

# **Development of Cable-In-Conduit Conductors at MIT**

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Workshop on Experience with Testing and Application  
of Cable-in-Conduit Conductors (CICC)  
Victoria, B.C.  
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# OUTLINE

- History of development of CICC at MIT
  - Summary of important results
  - Present program for development of ITER magnets
-

## ● Original Goals

- Increase superconducting magnet current densities
- Eliminate instabilities associated with two-phase helium cooling
- Incorporate structure in winding packs of high field, high stress magnets

## ● Early Work in Cooling with Supercritical Helium

- 1966 - Kolm, H.H., Leupold, M.J., Hay, R.D., "Heat transfer by the circulation of supercritical helium," *Advances in Cryogenic Engineering*, **11**, 530, Plenum Press (1966).

## ● Early Work in Forced-Flow Cooling of Superconducting Magnets

- 1970 - Morpurgo, M., "The design of the superconducting magnet for the 'Omega' project," *Particle Accelerators*, Gordon and Breach, **1**, 225 (1970)
- 1975 - Vecsey, G., "Forced Cooling of Superconducting Magnets," *Proceedings of 5th Int. Conf. on Magnet Tech.*, (MT-5) Roma (1975)

## CABLE-IN-CONDUIT CONDUCTOR (CICC)

aka

**INTERNALLY COOLED CABLED SUPERCONDUCTOR (ICCS)**

aka

**BUNDLE CONDUCTOR**

aka

**“ROPE-IN-A-PIPE”**

### ● **Earliest Work in CICC**

- 1975 - M.O. Hoenig, Y. Iwasa, and D.B. Montgomery, “Supercritical helium cooled ‘Bundle Conductors’ and their application to large superconducting magnets,” Proceedings of 5th Int. Conf. on Magnet Tech., (MT-5) Roma (1975)

### ● **First Large Coils in CICC - DC Coils**

- Westinghouse LCP, Nb<sub>3</sub>Sn, React and Wind
- MIT 12 Tesla Coil, Nb<sub>3</sub>Sn, Wind and React

### ● **First Pulsed Coils in CICC - DPC Program**

- JAERI/DPC-U1-U2, NbTi
- JAERI/DPC-EX, Nb<sub>3</sub>Sn, React and Wind, Rutherford Cable
- US-DPC, Nb<sub>3</sub>Sn, Wind and React

### ● **Latest Tokamak Fusion Applications**

- All ITER TF and PF magnets will be CICC
- All TPX/SSAT-S magnets will be CICC based on US-DPC design

## ● New Applications for CICC Other than Tokamaks

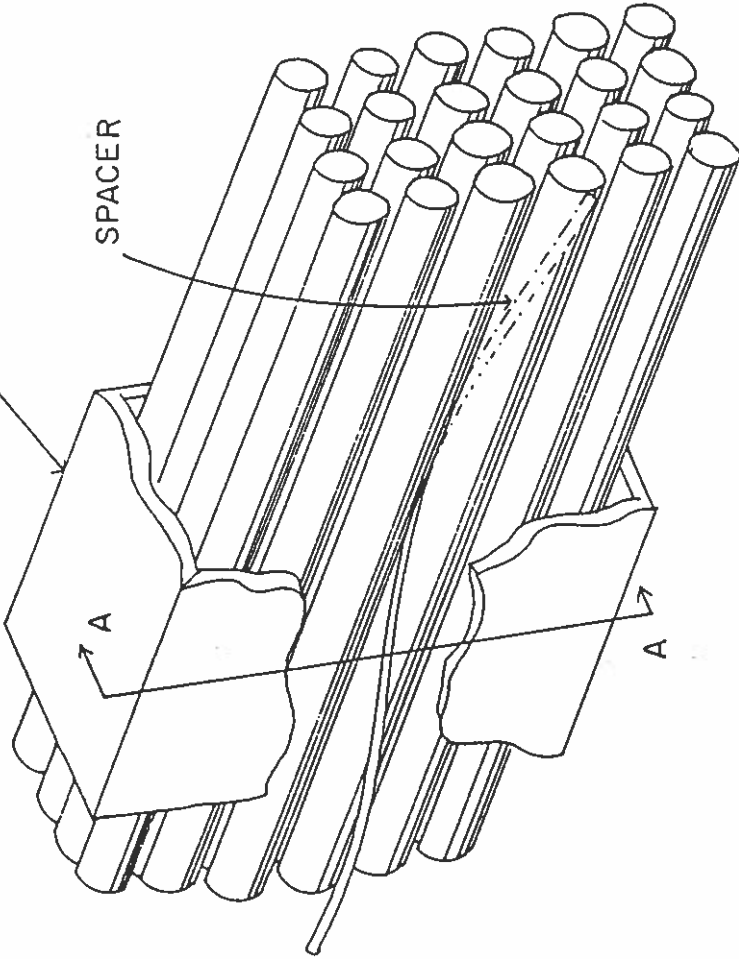
### Other Fusion

- Wendelstein VII-X - IPP Garching, Germany
- Large Helical Device, Nagoya, Japan

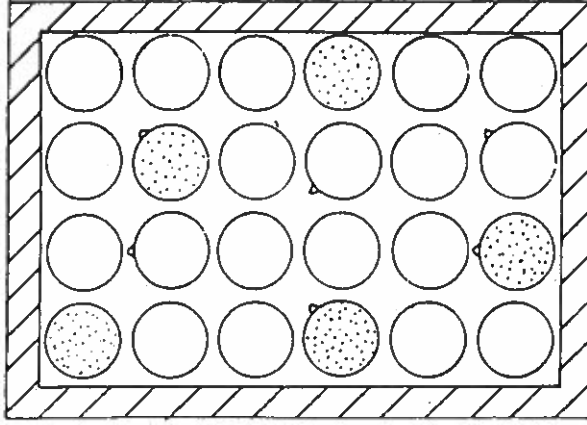
### Non-Fusion Applications

- ENEA 12 Tesla Coil for SULTAN
- NHMFL/FBNML 40 T Hybrid Coil
- SMES
- High Energy Physics - GEM Detector Magnet for SSC
- MAGLEV
- MHD
- ?

S/S OR ALUMIN. CONDUIT

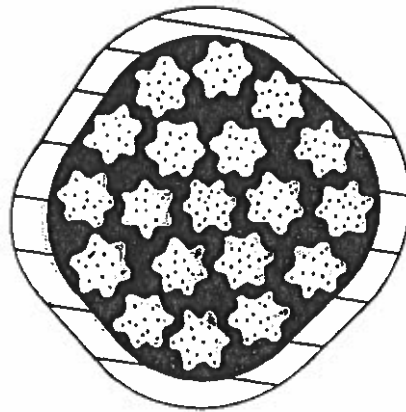


S/C FILAMENTS  
IN COPPER

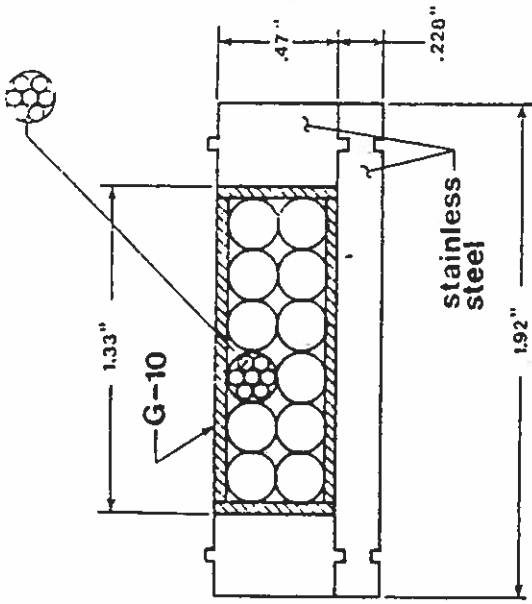


SECTION AA

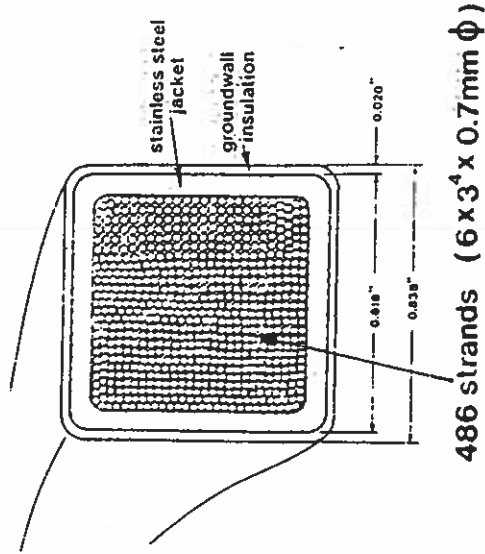
SUPERCONDUCTING CABLE WITH SPACERS BETWEEN STRANDS.



FLUTED-WIRE CONDUCTOR IN SQUARED-OFF CONDUIT.

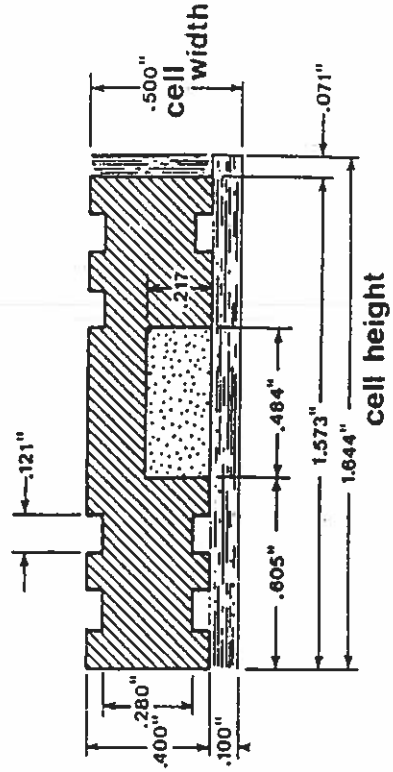


HIGH FIELD REGION (10.5T-12.0T)  
CONDUCTOR and STRUCTURE

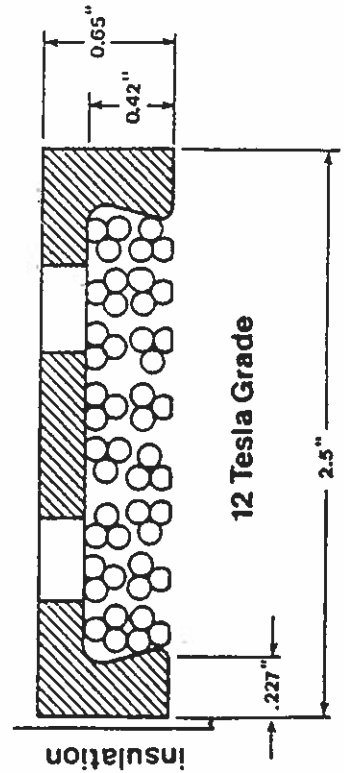


486 strands (6 x 3<sup>4</sup> x 0.7mm  $\phi$ )

all dimensions are in inches



FINNED CONDUCTOR



Cross Section of CONDUCTOR GRADE



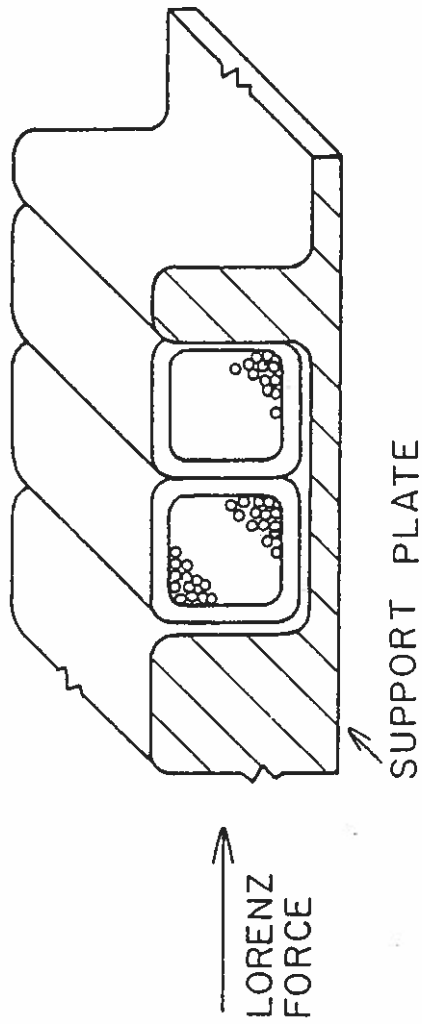
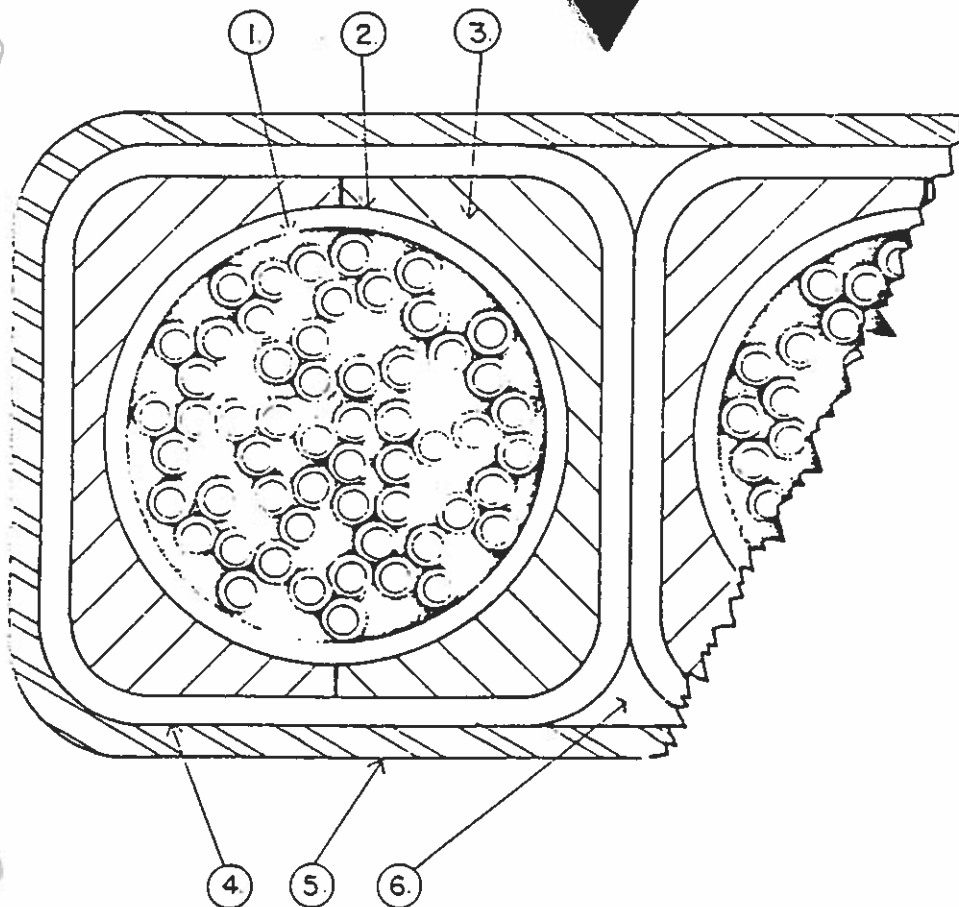
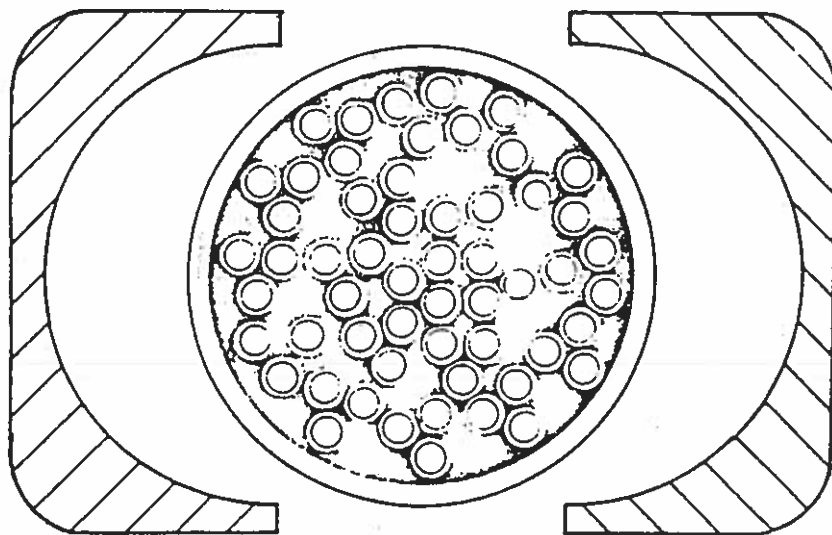
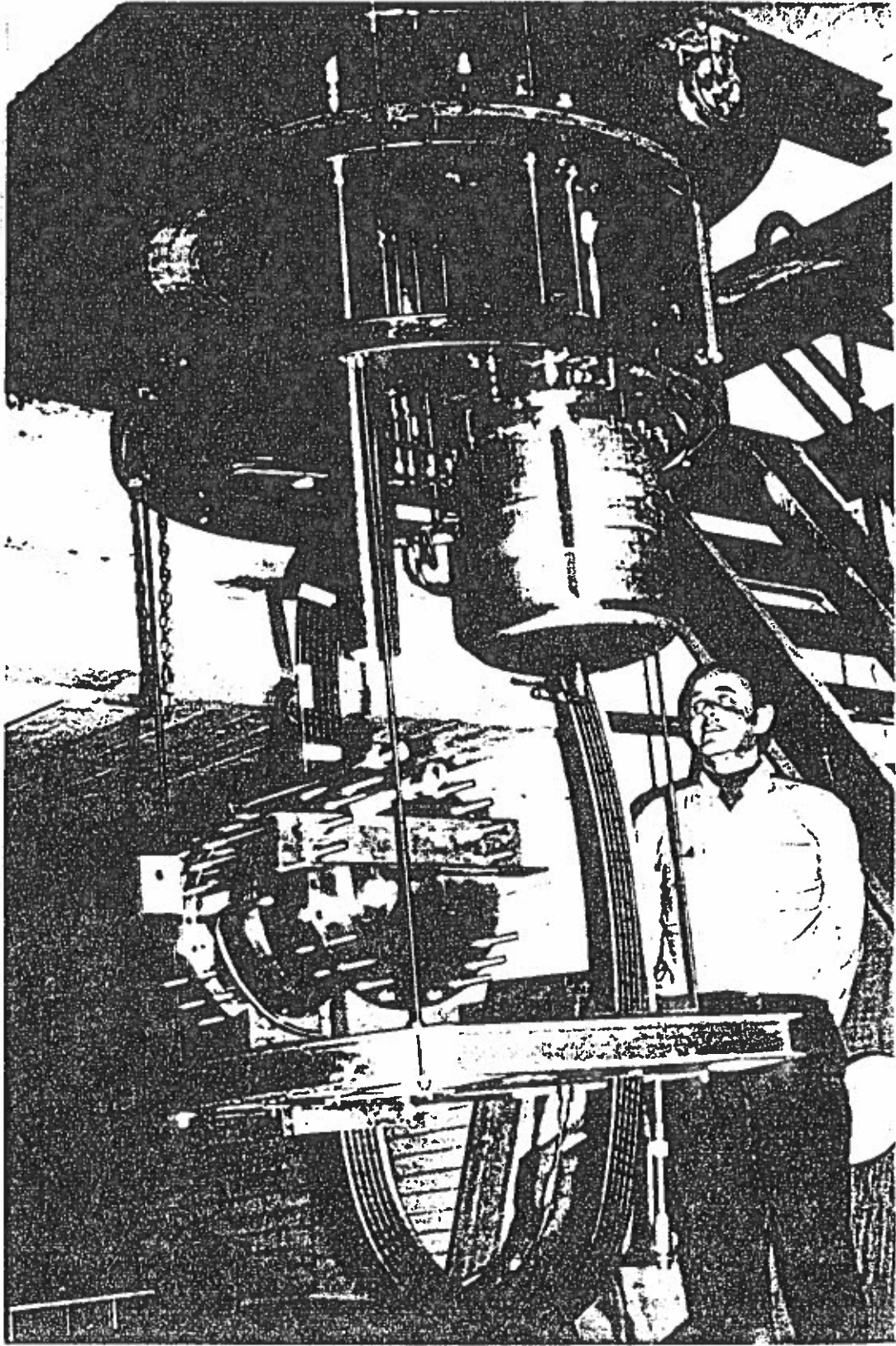


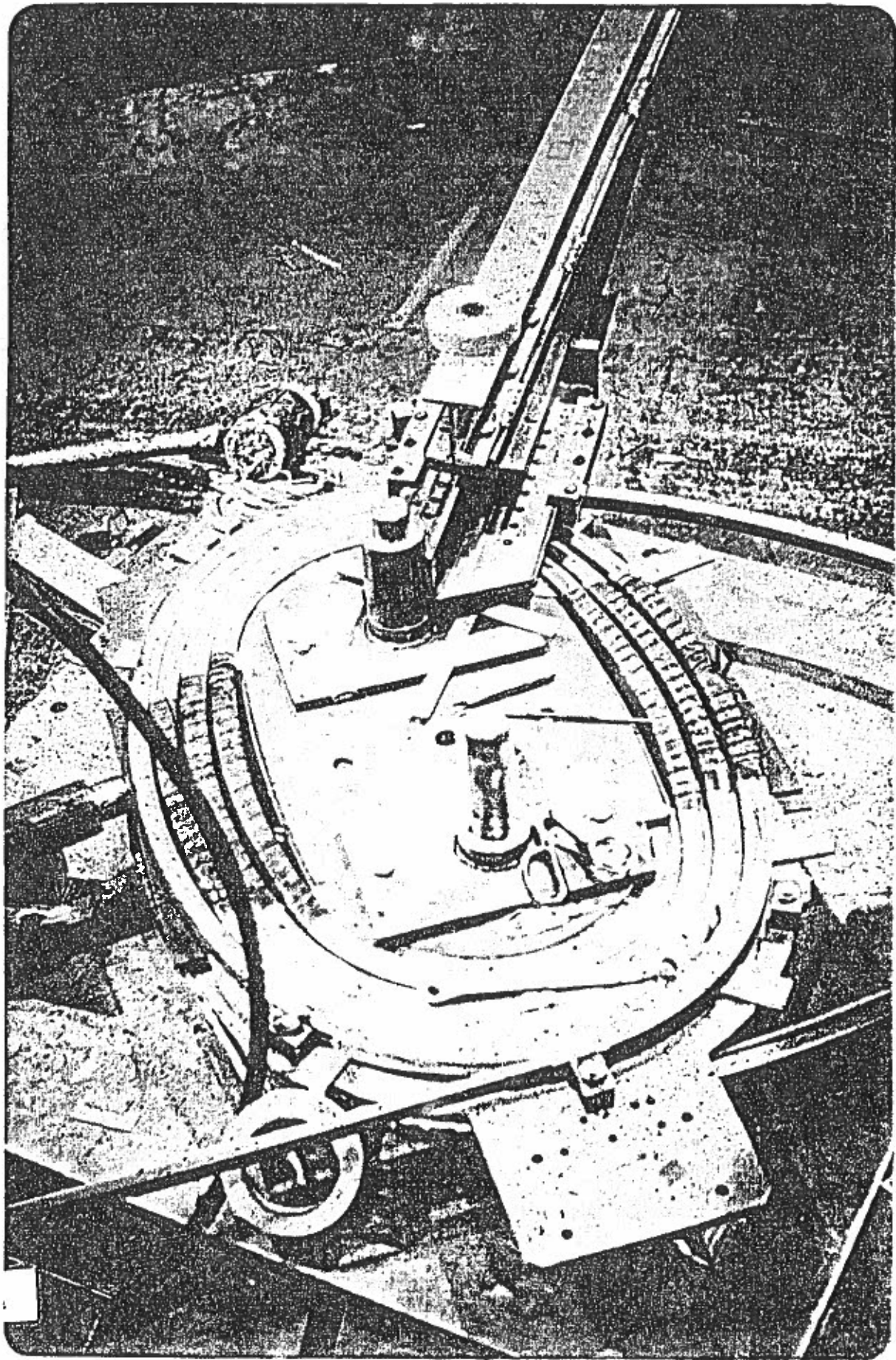
FIG. 14: STRUCTURE SUPPORTING TWO CONDUCTORS LAID INTO ONE GROOVE.



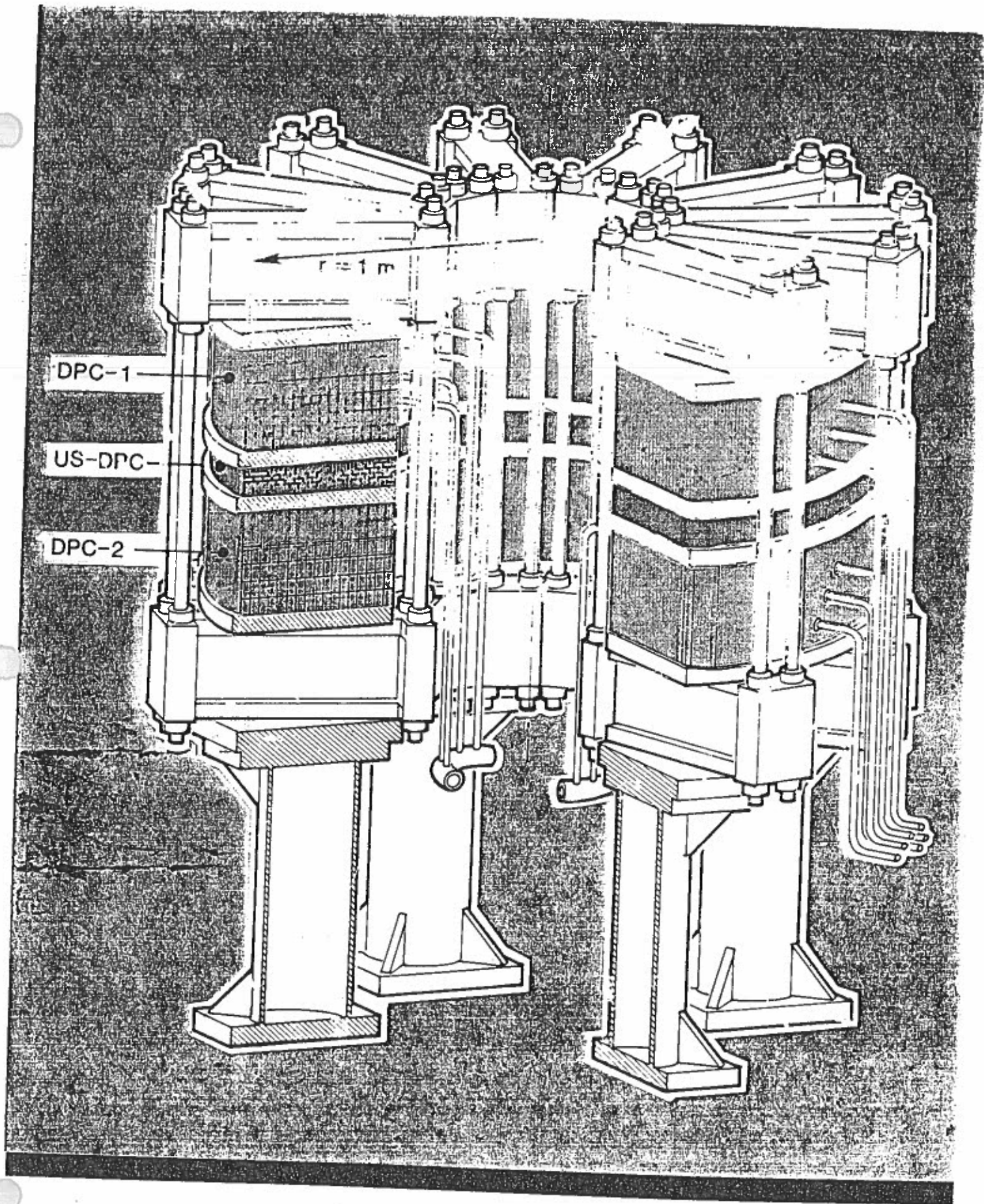
- ① COIL SPACE
- ② ALUMINUM TUBE (12mm. dia.)
- ③ ALUMINUM EXTRUSION (anodized)
- ④ FIBERGLASS INSULATION (epoxy impregnated)
- ⑤ INSULATION OVERWRAP (epoxy impregnated)
- ⑥ EPOXY FILLED SPACE

DEE COIL CONDUCTOR ASSEMBLY

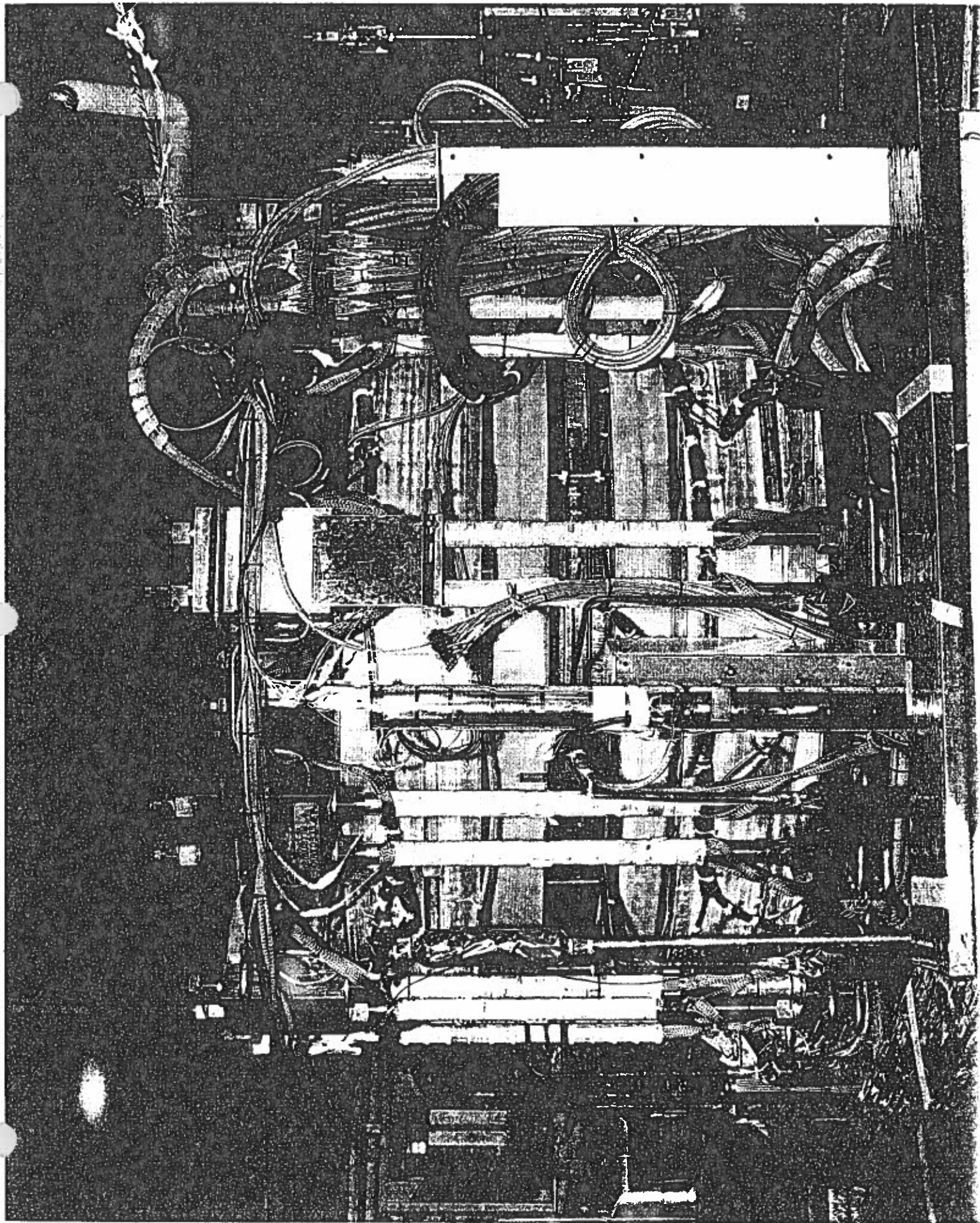








DEMONSTRATION POLOIDAL COIL (DPC) SHOWING  
MIT'S TEST COIL-THE "US-DPC" IN PLACE



## DESCRIPTION OF US-DPC

Field & ramp rate:  $\approx 10$  T, 10 T/s

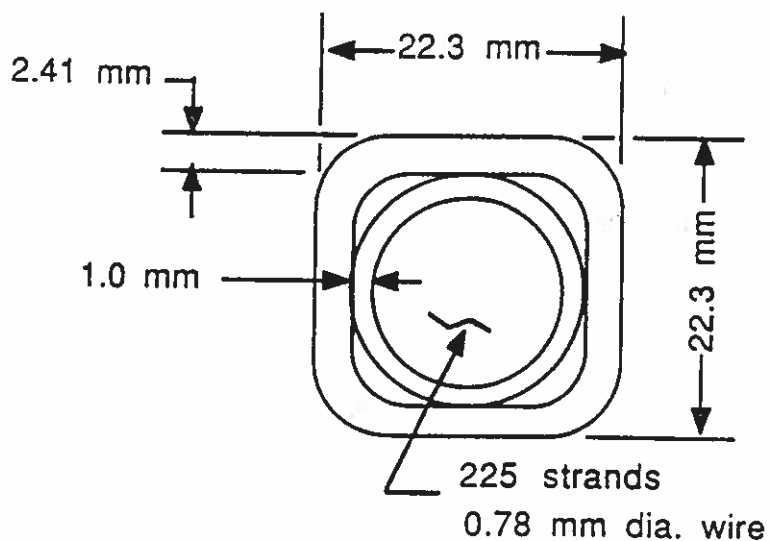
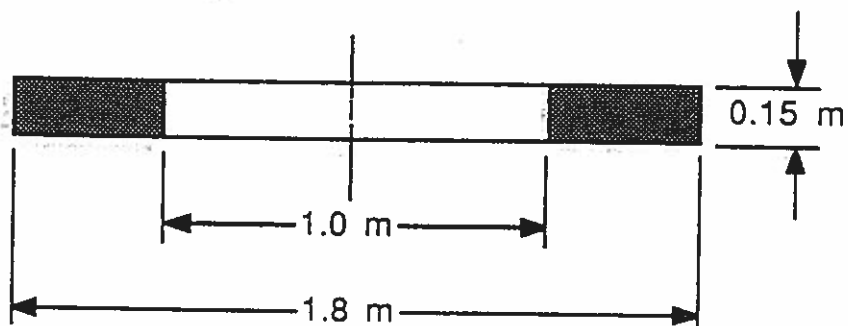
Current: 30 kA

Stored energy:  $\approx 8$  MJ

Superconductor:  $\text{Nb}_3\text{Sn}$  (wind and react)

Conduit: Incoloy 908

Cooling dual flow supercritical helium



## 1. The US-DPC experiment

- Dates: Nov. 5 - Dec. 20, 1990
- Goals: manufacturing process evaluation, AC operation to 10 T at 10 T/s; dual-flow cooling evaluation

## 2. Experiment statistics

- Two cooldowns, approximately 1 week each
- 305 runs: 73 DC and 232 AC
- 50 quenches
- Protection by bridge circuits and inlet flow reversal
- Maximum helium mass flow approximately 60 g/s
- Nominal operating condition of 4.5 K, 6 atm inlet
- Maximum test temperature 14.8 K; minimum 4 K
- Minimum flow 15 g/s
- Single-coil peak field of 5.7 T at 30 kA; 6.6 T at 35 kA
- Series peak field of 8.0 T at 25.9 kA

## 3. Single-coil DC tests (zero background field)

### 3.1 System and coil-fabrication checks

- Leak tightness: ok (vacuum vessel  $\approx 3 \times 10^{-7}$  Torr)
- Flow/cryogenic system: ok (4.5 K, 6 atm, 60 g/s)
- Lap joint resistance: ok ( $\approx 5 \times 10^{-10}$  ohms at 30 kA)
- Protection system: ok (balance circuits; flow reversal)
- Significance: basic fabrication ok



## DESCRIPTION OF RAMP-RATE LIMITATION

### 1. Single-coil AC tests at JAERI

- Ramps with 3 s flat tops (no quench):

run	ramp rate	peak field	current
139	19 T/s	3.8 T	20 kA
128	4.3	4.3	23
122	2.7	4.7	25
124	0.71	5.7	30
134	0.55	6.0	32

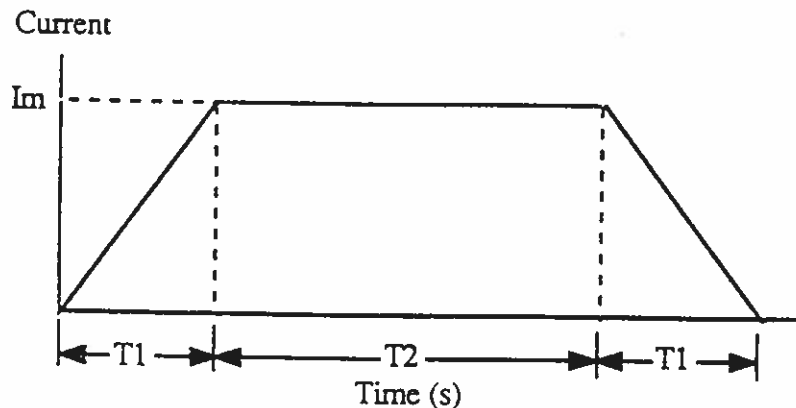
- Attempts to exceed values listed resulted in quench at or near the transition to flattop

### 2. Series AC tests

run	ramp rate	peak field	current
265	6.4 T/s	6.4 T	21 kA
266*	11	9.2	30
271	2.3	6.8	22 ramp+half sine
277	6.8	6.8	22 ramp+ripple

\* quench at transition to flattop

- Run 266 - no quench during ramp! Wire went to 100% of critical current



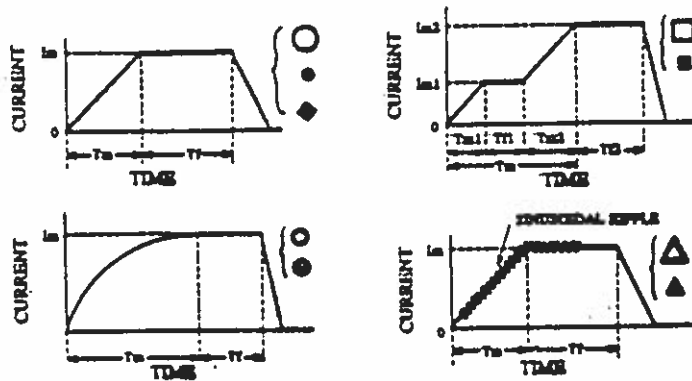
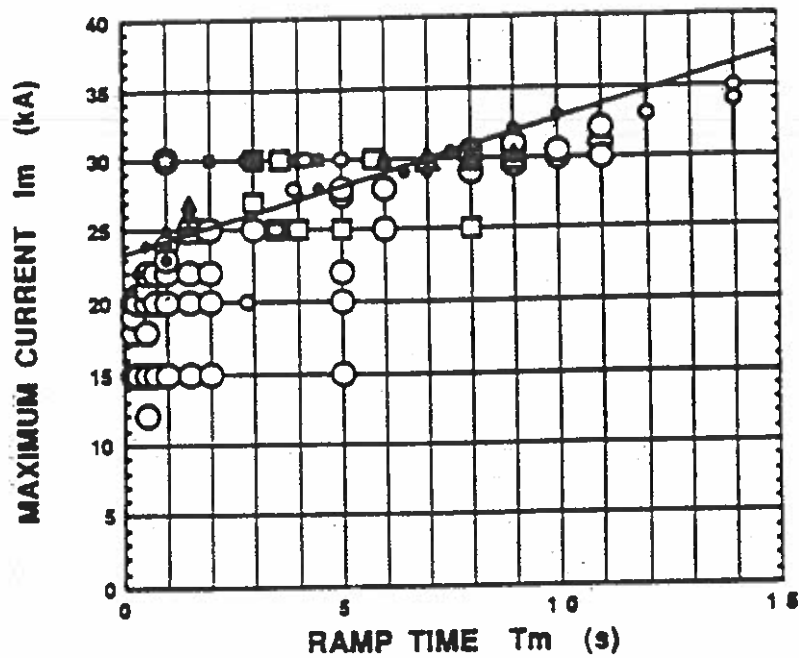
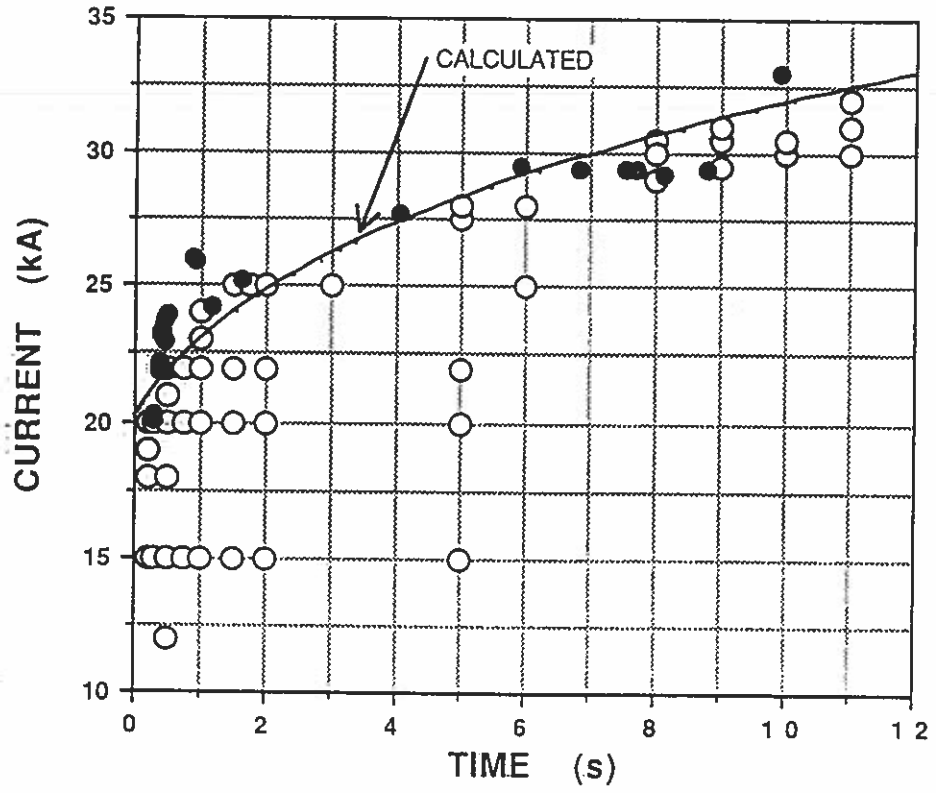


Fig. 7. Current versus ramp time in single-coil mode for four pulses: trapezoids (large circles; diamonds for joint quenches), two-step ramps (squares), ramps with rounded edges (small circles; crossed circles for quenches), and ramps with superimposed ripple (triangles). The solid marks indicate quenches. The circled star shows expected operation. The line is a fit to the solid circles (quenches with trapezoidal waveforms).

US-DPC SINGLE OPERATION  
(Quench Data : USVB-56  $V_b = 33$  mV)

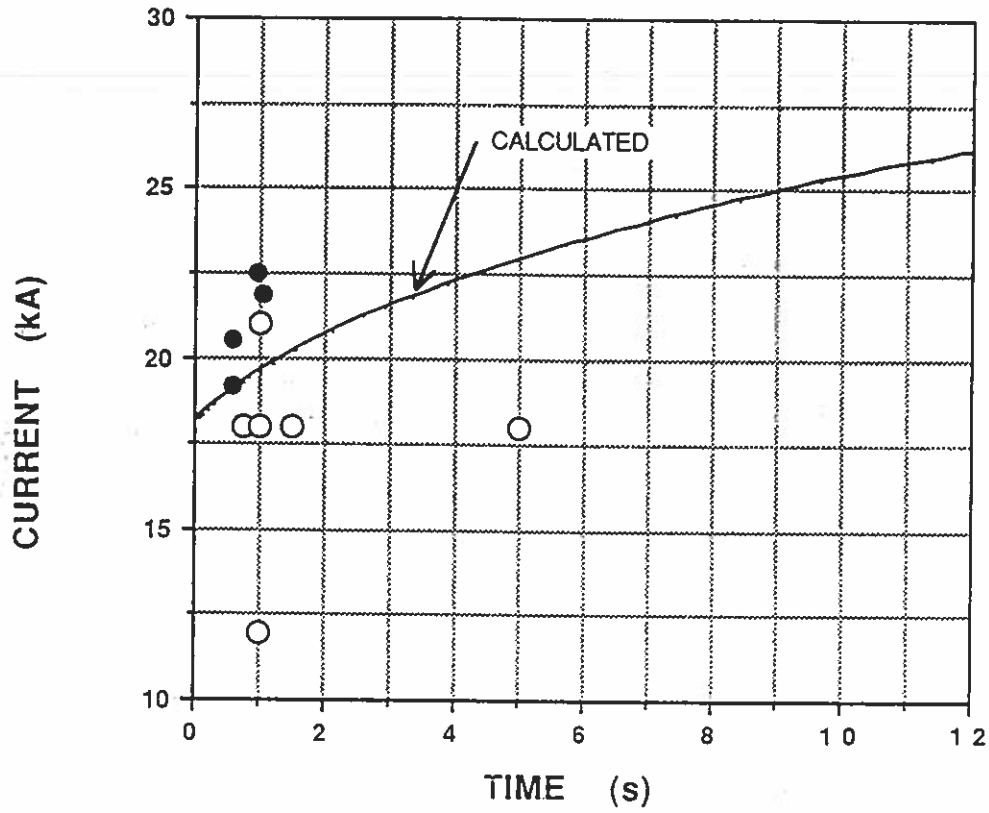
FILE : US-DPC FIT single



US-DPC SERIES OPERATION

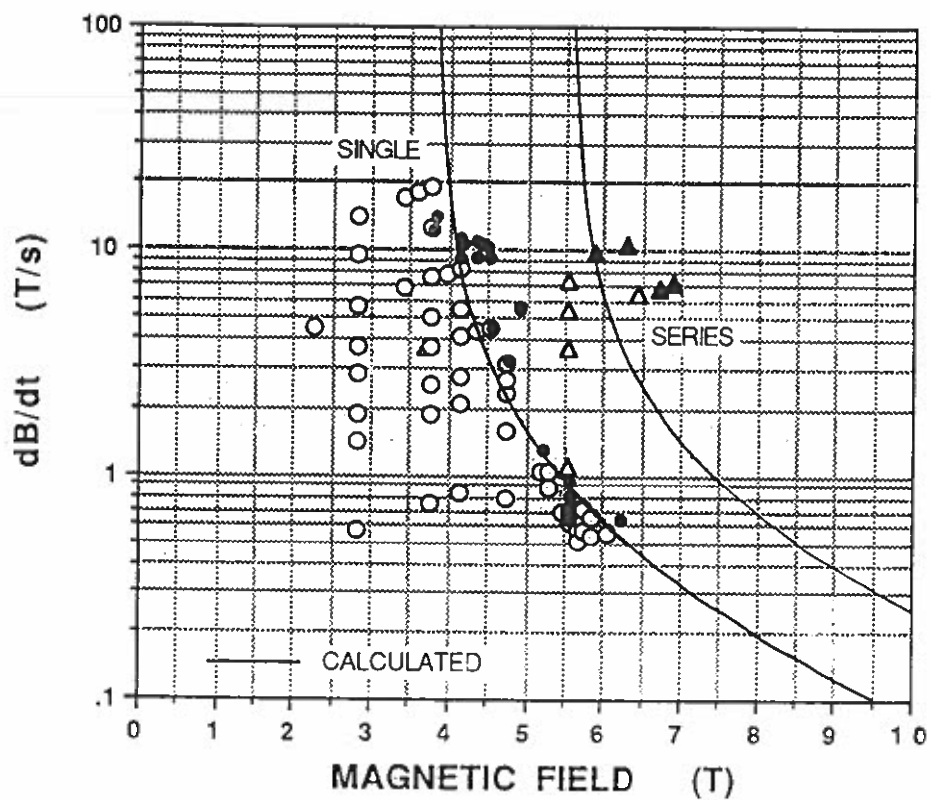
FILE : US-DPC FIT series 14/8-GF

(Quench Data : USVB-56  $V_b = 33$  mV)



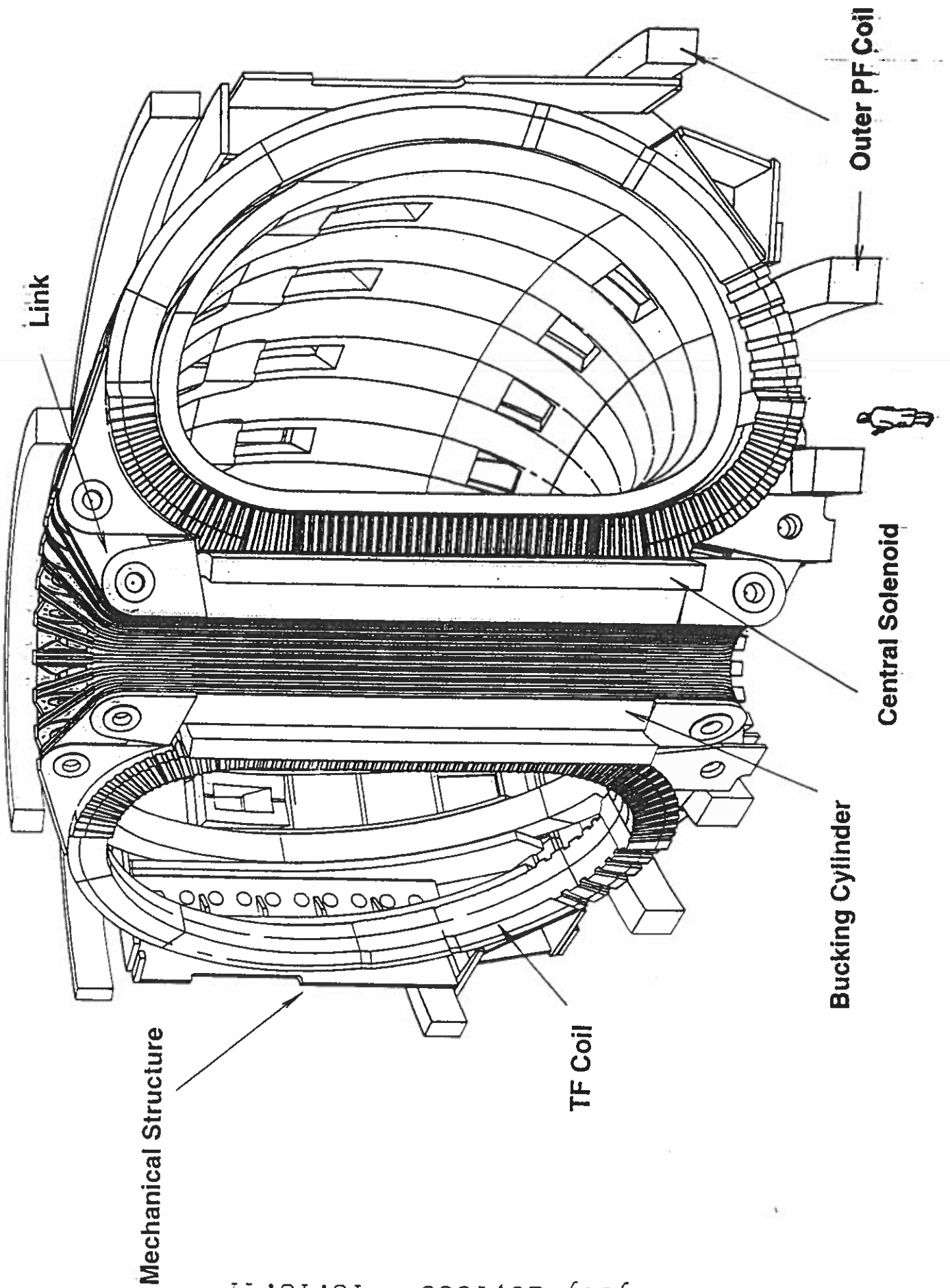
US-DPC SINGLE AND SERIES TESTS

FILE : US-DPC FIT dB 14/8-GF



## Summary of Important Results

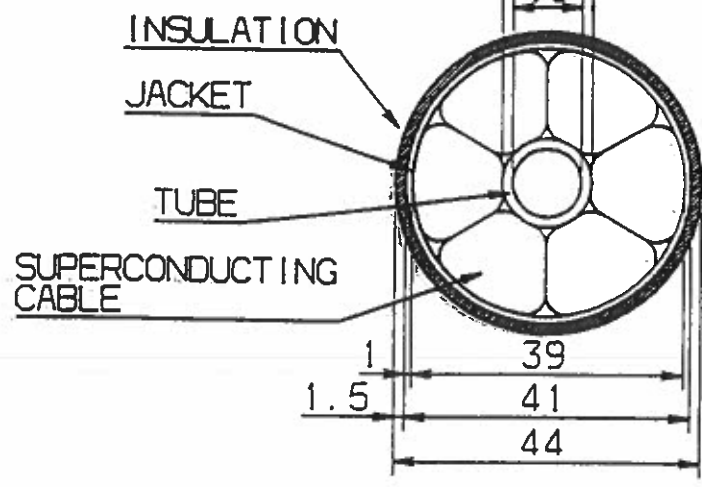
- *Induced flow* - high transient heat transfer, net mass flow required primarily for steady state heat removal, not for stability (Shanfield)
- *Effect of conduit material and void fraction on critical current* - strain effect on  $J_c$  due to different COE of conduit and  $Nb_3Sn$  strand (Steeves)
- *Development of strain compatible conduit material* - Incoloy development leading to INCO Alloy 908 (INCO and MIT (R. Ballinger))
- *Wind, react, insulate coil fabrication method* - MIT 12 T coil and US-DPC coil (Steeves, Olmstead and Hoenig).
- *Chrome plating* - to prevent sintering of strands and reduction of cable AC losses (Montgomery)
- *Dual channel cooling* - Used in US-DPC coil for enhanced heat removal (Hoenig)
- *Low resistance joints* - US-DPC coil, including parametric study of materials, processes and geometry affecting joint resistance (Steeves).
- *Stability characterization of  $Nb_3Sn$  cables* - experimental and theoretical (Minervini, Steeves, Hoenig, Schultz)
- *Ramp-Rate limitation in pulsed coil operation* - Testing of the US-DPC at JAERI
- *Characterization of inter-strand contact resistance under Lorentz force* - (Takayasu)
- *Calorimetric AC loss for simultaneous full-field and current swings* - (Gung, Takayasu)
- *Thick walled seamless Incoloy 908 conduit* - development for ITER (INCO, Steeves and Randall)  
- also material characterization and welding development (Hwang, Morra, Jang, Ballinger)
- *GEM conductor development and manufacturing* - Aluminum sheath protection and roll-forming of 18 m diameter turns. (Marston, Smith, Camille, Vieira, Hale, etc.)



YUUKIA PRIME 1 JULY 20, 1993 10.40.33

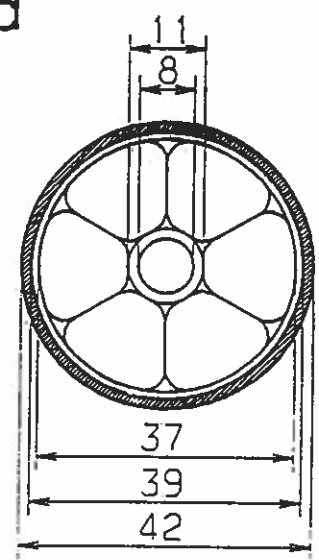
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### High Field



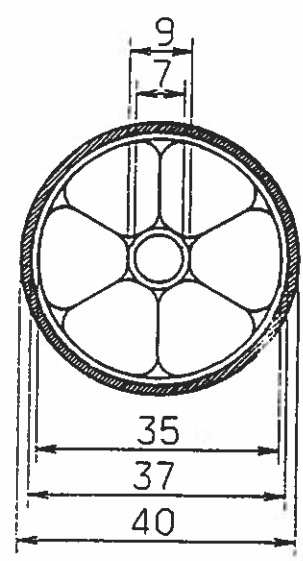
CONDUCTOR 1

### Medium Field



CONDUCTOR 2

### Low Field

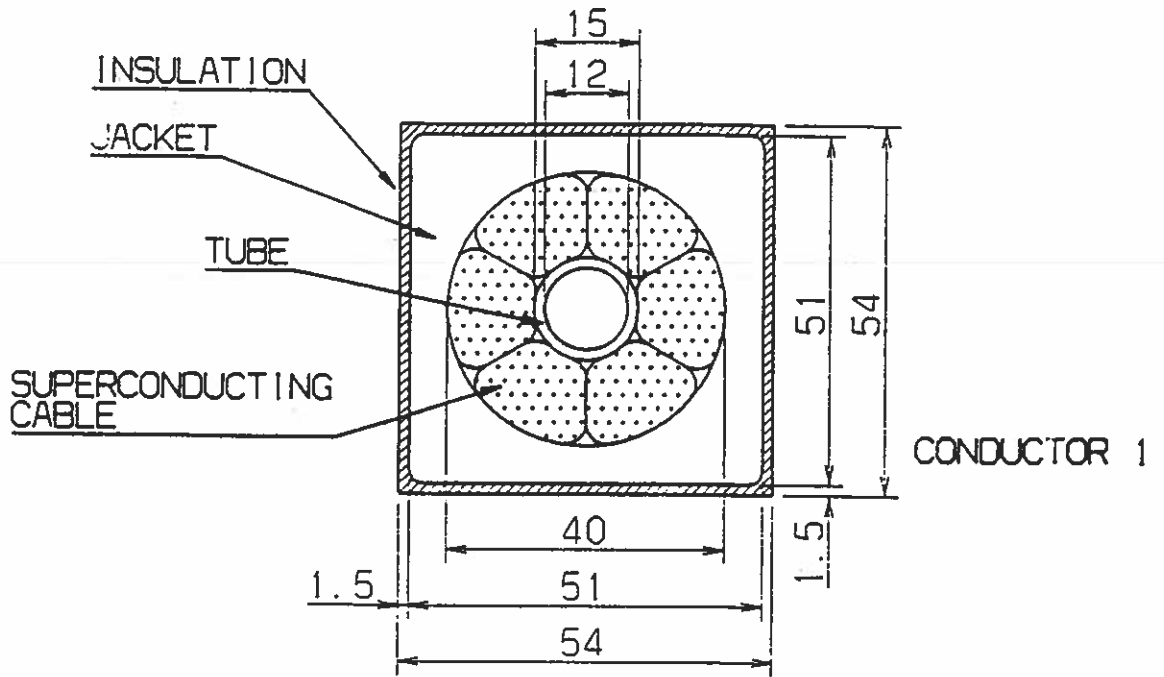


CONDUCTOR 3

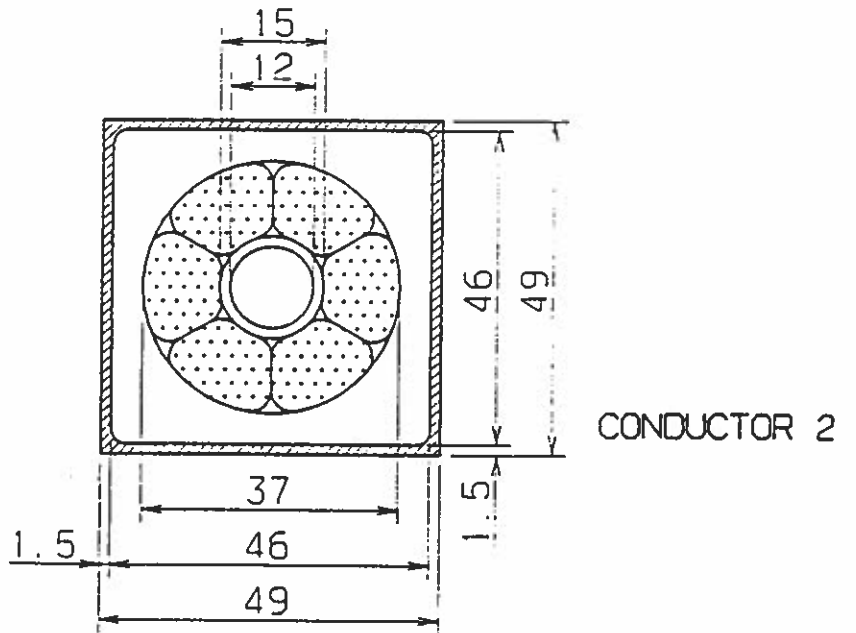


CS

### High Field



### Medium Field



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## Program for ITER Magnet R&D

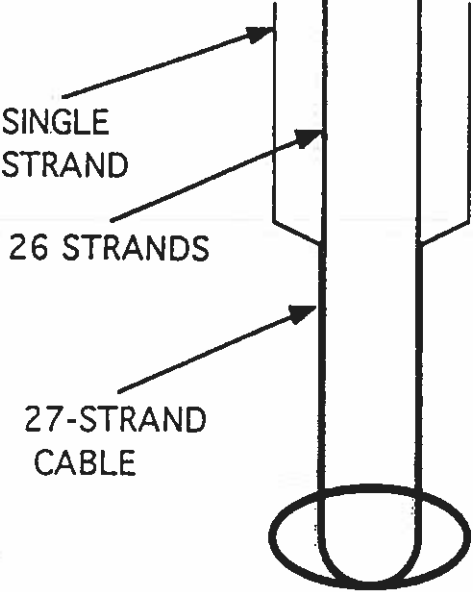
- Full-size conductor development for TF and CS model coils
  - strand development and procurement (w/ LLNL)
  - cable production
  - conduit production
  
- Model coil design and manufacturing
  - General Dynamics/Westinghouse* as prime industrial contractor
  
- Full-size conductor and joint testing
  - Program run by LLNL in FENIX facility
  
- Supporting laboratory and sub-size conductor R&D program

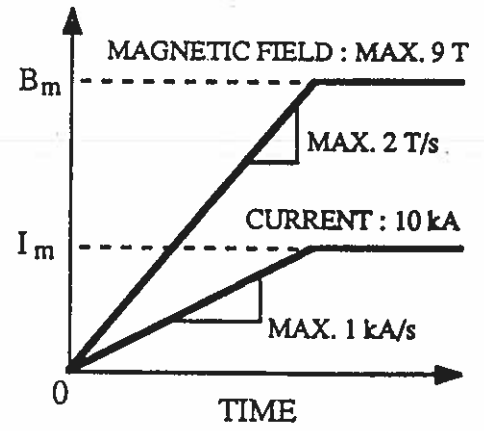
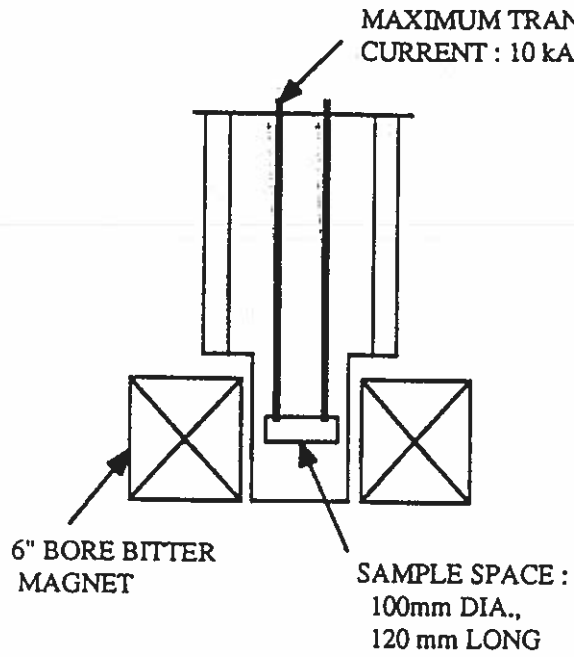
## Supporting Laboratory and Sub-Size R&D Program

- Materials database
  - Conduit physical, mechanical and processing properties (MIT & NIST)
  - Insulation physical, mechanical, radiation and processing properties (R. Reed, CTD, NIST, ...)
  
- Sub-Scale Tests and Measurements
  - Strand characterization (MIT, UW, BNL, NIST, LLNL)
  - Stability and ramp-rate
  - Quench detector development

*Focus is on:*

- simultaneous ramping of both current and field
- study of current distribution in cable during ramping
- effect of Lorentz force on contact resistance and AC losses

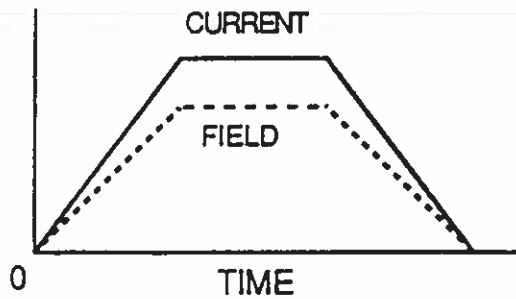




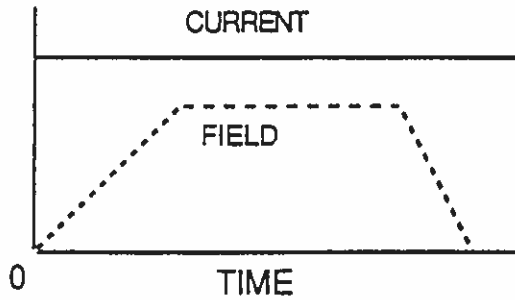
# RAMP RATE LIMITATION EXPERIMENTS USING 27-STRAND CABLE

## Experimental Method

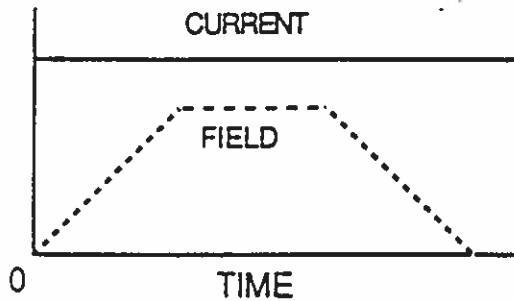
### a. US-DPC Simulation

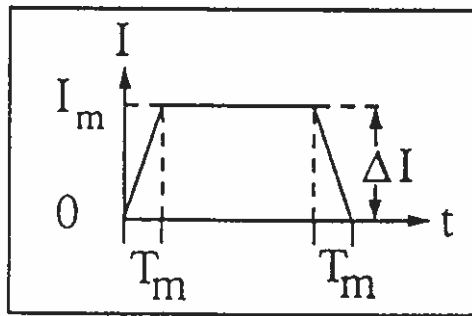
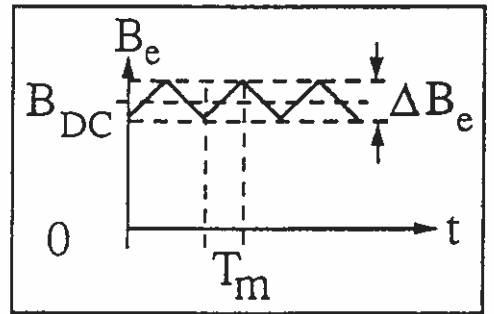
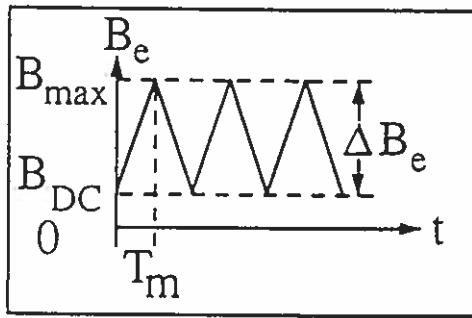
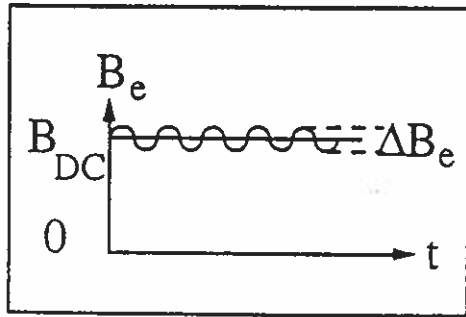
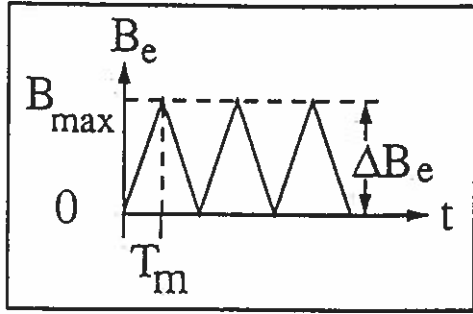


### b. Ramp-down Field with DC Current

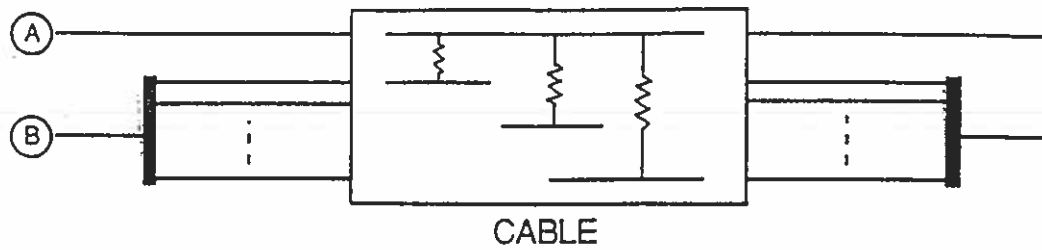


### c. Ramp-up Field with DC Current





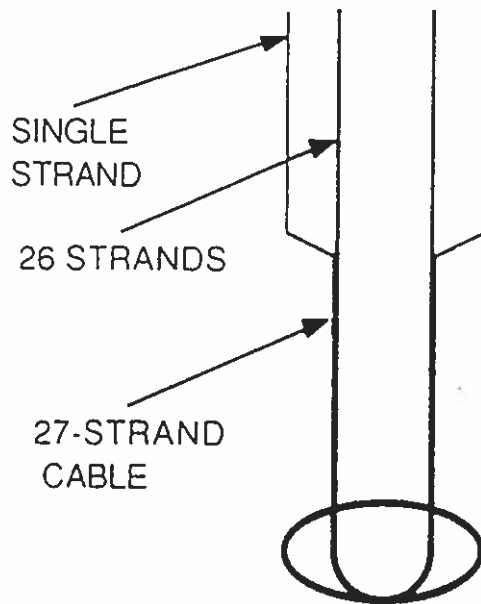
# CONTACT RESISTANCE BETWEEN STRANDS



## CONTACT CONDUCTANCE

$$G = \frac{1}{R} \quad (\text{mho/m})$$

R = Measured resistance R for 1 m cable between "A" and "B".





CONTACT RESISTANCE OF A SINGLE STRAND  
IN 27-STRAND CABLE

Data from "RAMP #11 RESIST-TB"  
FILE : RAMP #11 RESIST R v I-GF

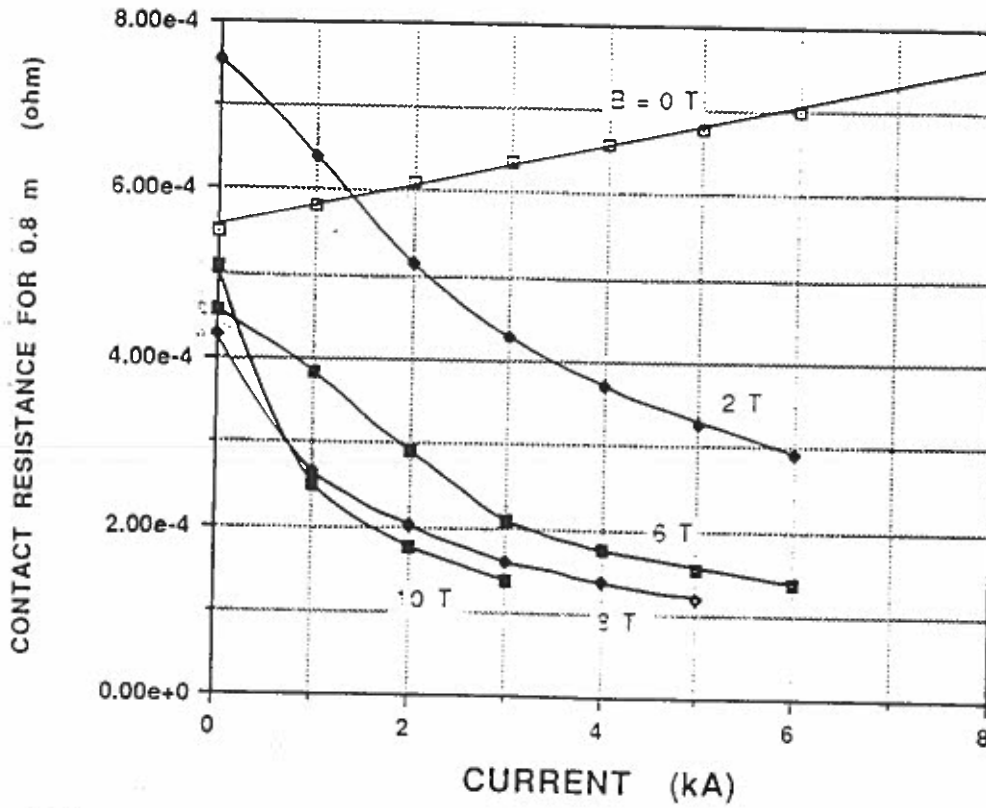


Fig. 1

CONTACT RESISTANCE OF A SINGLE STRAND  
IN 27-STRAND CABLE

Data from "RAMP #11 RESIST-TB"  
FILE : RAMP #11 RESIST v I-GF

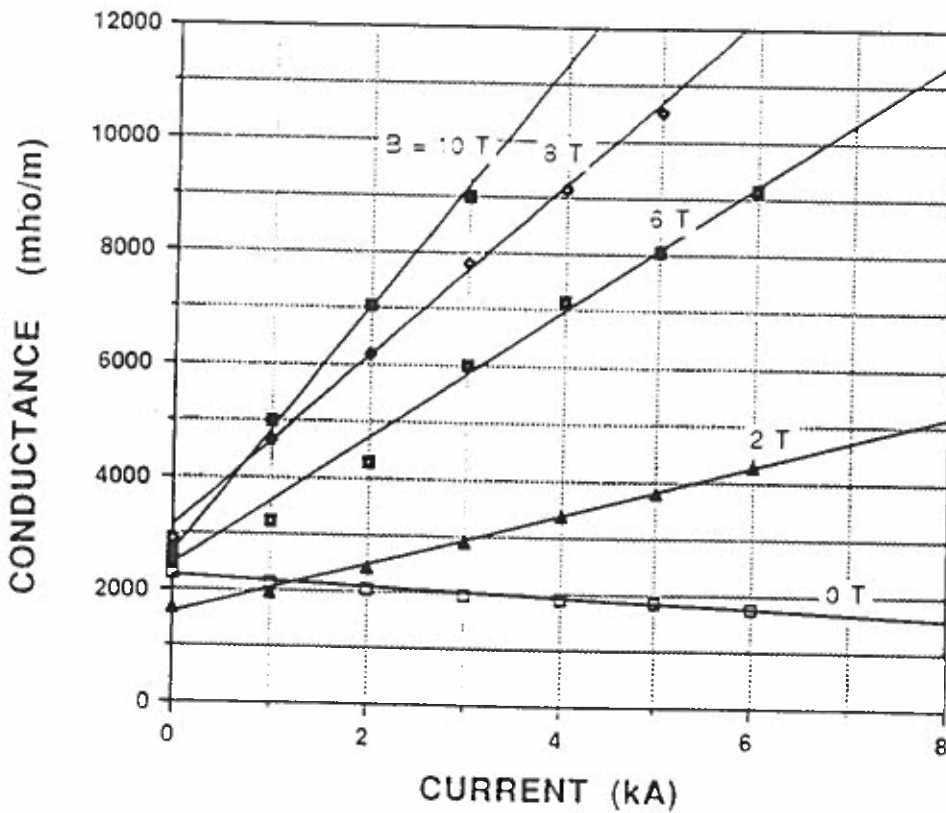


Fig. 2

CONTACT RESISTANCE OF A SINGLE STRAND  
IN 27-STRAND CABLE

Data from "RAMP #11 RESIST-TB"  
FILE : RAMP #11 RESIST-GF

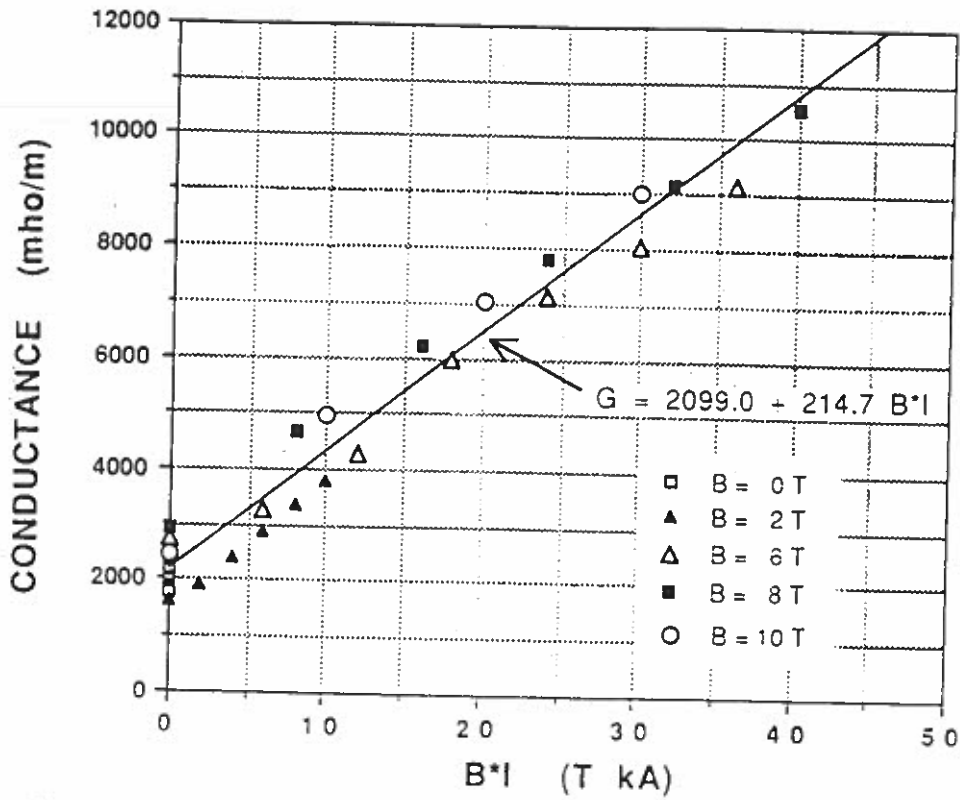
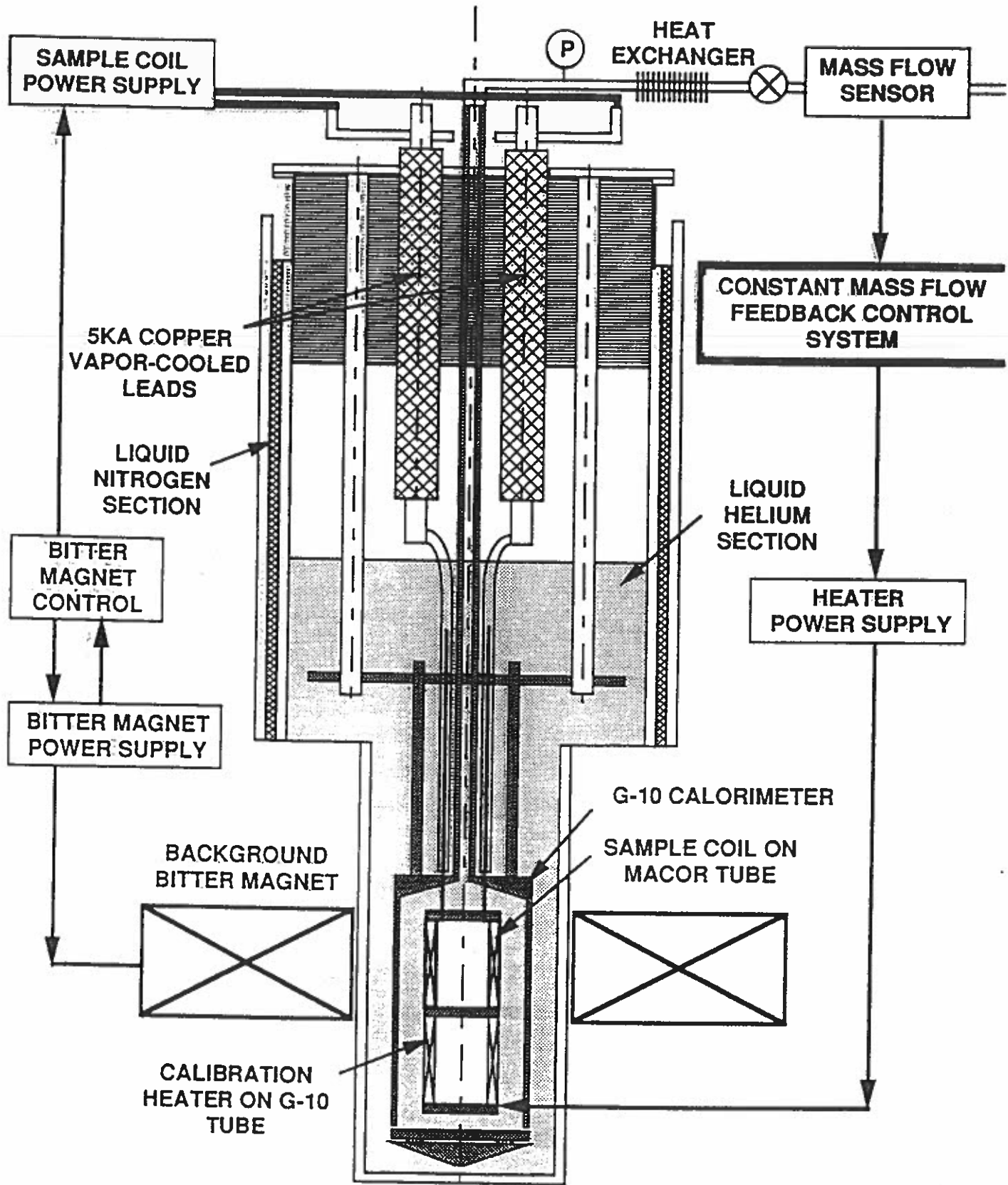


Fig. 3



EXPERIMENTAL SETUP OF ISOTHERMAL CALORIMETRIC AC-LOSS MEASUREMENT WITH CONSTANT-FLOW CONTROL SYSTEM