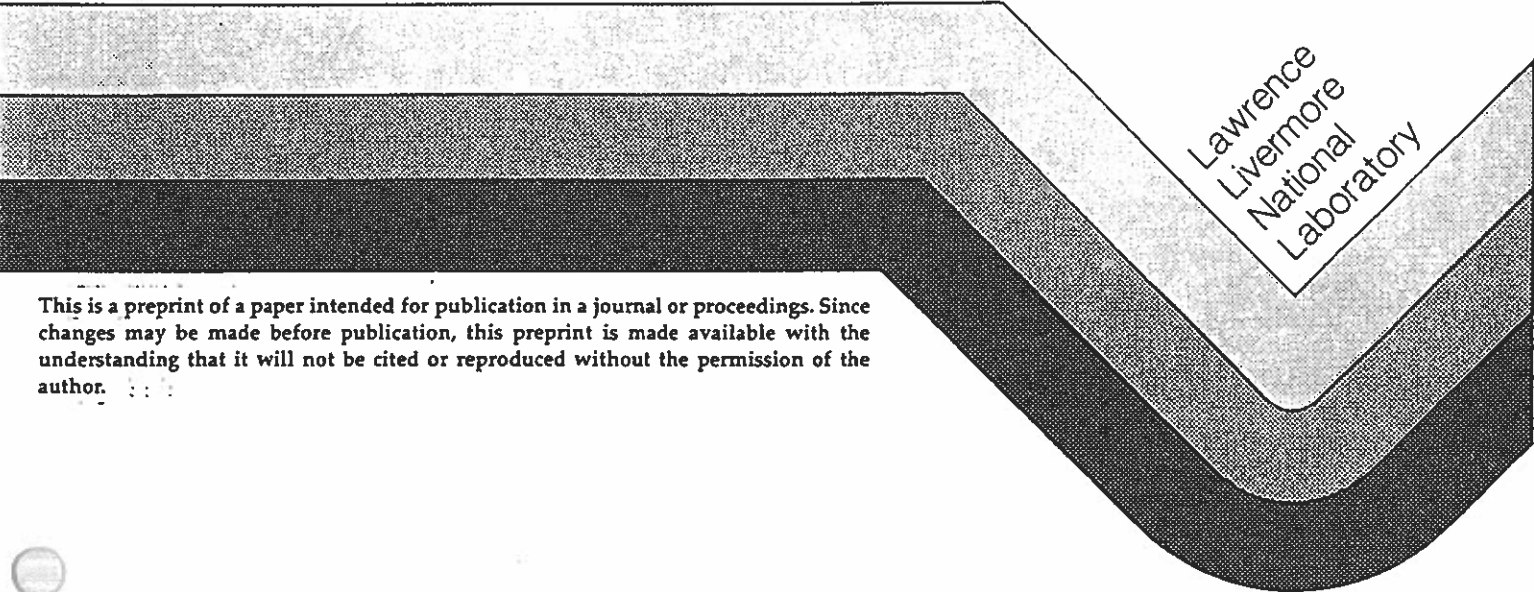


High-Field Conductor Testing at FENIX Facility

S.S. Shen, M.R. Chaplin, B. Felker,
W.V. Hassenzahl, K.I. Kishiyama,
and J.M. Parker

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Madison, WI
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April 5, 1993

The logo of Lawrence Livermore National Laboratory is a stylized, multi-layered 'V' shape. It consists of several horizontal bands of different shades of gray and black, creating a sense of depth and movement. The text 'Lawrence Livermore National Laboratory' is written in a sans-serif font, slanted upwards, across the right side of the 'V' shape.

Lawrence
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Livermore, CA 94551

Abstract

The Fusion ENgineering International eXperiments (FENIX) Test Facility,¹ which was commissioned at the end of 1991, is the first facility in the world capable of testing prototype conductors for the International Thermonuclear Experimental Reactor (ITER) superconducting magnets. The FENIX facility provides test conditions that simulate the ITER magnet operating environment; more importantly, it also accommodates specific experiments to determine the operational margins for the prototype conductors.

The FENIX facility generates magnetic fields close to 14 T and transport currents over 40 kA for testing the prototype conductors. This paper describes an experimental program that measures critical currents, current-sharing temperatures, forced-flow properties, and cyclic effects.

INTRODUCTION

In the current design of the ITER machine, the Nb₃Sn cable-in-conduit conductor (CICC) has been chosen for both the toroidal and central solenoid systems. For the ITER magnet research and development program, the fabrication and testing of short lengths of such conductors are of prominent importance. The FENIX facility was designed and constructed for meeting the urgent needs of the ITER conductor development program.

Construction started in 1989, and the facility was completed in early 1991. After a series of checkouts and modifications, the facility was commissioned for conductor testing in December 1991 (Fig. 1). The major operation parameters are listed in Table 1.

FACILITY OPERATION

Both the FENIX-magnet cryogenic systems and test-sample cryogenic systems are operating well and can fully simulate ITER operating conditions. The 14-T

Samples under test in FENIX are cooled by forced-flow helium. Room-temperature helium flows to the test well, passes through a counterflow heat exchanger in the upper part of the well, and then passes through a helium bath. Just past the bath, for each leg of the conductor sample, a heater is provided for each cooling circuit to control temperature. Flow returns from each leg to the counterflow heat exchanger and then exits with flow instrumentation and control. The instrumentation and control scheme, as shown in Fig. 2, is designed for

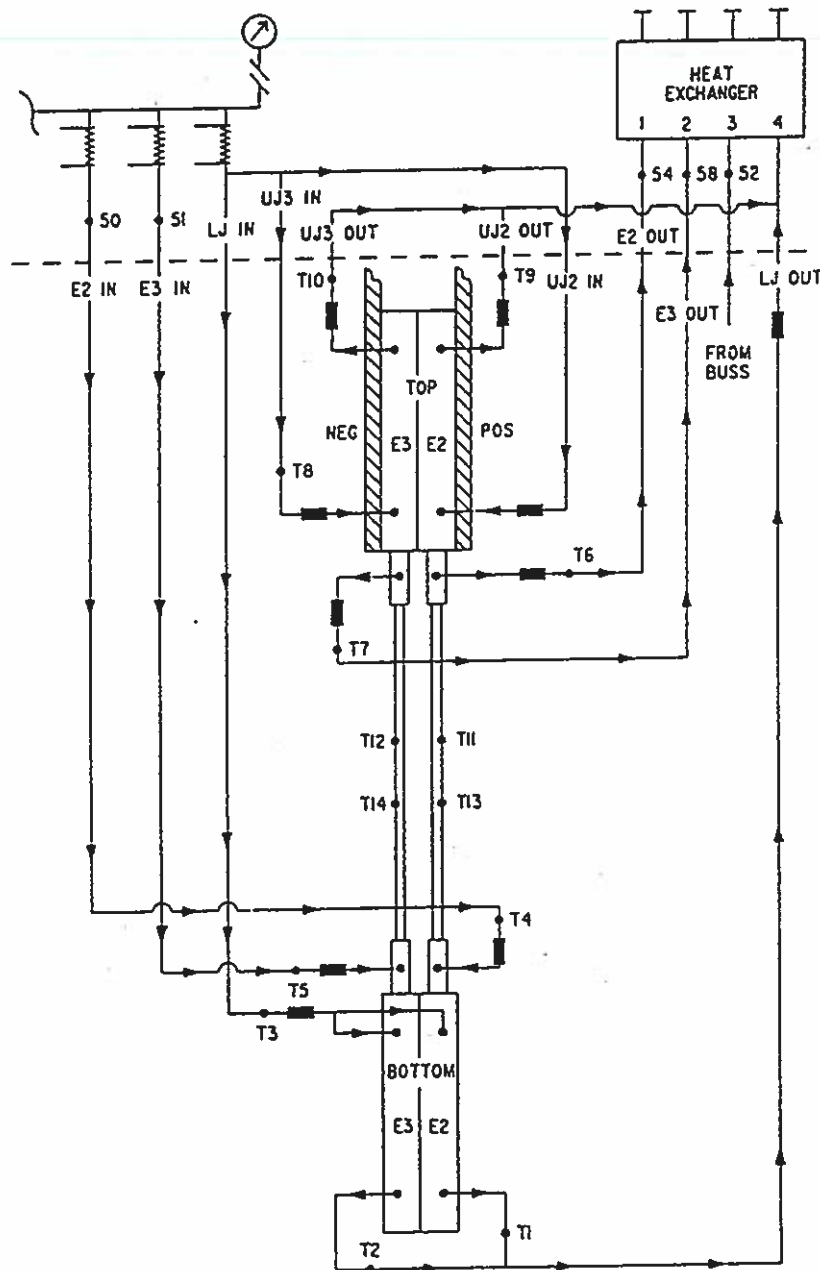


Fig. 2. Schematic of cryogenic instrumentation and control for typical FENIX sample conductor assembly.

CONDUCTOR TESTS AND RESULTS

In 1992 four sample conductors were tested in the FENIX facility through the ITER collaboration. The design features of each sample are summarized in Table 2. In Fig. 3, three European Community's/ITER sample cross sections are shown. An extensive test program was developed and executed to characterize these samples. Following is a summary of the test results of some specific experiments.

All sample conductors are designed for stable operation at 12.5 T and 40 kA. The FENIX facility not only validated the design parameters but also tested the conductors to the limits of temperature where current sharing takes place. Typical results of three EC samples are illustrated in Fig. 4, where the fitting to the results indicated that the effective strain on the strand was about -0.5%, which is considerably lower than expected for CICC conductor using stainless-steel sheath. This encouraging result also suggests that any degradation during the conductor fabrication process was minimal. Another major result is shown in Fig. 5, where the effect of forced-flow cooling on the performance of such large CICC conductor is illustrated by its current-sharing curves, measured by sample voltage versus temperature. The signatures of such effects are clearly seen on samples with different designs. The cyclic effects were also studied by pulsing a 40-kA current at 12.5 T field. The induced average transverse stress on the cable was estimated to be about 15 MPa. No degradation was detected after 6000 current cycles.

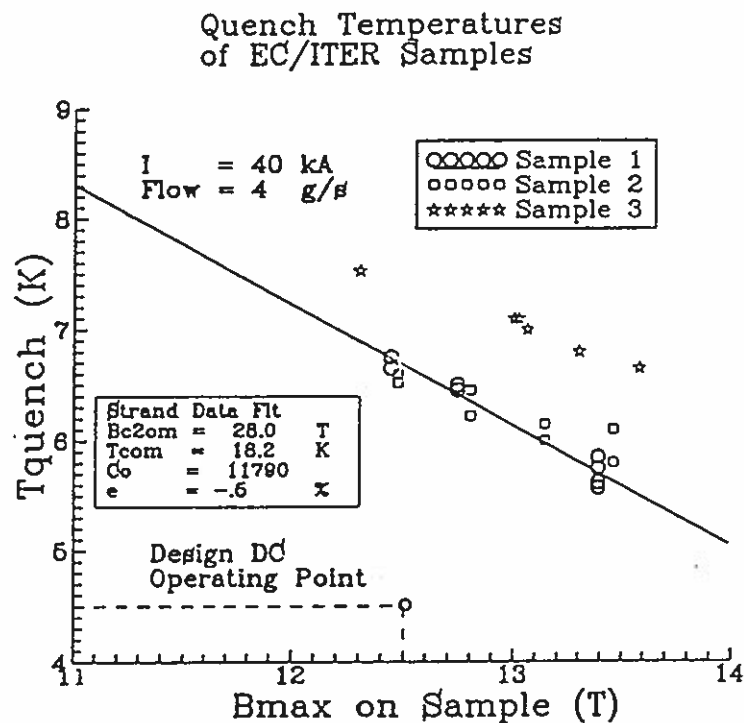
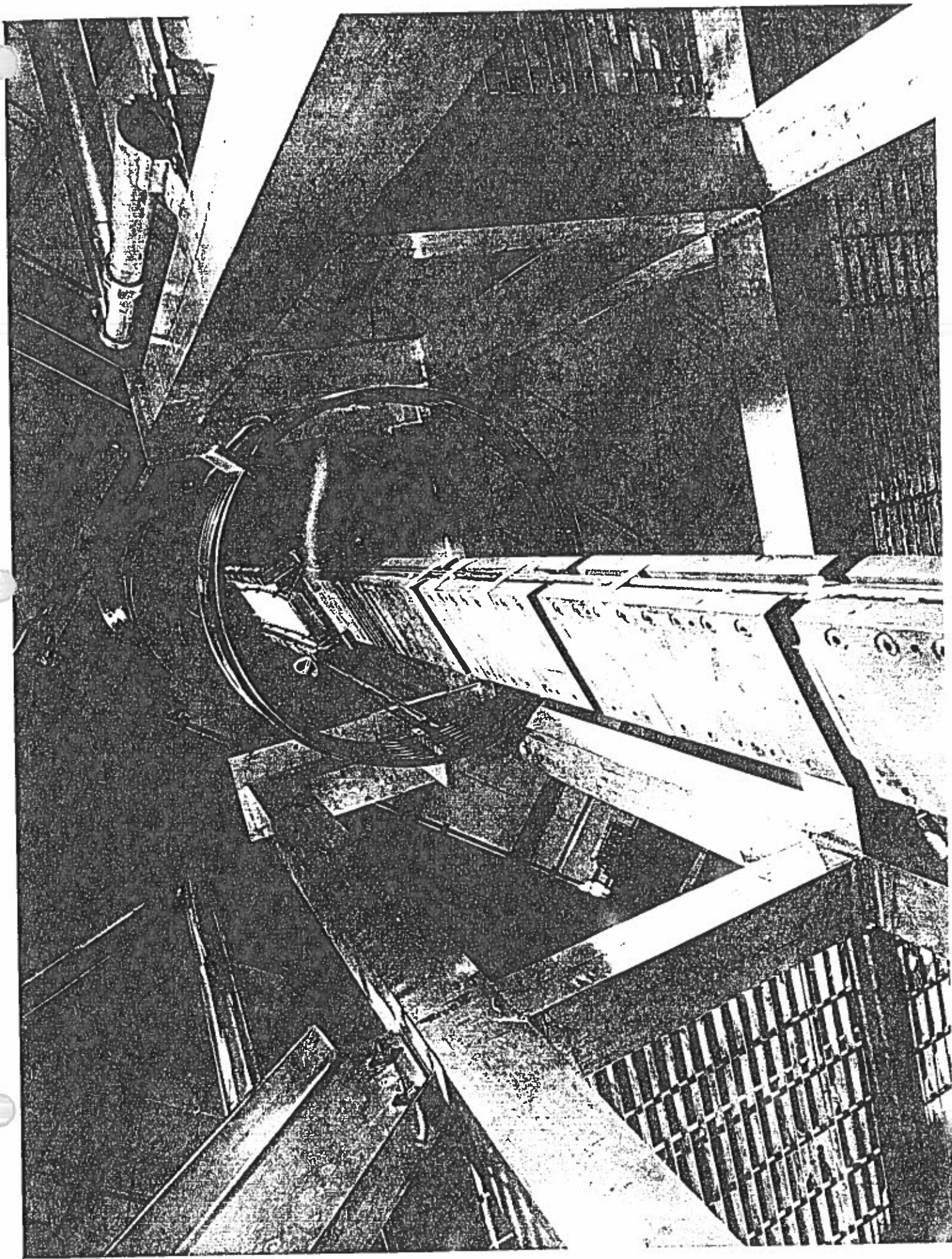
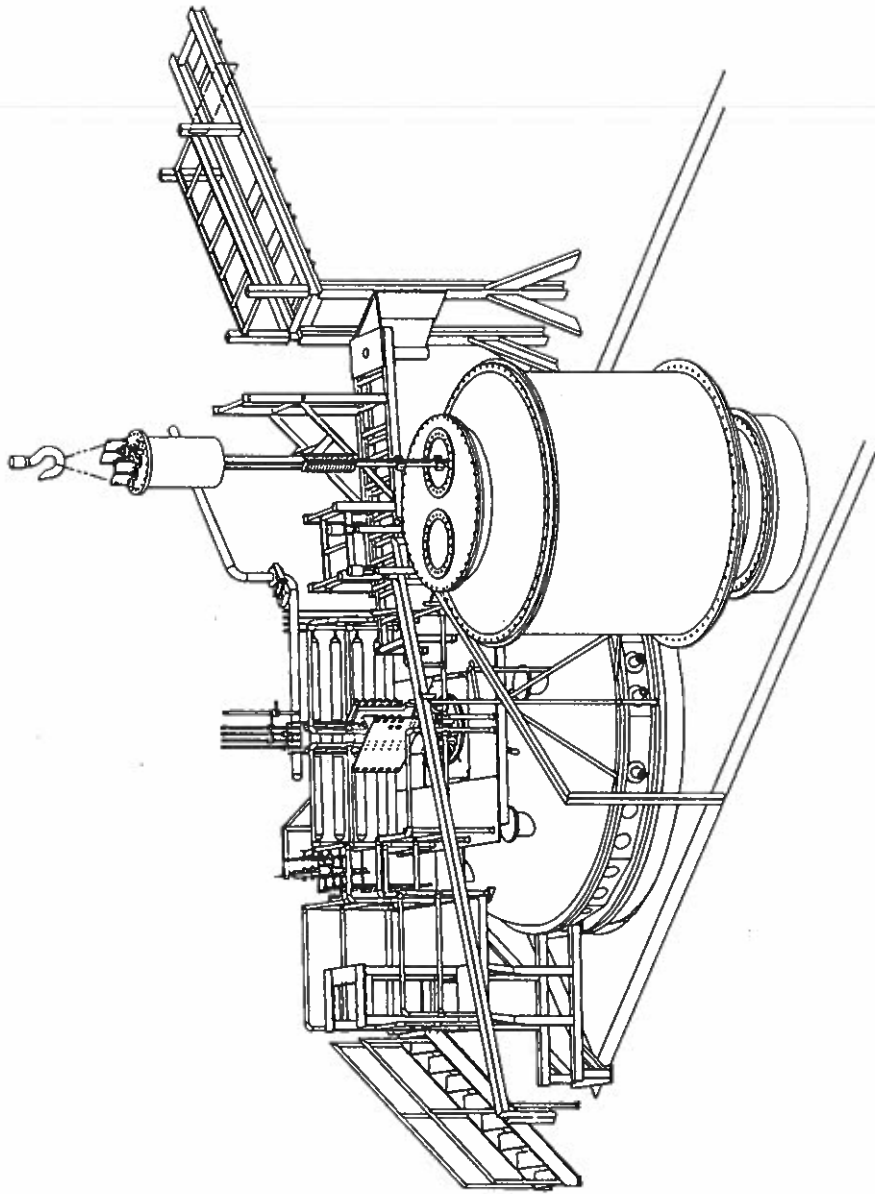


Fig. 4. Measured quench temperatures of EC/ITER samples





Experience with Testing & Application of CICC



High-Field Tests of ITER Prototype CICC

Stewart S. Shen
Applied Superconductivity Group
Lawrence Livermore National Laboratory

Presented at

CICC Workshop
Victoria, Canada
September 24, 1993

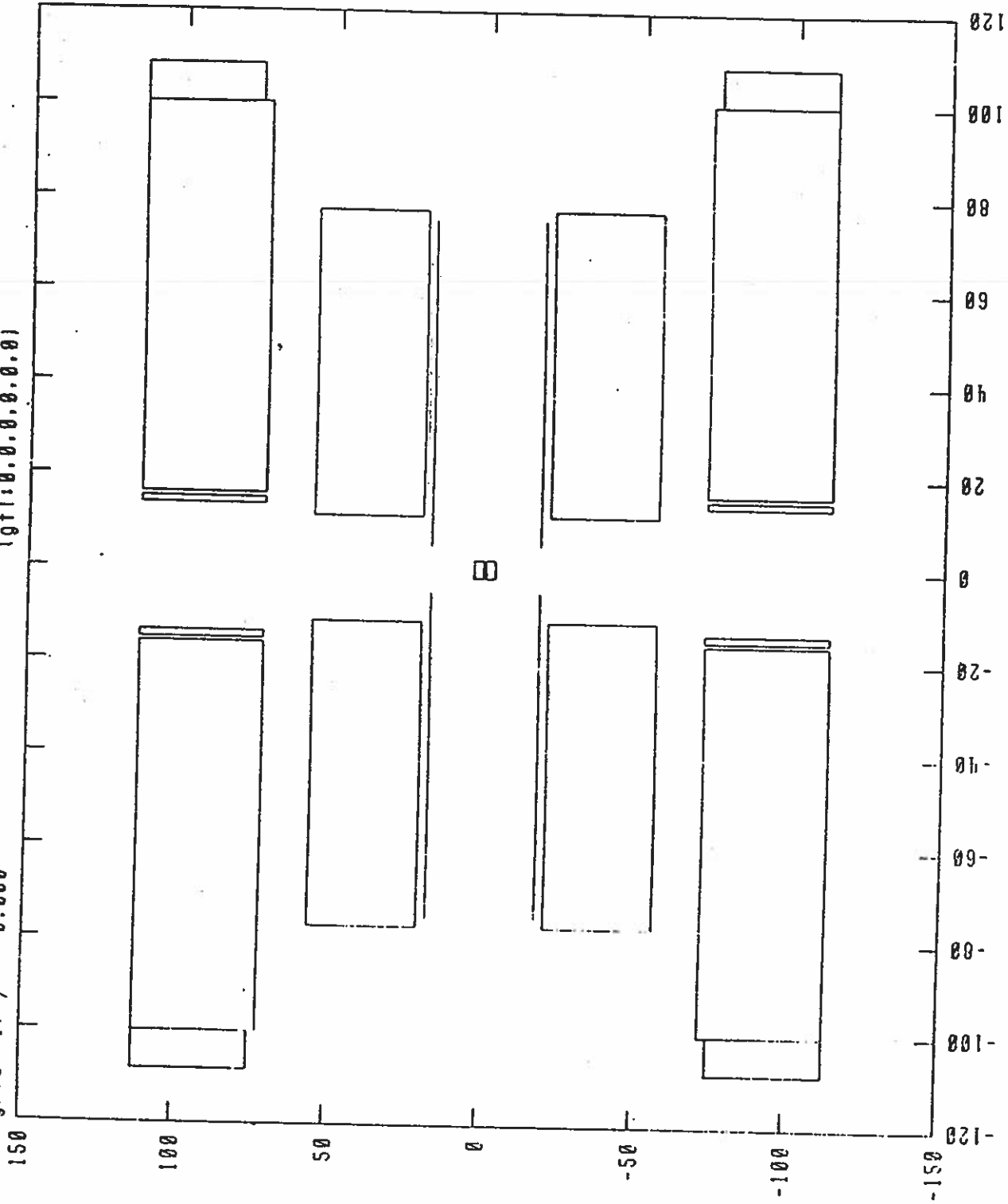
*This work was performed under the auspices of the U.S. Department of Energy by
Lawrence Livermore National Laboratory under contract number W-7405-ENG-48.*

TABLE 1
 MAJOR PARAMETERS OF FENIX CONDUCTOR TESTS

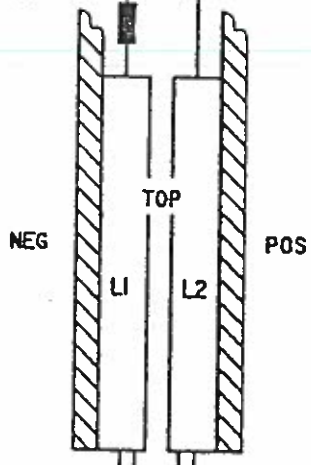
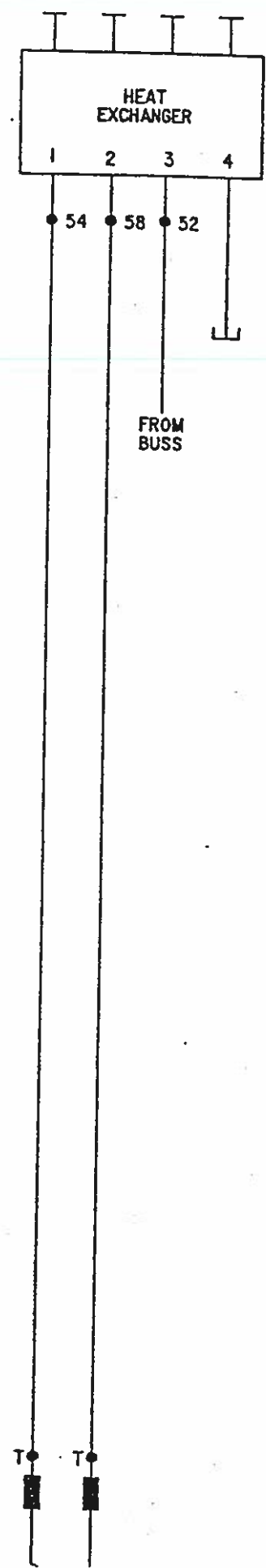
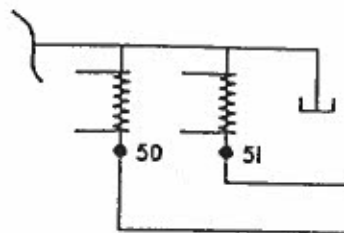
Maximum field	(T)	14
Maximum current	(kA)	50
Maximum conductor length	(m)	4.7 * 2
Uniform high-field length	(m)	0.4
Conductor forced cooling		
Number of paths		2
Inlet pressure	(MPa)	0.5 to 2.5
Maximum total flow rate	(g/s)	10
Conductor bath cooling		
Bath temperature	(K)	4.2 to 4.4

Fenix With Sample 8/1/90
Grid I. y. 0.000

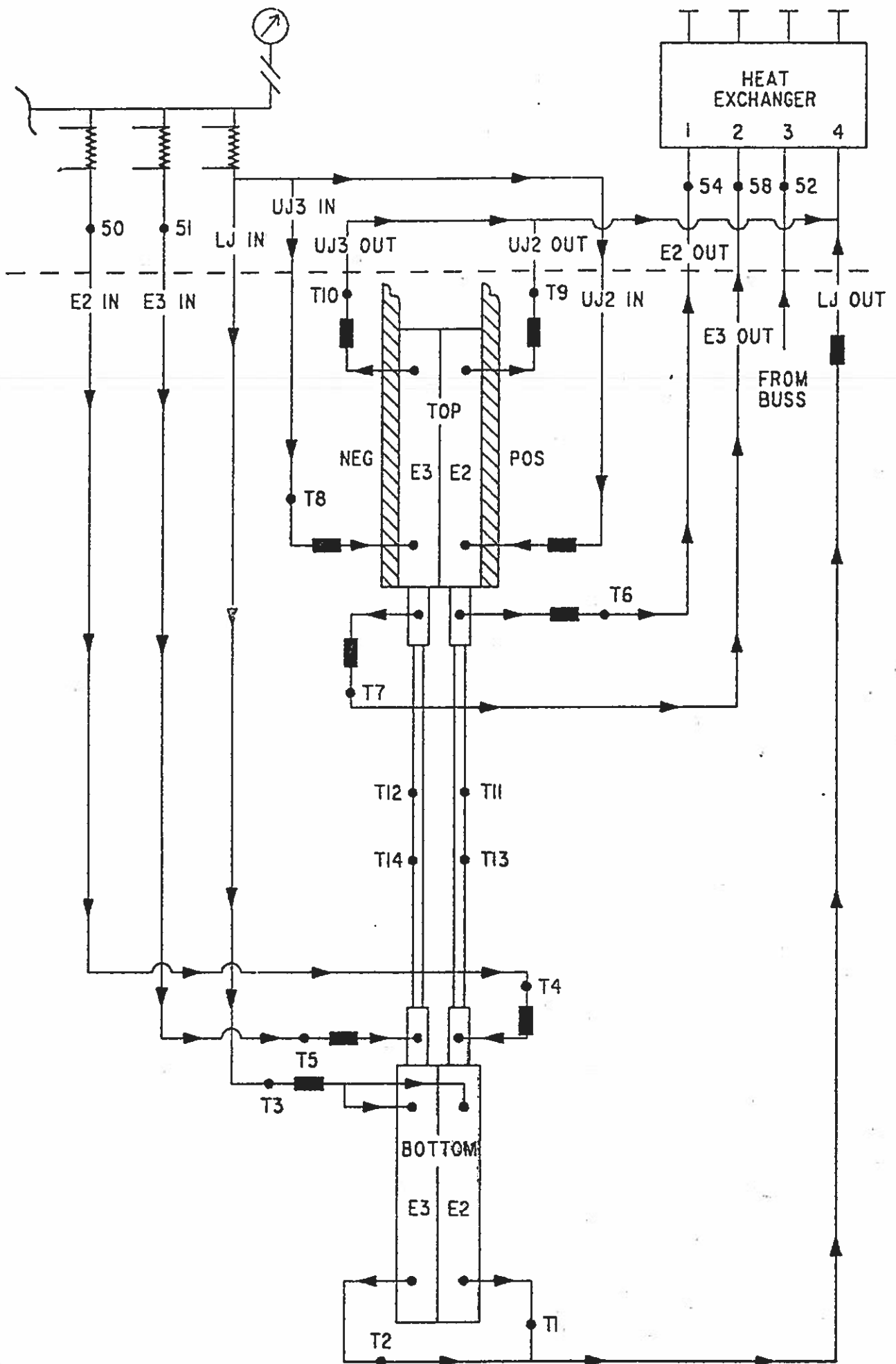
15:51:12 b 08/09/90
(gtl:0.0.0.0.0.0)

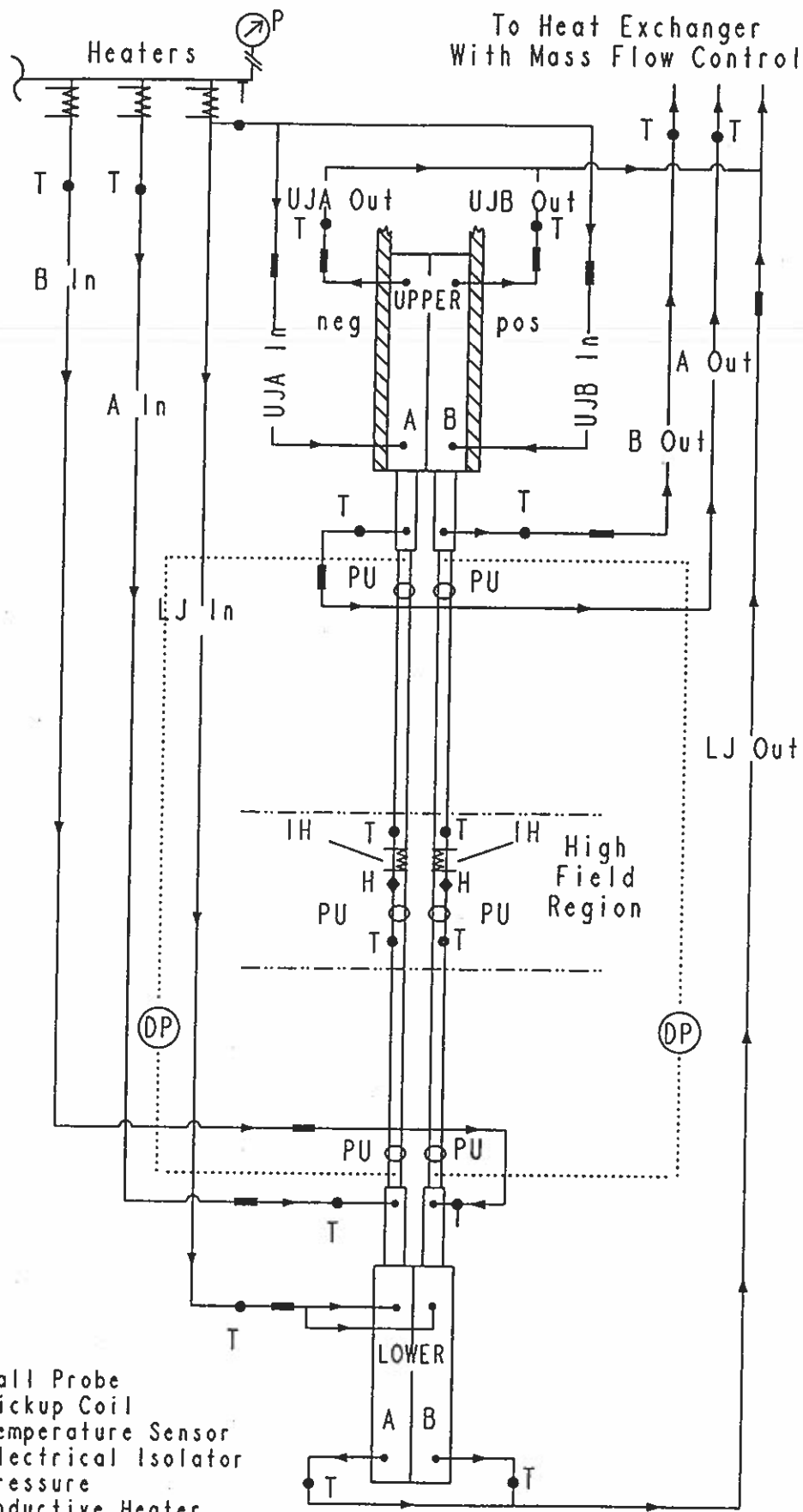


Fenix (with sample)



FENIX
 NET SAMPLE
 ABB
 3-04-91





- H Hall Probe
- PU Pickup Coil
- T Temperature Sensor
- Electrical Isolator
- P Pressure
- IH Inductive Heater
- DP Differential Pressure
- 14 Voltage Taps Per Conductor Leg Not Shown

FENIX Conductor Testing



Main Objective

To obtain the following properties of the ITER prototype conductor:

- Critical current and Tcs for field up to 14 T
- Forced-flow properties
- Cyclic fatigue effect
- Residual resistance ratio
- Stability tests by inductive heaters

and

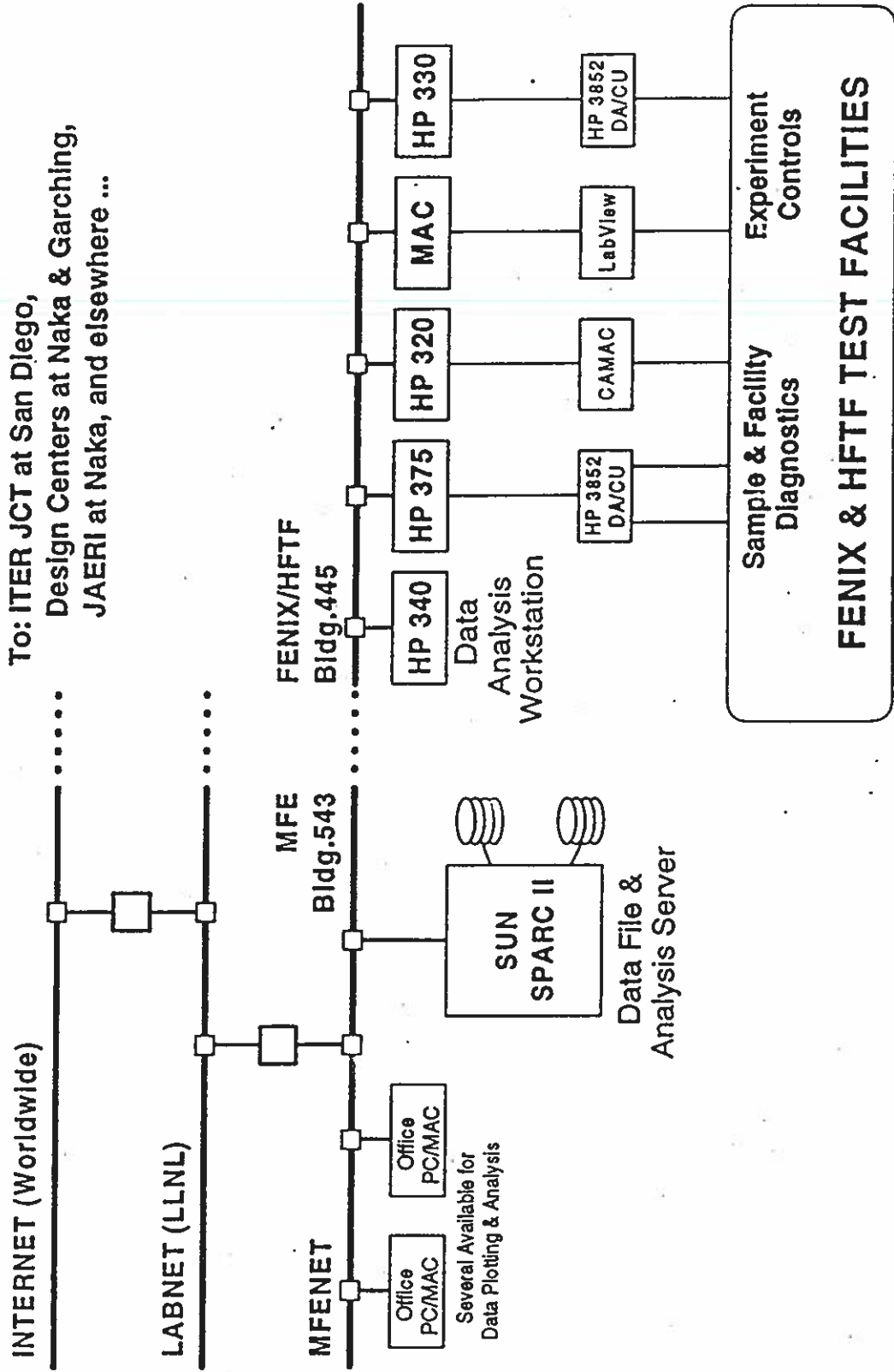
- Joints
- Quenching properties
- Pulsed-field effects.

Major CICC Design Parameters



Parameters	Descriptions	FENIX Experiments
Cable configurations	Cable patterns Cable composition (Cu) Voids arrangements (dual flow)	T _{cs} , stability T _{cs} , stability Flow, T _{cs} , stability
Cable insulations	Cr or alternatives	Ac losses, fatigue, stability
Superconductors	Nb ₃ Sn, Nb ₃ Al, NbTi	T _{cs}
Sheath materials	Incoloy, Ti and SS	T _{cs}
Joints	Butt, praying hands, shaking hands	T _{cs} , dc, and ac tests, stability, ac losses

FENIX Data Systems & Network



NET-LMI Sample, B=12.8T, FENIX Run # 453

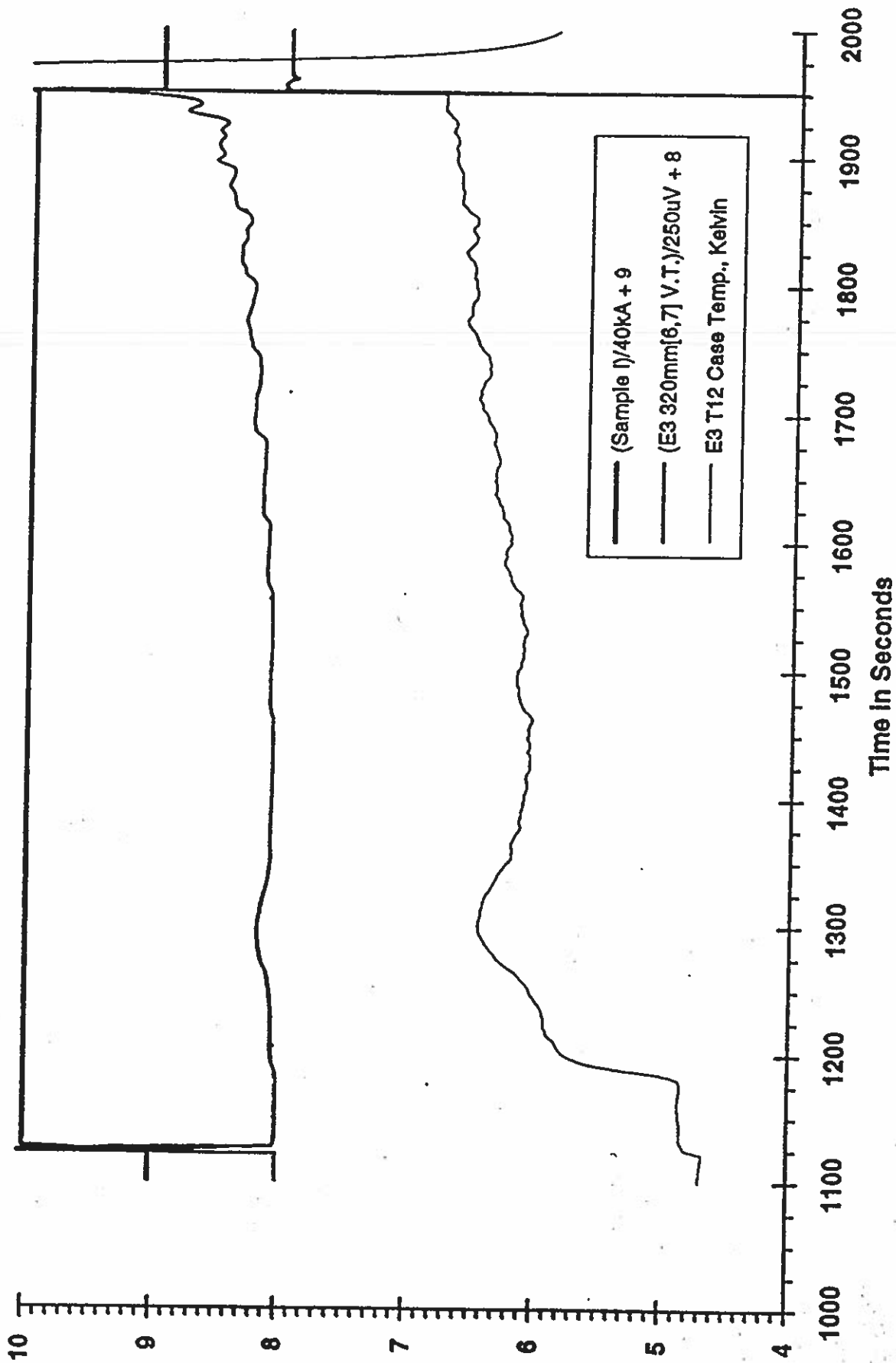
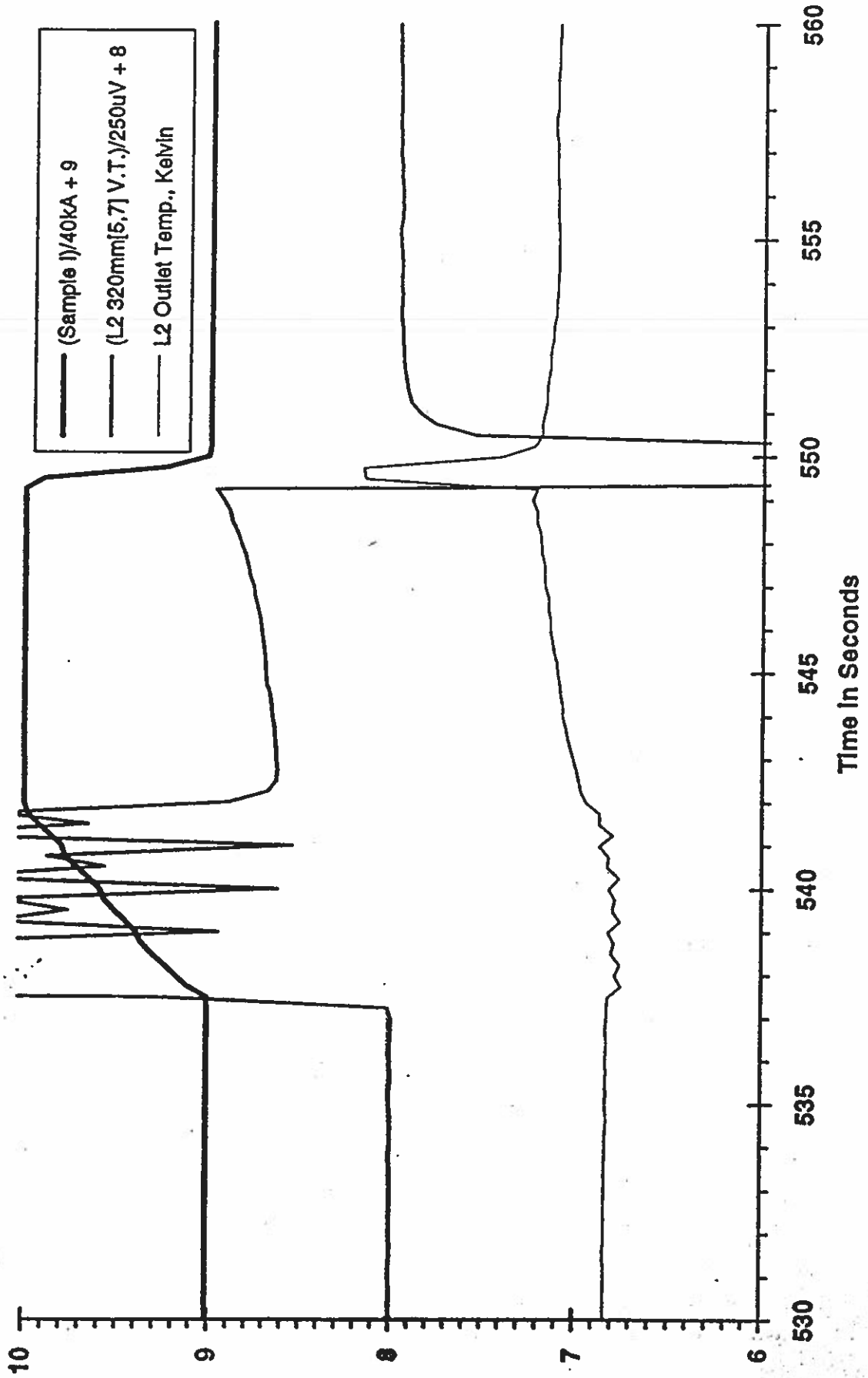
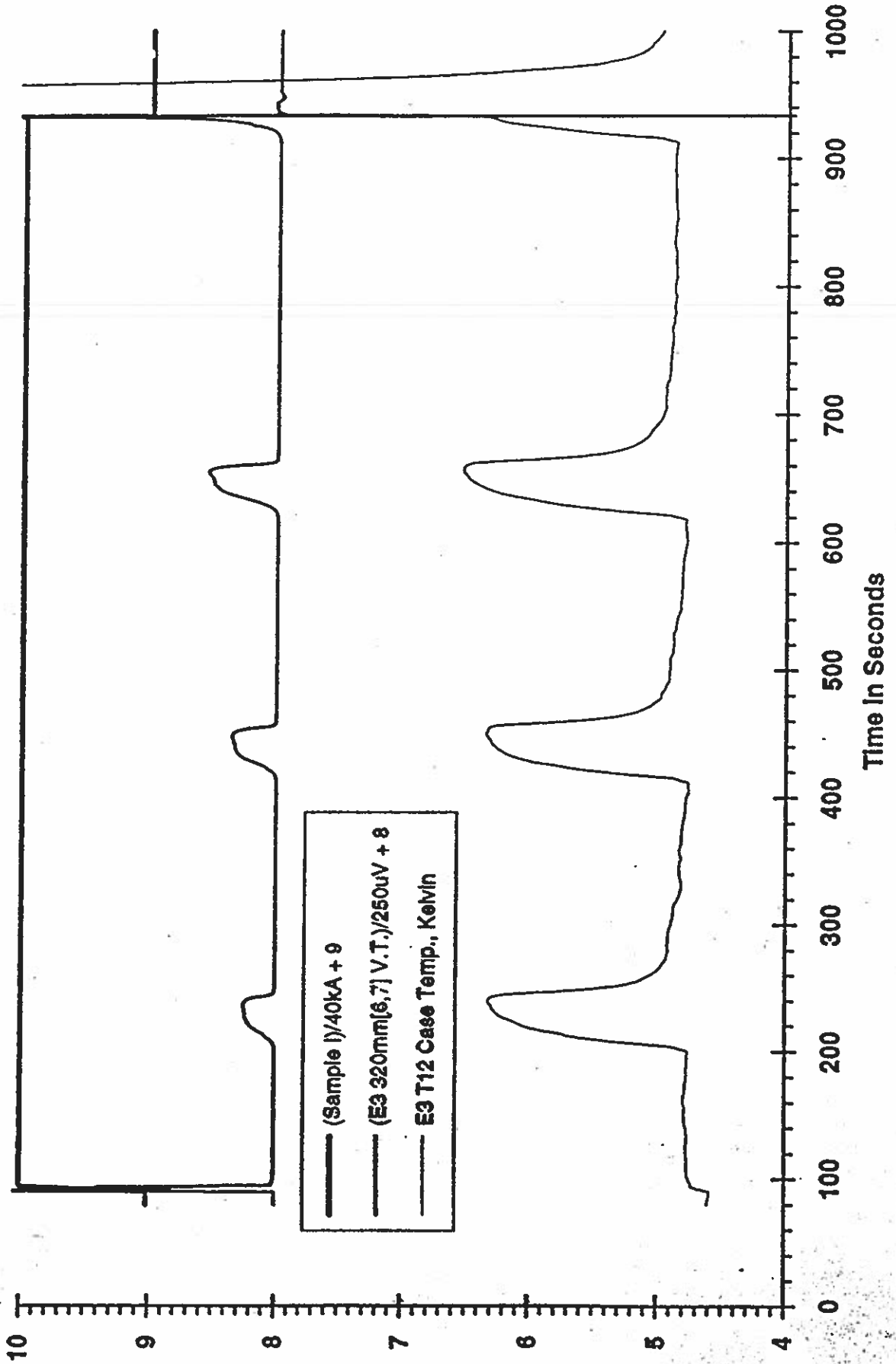


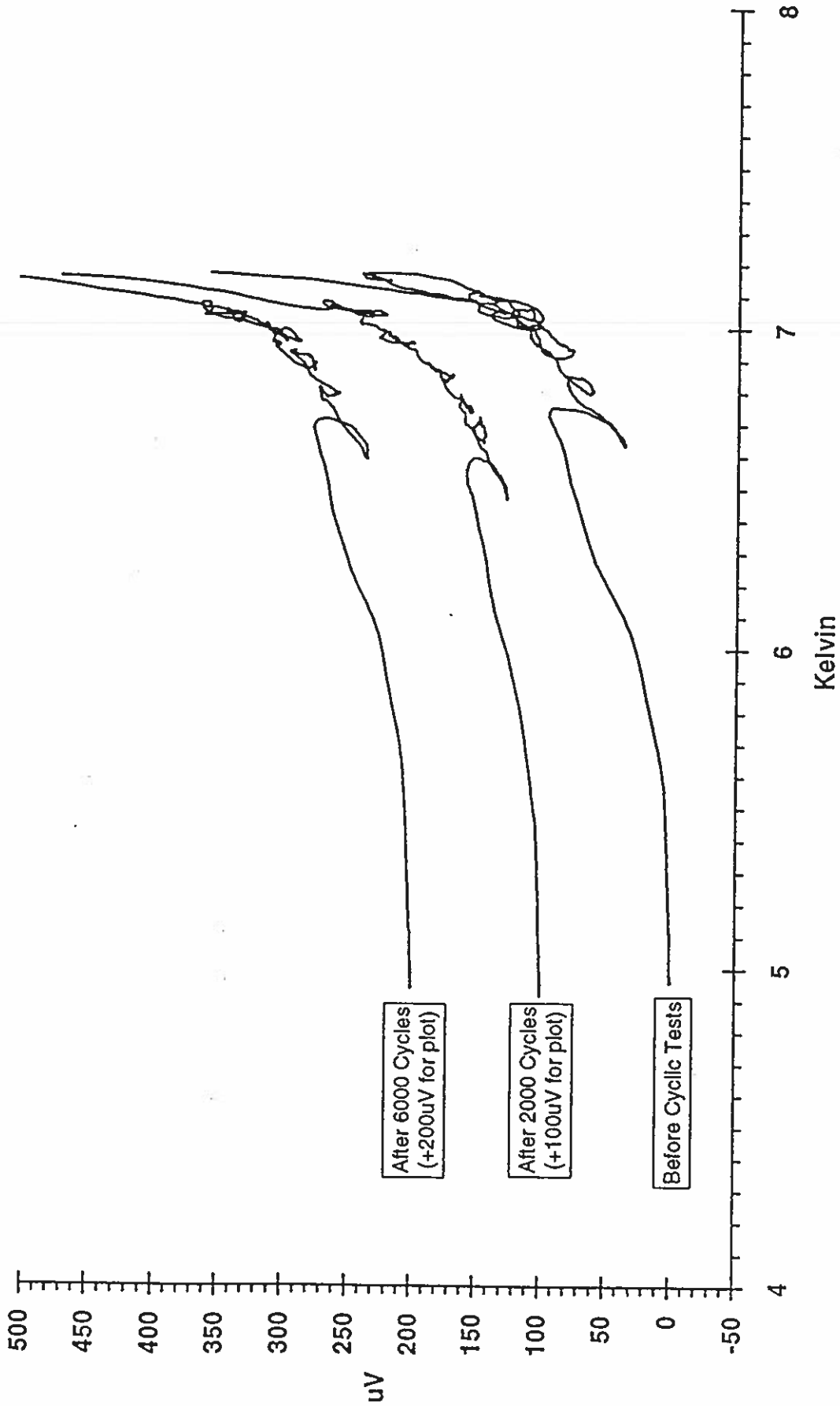
ABB-braided, B=11.8T, Run # 295
NET L1, L2 Sample at FENIX



NET-LMI Sample, B=12.8T, FENIX Run # 453



E3 320mm(6,7) Voltage Tap vs. E3 Case Temperature
I=40kA; B=12.5T; Run #s 538, 543, 549
NET-LMI Test Sample at FENIX

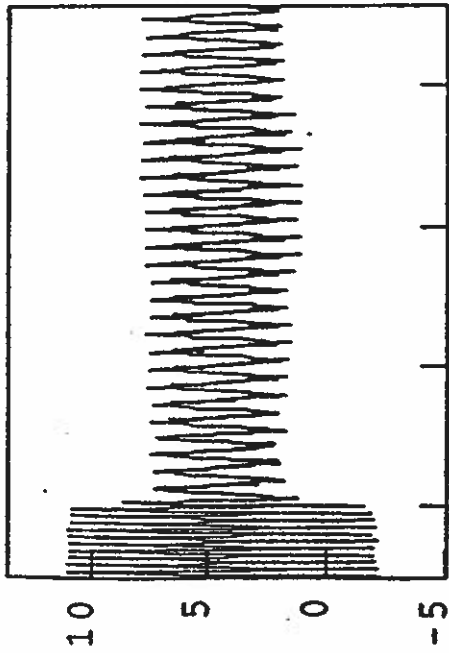


Full-Size Conductor Tests



- Stability Experiments
 - Stability margin
 - Ramp-rate limits
 - Current distribution
- RRR Measurements

v5a v5b vt filtered shot 10733



X
v 1
o 0
l ^
t -
s 3

time_2 seconds

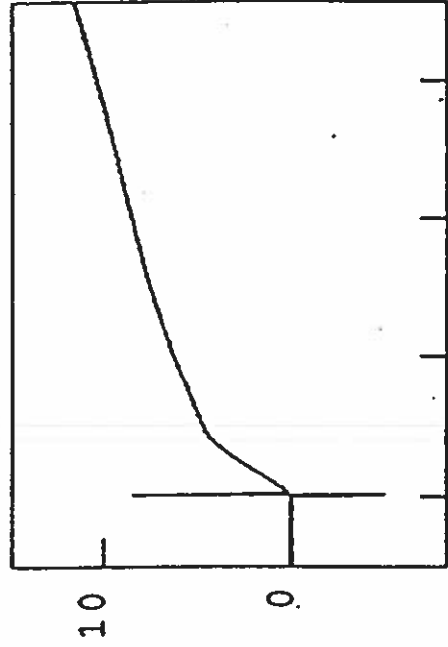
v12 v13 vt filtered shot 10733



X
v 1
o 0
l ^
t -
s 2

time_2 seconds

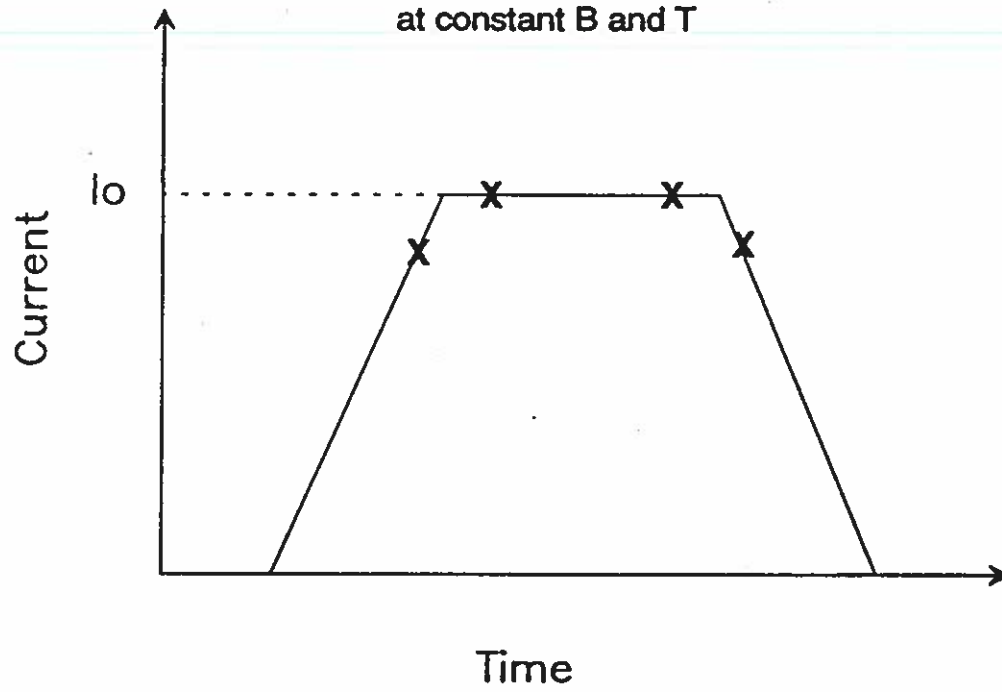
v10 v18 vt filtered shot 10733



time_2 seconds

**Normal-zone Voltage Measured
After A Conductor Quench
Induced By Inductive Heater Pulse
@ High Field (12 T) and
Constant Transport Current (30 kA)**

X Stability Tests
at constant B and T



Dynamic Stability Tests

LMI E2, E3 Sample, field = 12.8T run #4
 Date of Test - 9 Jun 1992
 vs Real Time 5 Seconds/Centimeter

E3 Case CGR T12 .2 Kelvin/cm From 10

E3 Case CGR T14 .2 Kelvin/cm From 10

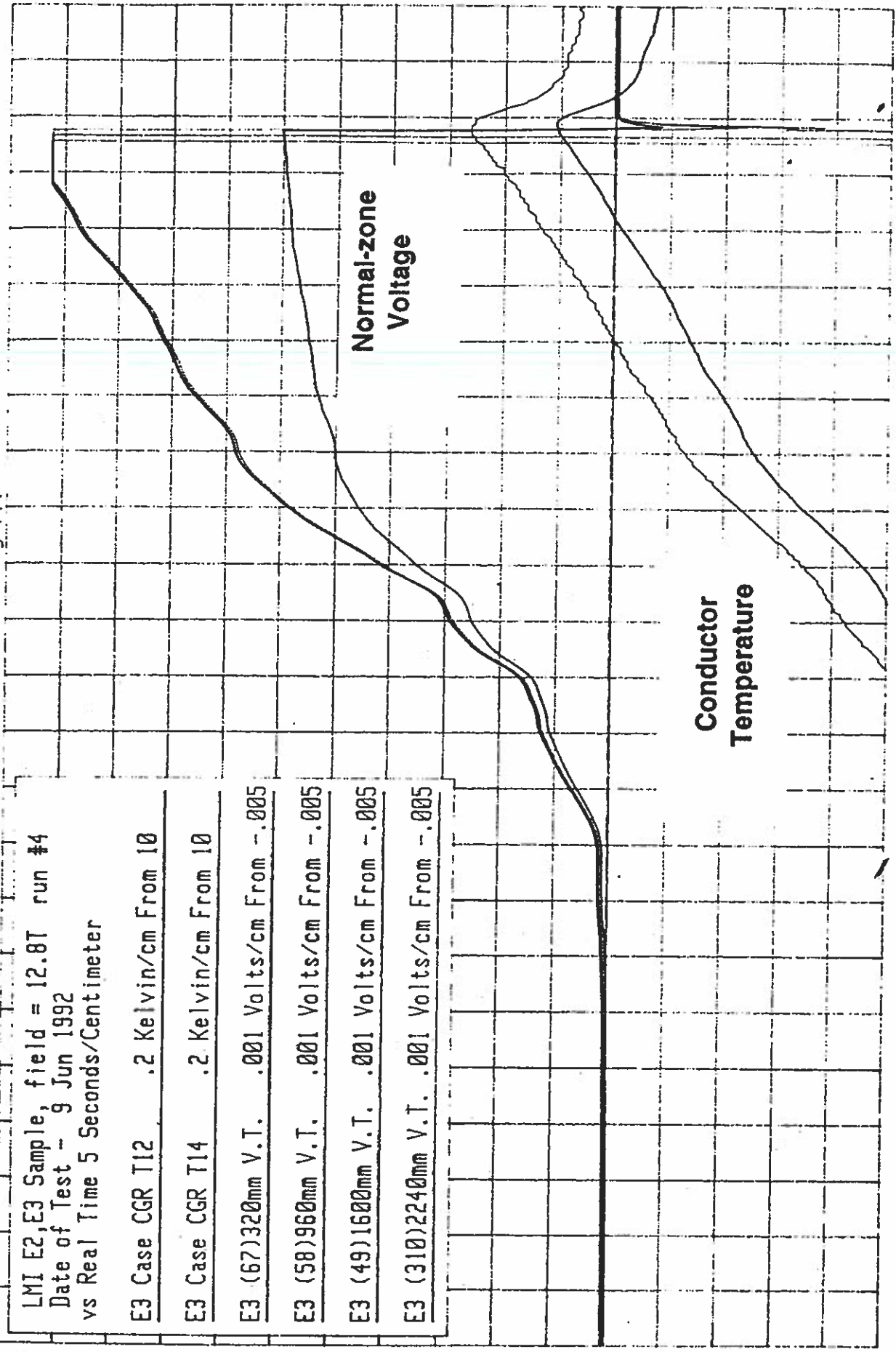
E3 (67)320mm V.T. .001 Volts/cm From -.005

E3 (58)960mm V.T. .001 Volts/cm From -.005

E3 (49)1600mm V.T. .001 Volts/cm From -.005

E3 (310)2240mm V.T. .001 Volts/cm From -.005

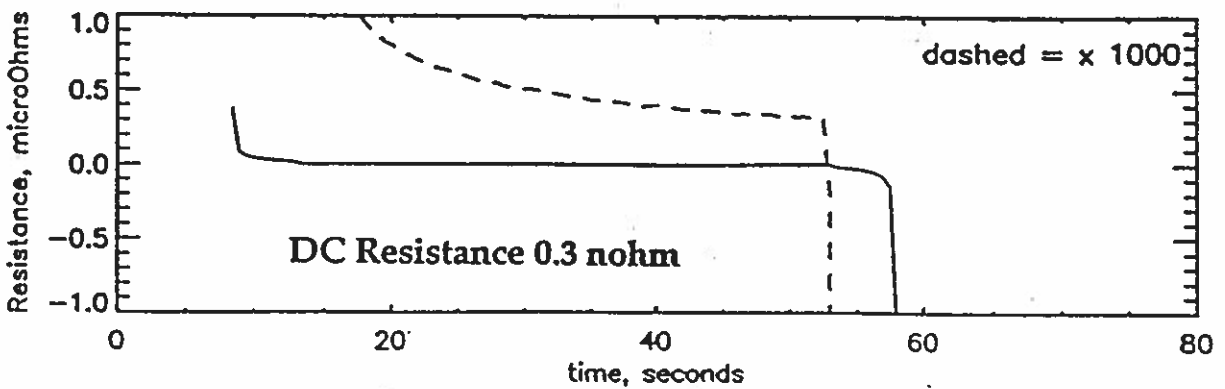
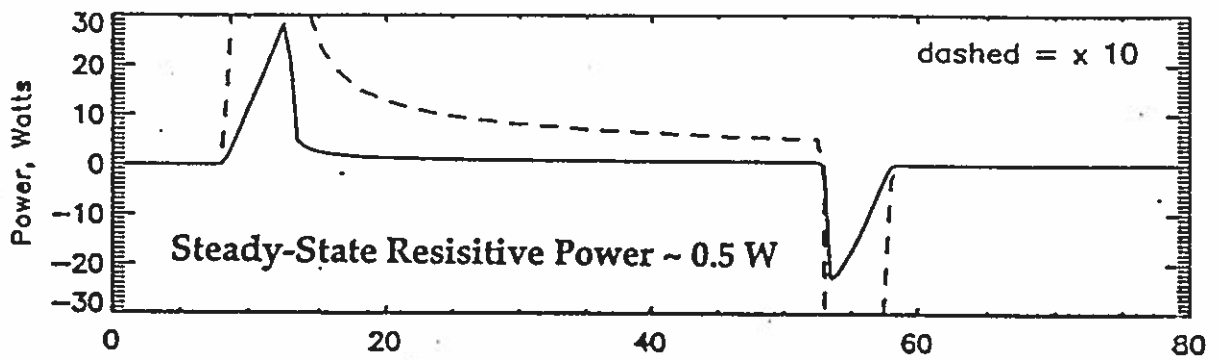
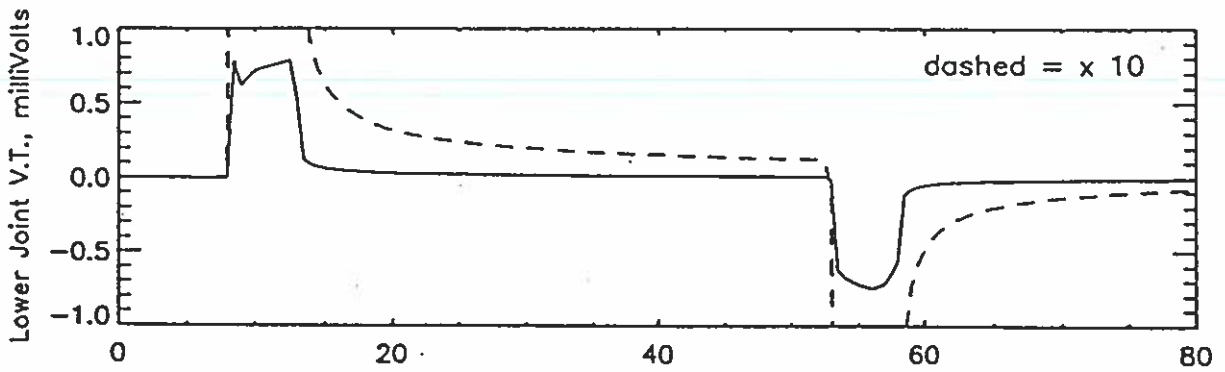
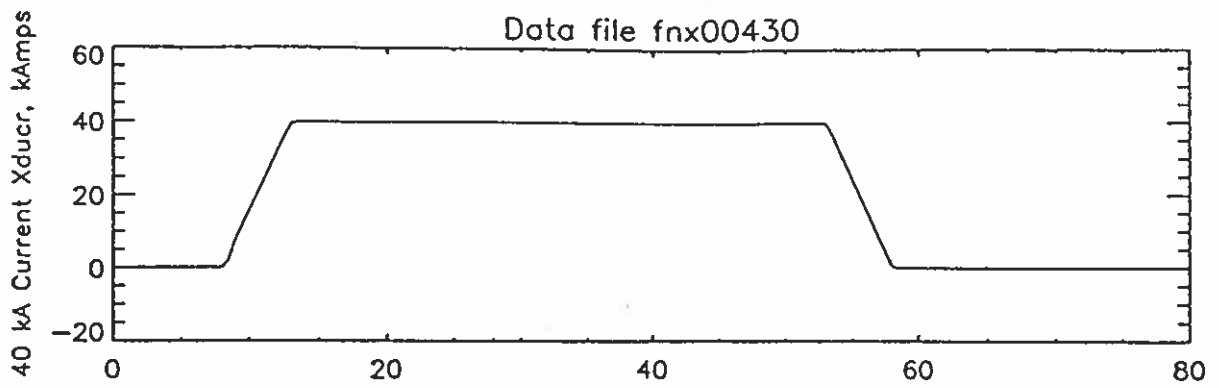
5 kA



Normal-zone
Voltage

Conductor
Temperature

Normal-Zone Resistance Measurement @ 5 kA and 12.8 T



Performance of a 40-kA Lap Joint Measured @ FENIX Facility

B~IT

Need for a Pulsed Test Facility



FENIX tests verify capabilities of CICC:

Flow properties
Current-sharing temperatures
Fatigue caused by cyclic current tests
Stability
Current distribution
Quench properties (normal-zone voltage, RRR)
Quench detection
Ac losses (time constant)
Joint dc tests

Additional tests required to certify conductor and joints for ITER operation:

- AC conductor
- Joint

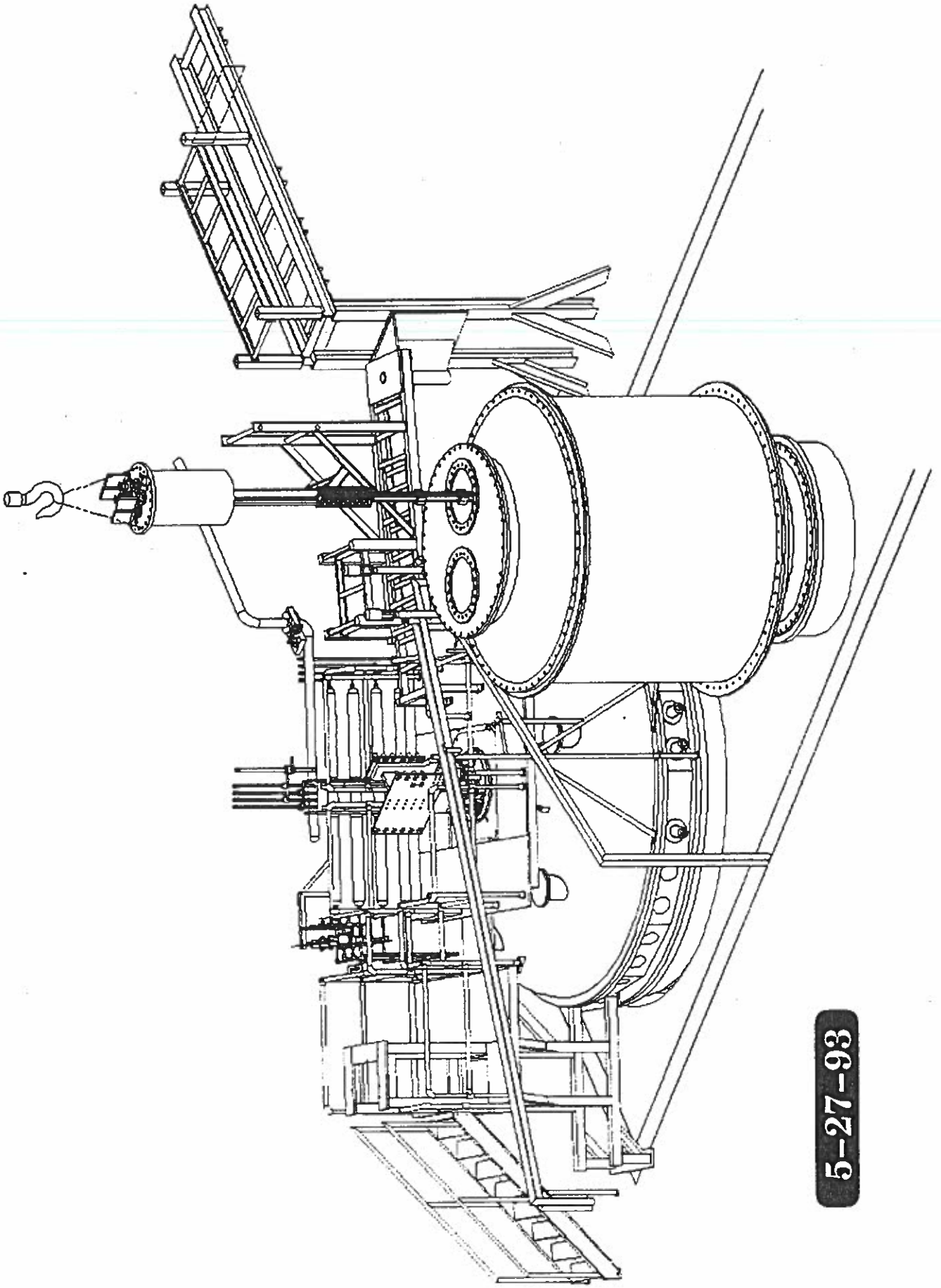
FENIX and PFT



- The Pulse-Field Test is designed to test the same FENIX CICC sample, including the joint, under an ac magnetic field.
- Ac properties of the CICC and the joint can be measured, including ac losses. The sample is subject to a peak field of about 6 T with a rate change up to 12 T/s.



PULSE FIELD TESTING OF FENIX SAMPLE



5-27-93

ITER PROTOTYPE CONDUCTOR SAMPLES FOR FENIX

Specifications/Descriptions	JA/ITER 2		JA/ITER 3	US/ITER 1
	Leg F	Leg H		
Strands Manufacturer Process Diameter (mm) Ic @ 13 T (A)	Nb3Sn Furukawa Bronze 0.92 155	Nb3Sn Hitachi Cable Bronze 0.92 161	Nb3Al Sumitomo Jelly-Roll	Nb3Sn TWCA Jelly-Roll/Internal-Tin 0.78 110
CICC Manufacturer Sheath Material No. of strands (n) Diameter (mm) n*Ic @ 13 T (kA) Cooling design	Furukawa Ti 765 33 119 conventional	Hitachi Cable Ti 675 33 109 conventional	Sumitomo Ti ITER with center hole	BIW / INCO Incoloy 908 1350 46 149 ITER with center hole
FENIX Sample with Terminations and Joint Manufacturer	Mitsubishi Electric	Hitachi	Fuji Electric	Westinghouse