30th International Conference on Ultra-relativistic Nucleus-Nucleus Collisions (QM 2023)

# Exploring the Freeze-out Hypersurface with a Rapiditydependent Thermal Model

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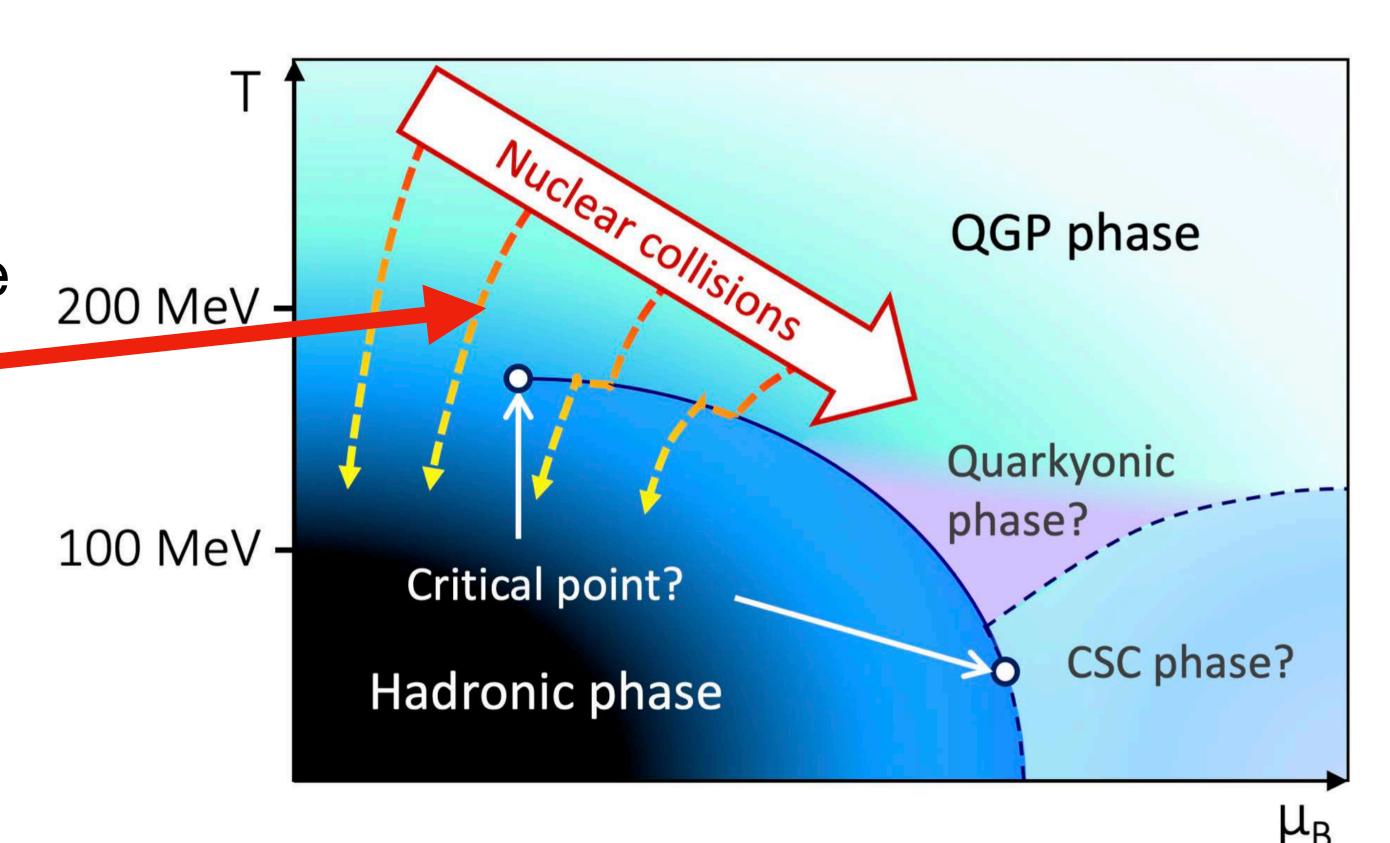
McGill University



Based on Lipei Du, HG, Sangyong Jeon & Charles Gale, 2302.13852 HG, Lipei Du, Sangyong Jeon & Charles Gale, 23xx.xxxx

#### QCD phase diagram

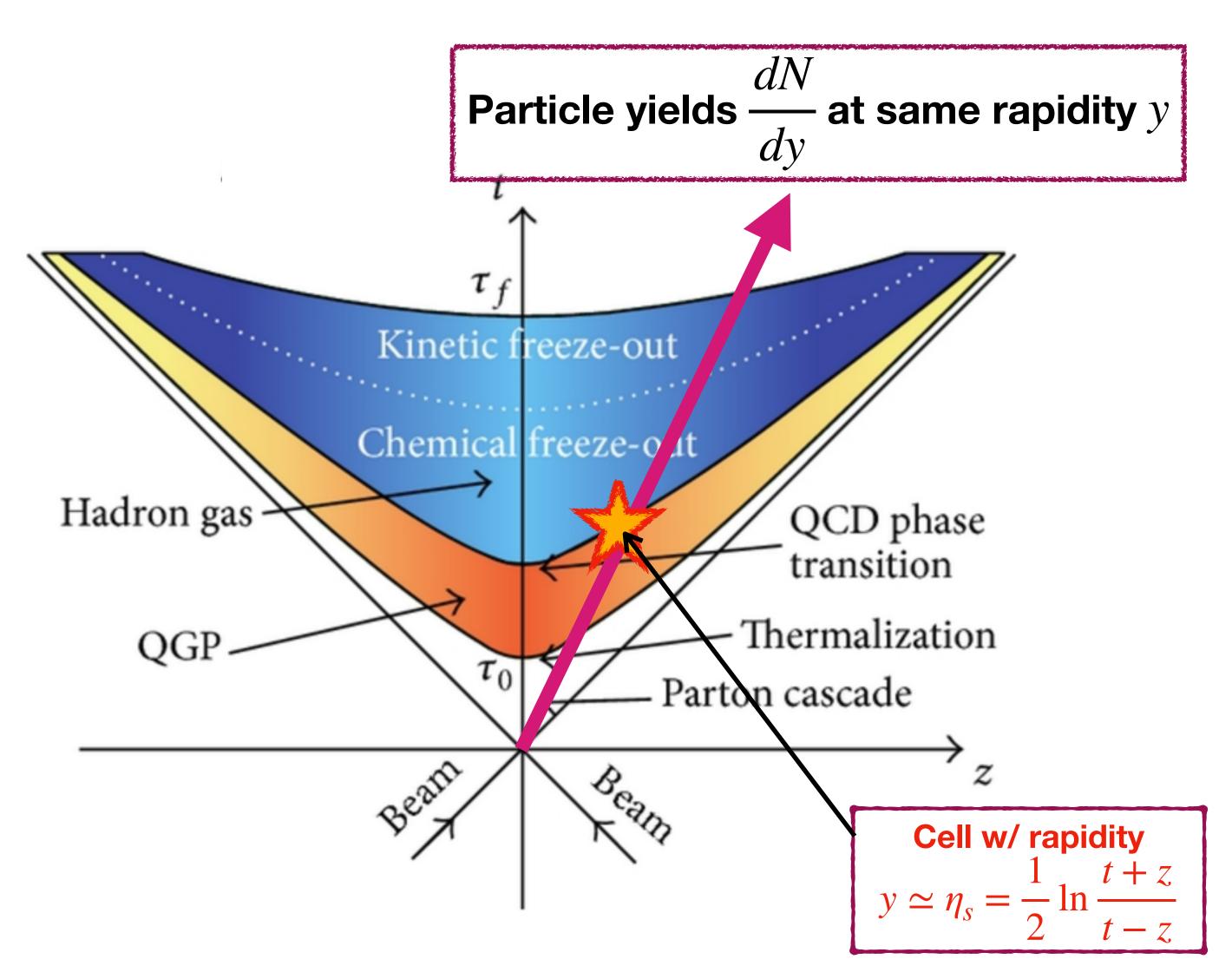
- Beam energy scan: Mapping out the phase diagram by varying the collision energies.
- Thermal Models: particle multiplicities —> thermodynamics: including Hadron Resonance Gas model (HRG).
- Tools available on the market, e.g. [V. Vovchenko & H. Stoecker, Comput. Phys. Commun. (2019)]



A. Monnai, et al, IJMPA (2021)

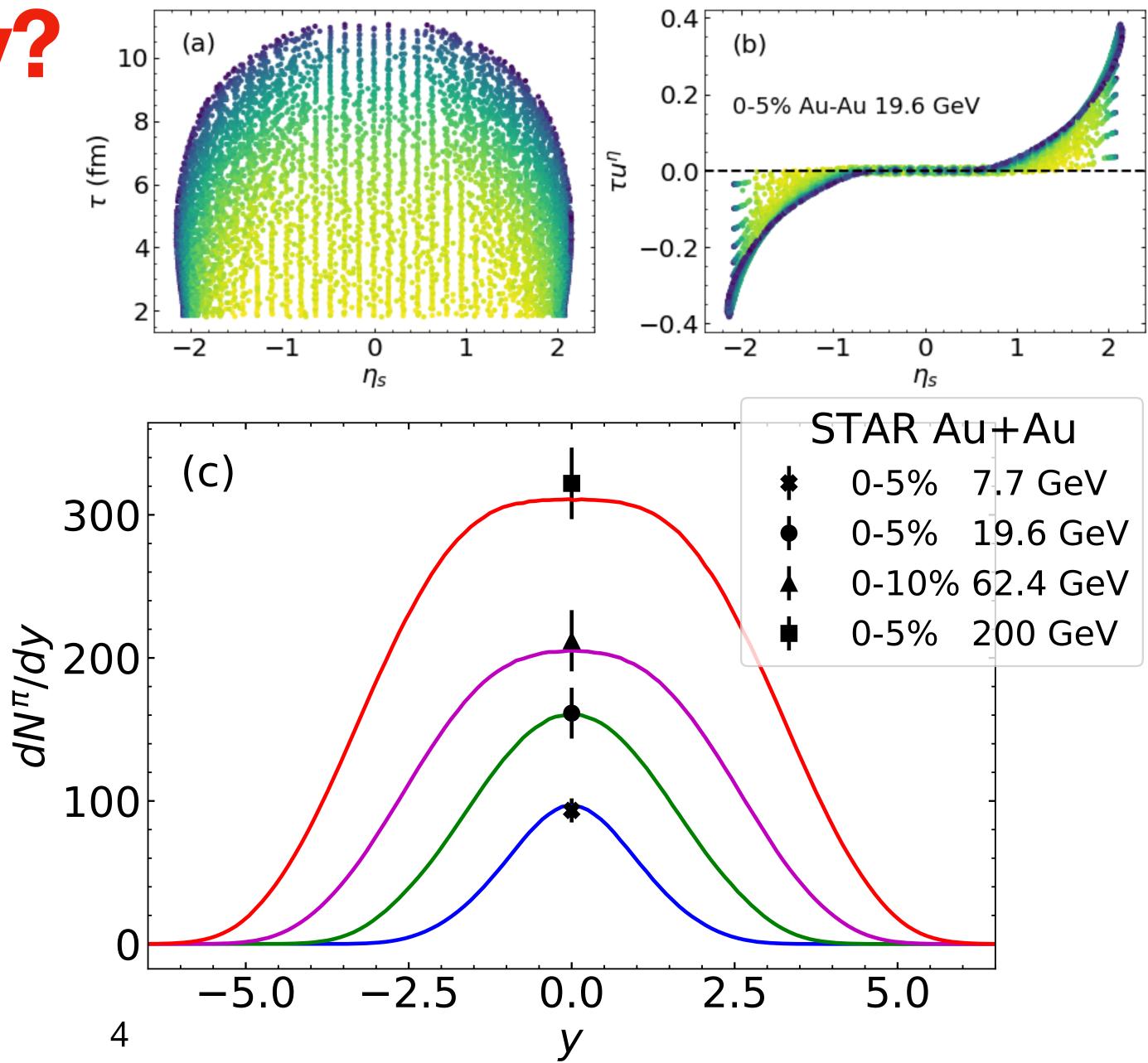
#### Rapidity scan along the freeze-out surface

- Freeze-out surface is not homogenous.
- Rapidity scan: inferring freeze-out thermodynamics for cells at different rapidity  $\eta_s$  from particle yields dN/dy.
- Commonly used practice: using HRG for each rapidity bin independently. See, e.g. [V. Begun, et al, PRC (2018)]



## About large rapidity?

- Multistage hydro => freeze-out cells live within a limit range of  $\eta_s$ .
- E.g., right fig.  $|\eta_s| < \eta_{max} \approx 2$  for  $\sqrt{s} = 19.6$  GeV.
  - Particle yields reach  $y \approx 4$
  - How to improve the "commonly used practice" (independent y bins) for large rapidity (tail) region?

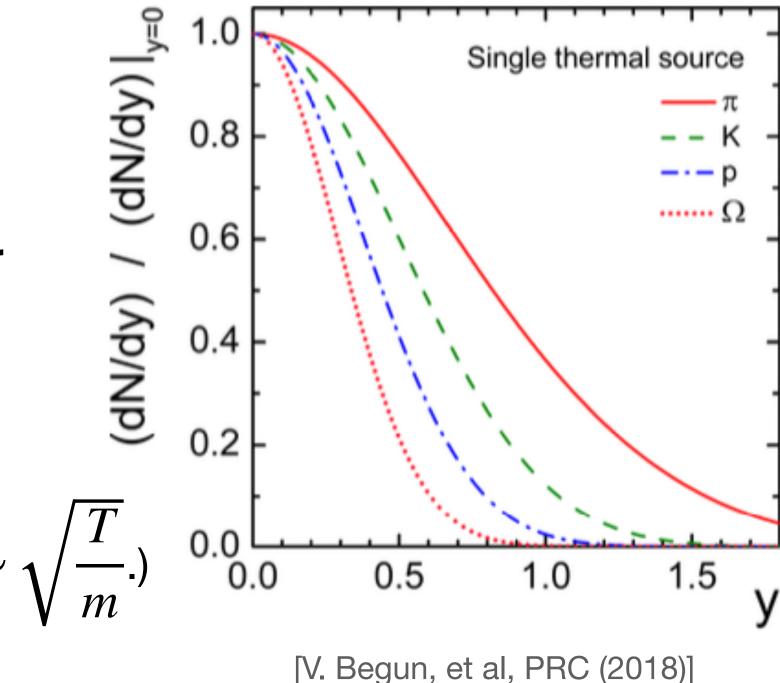


#### Two effects

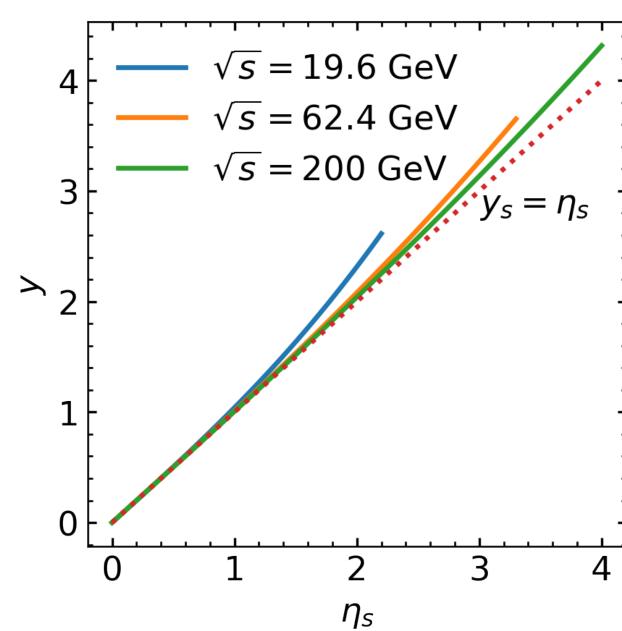
• Thermal smearing: a thermal source with rapidity  $y_s$  contributes to particle yields at other rapidities.

Fig: yields from a resting source (y=0).

Significant smearing effect for lighter particles (e.g.  $\pi$ . smearing width  $\Delta y \sim 1$ 



- Longitudinal boost: Deviation from Bjorken
- Flow as  $\sqrt{s} \downarrow : \eta_s < y_{s^*}$  subscript s = source, here FO cells
- Particles produced as a freeze-out cell with small  $\eta_s$  can be boosted to a large rapidity y.

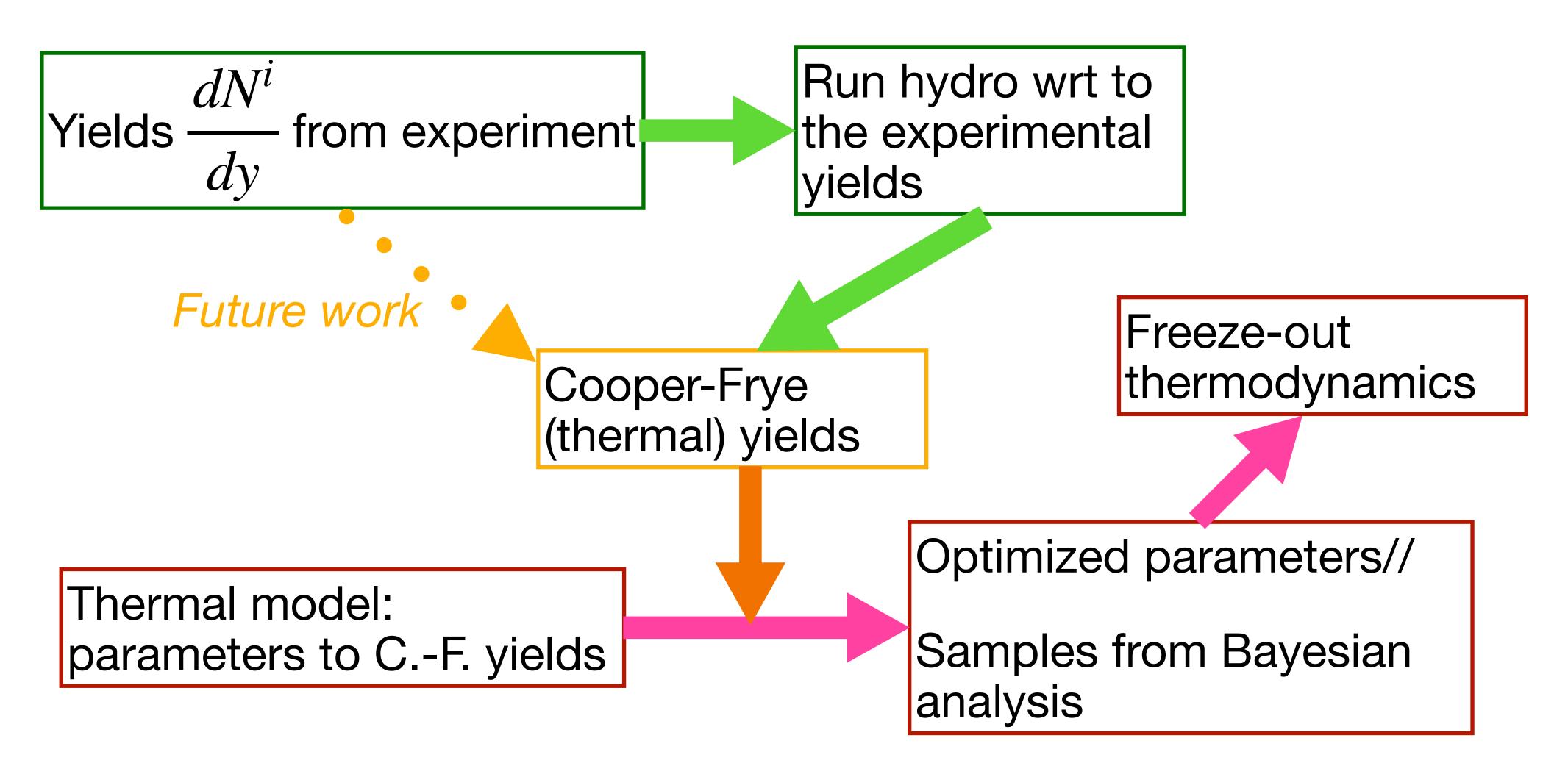


#### A thermal model with smearing effect + longitudinal flow

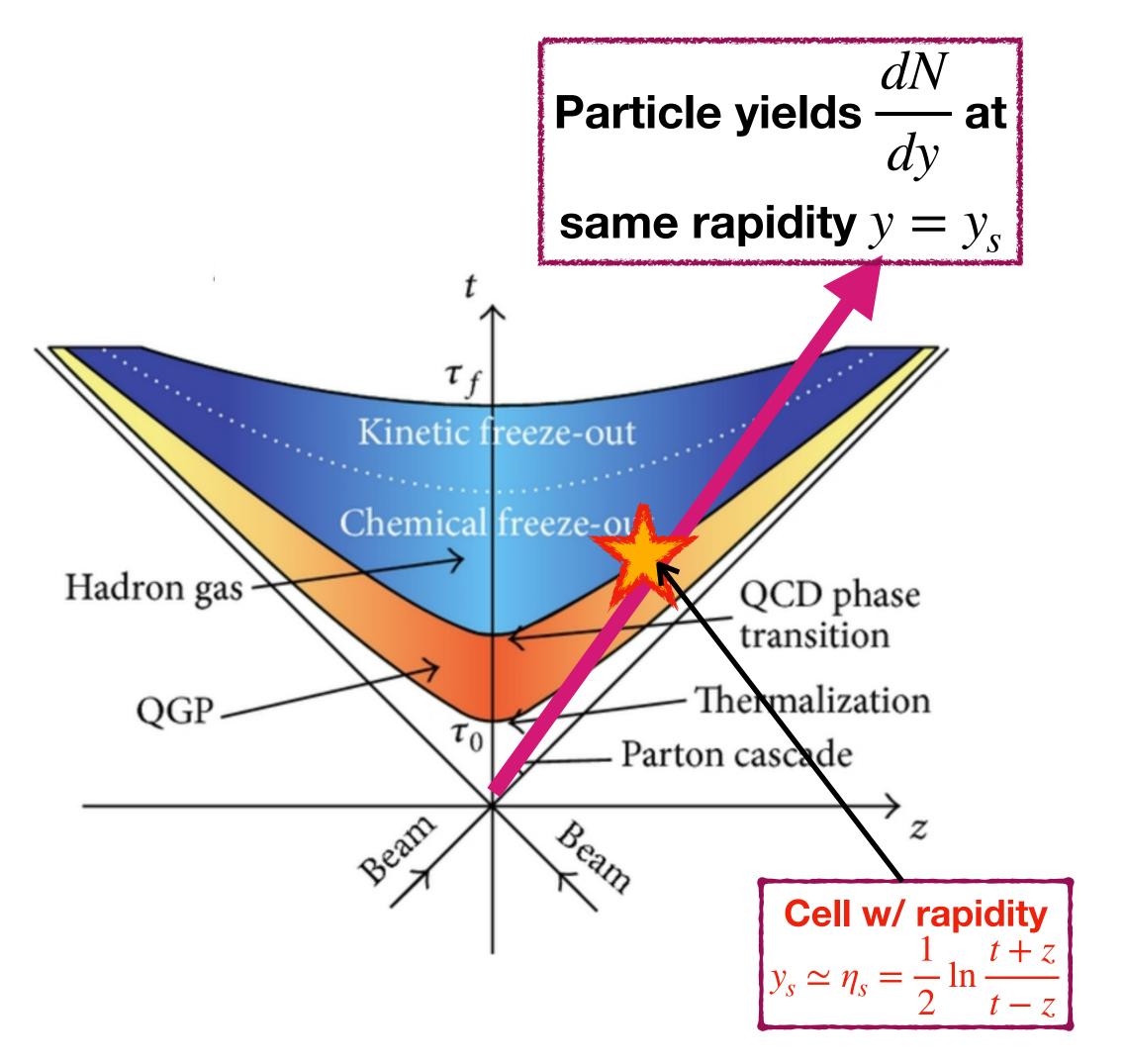
- Parametrizing  $T(\eta_s) = T_0 + T_2 \eta_s^2 + \dots$ ,  $V(\eta_s), \mu(\eta_s)$ ;
- Convert cell's space-time rapidity  $\eta_s$  to rapidity  $y_s$  by kinematics  $\tau u^{\eta} = \alpha \eta_s^3$ .
- . For a cell with  $y_s=0$ , thermal yields worked out as  $\dfrac{dN^i}{dy}\equiv K^i(y;T,\mu,V)$ . \*  $i=\pi^+,K^+,p-\bar{p}$
- Integrating over all cells (with different  $\eta_s$ ) by

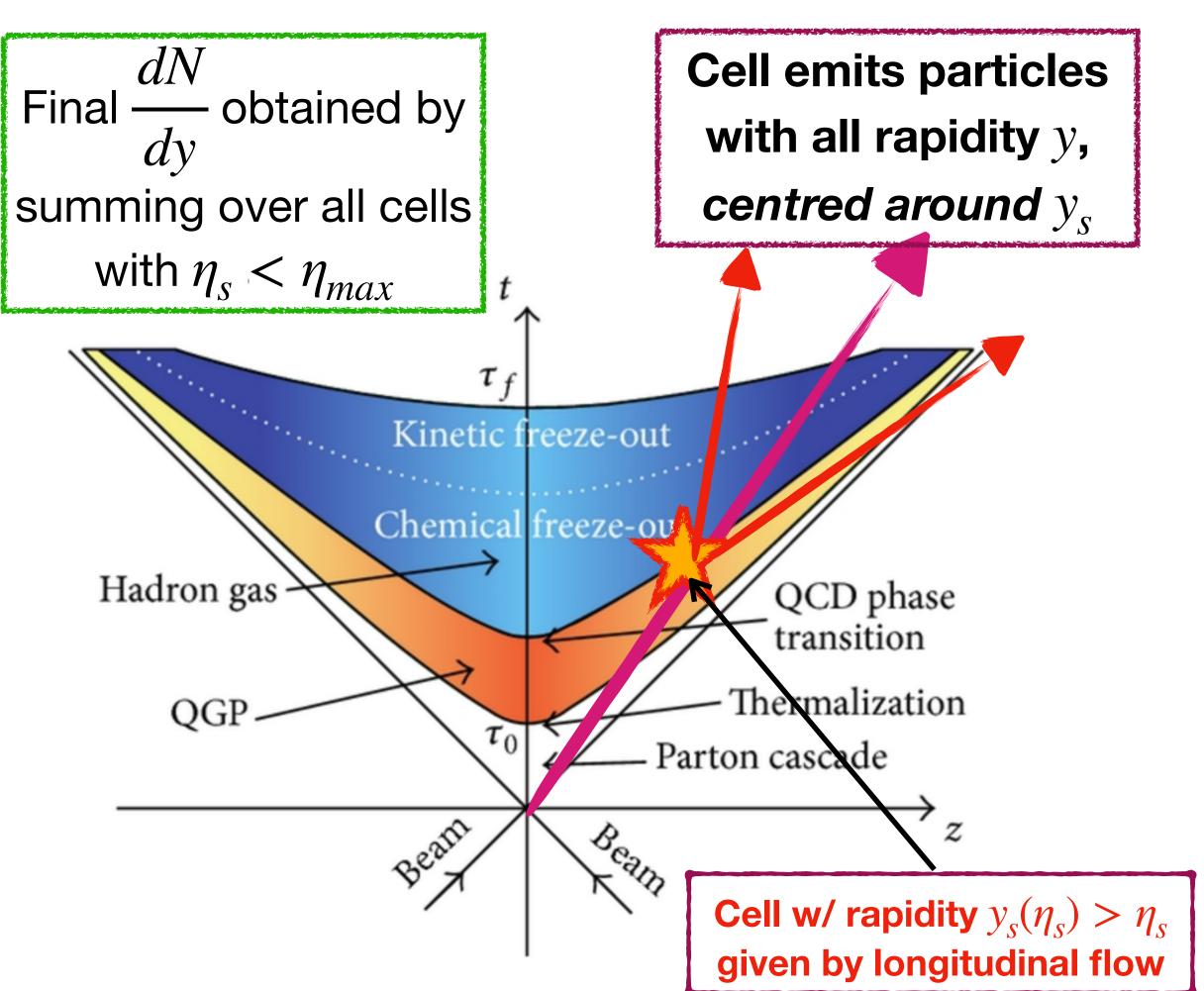
$$\frac{dN^{i}}{dy} = \int_{|\eta_{s}|} d\eta_{s} K^{i}(y - y_{s}(\eta_{s}); T(\eta_{s}), \mu(\eta_{s}), V(\eta_{s}))$$
Longitudinal dynamics

# Workflow: implementing the model



#### "Discrete" v.s. "Continuous" thermal model

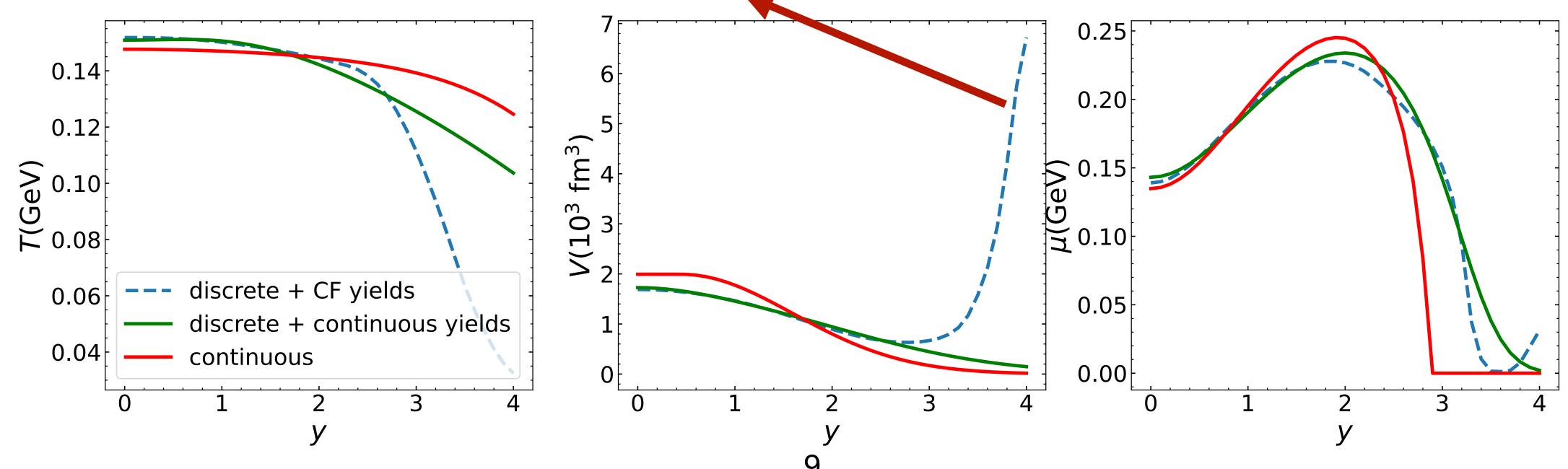




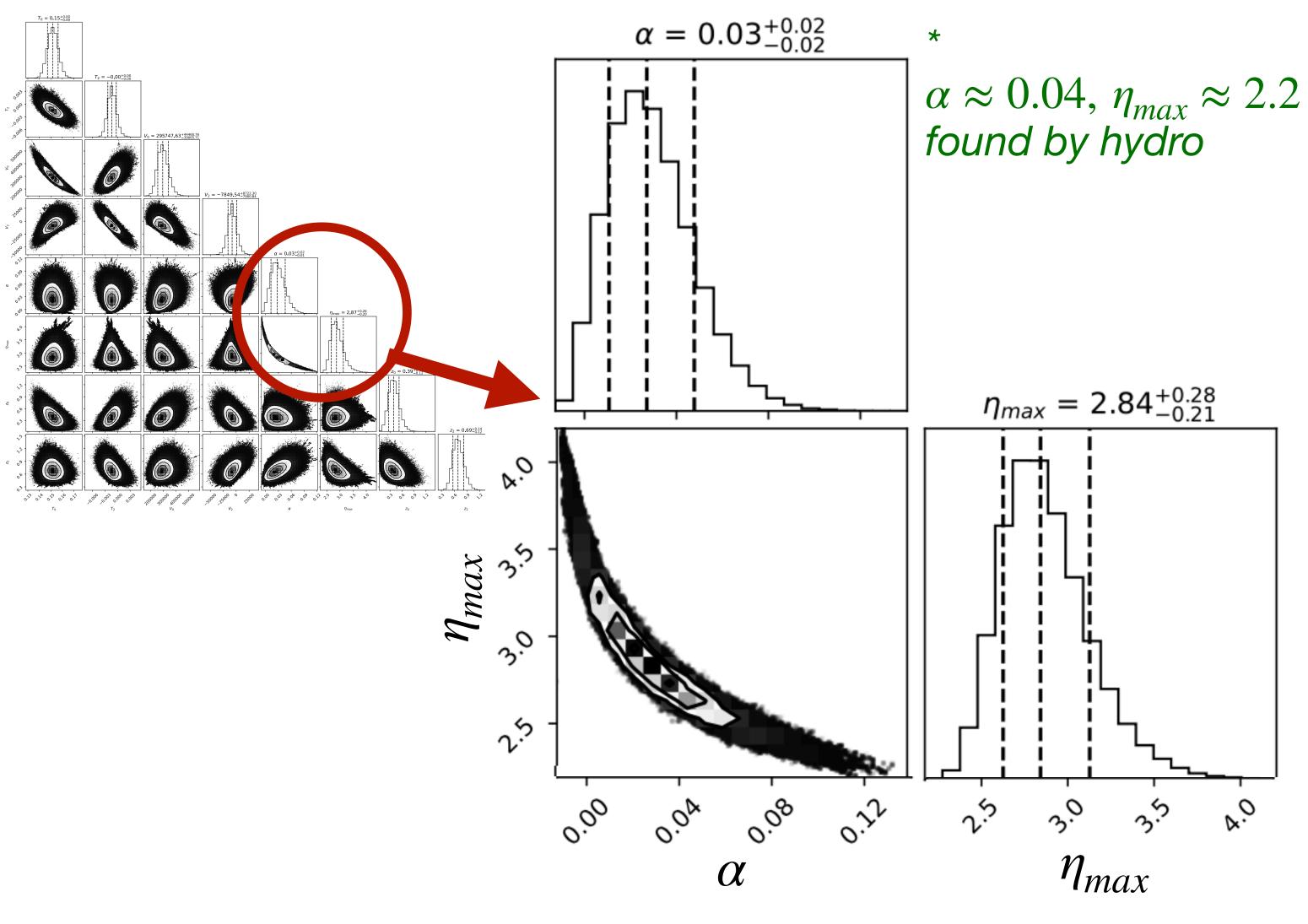
#### Comparison: "discrete" and "continuous" models

- Fit C.-F. yields from a multistage hydro @ 19.6 GeV; longitudinal flow turned off in thermal model. Red/Green lines: two models applied to the same yields.
- Similar  $(T, \mu_B)$  given around mid-rapidity  $|y_s| < 2$  from both models => can safely use the independent-rapidity-bin method for mid-rapidity.

Large uncertainty and unphysical result given by discrete model at large rapidity.



## A Bayesian study: Longitudinal dynamics

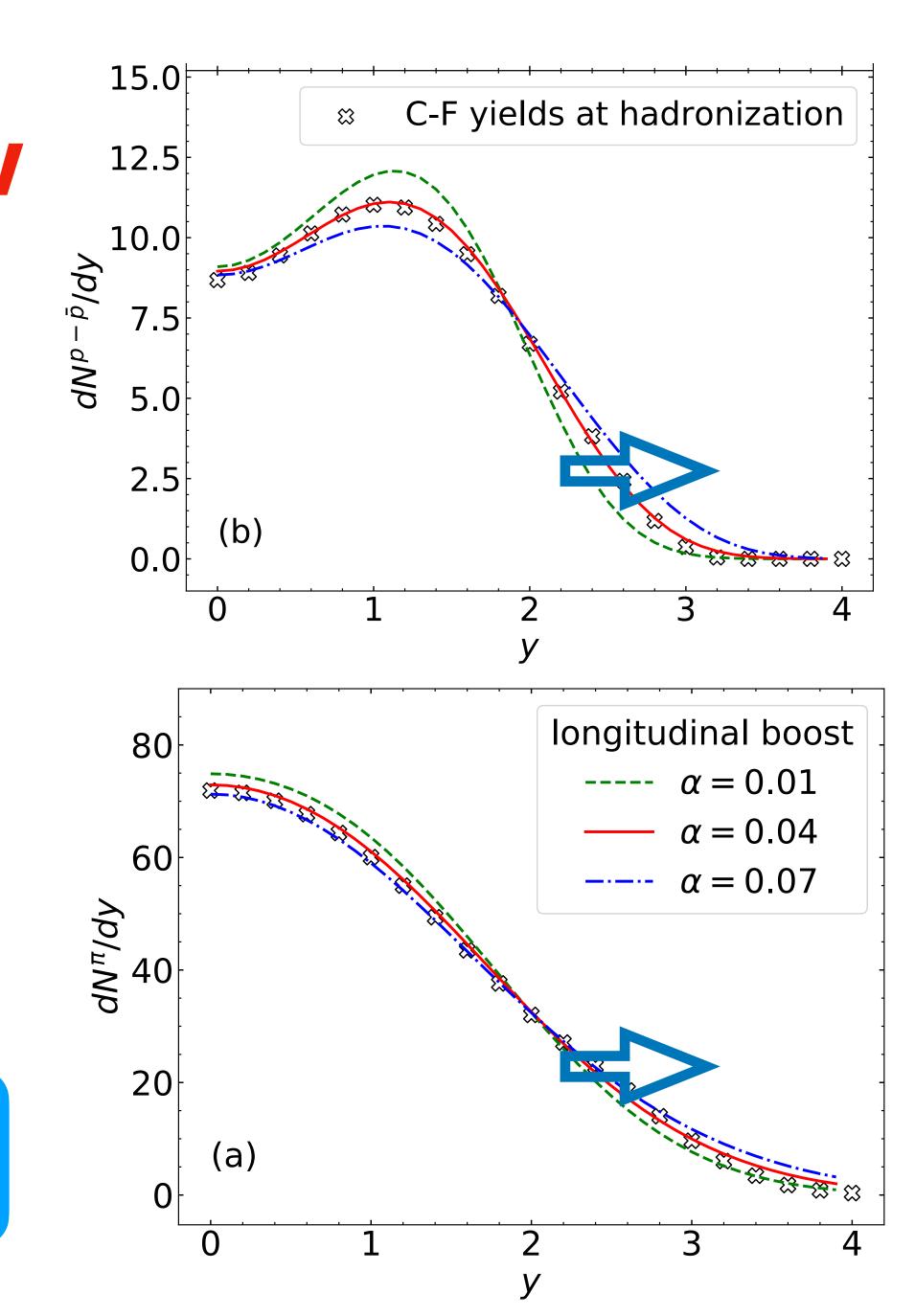


- A strong correlation between system size  $\eta_{max}$  and flow strength  $\alpha$ .
- Flow parameters can still be constrained.
- A positive  $\alpha$  is favoured => see longitudinal dynamic from a thermal model!

#### Effects on yields from the flow

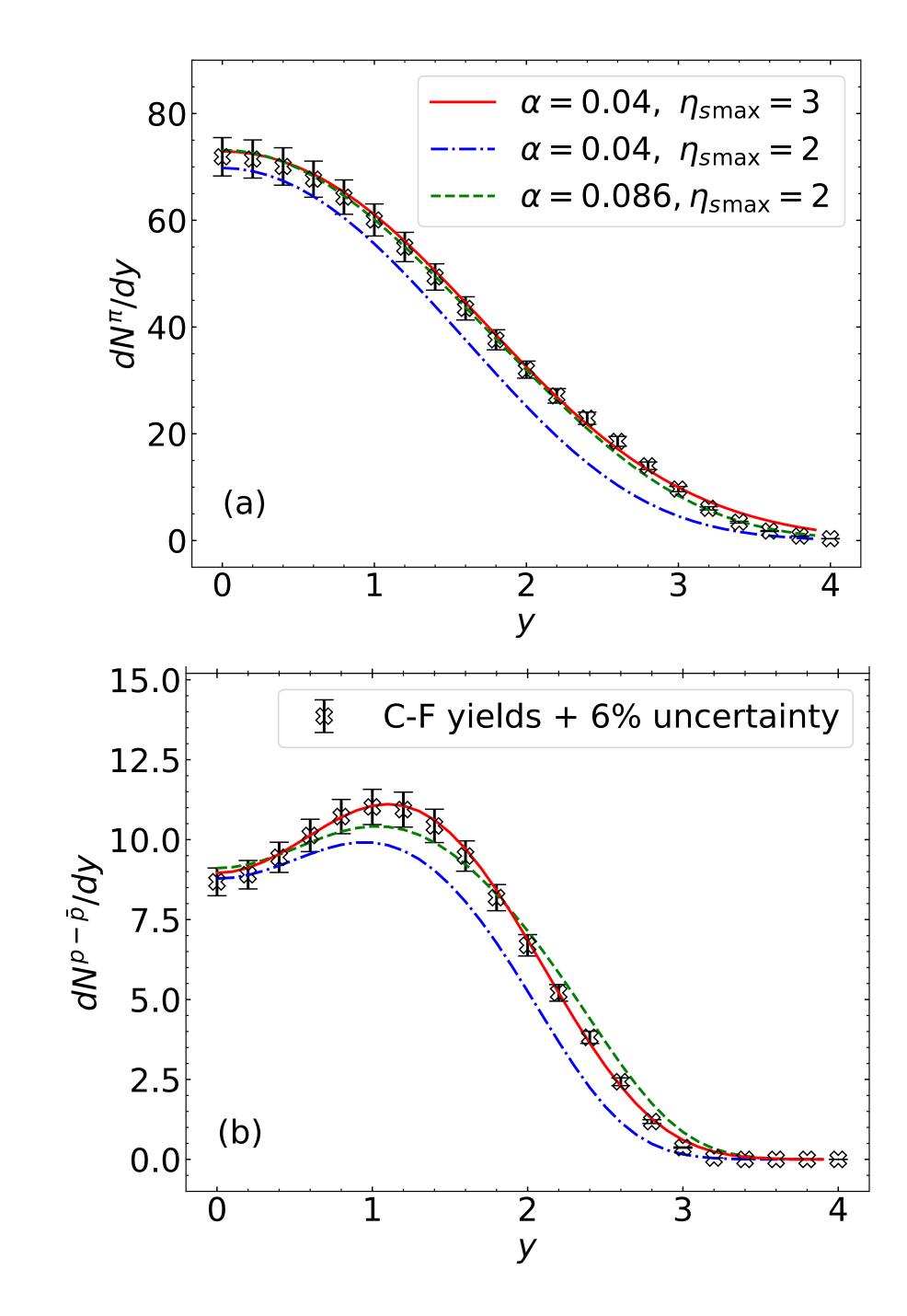
- From hydro profile @19.6 GeV: longitudinal flow  $\alpha = 0.04$ .
- Fix  $\alpha$  but  $\eta_{max}=\infty$  => Obtaining  $T(\eta_s), \mu(\eta_s), V(\eta_s)$  profile by fitting the Cooper-Frye yields.
- Keeping the  $T(\eta_s), \mu(\eta_s), V(\eta_s)$  profile obtained and varying  $\alpha =>$  Exploring the role of longitudinal flow

Larger flow => More particles boost to large y from mid rapidity

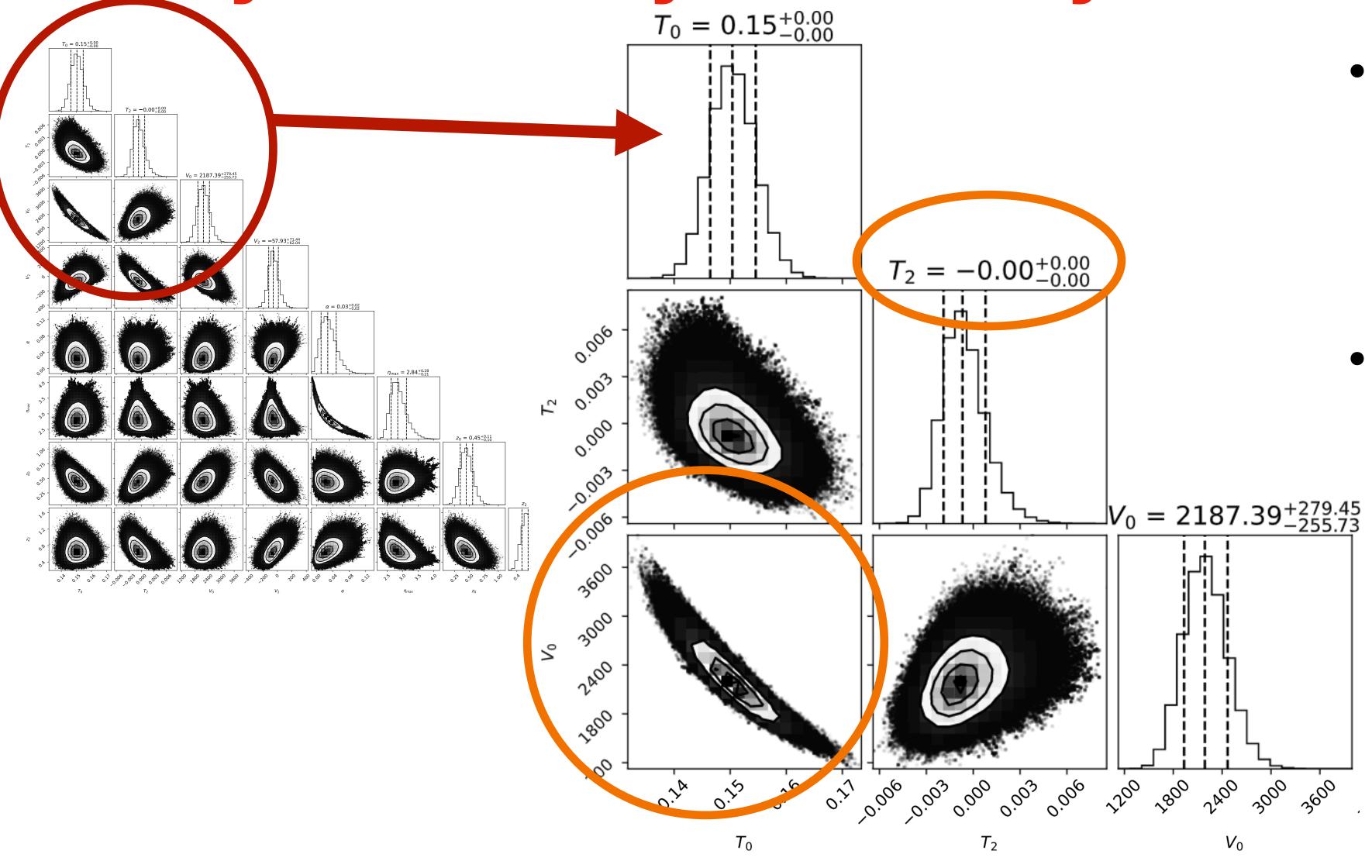


# Coupling between system size and flow

- Now we turn on a finite system size  $\eta_{max} = 2 =>$  yields overall smaller => smearing effect manifested.
- Smaller system size can be partially compensated by a stronger flow => coupling between  $\alpha$  and  $\eta_{max}$ .



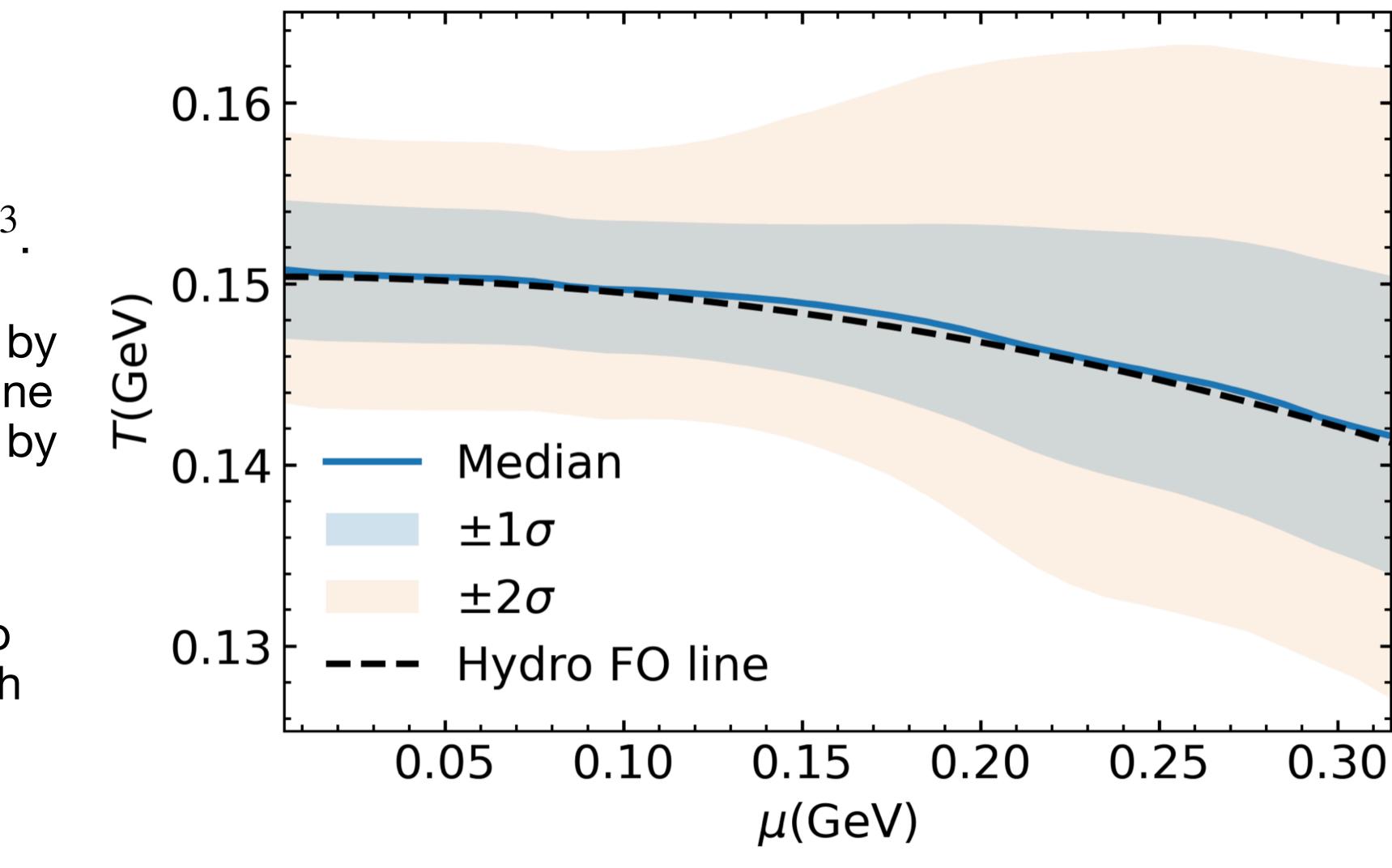
#### A Bayesian study: Thermodynamics



- Almost isothermal freeze-out surface:  $T(\eta_s) = T_0 + T_2 \eta_s^2$  w/ a very small  $T_2$ .
- Large correlation between mid-rapidity temp  $T_0$  and transverse system size  $V_0$ : total **entropy**  $\sim VT^3$  should be conserved.

#### Consistency check w/ hydro freeze-out

- Freeze-out condition used in our hydro: constant energy density  $e_{fo} = 0.26 \text{ GeV/fm}^3$ .
- Yields are generated by hydro => Hydro FO line should be respected by the thermal-model samples.
- After considering two effects, a good match is indeed achieved.



#### Summary and Outlook

- Thermal model is a popular and intuitive way to extract freeze-out thermodynamics. Inspired by hydro, we incorporated both smearing effect and longitudinal flow into thermal model. Applied to C.-F. yields from a multistage hydro.
- Large rapidity: yields get contributions from mid-rapidity, by both effects => Can't use independent-rapidity-bin approach.
- Mid-rapidity: smearing effect doesn't give a significant correction in extracting freeze-out thermodynamics.
- Correlation between longitudinal system size and flow strength.
- A Bayesian analysis favours the existence of a longitudinal flow.
- **To do**: applying the model directly to experimental data (BRAHMS, BES...) => need to deal with the feed-down effect. Confirming our findings w/ hydro yields.

# Backup

#### Uncertainty of discrete model for small yields

T uniquely given by the ratio 
$$\frac{n^{\pi}}{n^{K}} = \frac{m_{\pi}^{2}}{m_{K}^{2}} \frac{\sum_{n=1}^{\infty} (-1)^{n-1} K_{2}(nm_{\pi}/T)}{\sum_{n=1}^{\infty} (-1)^{n-1} K_{2}(nm_{K}/T)}.$$

$$\delta T = \frac{dT}{dr_{\pi/K}} \delta \left(\frac{n^{\pi}}{n^{K}}\right) = \frac{dT}{dr_{\pi/K}} \frac{n^{K} \delta n^{\pi} - n^{\pi} \delta n^{K}}{(n^{K})^{2}}.$$
 
$$\frac{dT}{dr_{\pi/K}} \sim O(0.01 \text{ GeV})$$

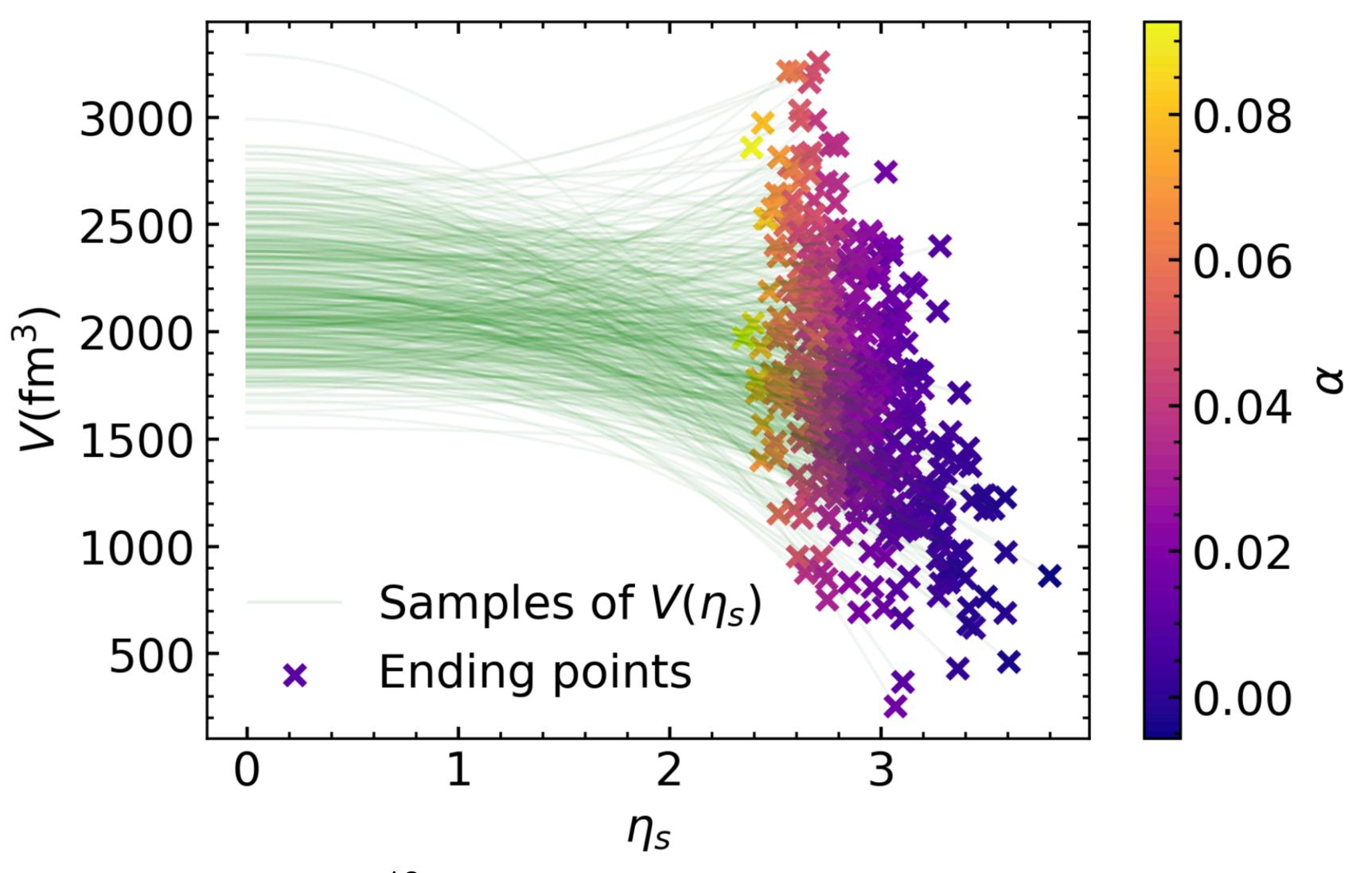
Tail region  $n^K \to 0 =>$  Significant  $\delta T$ 

 $VT^3 \sim \text{const.} => \delta V/V \sim 3\delta T/T => \delta V$  expected to be even larger.

Discrete model gives thermodynamics that is too sensitive to any kinds of uncertainty in yields => the unphysical result is actually "not to be believed"

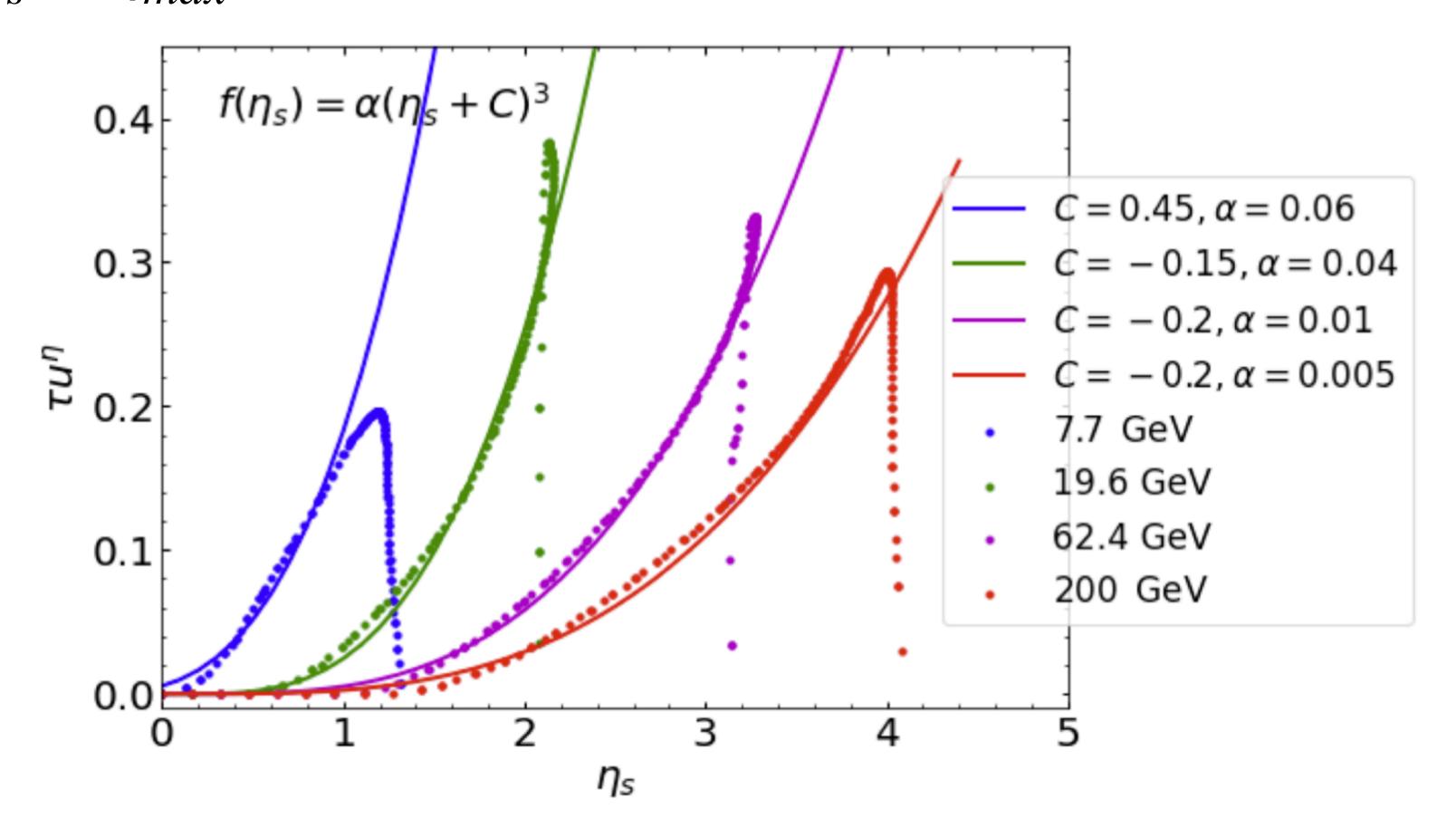
#### System size and the flow

- System size limited within  $\eta_s < \eta_{max}$ , marked with "x".
- Small  $\eta_{max}$  compensated by large  $\alpha$ .
- Decreasing  $V(\eta_s)$  suggested by most samples.



## Longitudinal flow: parametrization

• Evident in hydro: parametrized as  $\tau u^{\eta} = \alpha \eta_s^3, \eta_s < \eta_{max}$ .



# Longitudinal flow: $y - \eta_s$ conversion

$$ds^{2} = dt^{2} - dz^{2} = d\tau^{2} - \tau^{2}d\eta_{s}^{2}, \qquad \Longrightarrow \qquad u^{\tau} \equiv \frac{d\tau}{ds} = \sqrt{1 + (\tau u^{\eta})^{2}}.$$

$$\begin{pmatrix} dt \\ dz \end{pmatrix} = \begin{pmatrix} \cosh \eta_{s} & \tau \sinh \eta_{s} \\ \sinh \eta_{s} & \tau \cosh \eta_{s} \end{pmatrix} \begin{pmatrix} d\tau \\ d\eta_{s} \end{pmatrix} \implies v^{z} = \frac{\tanh \eta_{s}d\tau + \tau d\eta_{s}}{d\tau + \tau \tanh \eta_{s}d\eta_{s}} = \frac{\tanh \eta_{s}\sqrt{1 + (\tau u^{\eta})^{2}} + \tau u^{\eta}}{\sqrt{1 + (\tau u^{\eta})^{2}} + \tau u^{\eta} \tanh \eta_{s}}.$$

$$y = \frac{1}{2} \ln \frac{E + p^z}{E - p^z} = \frac{1}{2} \ln \frac{1 + v^z}{1 - v^z}. \implies y(\eta_s) = \frac{1}{2} \ln \frac{(\sqrt{1 + (\tau u^{\eta})^2} + \tau u^{\eta})(1 + \tanh \eta_s)}{(\sqrt{1 + (\tau u^{\eta})^2} - \tau u^{\eta})(1 - \tanh \eta_s)}.$$

Rapidity of the source

#### Backup slides: thermal models

$$\frac{d^3N}{d^3\vec{p}} = \frac{V}{(2\pi)^3} f(\vec{p}; T, \mu)$$

 $f(\vec{p};T,\mu)$ : Fermi-Dirac/Bose-Einstein distribution; expanded as series of

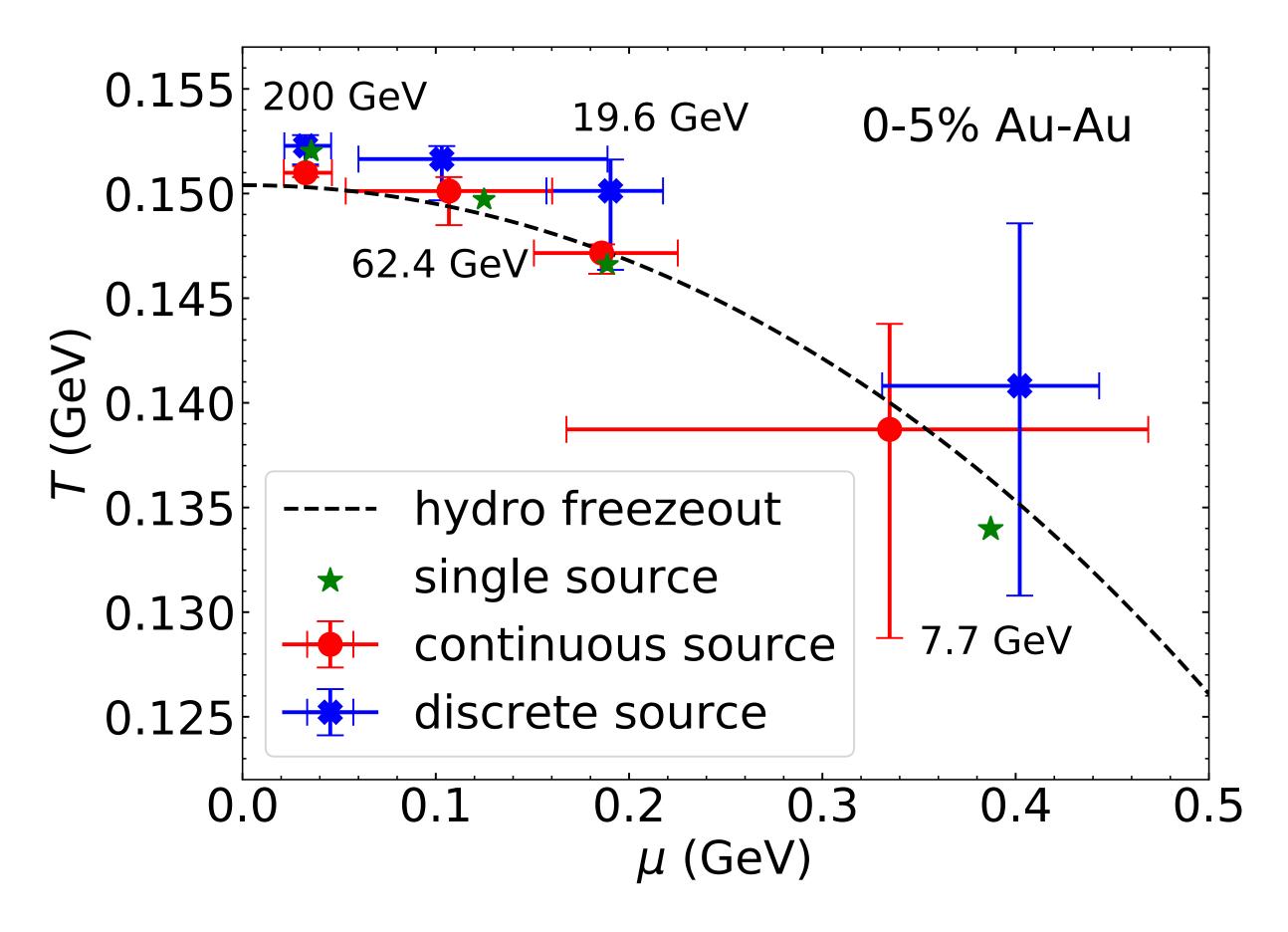
Boltzmann/Maxwell dist.

Discrete model: 
$$N = \int d^3\vec{p} \frac{d^3N}{d^3\vec{p}} \implies (T, \mu, V) \rightarrow (N^{\pi}, N^K, N^{p-\bar{p}})$$

Continuous model (with smearing):  $(p_x, p_y, p_z) = (p_T \cos \phi, p_T \sin \phi, m_T \cosh y)$ 

Integrating over 
$$(\phi, m_T) = > \frac{\frac{dN_i}{dy}\Big|_{y_s=0}}{1 + \frac{n^2 m_i^2}{T^2}} \sum_{n=1}^{\infty} \left(\frac{1}{n}\right)^3 \left(\frac{2}{\cosh^2 y} + \frac{n m_i}{T} \frac{2}{\cosh y} + \frac{n m_i}{T} \frac{2}{\cosh y}\right) + \frac{n^2 m_i^2}{T^2} \exp\left(-\frac{n m_i \cosh y}{T}\right), \quad (10)$$

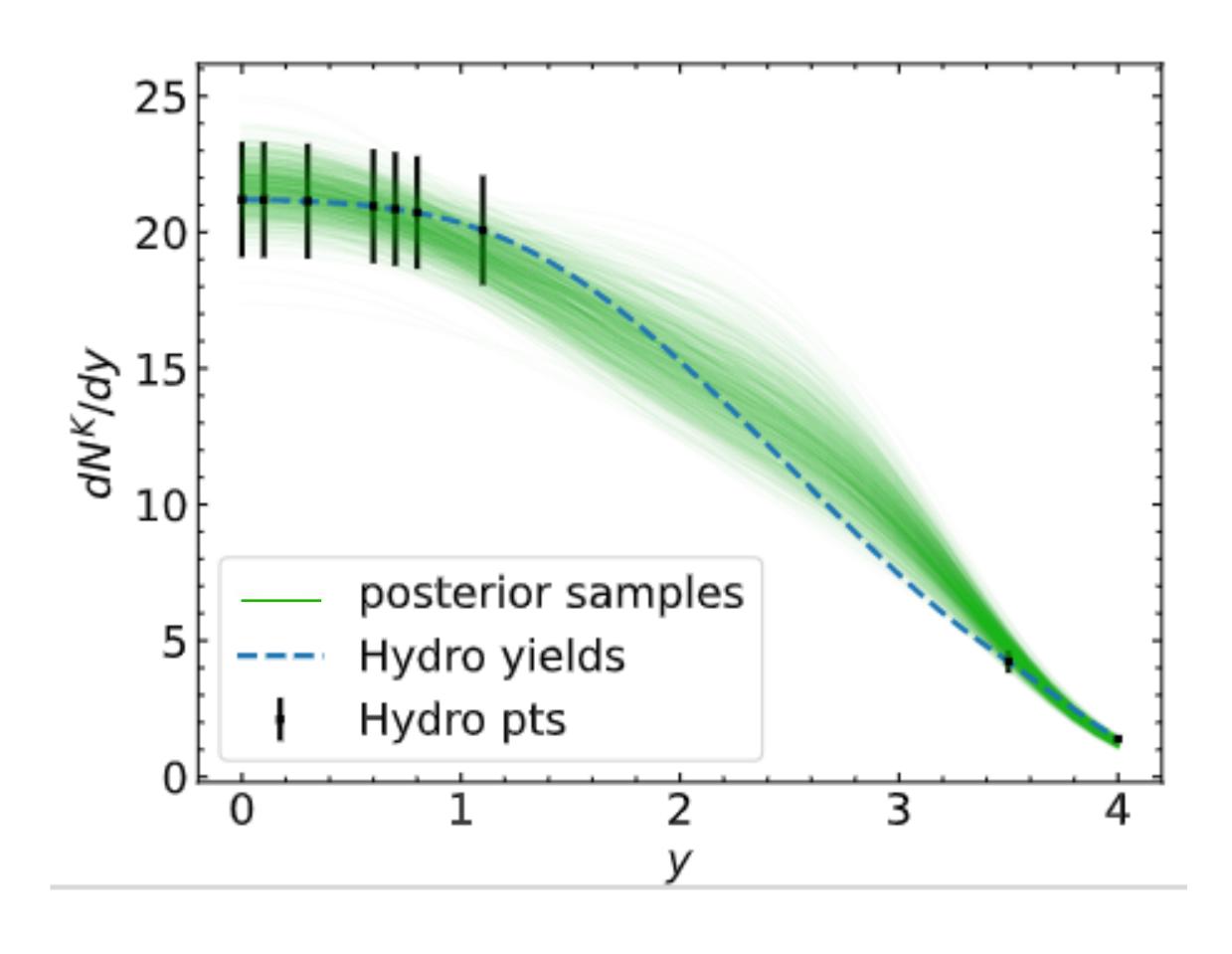
#### Distribution of freeze-out cells on $(T, \mu_B)$ diagram

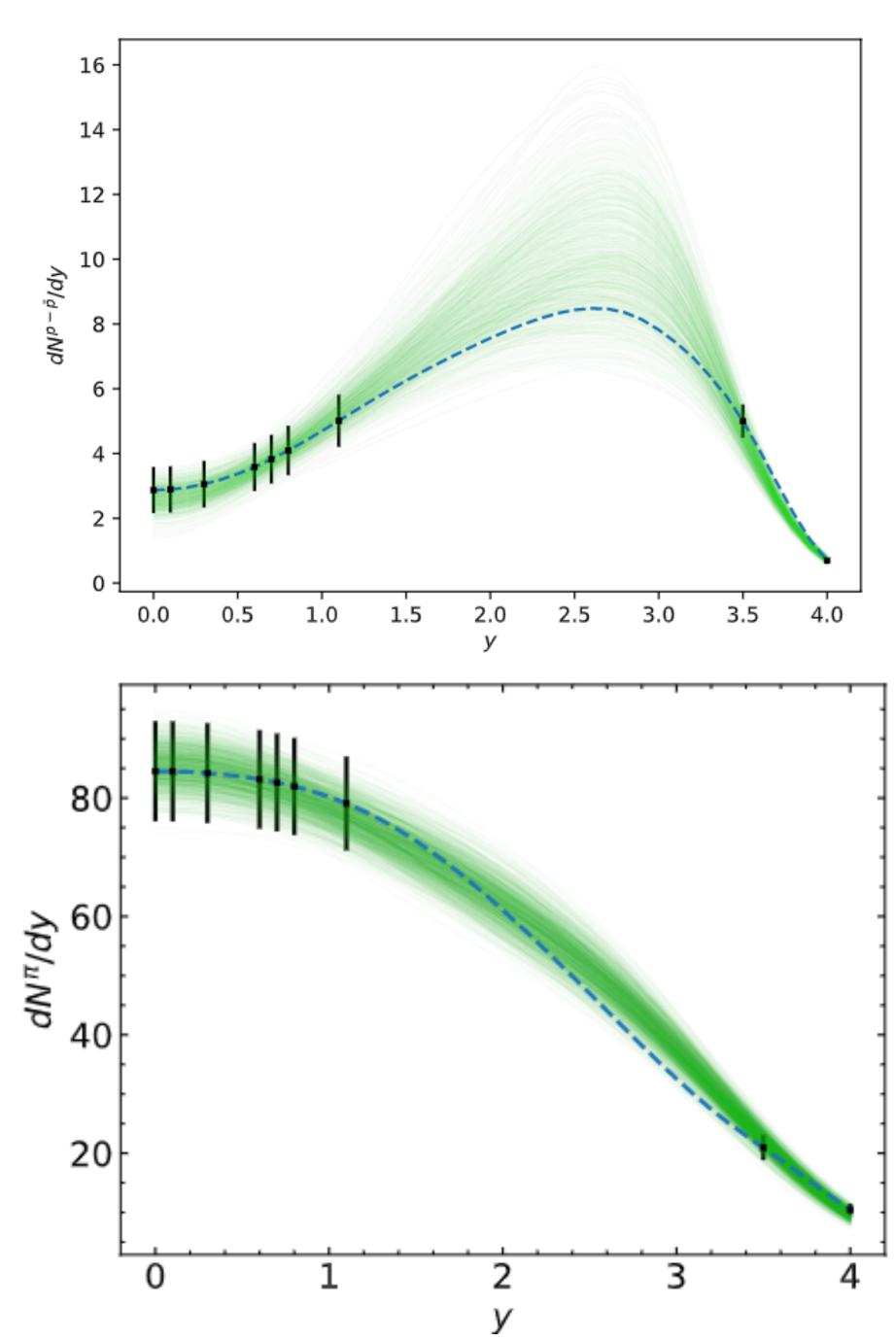


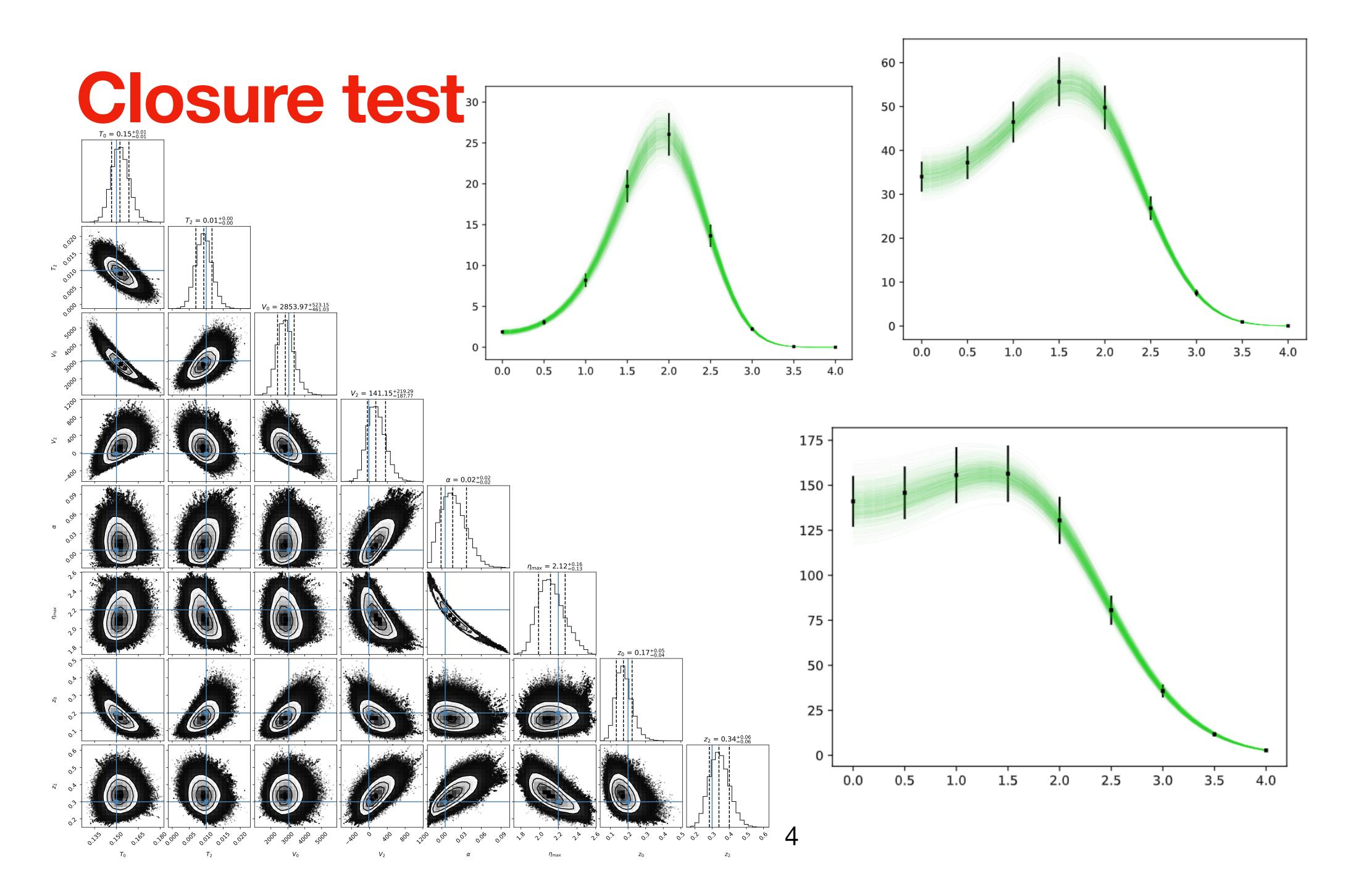
- Errorbars: median and 25% and 75% percentiles of freeze-out cells'  $(T,\mu_B)$  distribution.
- Continuous model gets result closer to the hydro freeze-out line.
- Qualitatively similar traits by both models: as  $\sqrt{s}$  ↑

higher T, more homogenous,...

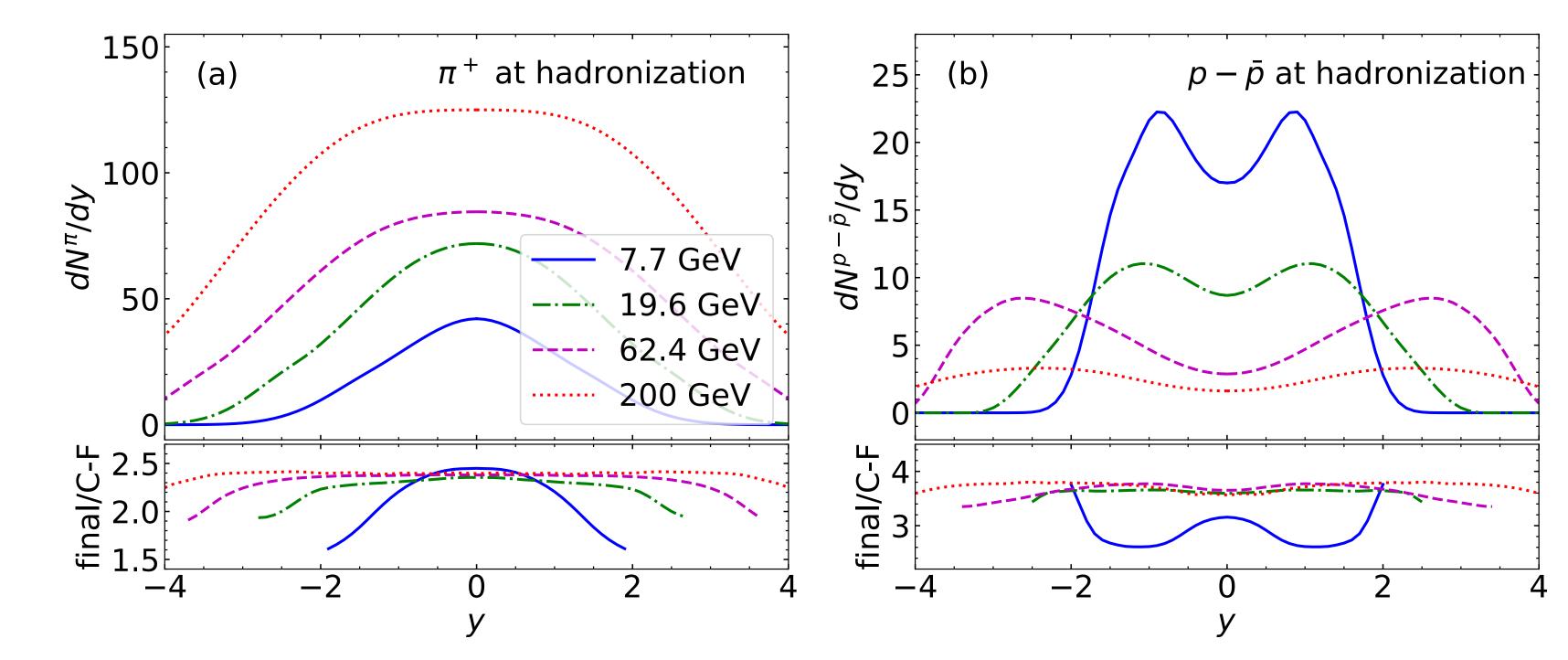
#### Posterior validation





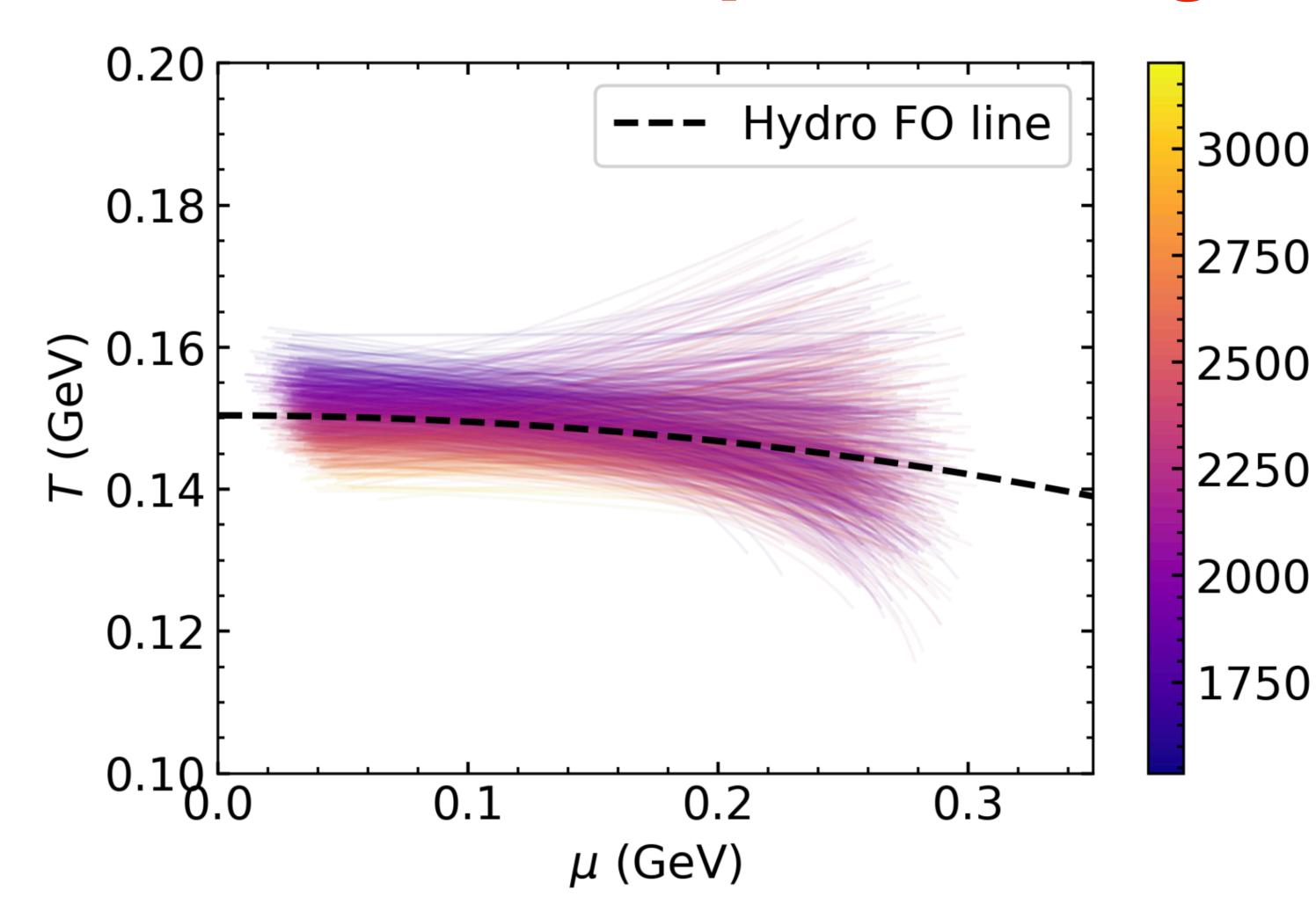


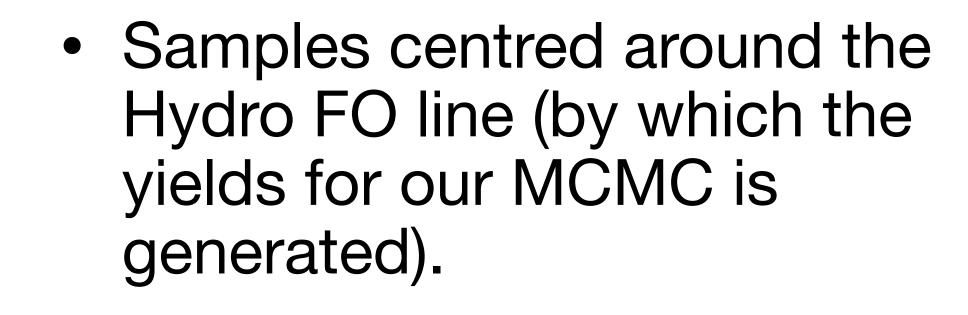
#### Yields at chemical freeze-out



- Particle yields differ from "purely thermal yields" because of resonance decays.
- Thermal model considering both smearing and decay is hard! => Make use of multistage hydro, find  $\frac{\text{final yields}}{\text{Cooper} \text{Frye yields}}$

#### "Freeze-out" phase diagram





- Lower temperature compensated by larger volume.
- Flat FO line for small  $\mu_B =>$  Isothermal