

Mechanical studies of the cryomodule

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1. Introduction

Calculations carried out with the aim of evaluating possible support solutions for the components of the SPL cryomodule and the SPL test cryostat.





Transversal position tolerance of cavities inside cryostat

BUDGET OF TOLERANCE					
Step	Sub-step	Tolerances (3σ)	Total envelopes		noricion
	Cavity and He vessel assembly	± 0.1 mm (TBD)	Positioning of the cavity w.r.t. beam axis ± 0.5 mm		
Cryo-module assembly	Supporting system assembly	± 0.2 mm (TBD)			tructi
	Vacuum vessel construction	± 0.2 mm (TBD)			
Transport and handling (± 0.5 g any direction)	N.A.	± 0.1 mm (TBD)			Å
Testing/operation	Vacuum pumping		Stability of the cavity w.r.t. beam axis ± 0.3 mm		ilidet ilidet
	Cool-down				
	RF tests	± 0.2 mm (TBD)			na-to
	Warm-up				_
	Thermal cycles			_	l



Possible supporting schemes

"Standard" supporting scheme



Two-support preferrable \rightarrow isostatic (=well defined forces on supports) ...but is cavity straightness enough?? If not...







Possible supporting schemes

"Standard" supporting scheme





Possible supporting schemes

Alternative: coupler supporting scheme



...the coupler is also a supporting/aligning element

RF coupler + longitudinal positioner + vertical support

Intercavity support structure

External supports (jacks)

2. Supporting system – required stiffness

Calculations performed with the aim of estimating the stiffness which the support system ("Standard "supporting solution) of the SPL cavities would have to provide for the string of cavities to be kept inside a certain alignment tolerance.

- Beam simply and symmetrically supported on two points, loaded by the weight of the cavities and by its own weight.

- Loads are distributed uniformly along the beam

-The cavities and the supports are considered to be rigid -maximum beam deflection is a measure of the maximum cavity misalignment.





2. Supporting system – required stiffness

Required stiffness – different cross sections



2. Supporting system – required stiffness

Third support? – Comparison with 2 supports

	S [<i>m</i> ²]	<i>I</i> [<i>m</i> ⁴]	Deflection; 2 supports (analytical) [<i>mm</i>]	Deflection; 3 supports (FE beam analysis) [<i>mm</i>]
Circular tube <i>tck.</i> 6 mm diam. 300 mm	0.0055	5.99E-05	2.3	0.358
Circular tube <i>tck.</i> 12 mm diam. 1000 mm	0.0372	4.55E-03	0.075	0.018

- Three vertical displacements (simple supports)
- Loads remain the same.
- One support in the middle of the beam, the other two at a distance of 0.16 *L* from each end of the beam.



3. Power coupler as support

Two different support scenarios : 1. cavity supported only by a fixed support on the Power Coupler flange, 2. cavity supported by the PC and by a vertical support on the other extremity of the Helium Vessel.

Loads: Weights of the represented parts (1068 N) plus weight of the tuner (147N)

Materials: Titanium for the Helium Vessel and Stainless steel for the other parts.







These models are previous versions.







Coupler supporting scheme





Conceptual design:



Stainless steel cylinders: length of 420 mm and diameter of 40 mm.

Size of stiffeners increased for better results:



Inter cavity support's stiffness:



Analysis with one He vessel / cavity and two power couplers (double tube):





von Mises stress (Pa):



Vertical displacement (colour) [m]:



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Body deformation amplified 300x



Analysis of string of 4 cavities:





Vertical displacement (colour) [m]:



Body deformation amplified 300x

von Mises stress (Pa):



Three different vessels were modelled with the same thickness and supports. Two different shapes are analysed. All these calculations refer to conceptual designs.

A larger diameter may be a requirement for a circular vessel due to assembly.



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5. Vacuum vessel design

Different sets of loads were applied:

1. Weight loads: weight of vessel plus loads caused by weight of the string of cavities

- 2. Pressure loads: external pressure of 1 bar
- 3. Weight loads plus pressure

Weight loads plus pressure:





Results:

		Loads			
	Vessel	Weight	Pressure	W + P	
Max. absolute displacement of vacuum vessel [mm]	1. "O" 1400	0.47	0.31	0.47	
	2. "O" 1016	0.15	0.36	0.40	
	3. "U" 1020	0.19	4.3	4.3	
Max. vertical displacement of PC flanges [mm]	1. "O" 1400	0.061	0.31	0.36	
	2. "O" 1016	0.062	0.35	0.39	
	3. "U" 1020	0.19	0.52	0.44	

Results: Vertical displacement [m] under external pressure of 1 bar:



Analyses with string of cavities: smaller circular vessel and "U" shape vessel. Weight Load



Thermal gradient: 10 K difference between top and bottom of vessel (tentative value – a full thermal model should be made, including active cooling of couplers).



	Vessel	Displacement
Max. absolute	1. "O" 1400	0.73
displacement of vacuum	2. "O" 1016	0.55
vessel [mm]	3. "U" 1020	0.50
Max. vertical	1. "O" 1400	0.51
displacement of PC flanges	2. "O" 1016	0.40
[mm]	3. "U" 1020	0.40





6. Recent models – comparison

New models of the vacuum vessel and power coupler were compared to previous models.



Main differences: thickness of the helium vessel, not constant in the first case (3 and 5 mm) and constant in the second (5 mm), thickness of the outer and inner walls of the power coupler, as well as the space between them (respectively 1.5, 2 and 4.5 mm for the older version and 2, 1.5 and 1 mm for the new version).

6. Recent models – comparison

Analyses single cavity



Model	Maximum deflection (mm)	
Older	2.3	
Older; altered	2.1	
reinforcements	۷.۱	
New; altered	1 5	
reinforcements	C.1	

Analyses string of four cavities cavity



Model	Maximum deflection (mm)	
Older; altered reinforcements	0.12	
New, original reinforcements	0.66	
New, altered reinforcements	0.091	

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7. Assembly tooling – Required stiffness

Different support scenarios were considered. FE calculations including the string of cavities were performed. Analytical calculations were carried out considering that the support system is comparable to a beam.



The length of the beam is 6.8 m for the 4 cavities test cryostat, and the double for the 8 cavities cryomodule.

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7. Assembly tooling – Required stiffness

FE analyses of the string of cavities, simplified model and loads:





Fixed inter cavity support (instead of sliding)



ERM



In red: von Mises stress values higher than half of the yield strength of stainless steel (~200 MPa):



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Support: Analytical calculation



Support: Analyses with the string of cavities; different sizes



Support height (h) [mm]	Maximum deflection Support [mm]	Maximum deflection String [mm]	Max stress Support [MPa]
50	10	10	157
100	8.1	8.3	134
200	3.3	3.4	17

Comparison: string of 8 cavities (symmetry applied) – 400x200 support Vertical displacement [m]



Comparison: sliding inter-cavity support – 400x200 support

Vertical displacement [m]





Spare Slides

Supporting system: Position of 2 supports

Definition of the supports' position



The position of the supports which minimizes the maximum deflection is a / L=0.2082

Non continuous "U" shape vessel



Two Alternatives: Reinforcement integrity (3b) vs. Free rotation (3c)



Loads

0.19

Pressure

0.52

0.65

0.78