

Developing an Optical Phased Array for the Breakthrough Starshot propulsion system

Presenter: Paul Sibley

Chathura Bandutunga, Michael Ireland



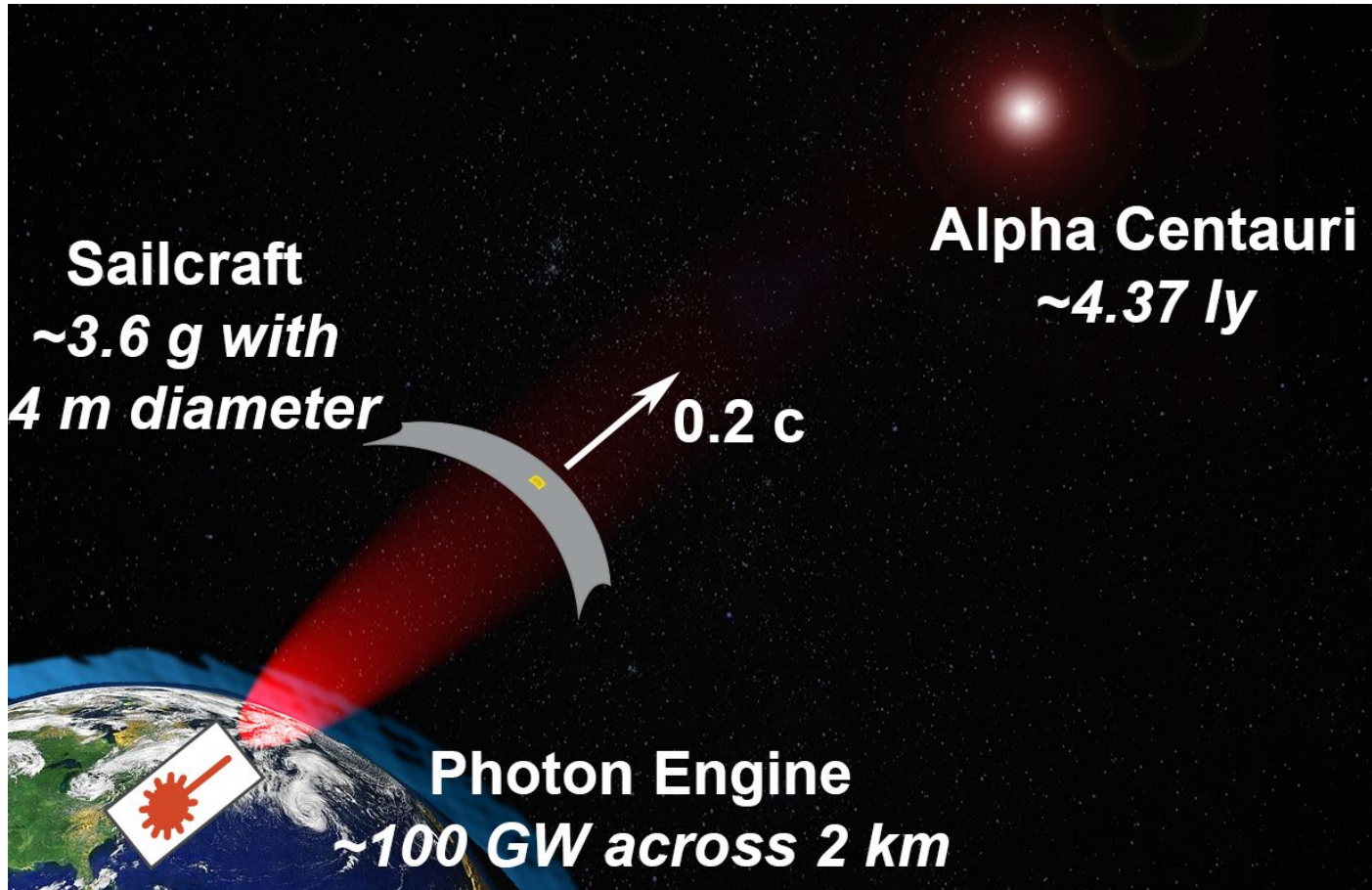
Applied Metrology Labs,
Centre for Gravitational Astrophysics, Research School of Physics, ANU.
Research School of Astronomy and Astrophysics, ANU



Australian
National
University



Breakthrough Starshot – at a glance



Photon Pressure

~3.6g (Initial proposed sailcraft weight)
10 minute illumination

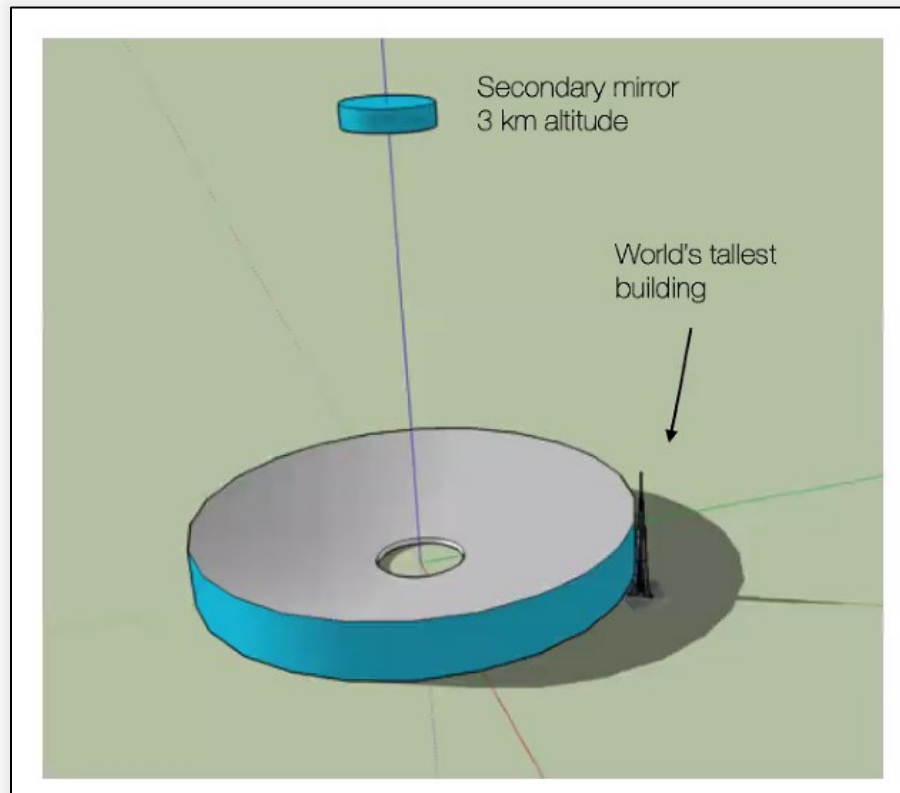
<i>10mW</i>	<i>→ 6μm/s</i>
<i>1kW</i>	<i>→ 2km/hr</i>
<i>100GW</i>	<i>→ ~20% speed of light</i>
<i>68 MW</i>	<i>→ 40km/s (~Voyager speed)</i>

$$v_{sc} = \frac{\text{LaserPower} \cdot \text{Time}}{\text{Mass} \cdot c}$$



Breakthrough Starshot – Optical phased array

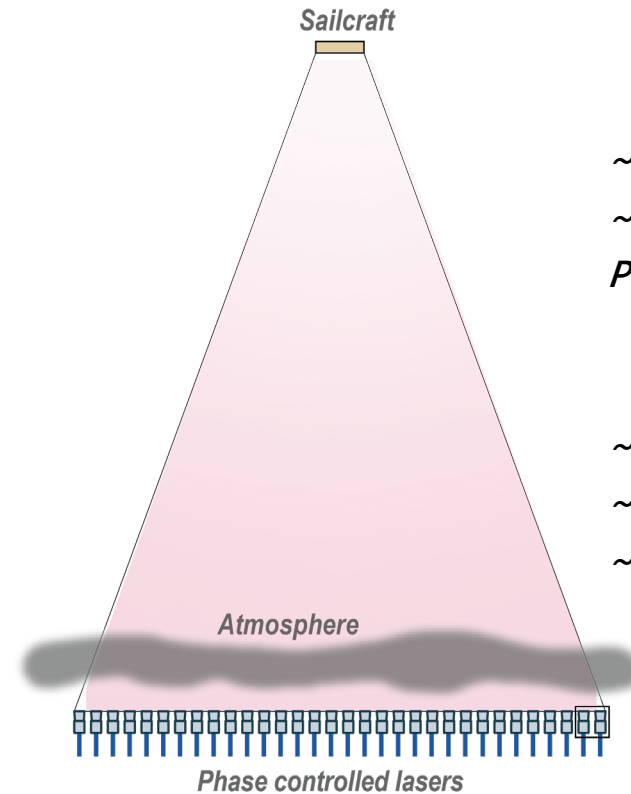
A conventional telescope approach



"What it can't be"

Breakthrough Starshot Communications Workshop

Optical phased array



Requirements (Estimated)

~2.8km Diameter

~100GW Power

Power on sailcraft throughout launch

Array parameters

~100M : Emitters

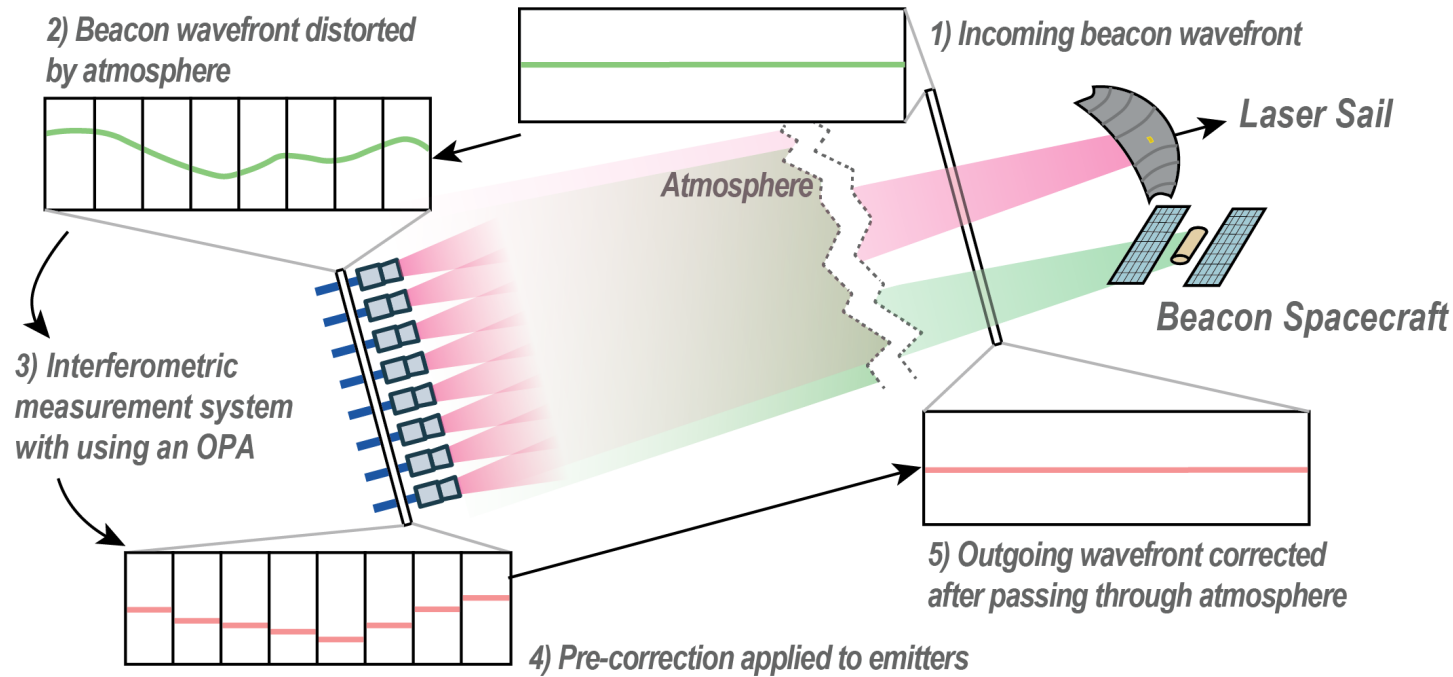
~10cm : Apertures

~1kW : Per Emitter

**Synthesize a large aperture telescope
with phase controllable apertures**



Cooperative interferometric sensing approach

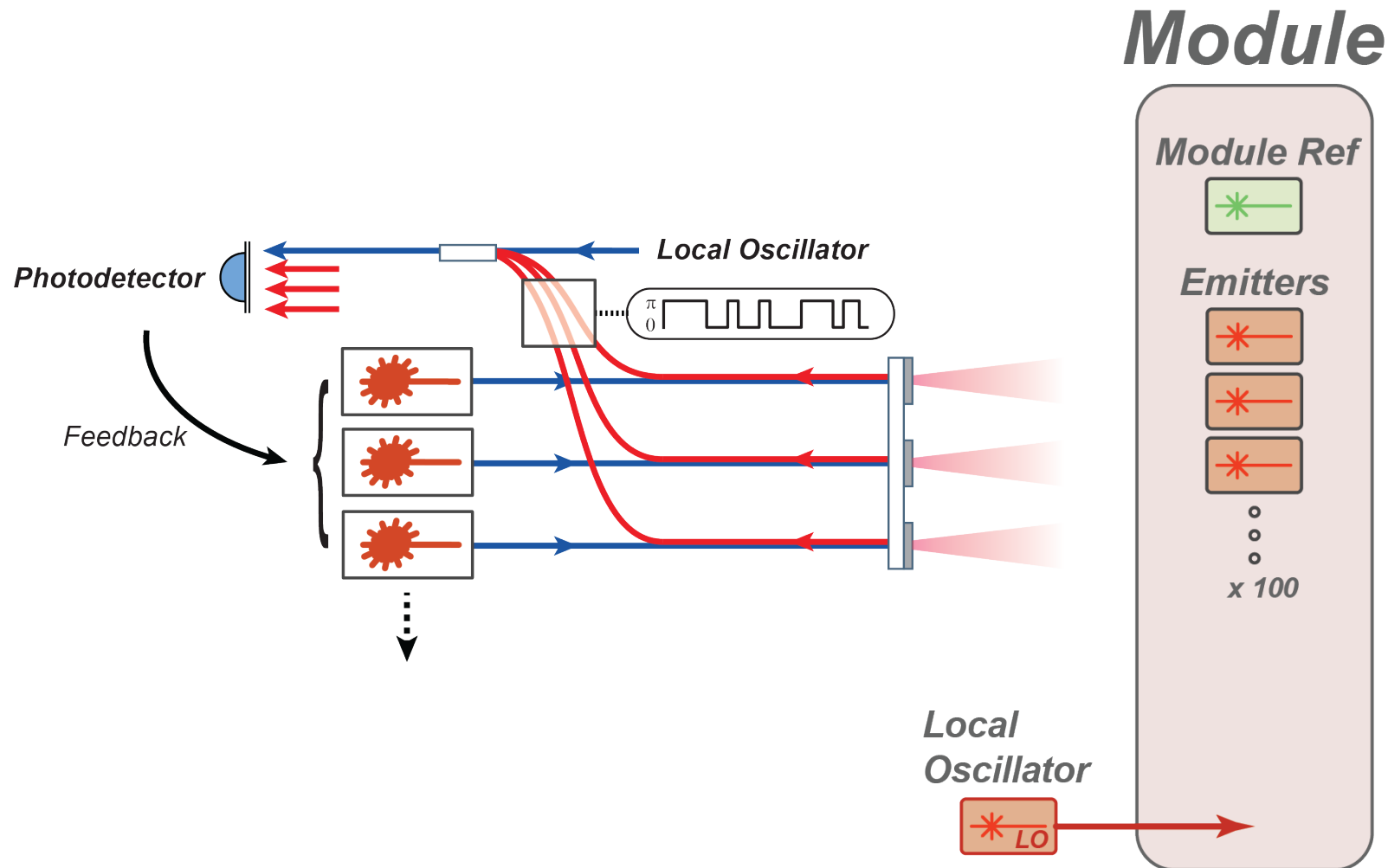


Two key concepts developed

1. Internally - A method to actively compare pathlengths between 10^8 emitters (give or take)
2. Externally - A method to measure the external pathlengths that deals with the expected large power disparity between the beacon and emitter lasers



Hierarchical Optical Phased Array



Within a tier:

Phase comparison using code division multiplexing, Digital Interferometry

Between tiers:

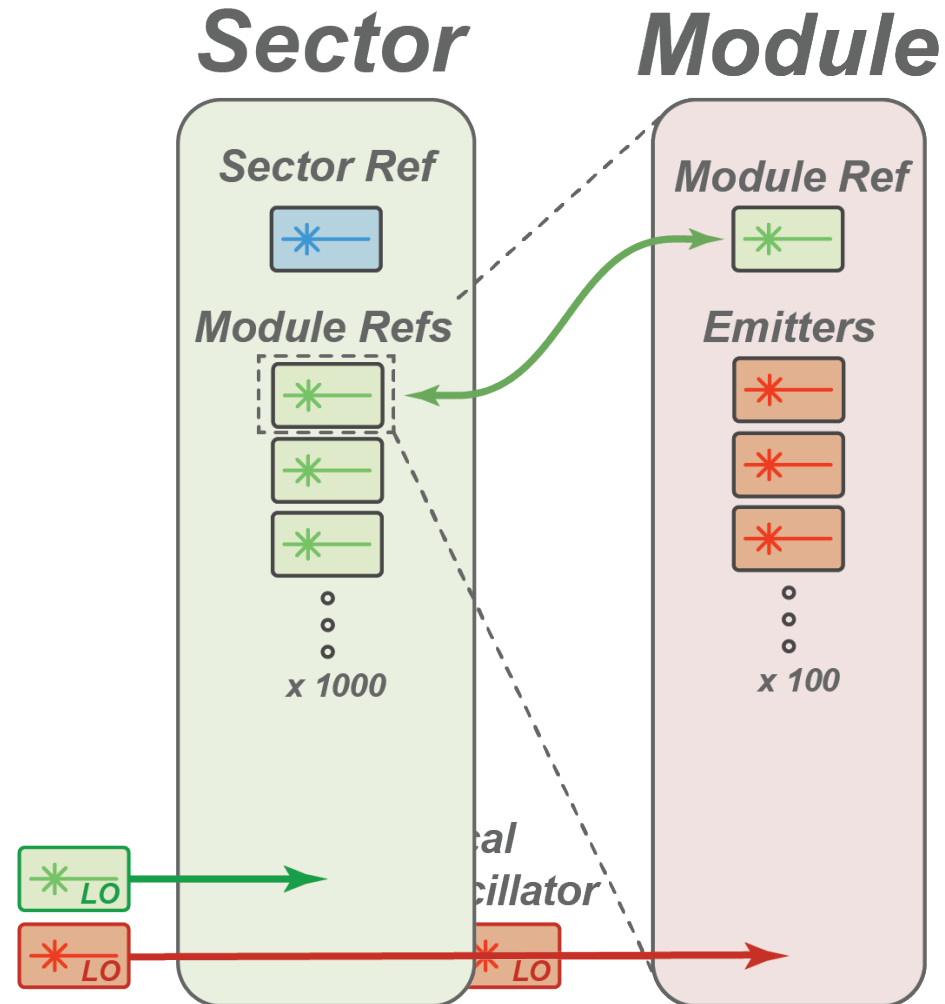
A wavelength offset reference separated by ~ 20 - 100 GHz links tiers to allow additional suppression of lower tiers

Size of a tier is limited by:

- Detector dynamic range (power saturation and shot-noise)
- Code division multiplexing crosstalk



Hierarchical Optical Phased Array



Within a tier:

Phase comparison using code division multiplexing, Digital Interferometry

Between tiers:

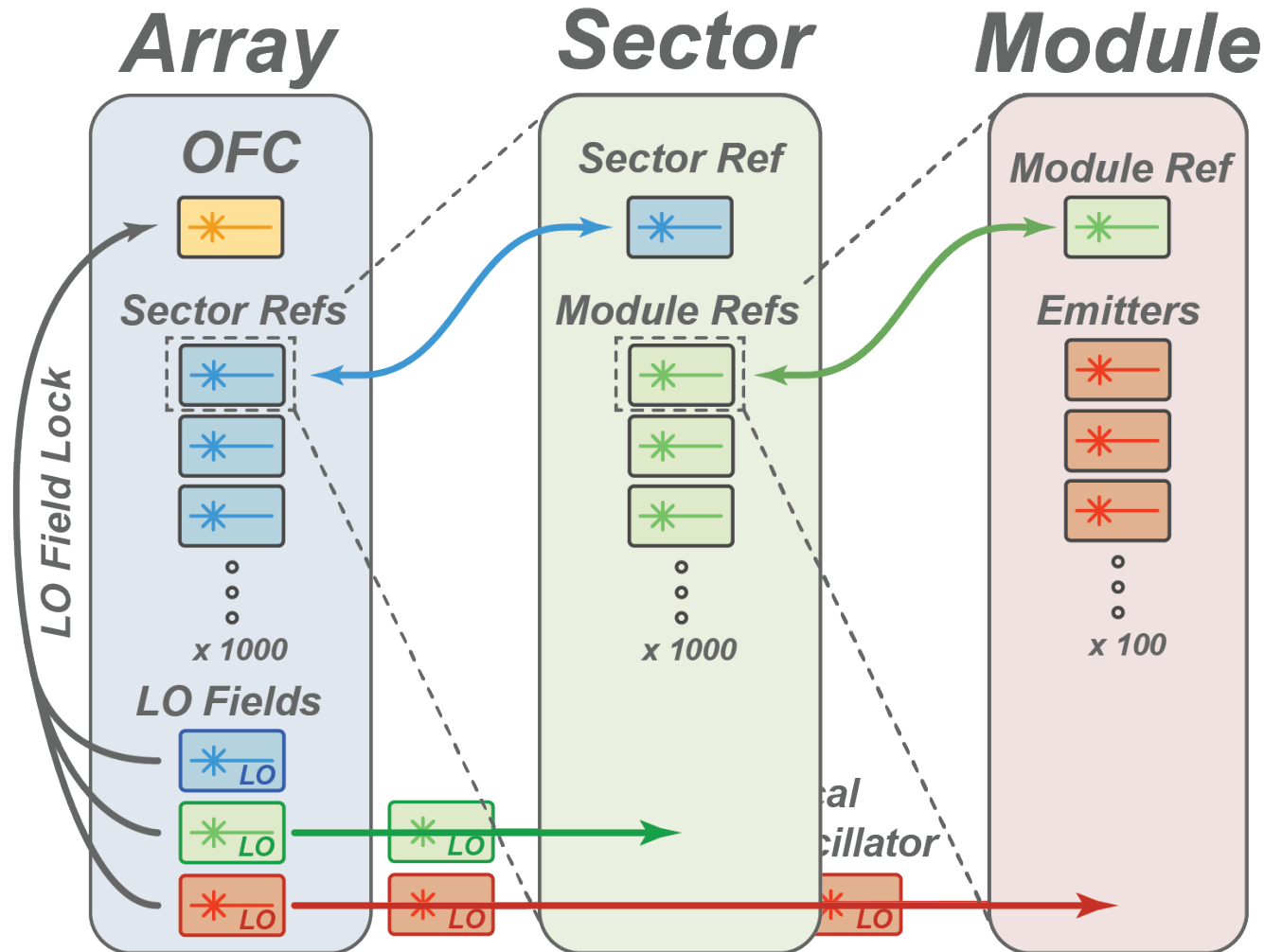
A wavelength offset reference separated by $\sim 20\text{-}100$ GHz links tiers to allow additional suppression of lower tiers

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Hierarchical Optical Phased Array



Within a tier:

Phase comparison using code division multiplexing, Digital Interferometry

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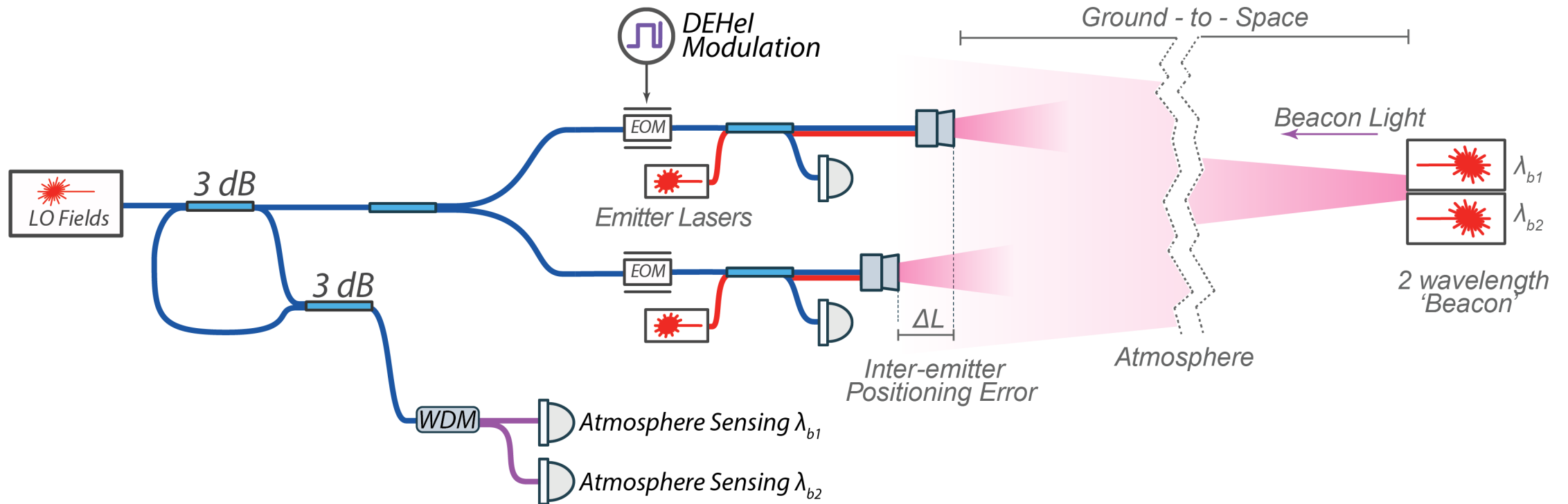
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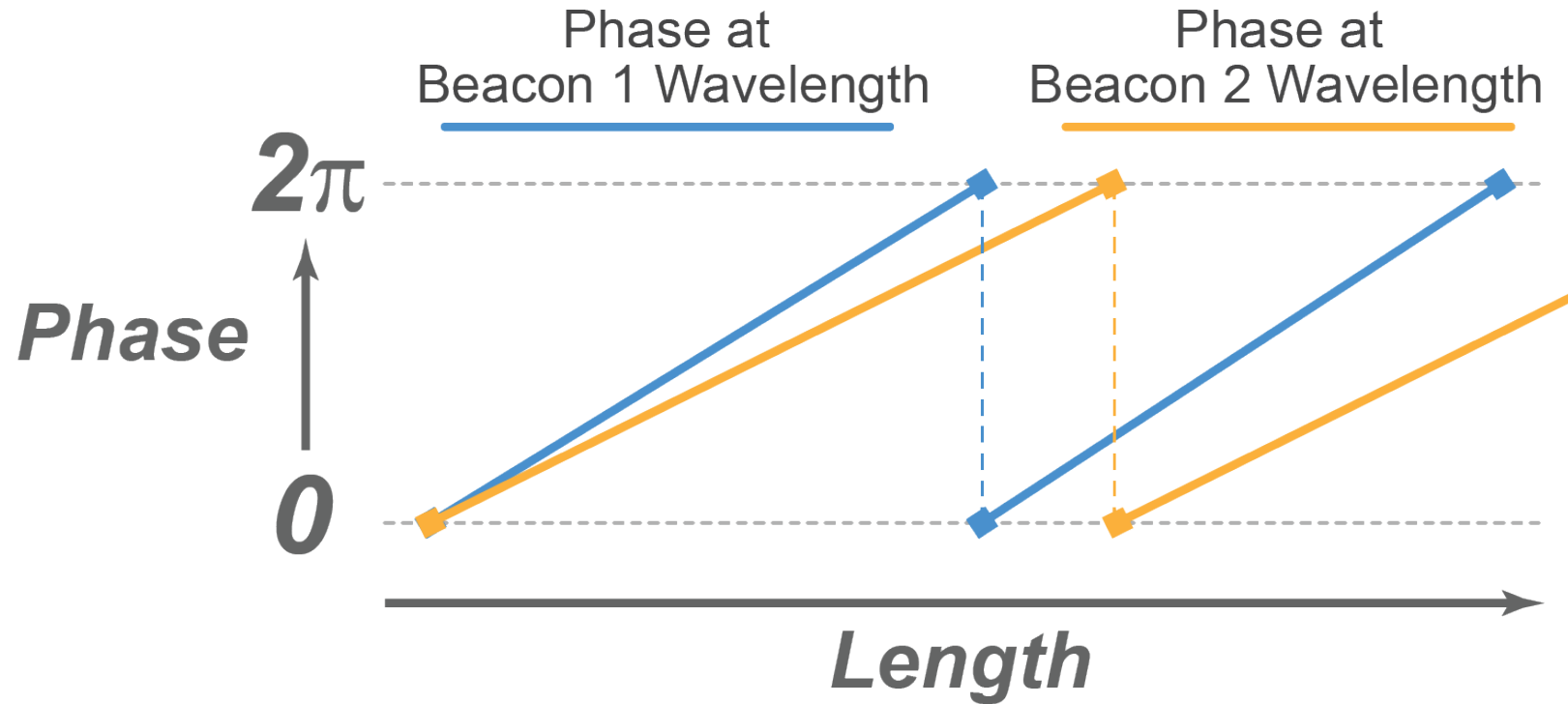
Beacon wavefront phase sensing



Optical power loss: ~80dB externally, ~50dB internally

Multi-wavelength phase sensing

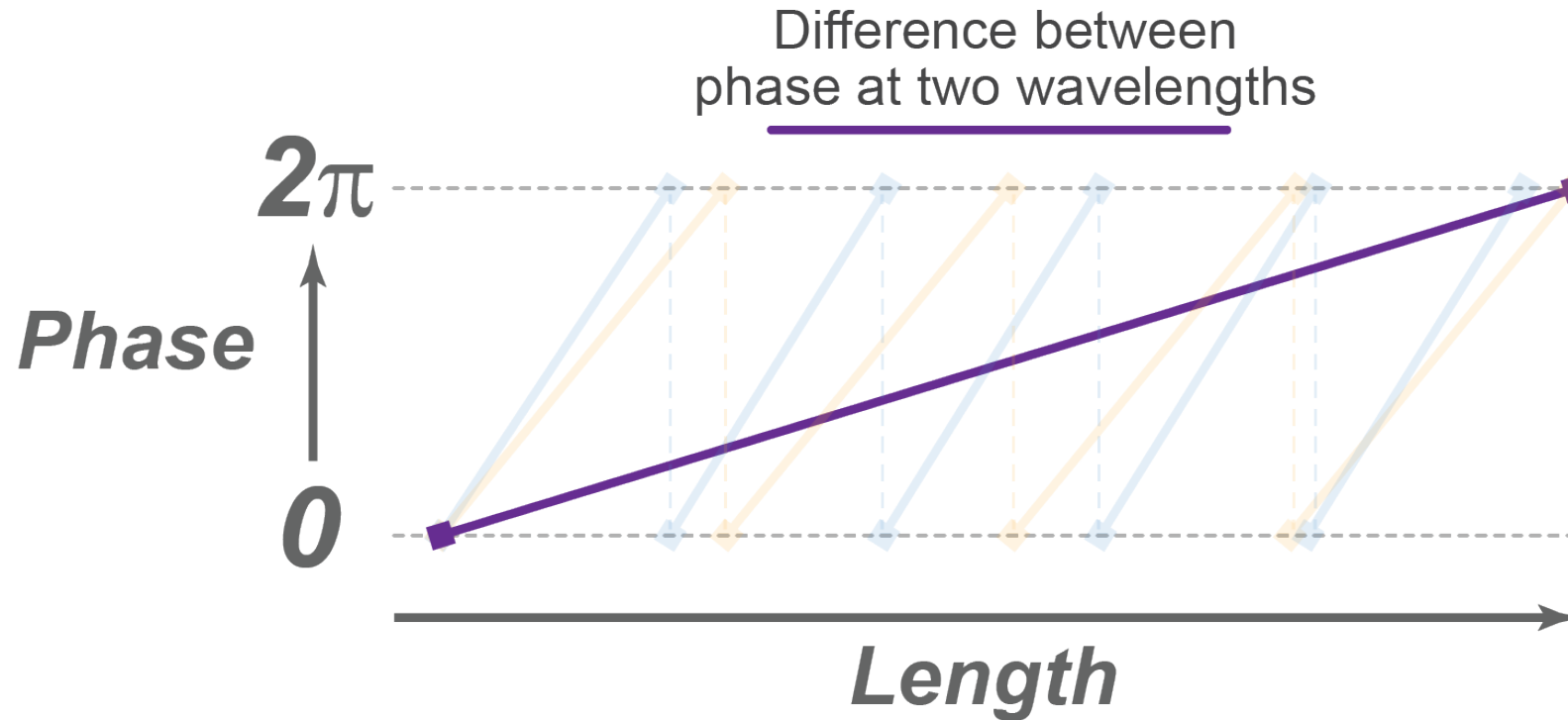
$$\text{Optical Phase} = \frac{\text{Optical pathlength}}{\text{Wavelength}}$$



Multi-wavelength phase sensing

$$\text{Optical Phase} = \frac{\text{Optical pathlength}}{\text{Wavelength}}$$

For a 100 GHz frequency shift, the synthetic wavelength is $\Lambda \approx 3 \text{ mm}$

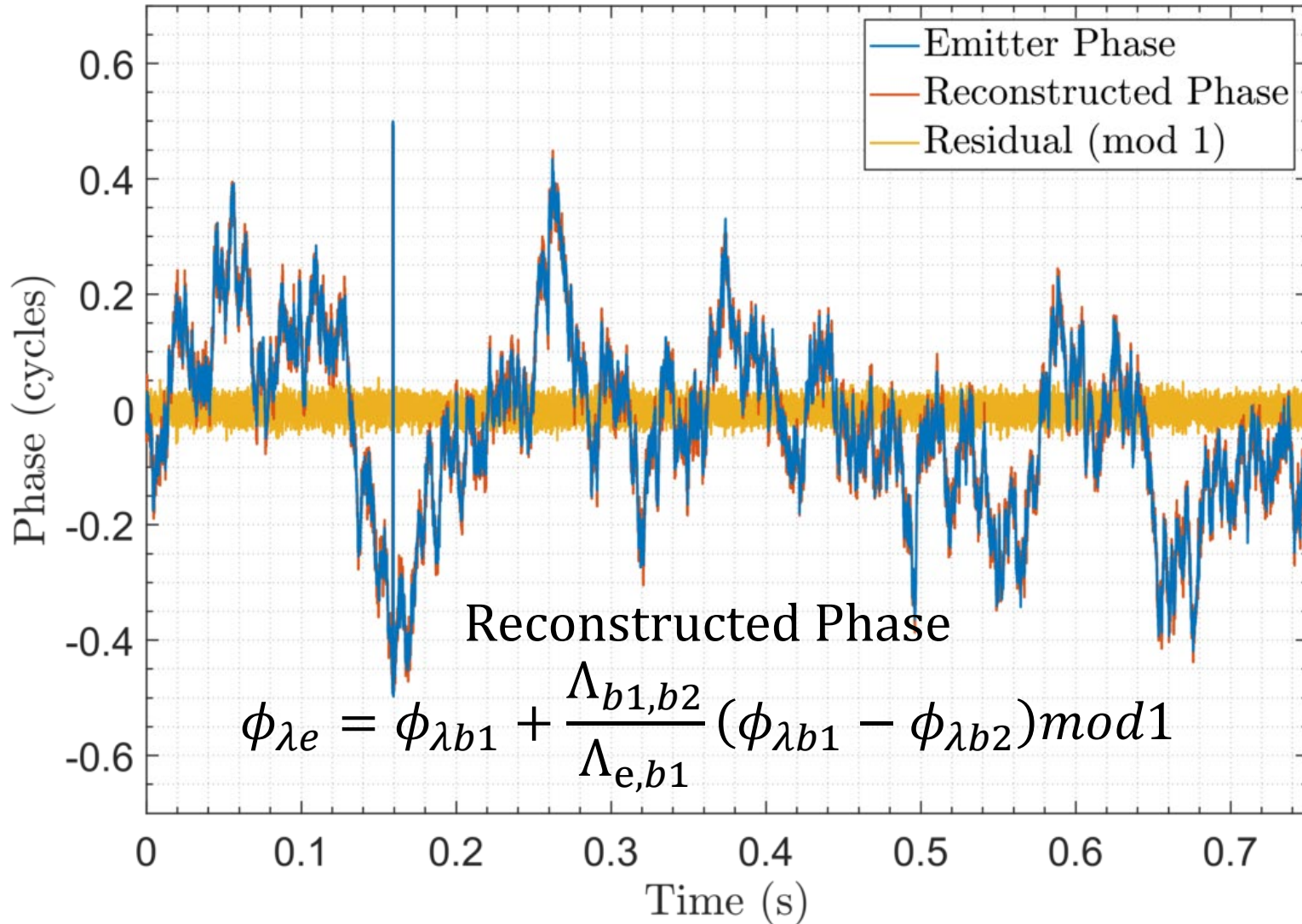


Using two wavelengths allows the length dependent phase error to be calculated

Specifically choosing these wavelengths significantly extends the unambiguous reconstruction range



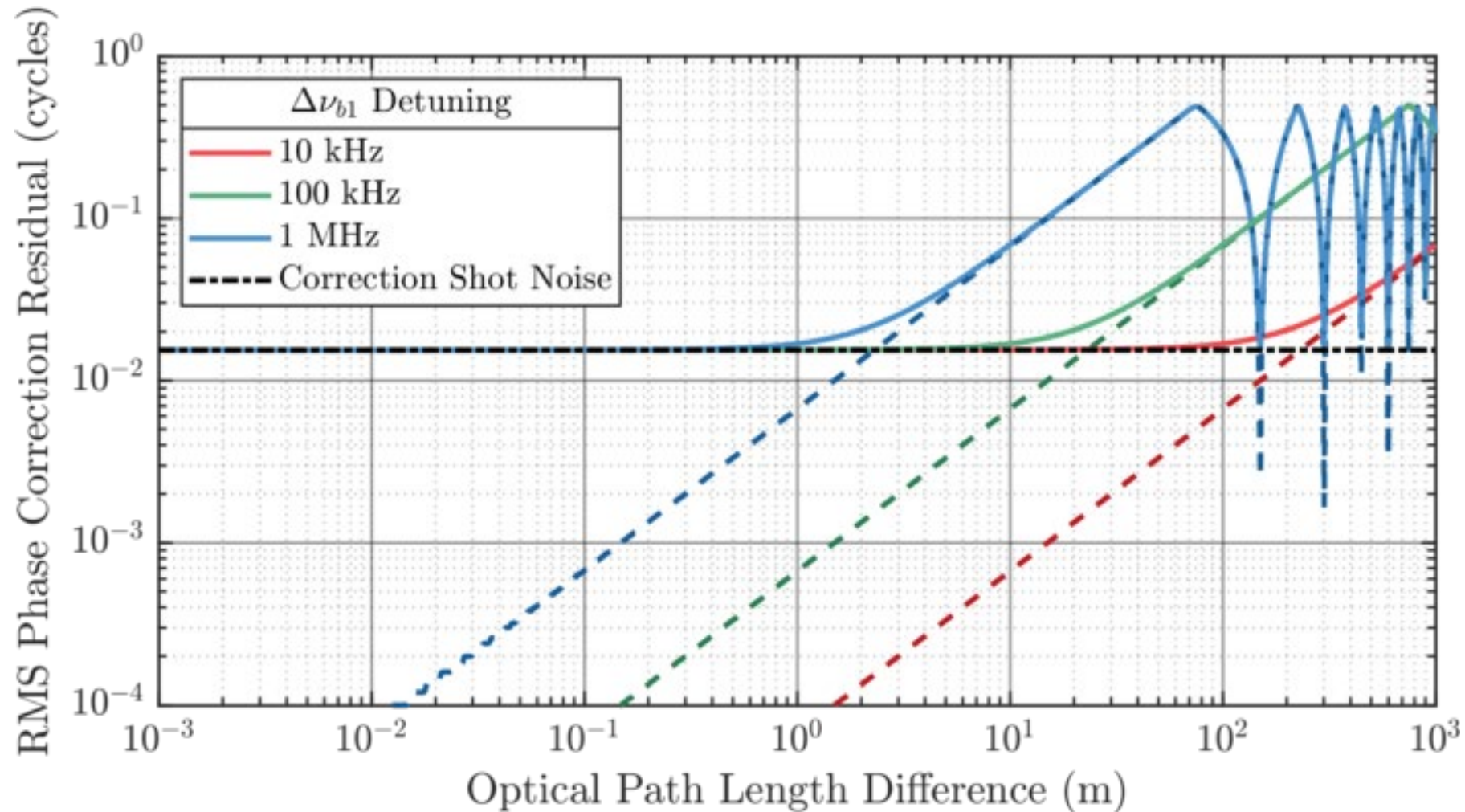
Simulated beacon phase measurement



Parameters:

- 10 cm length difference (with noise)
- Shot noise added for a 1 pW beacon (at detector)
- 10 kHz absolute frequency knowledge

Sensitivity to pathlength and wavelength differences



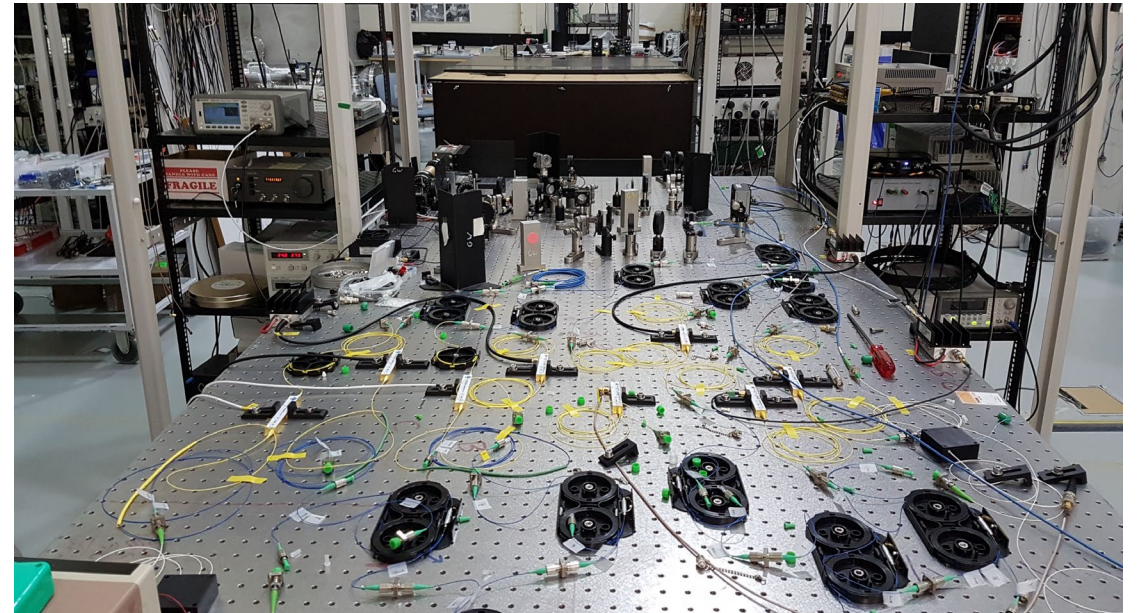
What's next?

Experimental proof of principles

- Begin proof-of-concept demonstrations
 - Hierarchical structure
 - Laser beacon-based wavefront sensing
 - Multi-wavelength phase reconstructions/corrections
- Integration of advances in integrated photonics, laser technologies and new interferometric signal processing methods

Challenges for wider Breakthrough Starshot

- Cost
- Sailcraft development
- Communication





Contact Us

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Image Credit: National Geographic

Additional *Concept System* Details

1000 channels is not 100,000,000
(this would need multi-THz sampling frequency)

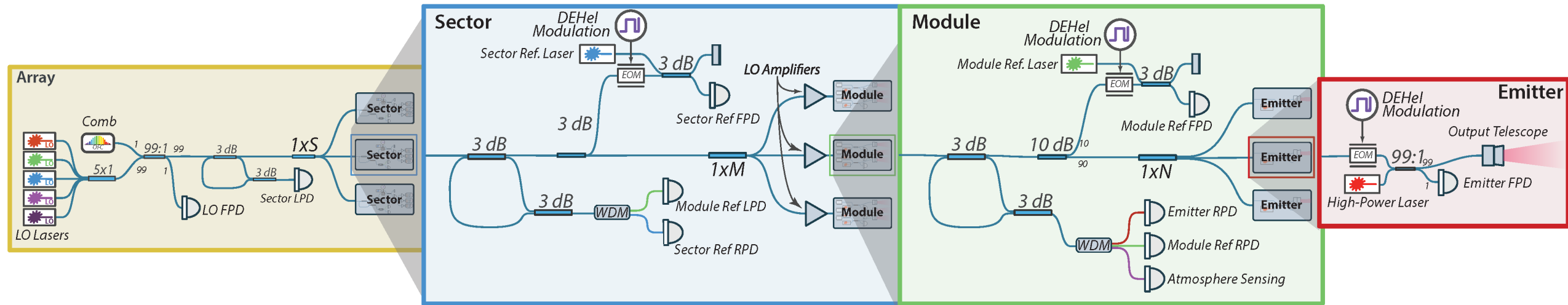
Sim

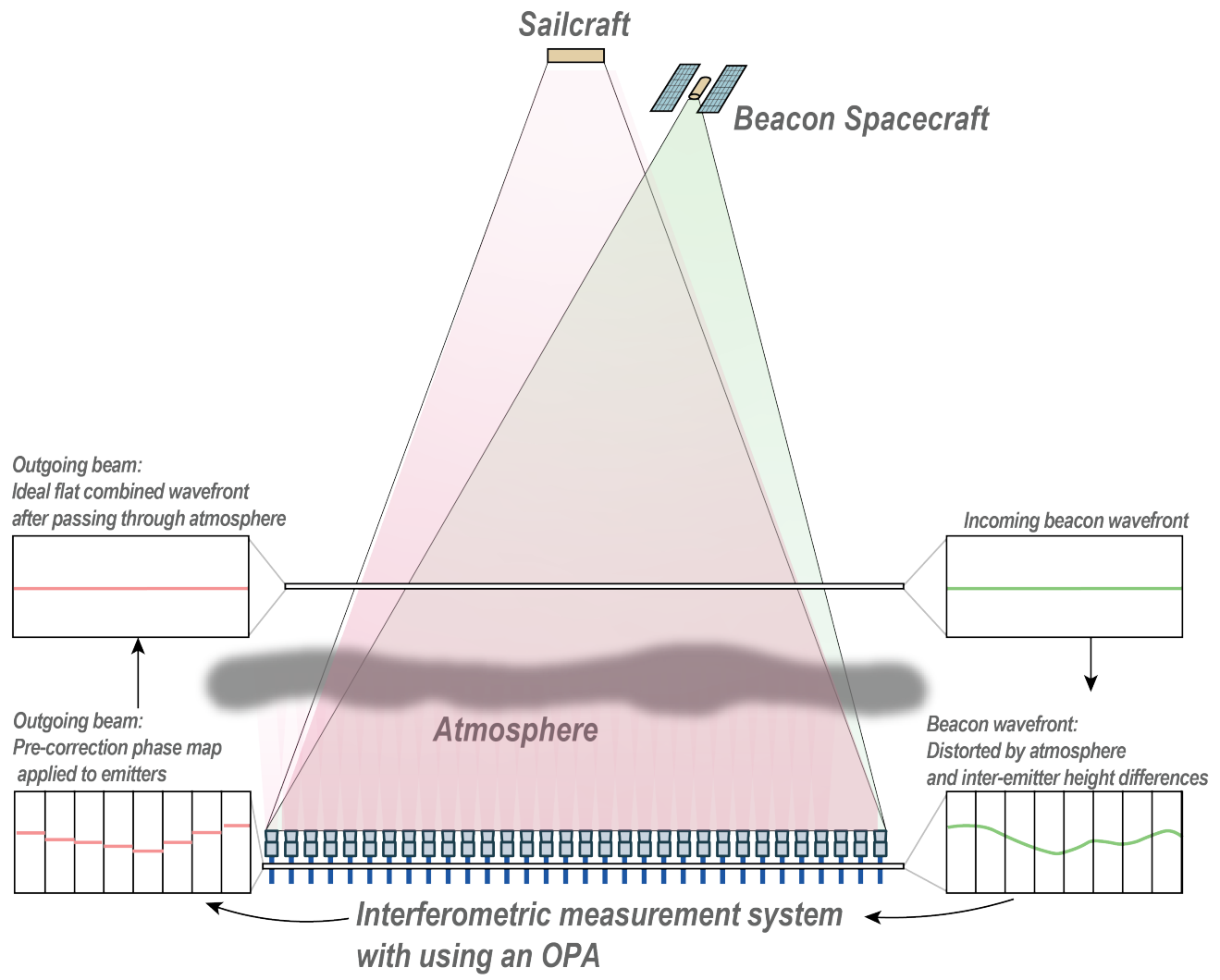
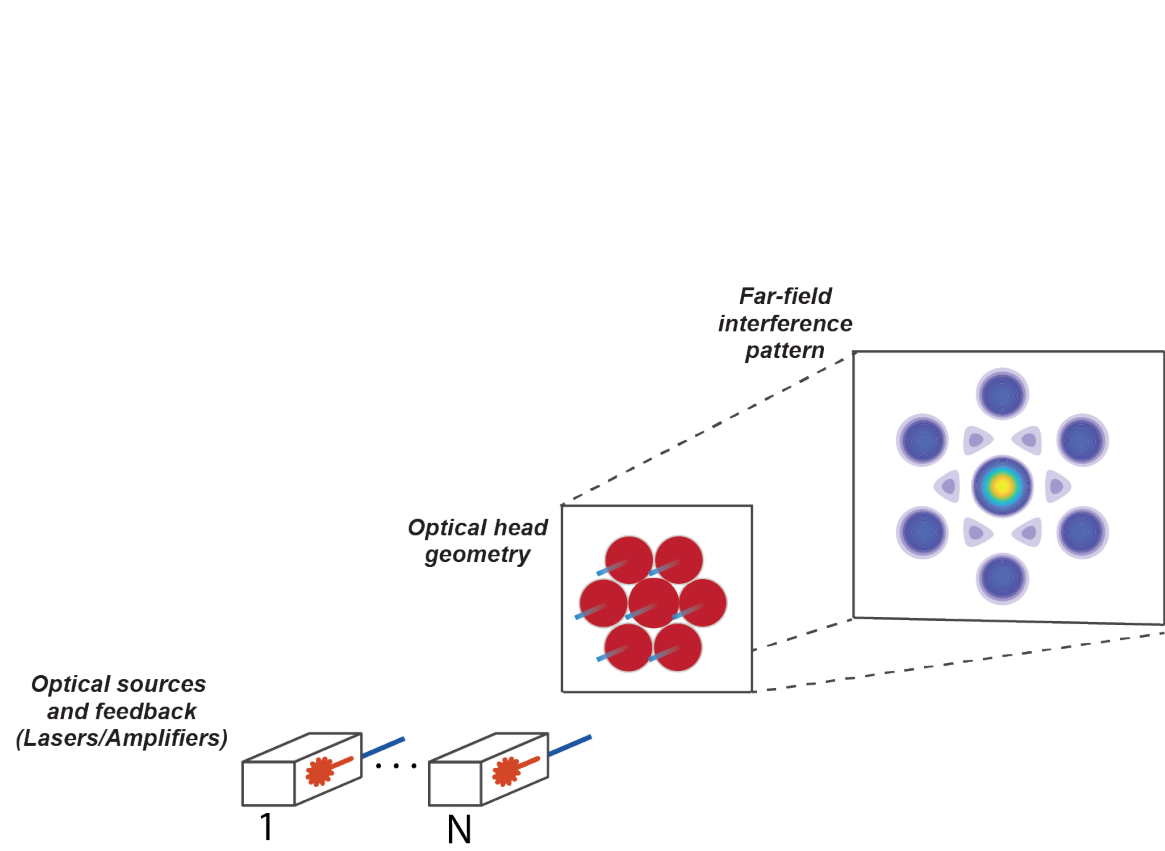
1. 656 MHz ADC
2. Phase readout rate 20 kHz
3. 1 kW individual emitters

Detection	λ_α	Phase
$\Phi_{FPD,e}[i, j, k]$	λ_e	$\phi A4_e + \phi A3_e[i] + \phi A2_e[i, j] + \phi A1_e[i, j, k] - \phi H1_e[i, j, k]$
$\Phi_{FPD,m}[i, j, R]$	λ_m	$\phi A4_m + \phi A3_m[i] + \phi A2_m[i, j] + \phi A1_m[i, j, R] - \phi H1_m[i, j, R]$
$\Phi_{RPD,e}[i, j, k]$	λ_e	$\phi A4_e + \phi A3_e[i] + \phi A2_e[i, j] + \phi LO1_e[i, j] - \phi H1_e[i, j, k] - 2\phi H2_e[i, j, k] - \phi A1_e[i, j, k] - \phi R1_e[i, j]$
$\Phi_{RPD,m}[i, j]$	λ_m	$\phi A4_m + \phi A3_m[i] + \phi A2_m[i, j] + \phi LO1_m[i, j] - \phi H1_m[i, j, R] - 2\phi H2_m[i, j, R] - \phi A1_m[i, j, R] - \phi R1_m[i, j]$
$\Phi_{FPD,s}[i, R, R]$	λ_s	$\phi A4_s + \phi A3_s[i] + \phi A2_s[i, R] - \phi H1_s[i, R, R]$
$\Phi_{LPD,m}[i, j, R]$	λ_m	$\phi A4_m + \phi A3_m[i] + \phi LO2_m[i] - \phi H1_m[i, j, R] - 2\phi H2_m[i, j, R] - \phi A1_m[i, j, R] - \phi A2_m[i, j] - \phi R2_m[i]$
$\Phi_{RPD,s}[i, R, R]$	λ_s	$\phi A4_s + \phi A3_s[i] + \phi LO2_s[i] - \phi H1_s[i, R, R] - 2\phi H2_s[i, R, R] - \phi A2_s[i, R] - \phi R2_s[i]$
$\Phi_{FPD,s}[R, R, R]$	λ_s	$\phi A4_s + \phi A3_s[R] - \phi H1_s[R, R, R]$
$\Phi_{LPD,s}[i, R, R]$	λ_s	$\phi A4_s + \phi LO3_s - \phi H1_s[i, R, R] - 2\phi H2_s[i, R, R] - \phi A2_s[i, R] - \phi A3_s[i] - \phi R3_s$
$\Phi_{RPD,s}[R, R, R]$	λ_s	$\phi A4_s + \phi LO3_s - \phi H1_s[R, R, R] - 2\phi H2_s[R, R, R] - \phi A3_s[R] - \phi R3_s$



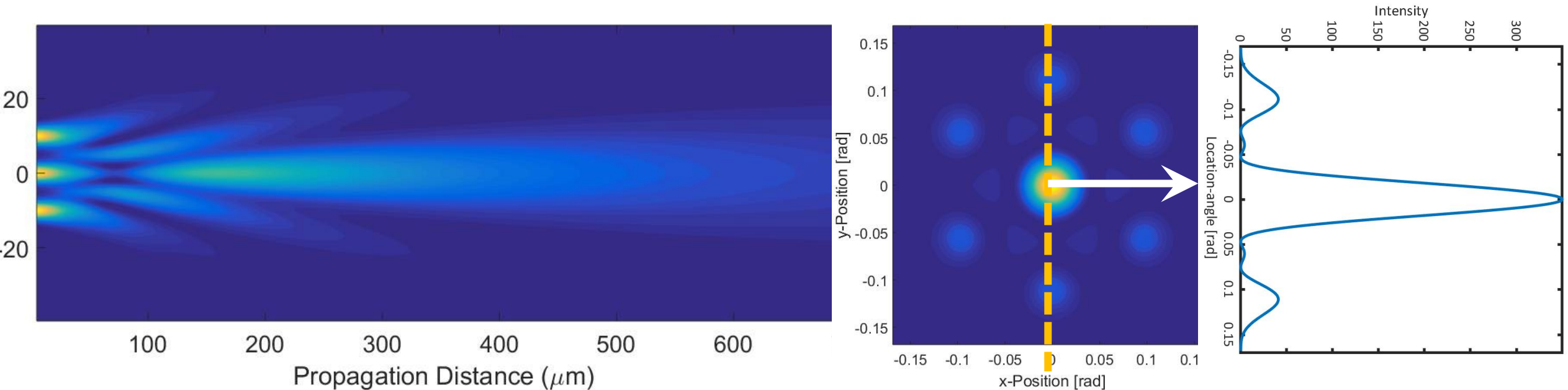
Detailed Optical Layout





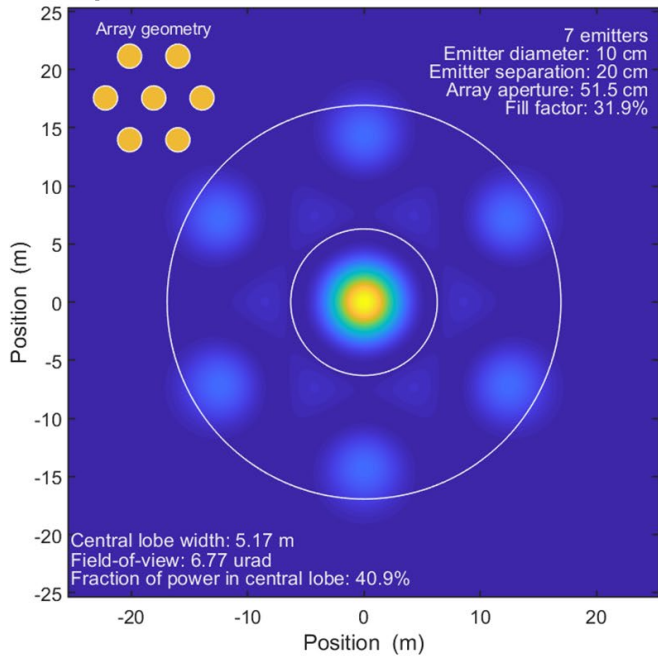
Far-field spatial interference

$$\sum_{i=1}^N \underbrace{\sqrt{P_i} \frac{W_0}{W(z)}}_{\text{Electric field amplitude}} \underbrace{e^{\frac{-\rho_i(x,y)^2}{W^2(z)} - ik \frac{\rho_i(x,y)^2}{2R(z)}}}_{\text{Wavefront curvature}} \underbrace{e^{ik(z+z_i(t)) - i(\omega t) + i\zeta(z)}}_{\text{Piston phase}}$$

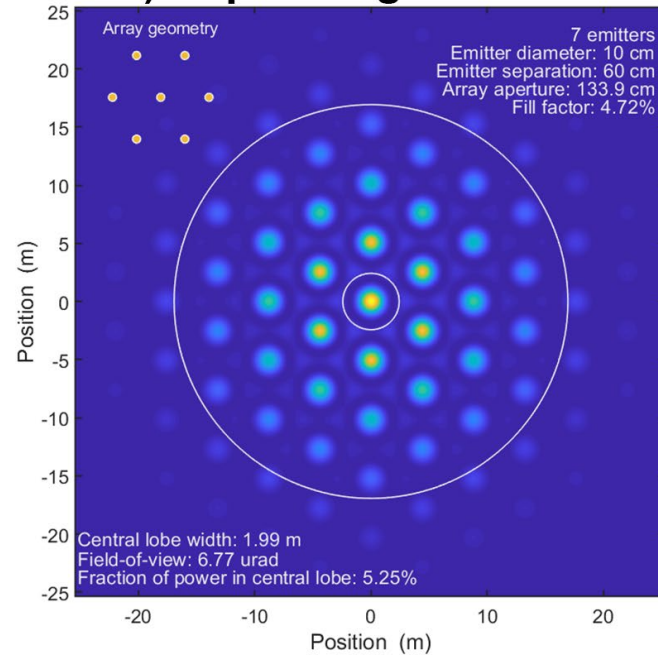


Simulated beam intensity from 7 emitters in a hexagonal configuration and 10 μm separation. From left to right: Cross section along the x-axis, Cross section along the z-axis (at z=1m), Cross section along the z and x axis

a) Baseline

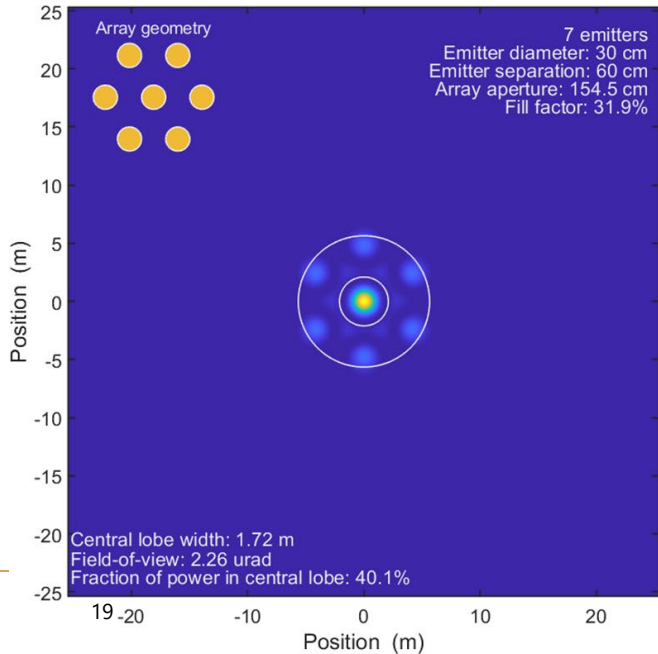


b) Separating emitters

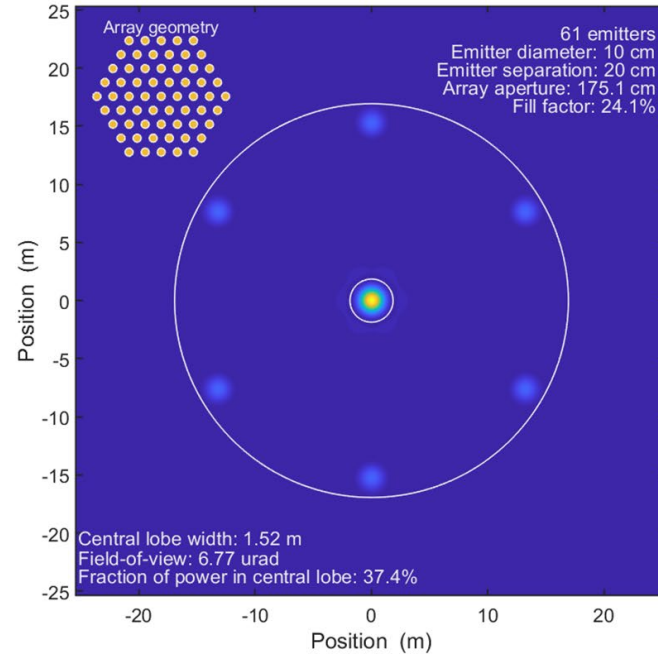


- Can be predicted using the wavefront curvature term:
$$e^{-\frac{\rho_i(x,y)^2}{W^2(z)}} - ik \frac{\rho_i(x,y)^2}{2R(z)}$$
- Different optical head geometries can result in vastly different output patterns

c) Increasing emitter apertures



d) Increasing number of emitters



- $$\rho_i(x, y) = \sqrt{(x - x_i)^2 + (y - y_i)^2}$$
- Key parameters:
 - Central lobe width
 - Field of view and steering range
 - Power in the central lobe



Beacon Reconstruction Algorithm

$$\Lambda_{e,b1} = \frac{1}{\lambda_e} - \frac{1}{\lambda_{b1}} = \frac{c}{\Delta\nu_{b1}}$$

For a 100 GHz frequency shift, the synthetic wavelength is ~3 mm

Conversion using multiple beacons:

$$\phi_{\lambda_e} = \phi_{\lambda_{b1}} + \frac{\Lambda_{b1,b2}}{\Lambda_{e,b1}} (\phi_{\lambda_{b1}} - \phi_{\lambda_{b2}}) \text{ mod } 1$$

Residual:

$$\frac{\Lambda_{b1,b2}}{\Lambda_{e,b1}} \left(\left\lfloor \frac{\Delta L}{\lambda_{b1}} \right\rfloor - \left\lfloor \frac{\Delta L}{\lambda_{b2}} \right\rfloor \right) \text{ mod } 1$$

“Ideal” Condition:

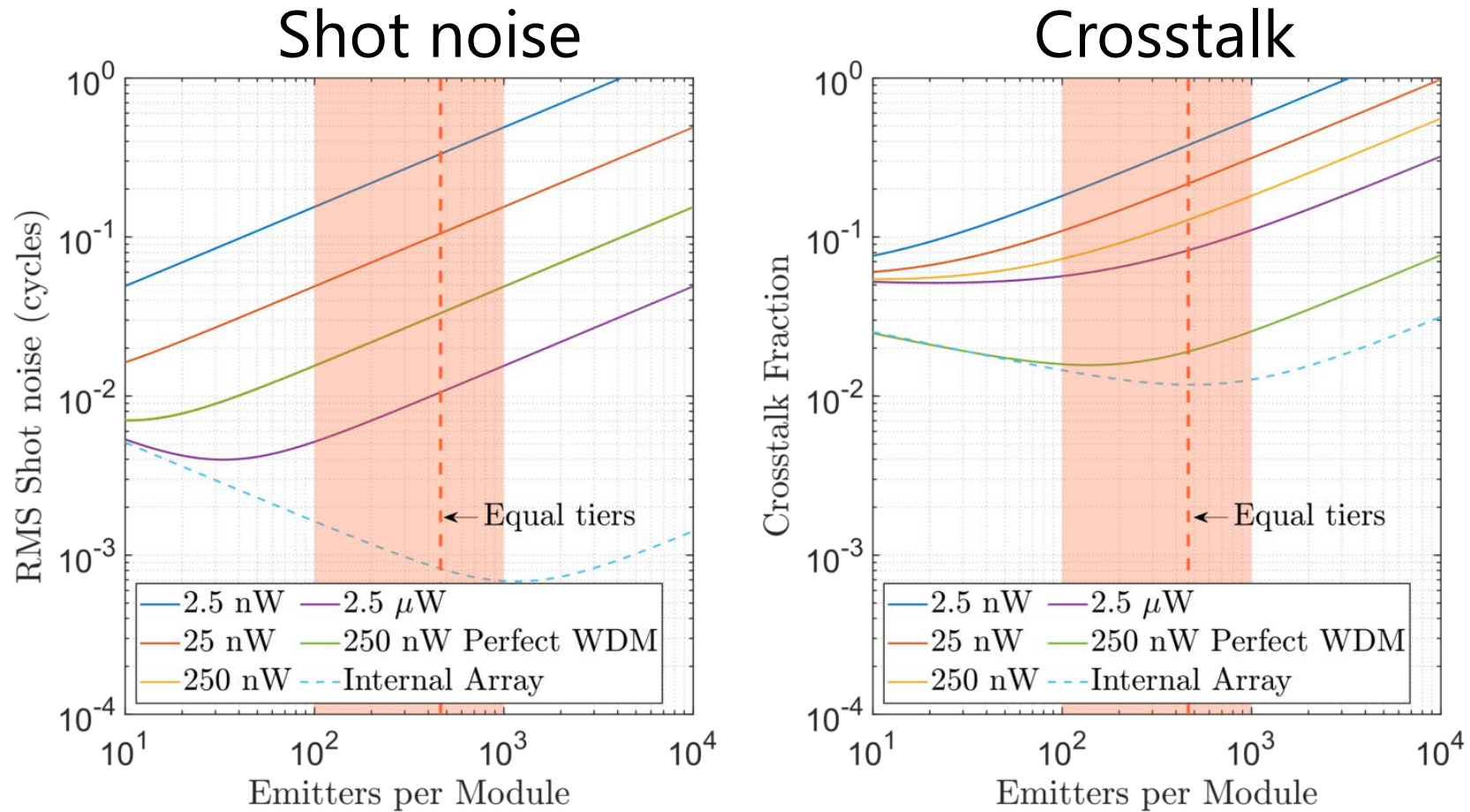
$$\Delta\nu_{b2} = \Delta\nu_{b1} + \frac{\Delta\nu_{b1}}{K}$$

$$\Lambda_{e:b1} = K\Lambda_{b1:b2} \text{ (where } K \text{ is an integer)}$$

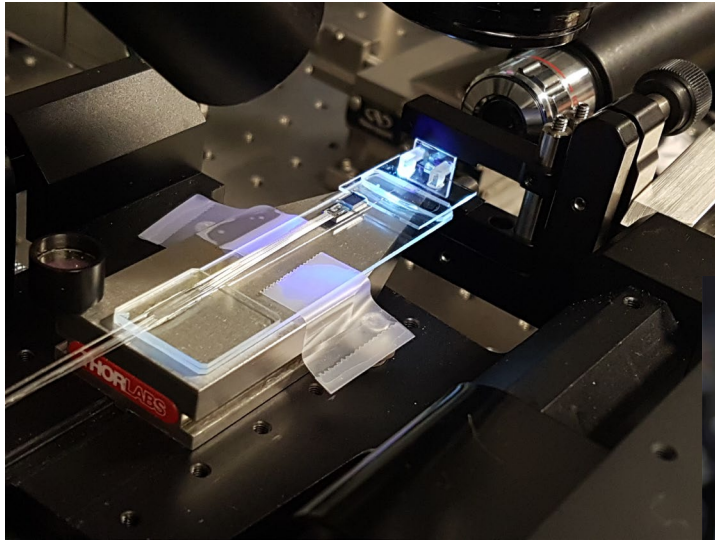


Predicted hierarchy OPA performance

Choosing parameters for the array



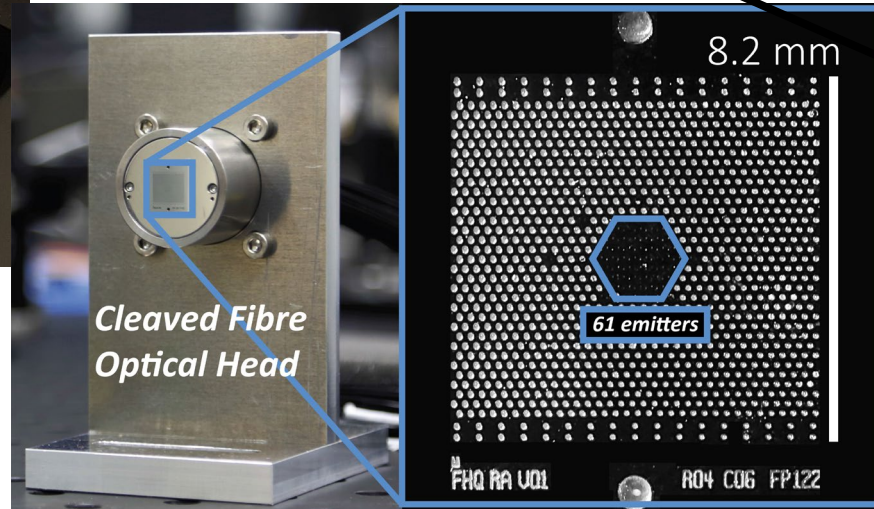
Different OPA Scales



Emitter Size



Radar Phased Arrays



Cleaved Fibre
Optical Head

61 emitters

Roberts, L.E., *Internally Sensed Optical Phased Arrays*. 2016. – PhD Thesis

- Photonic integrated circuits
- Optical fibres / Microlens arrays
- Larger collimators



<https://www.iiviad.com/portfolio/fiber-array-technology/>



Wavelength multiplexed detector

Possible Solution:

Fibre Bragg gratings combined with optical circulators used to separate wavelengths.

DWDM communications readily achieve >20 dB channel isolation in the telecoms band with 100 GHz channel spacing

Proposed topology allows for a worst case 20 dB isolation with 100 GHz wavelength separation

