

BNG Industrial experience on Superconducting Undulators

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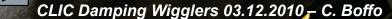


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Short history of BNG in SC undulators



- **2007** Nb₃Sn short prototype built for KIT and tested at CERN
- **2007** Collaboration with KIT on SCUs and SCU15 contract
- 2008 SCU15 demonstrator
- 2009 SCUW prototype: design and fabrication based on KIT concept with test by KIT
- 2010 SCU15 1.5m long coils completed and tested by KIT at CERN
- 2010 First HTS SCU prototype: design and fabrication with test by KIT

SCU15: 15mm period undulator

SCUW : tripling period 15mm/45mm switchable device undulator/wiggler

BNG knowhow on SCUs

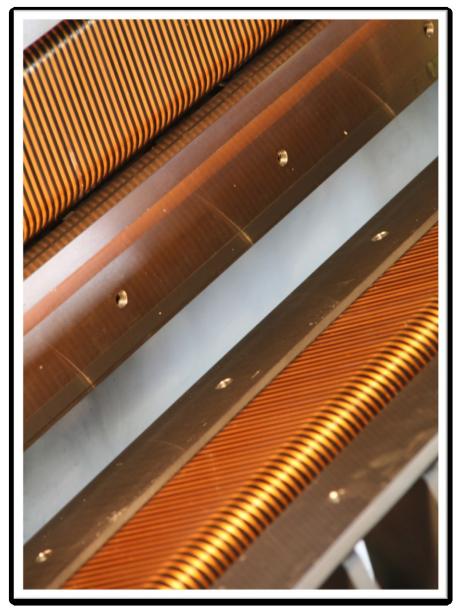


- Magnetic design: coil configuration, quench protection, correction coils.
- Mechanical design of the complete system from coils to cryostat.
- Cryogenic design: cryogen free system.
- Fabrication and high precision "alignment" of the yoke.
- Winding process.
- Vacuum-pressure impregnation.
- Assembly of the complete system.

Most of our existing knowhow had to be further pushed in the past 3 years in order to design and fabricate SCU15



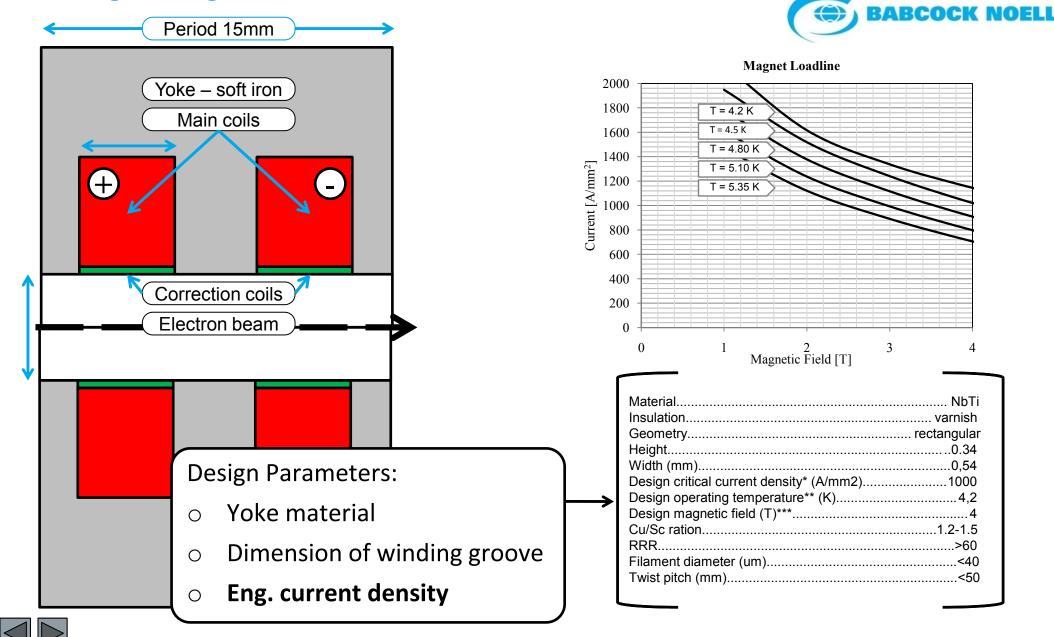
Specifications





Period lengthmm15Number of full periods-100.5Max field on axis with 8 mm magnetic gapT0.77Max field in the coilsT2.4Minimum magnetic gapmm5.4Operating magnetic gapmm8Gan at beam injectionmm16		Units	Value
Max field on axis with 8 mm magnetic gapT0.77Max field in the coilsT2.4Minimum magnetic gapmm5.4Operating magnetic gapmm8	Period length	mm	15
Max field in the coilsT2.4Minimum magnetic gapmm5.4Operating magnetic gapmm8	Number of full periods	-	100.5
Minimum magnetic gapmm5.4Operating magnetic gapmm8	Max field on axis with 8 mm magnetic gap	т	0.77
Operating magnetic gap mm 8	Max field in the coils	Т	2.4
	Minimum magnetic gap	mm	5.4
Gan at heam injection mm 16	Operating magnetic gap	mm	8
	Gap at beam injection	mm	16
K value at 5 mm gap - >2	K value at 5 mm gap	-	>2
Design beam heat load W 4	Design beam heat load	W	4
Phase error r.m.s.°3.5	Phase error r.m.s.	0	3.5

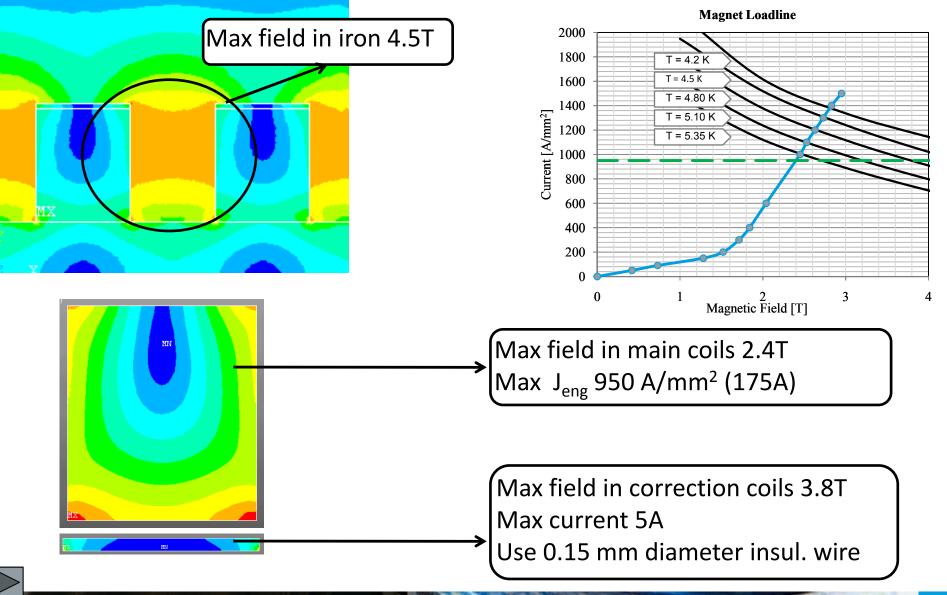
High eng. Current density -> magnetic design
 Tolerate beam heat loads -> cryogenic design
 High mechanical accuracy -> fabrication technology



Design – Magnetic field calculation I

Design – Magnetic field calculation II

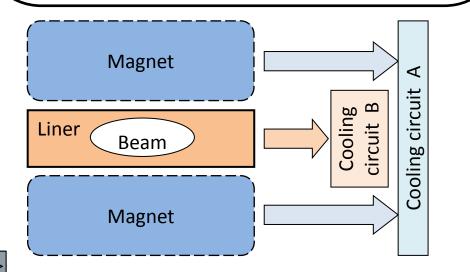




Design – Cryogenic circuit

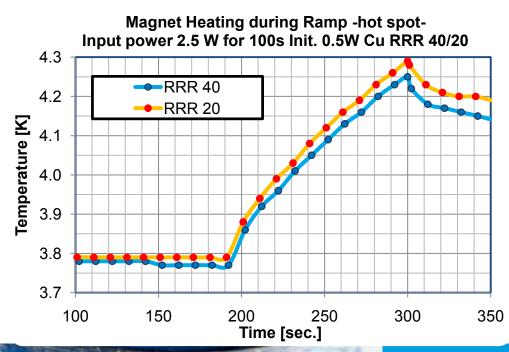
Main concepts:

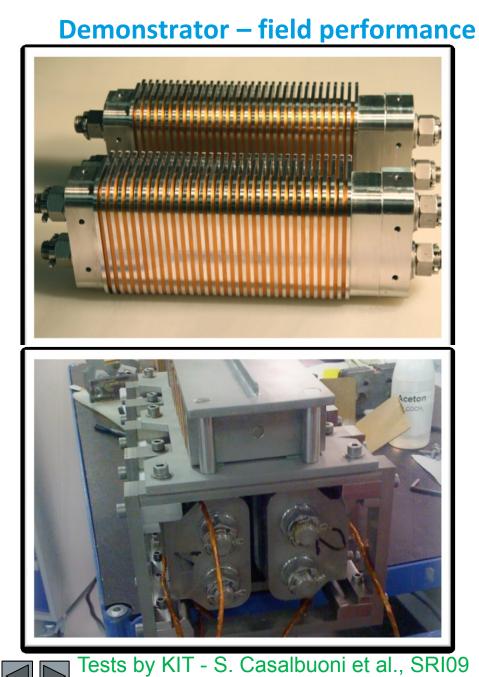
- Two separate circuits for magnet and beam liner.
- Two base temperatures: 4K for the magnet and 10K for the beam liner.
- Minimization of gradients between cold
 head and most distant point in the magnet.



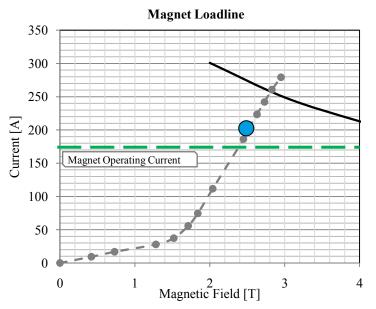


Heta Loads			
	Shield	Circuit B	Circuit A
Radiation	7.93	0.05	
Conduction	21.98	0.53	0.28
Current leads	18.80		0.13
Eddy currents			0.20
Hysteresis			0.14
Coupling SC			1.71
Beam Heat	16	4.00	
T otal (W)	64.71	4.58	2.46



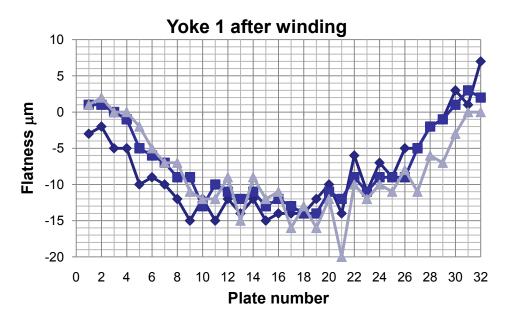






- \circ 16.5 periods
- \odot End field correction $\ensuremath{\overset{3}{4}}$ $\ensuremath{\overset{1}{4}}$
- \odot Quench protection with cold diodes
- Local shimming
- Single length wire winding
- Vacuum Pressure impregnation (VPI)
- Alignment of coils

Demonstrator – mechanical accuracies



Yoke 1 after impregnation 50 0 Flatness μm -50 -100 -150 -200 -250 3 21 23 25 27 29 31 1 9 11 13 17 19 Plate number C. Boffo et al., MT21



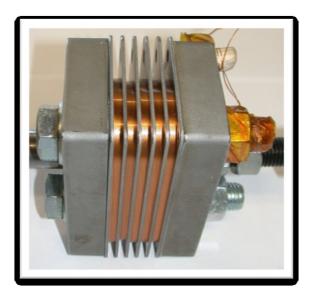
 \odot Yoke flatness measured after winding -> 20 $\mu m.$

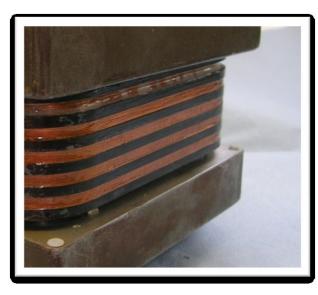
 \odot Yoke flatness measured after impregnation -> 250 $\mu m.$

The deformation is the result of the 180 C heating performed during impregnation.

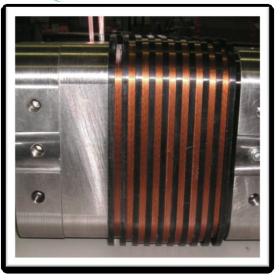
Several mixtures have been tested to eliminate the "high temperature" step while keeping the correct physical properties.

Prototypes







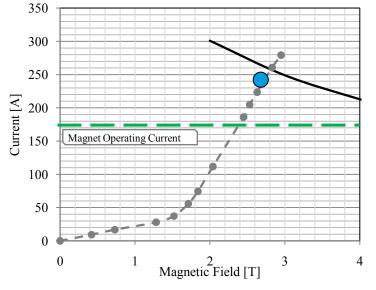


Magnet Loadline

Best test results:

- \odot Max current 240 A
- Max ramp rate 240 A/min
- \circ Max eng. current density above 1300 A/mm²
- Reached above 90% short sample limit

Tests by KIT - S. Casalbuoni et al., IPAC10



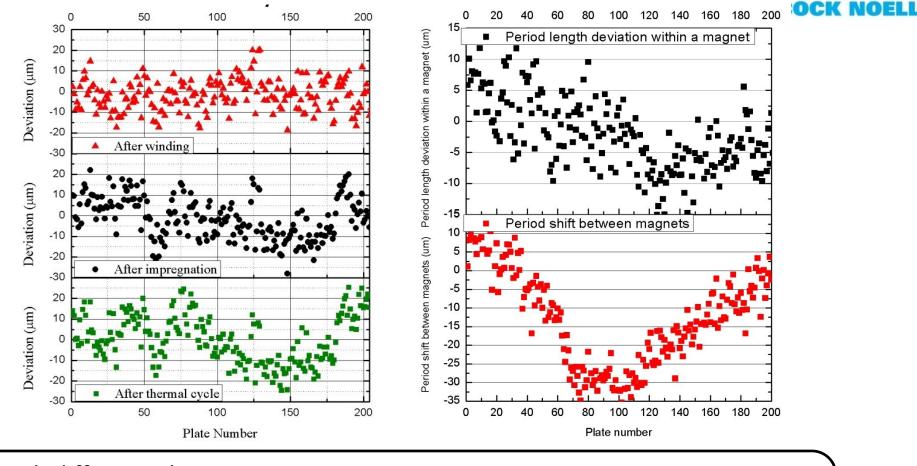
Fabrication





- Stapling and alignment of 205 plates for each yoke.
 Plates have been measured and positioned to minimize period length variations.
- \odot Winding with single wire.
- \odot Single joint per magnet at end.
- ${\rm \circ}$ Impregnation at room temperature.
- o Measurement of yoke flatness between fabrication steps.
- Support strongback in stainless steel.

Achieved accuracies



Length difference between magnets: $20 \ \mu m$ Yoke flatness along 1.5 m: $50 \ \mu m$ Maximum period length deviation: $30 \ \mu m$ Maximum deviation of relative position between the magnets: $50 \ \mu m$

C. Boffo et al., ASC2010

Tests at CERN

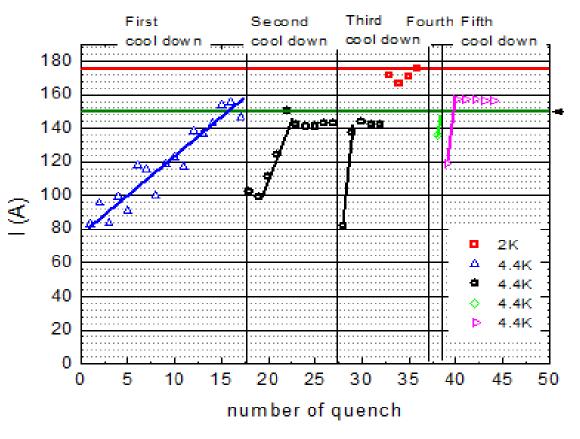


- •The magnet test was performed at CERN at BLOC4
- •Vertical configuration
- •Temperature between 4.5 and 2.2K
- •Tight quench detection system



Training and repairs





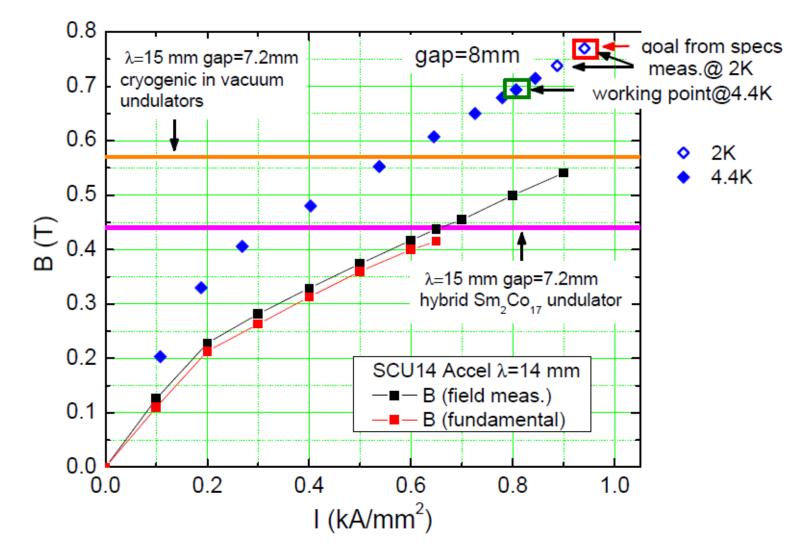
 $_{\odot}$ The weakest point in the magnet system is in the thin wire.

- \circ Difficult to wind
- \circ Easy to over bend
- Sensible on yoke defects
- \circ BUT small filaments and high packing factor
- $_{\rm O}$ Three repairs have been performed.
- A special technique has been
 developed to remove the impregnation
 and repair single coils.
- O Uncertainty on the joints in conduction cooling.

S. Casalbuoni et al., ASC2010

Field performance -1

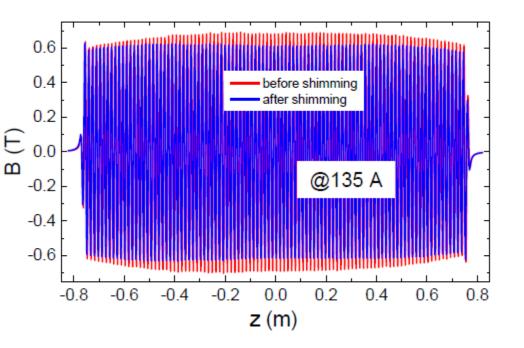


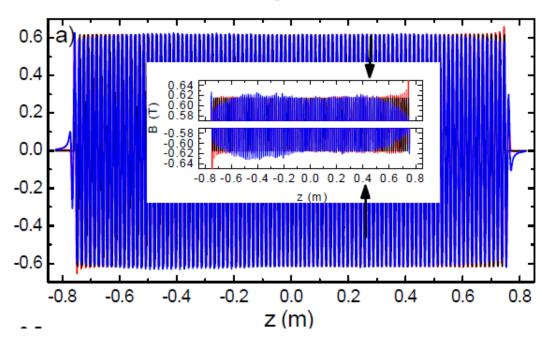


S. Casalbuoni et al., ASC2010

Field performance -2







Phase error of 7.4 degrees over a length of 0.79 m obtained by application of mechanical shims in the support device Good agreement between measurement and simulations performed at KIT taking into account the mechanical accuracies

S. Casalbuoni et al., ASC2010



 After three years of close collaboration between KIT and BNG a new 1.5 m long undulator has been fabricated.

 The specifications of the system are such that the technology for the fabrication of SC magnets had to be pushed over the envelope to meet the requirements.

• The magnet performs very satisfactory, close to the envisages specs defined at the start of the R&D.

 $_{\odot}$ The coils are being installed in the cryostat as we speak.

 $_{\odot}$ BNG has a demonstrated knowhow in SCUs design and fabrication.