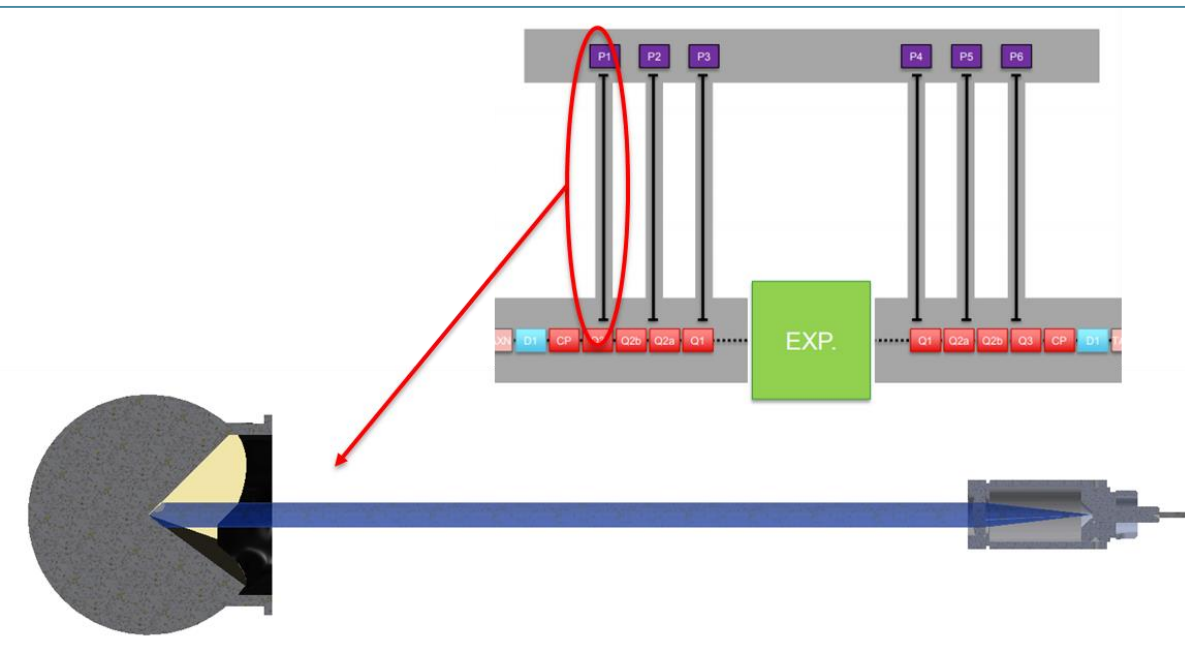
Multi-Target FSI – Long/Short distance measurement sensors

Distance measurement for UPS vs. Tunnel radial reference transmission

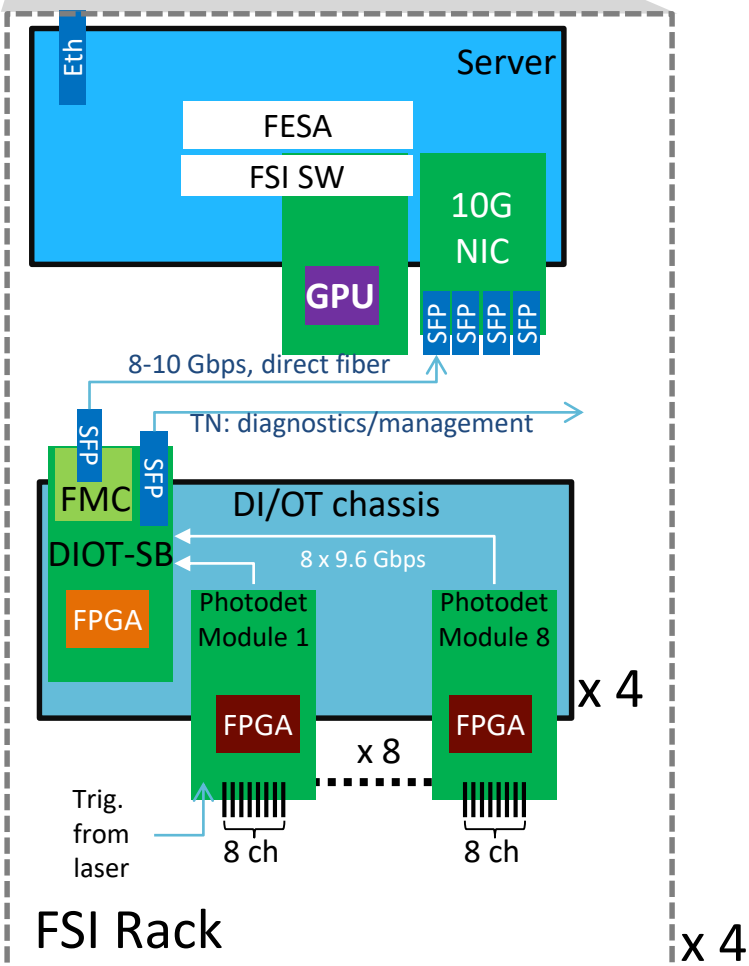
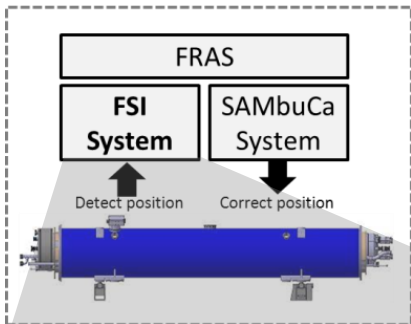
- ~15 m distance
- Standardized collimated optics to be used
- Expected measurement uncertainty < 40µm
- Precision ~5 µm
- Under development

Short distance measurement sensor (range ±5 .. 10mm)

- To replace current capacitive sensor
- Design with thin wall bellow protection against the dust
- Expected measurement uncertainty < 5µm
- Precision ~1 µm
- Maximally simplified (bare-ferrule + glass ball reflector) to increase reliability



Multi-Target FSI – interferometers



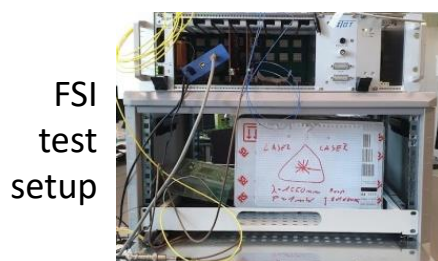
Measurement setups:

- Proof-of-concept with **2 channels** by BE-GM in **2017**
- Portable measurement setups (16..24 multiplexed channels) in 2019/20

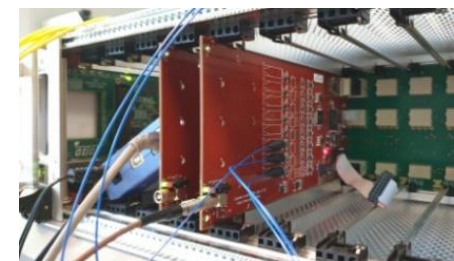


HL-LHC production setup(M. Lipinski – BE-CEM-EDL):

- Final system with **1000 channels** by BE-CEM for **LS3**
 - Based on **DI/OT**
 - Custom **photodetector acquisition module**
 - **10 Gbps Ethernet** links to GPU servers
 - **Advanced computations in GPUs** (FFT, linearisation, fitting)
 - Over **1 Tbps** of raw data produced by all channels
 - Over **3 GB** of data to be processed each second by 4 GPU servers
 - Demonstrator: end of 2021



FSI test setup



FSI photodetector module

Conclusions

- Fourier analysis based FSI allow to track distances to various types of reflectors or reflecting surfaces (with various intensities of interference beat signals)
- Appropriate approach to sensor design, combined with MT-FSI properties makes it possible to create very simple and robust sensors and sensor networks
- Reduction of the optics complexity, allowed to use absolute interferometry for big-scale installations



Thank you for your attention