

# Geometry optimization of AC-coupled LGADs for high precision 4D tracking

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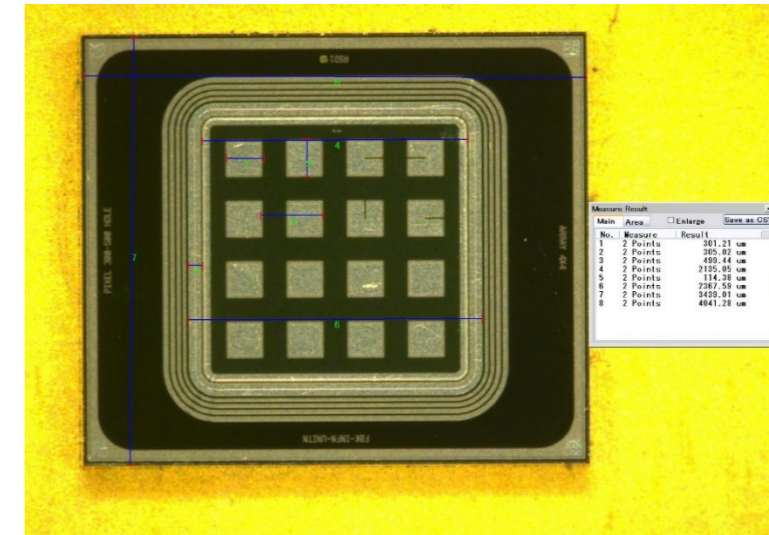
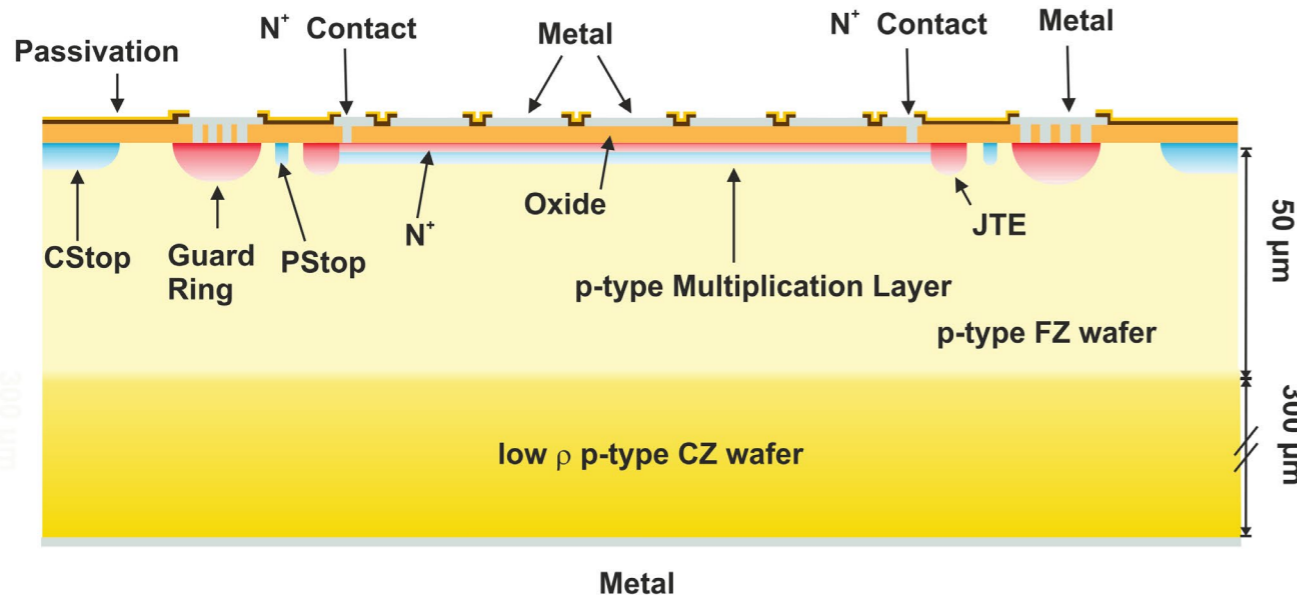
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(students at SCIPP, UC Santa Cruz)



# AC-LGADs

- Most advanced prototype of high granularity LGADs are AC-LGADs
  - (UCSC - US patent N. 9,613,993 B2, granted Apr. 4, 2017)
- Continuous sheets of multiplication layer and N<sup>+</sup> resistive layer
  - N<sup>+</sup> layer is grounded through side connections
- **Readout pads are AC-coupled** (Insulator layer between N<sup>+</sup> and pads)
  - Allows for 100% fill factor and fine segmentation
- Prototypes produced in this study by FBK
- **Many thanks for providing the devices to R. Arcidiacono, N. Cartiglia, M. Ferrero, M. Mandurrino, V. Sola, M. Boscardin, G. Borghi, G. Paternoster, F. Ficarella, M. Centis Vignali, G.F. Dalla Betta, L. Pancheri**
- Thanks a lot to F. Miserocchi for the help with the CAEN setup

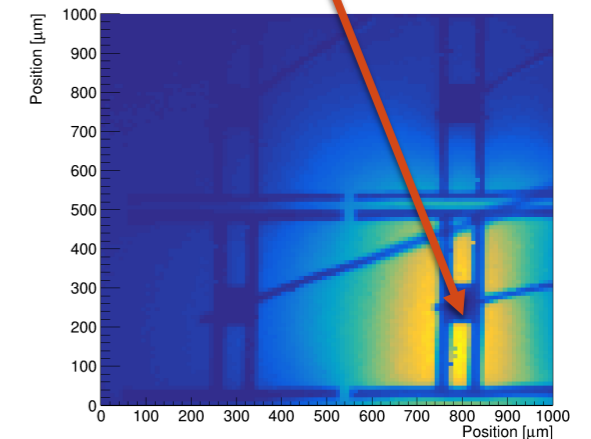
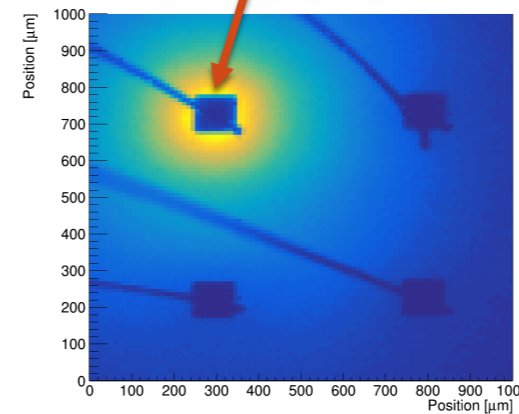
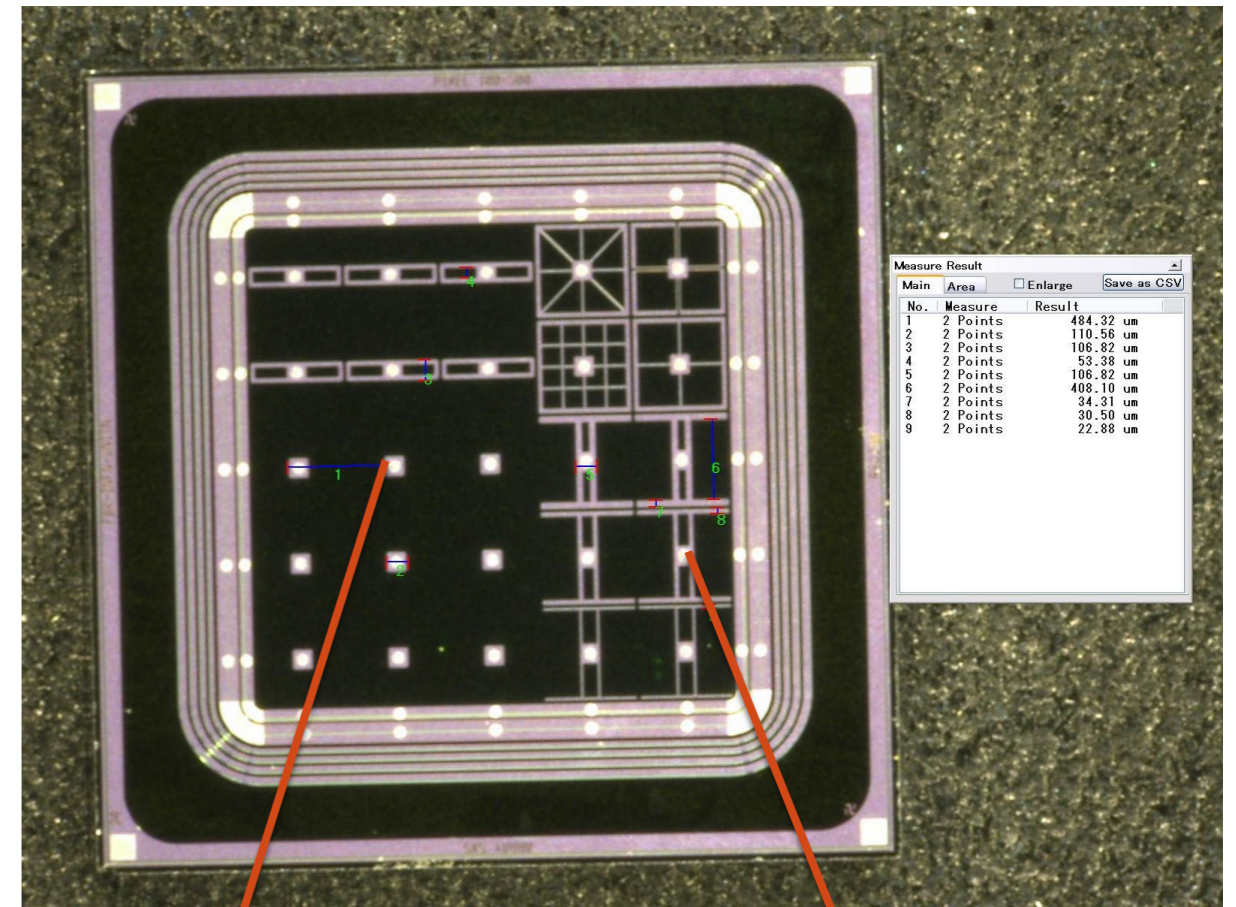
- **The response of the sensors can be tuned by modifying several parameters**
  - Pad distance
  - Resistivity of N<sup>+</sup> layer
  - Oxide thickness
  - Pad geometry and dimension



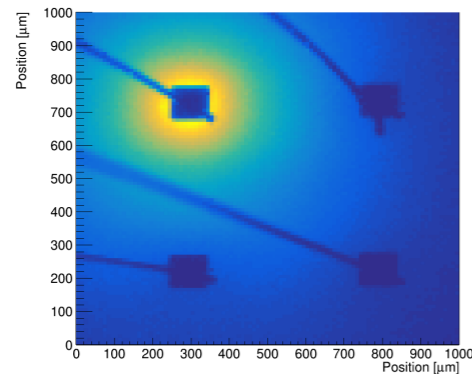
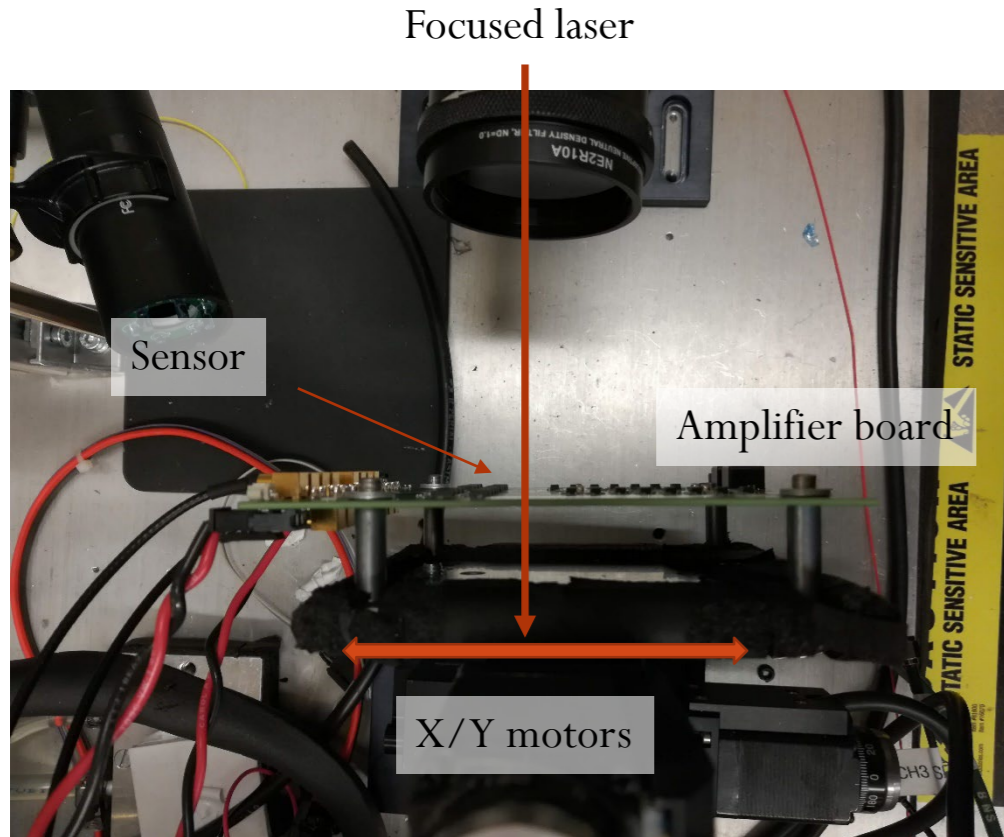
Prototype AC-LGAD from FBK, 500 μm pitch, 300 μm metal

# AC-LGAD geometry

- With AC metal it is possible to create non conventional geometries
  - Simple metal pattern on top, no underlying structures
  - **Allowing to optimize sensor metal shape for the specific application**
- Studies done on a **AC-LGADs** from FBK RSD2 production
  - Pad sensor featuring non conventional geometries, pitch of 500 $\mu\text{m}$
  - FBK RSD2 W13B 8-3 5X5 500  $\mu\text{m}$
  - Geometries: 100x100 $\mu\text{m}$  pads, microstrips, H-pads, cages. All have a 100x100 $\mu\text{m}$  “core” for wire bonding.
- Presented results
  - Capacitance characterization of different pads
  - 2D and 1D response profile (laser TCT)
  - Comparison of waveforms from different pads
  - Rudimentary position reconstruction and Jitter calculation



# Sensor testing – Laser TCT setup

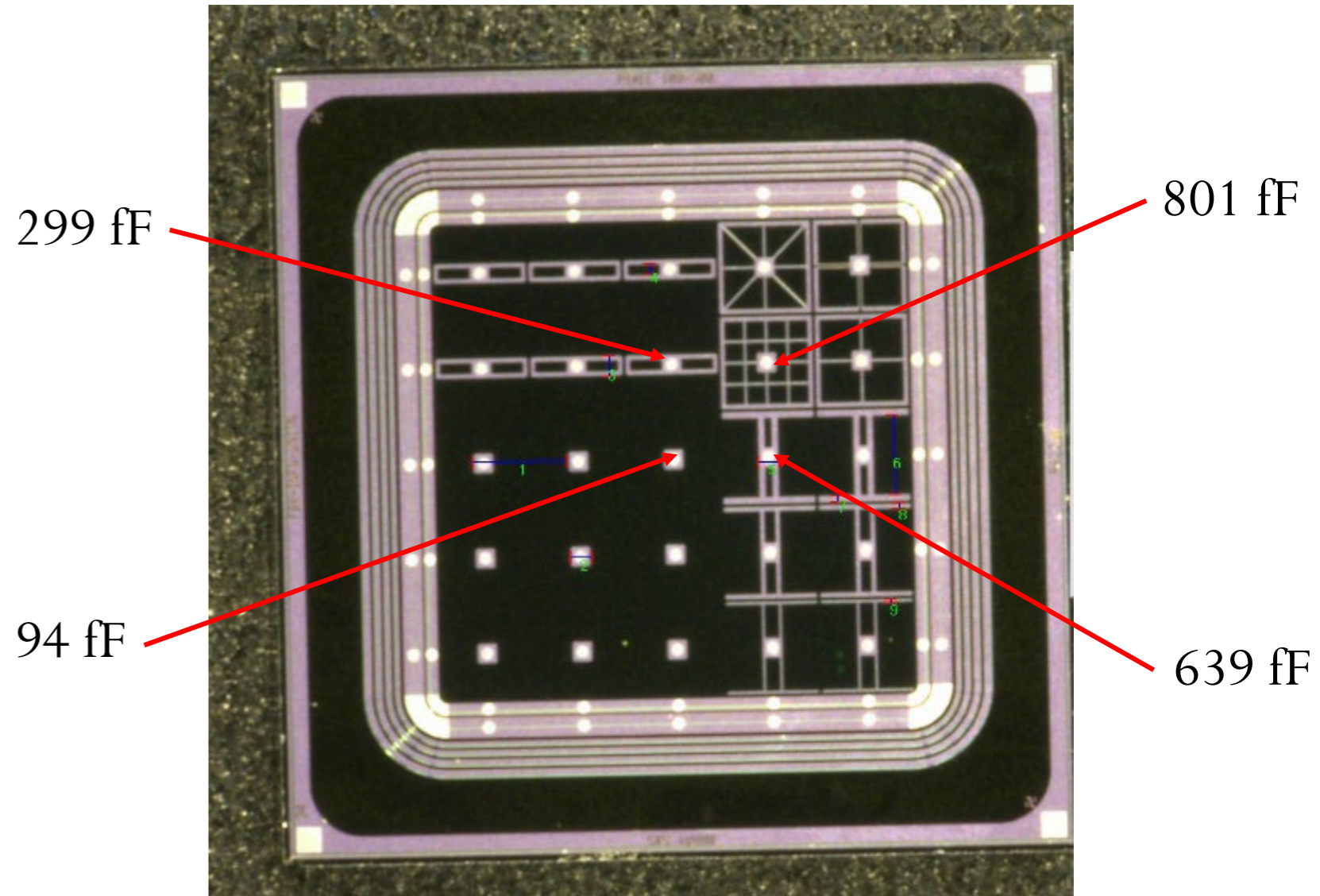
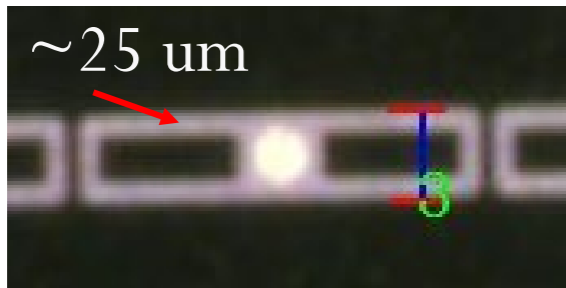


- Sensors are mounted on a multi-channel analog amplifier board with bandwidth  $\sim 1$  GHz
  - Response is readout by a fast oscilloscope (2 GHz/20 Gs) or a 16ch CAEN digitizer
- **IR laser (1064 nm)** mimics charge deposit of a MIP
  - Focused beam spot width of  $< 20$   $\mu\text{m}$
  - Metal structures of the sensors are not transparent to IR so no response can be seen when laser is on top of metal
- Amplifier board is mounted on X/Y moving stages
  - **Charge injection as a function of position**
- Laser scan of a 100x100 $\mu\text{m}$  pad: example 2D Pulse maximum (Pmax) map vs X/Y position



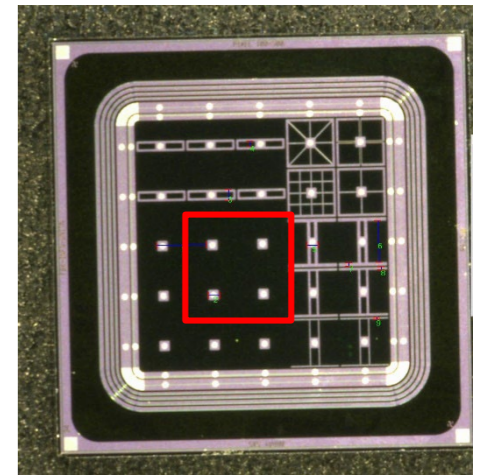
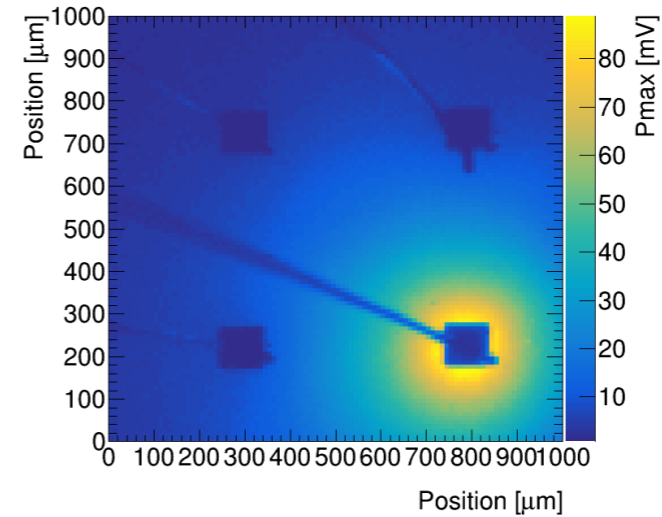
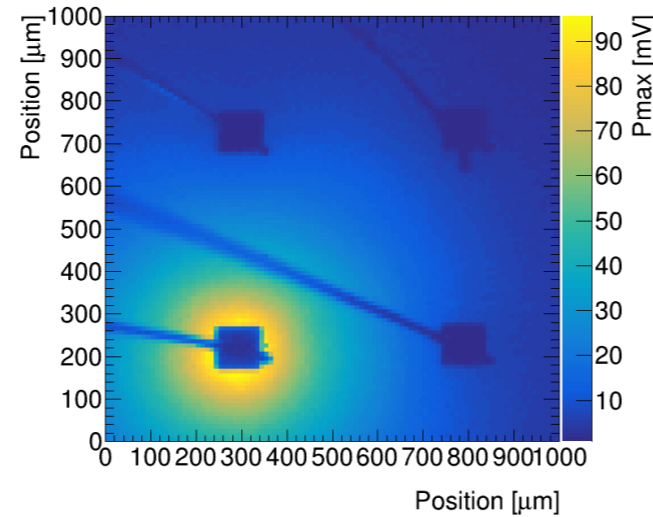
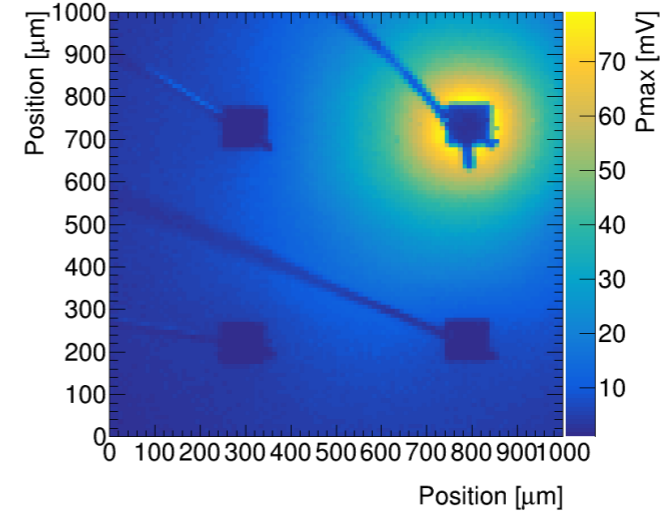
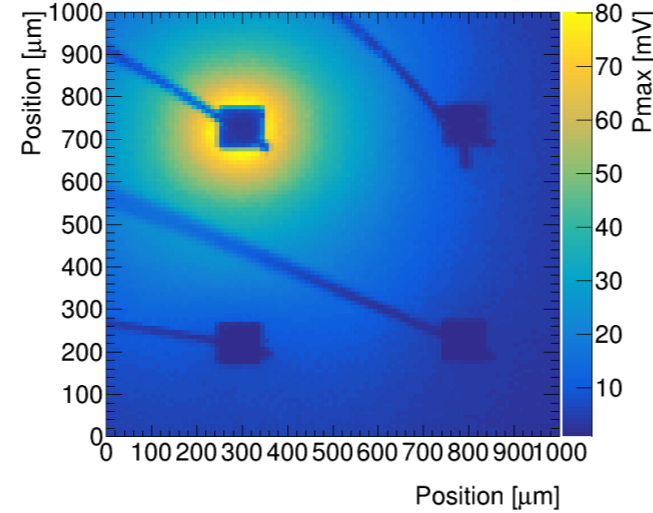
# AC-LGAD AC-capacitances

- Measurement of the pad capacitance for each different type of pad
  - HV from the backside, N+ and guard ring grounded, capacimeter connected to top metal
  - The rest of the metal pads around it are floating
- Pad's capacitance scales with amount of metal coverage on top as expected
- **Opening in the metal does reduce the capacitance**
  - Micro-strips are  $\sim 100 \times 500$   $\mu\text{m}$  but the capacitance is not 5 times the one of  $100 \times 100$   $\mu\text{m}$  pads
  - Capacitance is only  $\sim 3$  times
  - Scales with the (2x)  $175 \times 50$   $\mu\text{m}$  area of the opening
  - H-pad measured has thicker arms so the capacitance is significantly higher



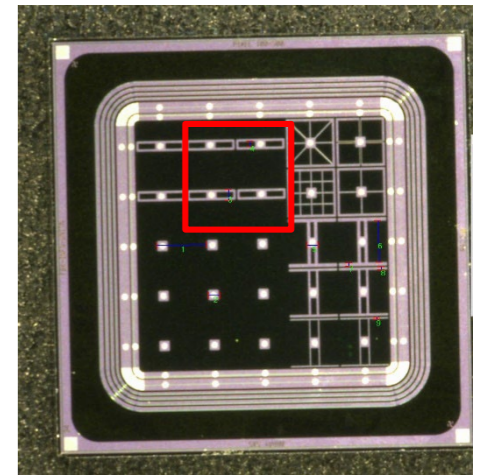
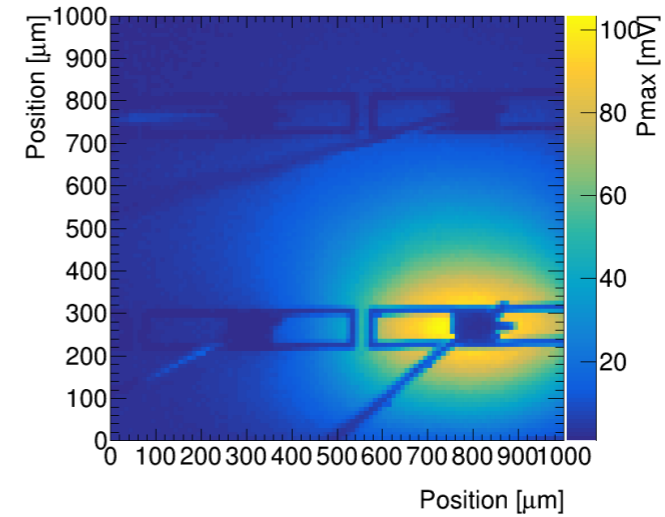
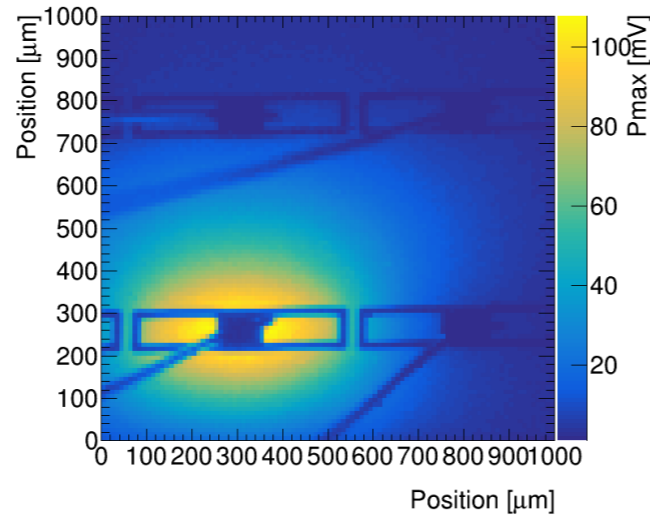
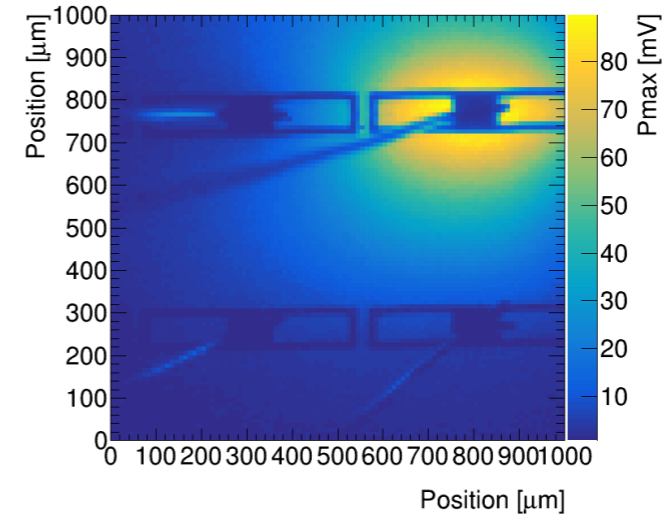
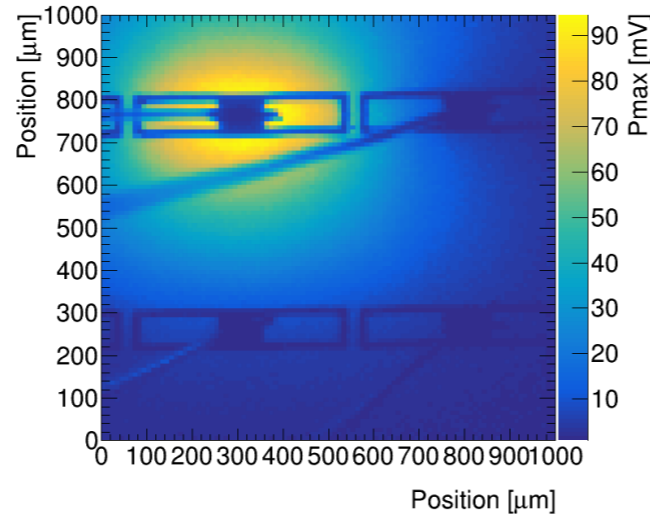
# AC-LGAD 100x100 $\mu\text{m}$ pads

- Pro
  - Homogeneous in X-Y
  - Likely good reconstruction in the region in between pads
  - Small input capacitance
- Cons
  - Smaller signal



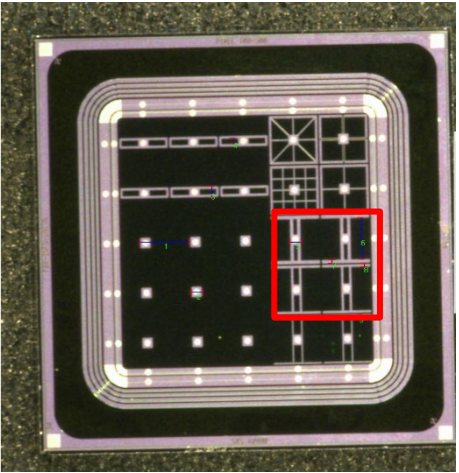
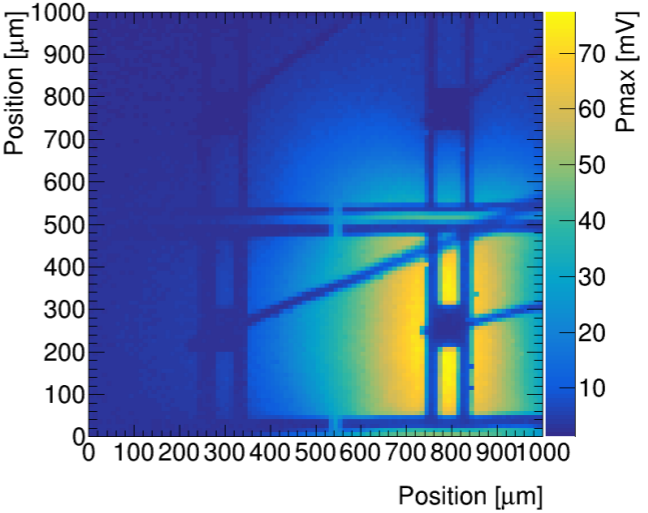
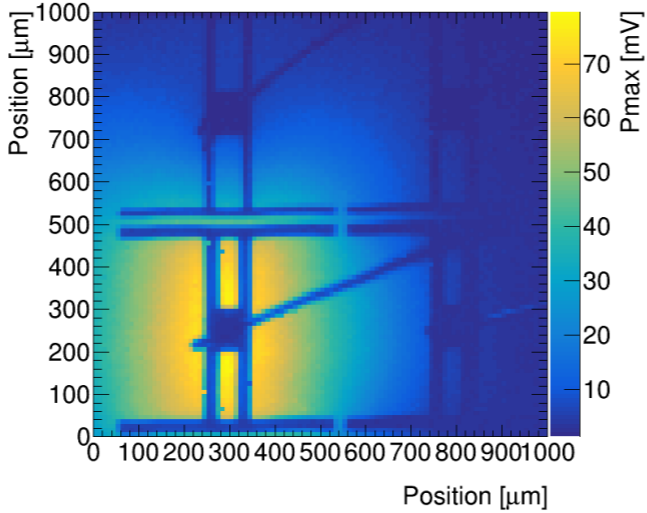
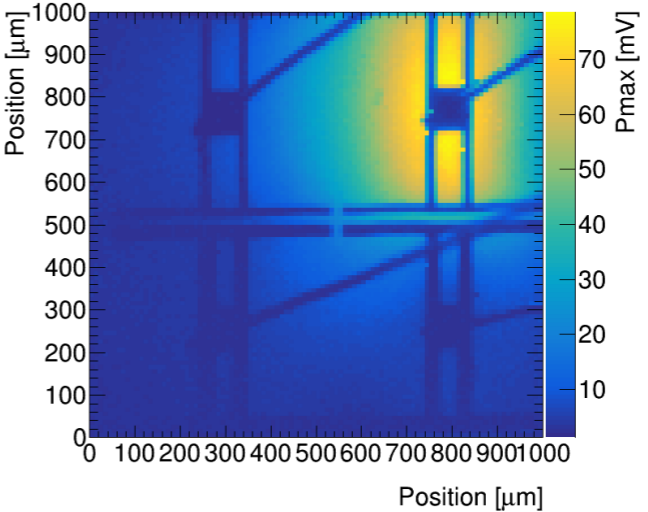
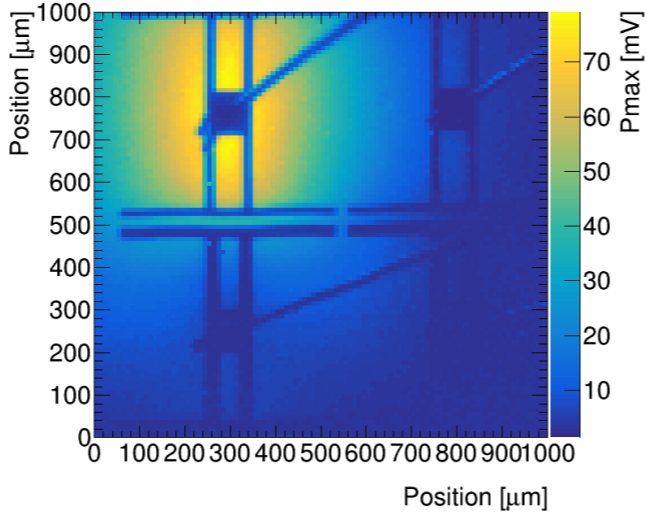
# AC-LGAD 100x500 $\mu\text{m}$ micro-strips

- Pro
  - Bigger signal
  - Better position resolution in Y
- Cons
  - Increased input capacitance
  - Worse position resolution in X



# AC-LGAD 500x500 $\mu\text{m}$ H-pads

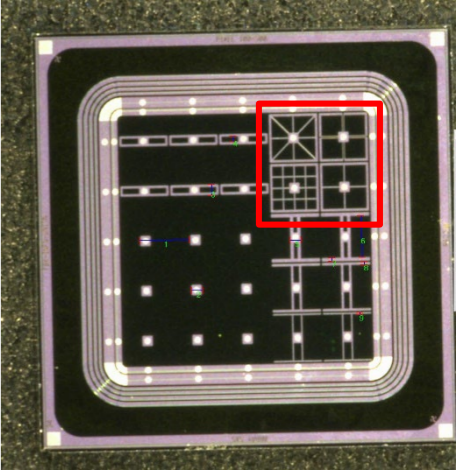
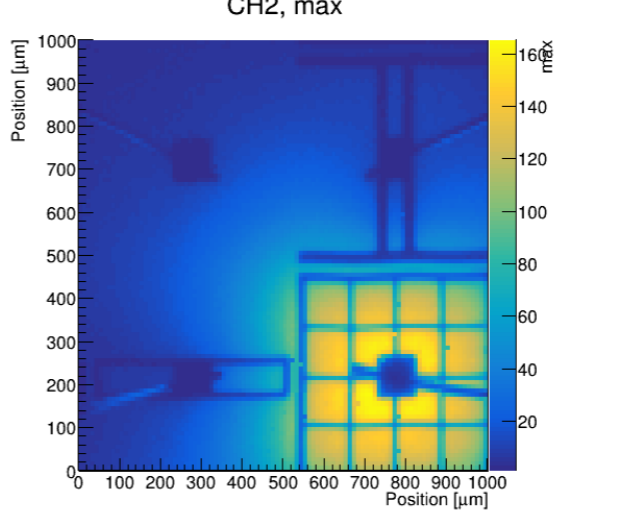
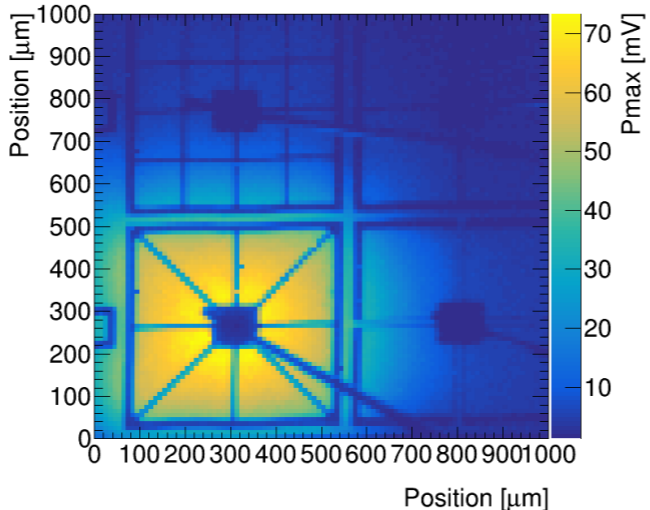
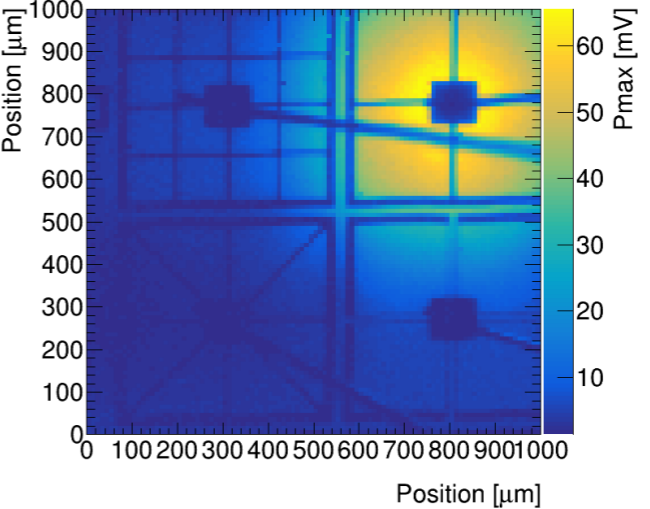
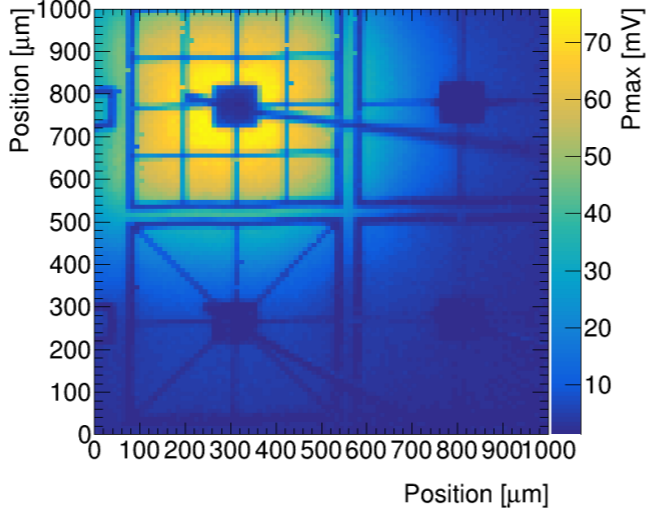
- Pro
  - Bigger signal
  - Better position resolution in X
- Cons
  - Increased input capacitance
  - Worse position resolution in Y



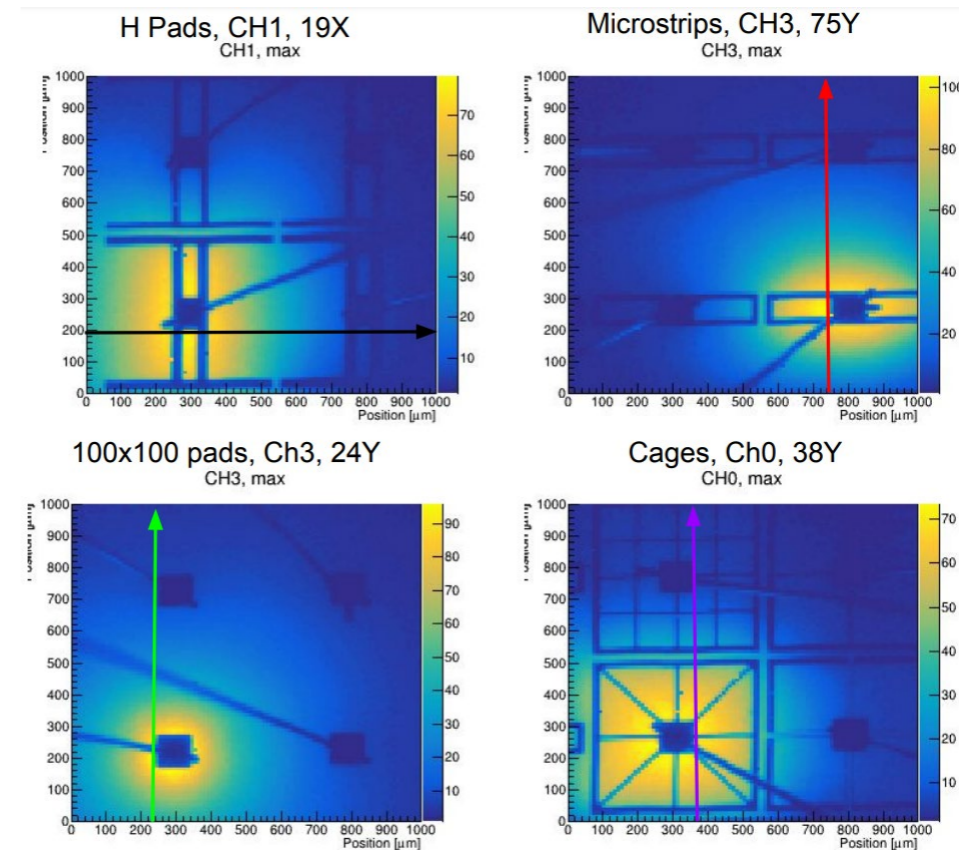
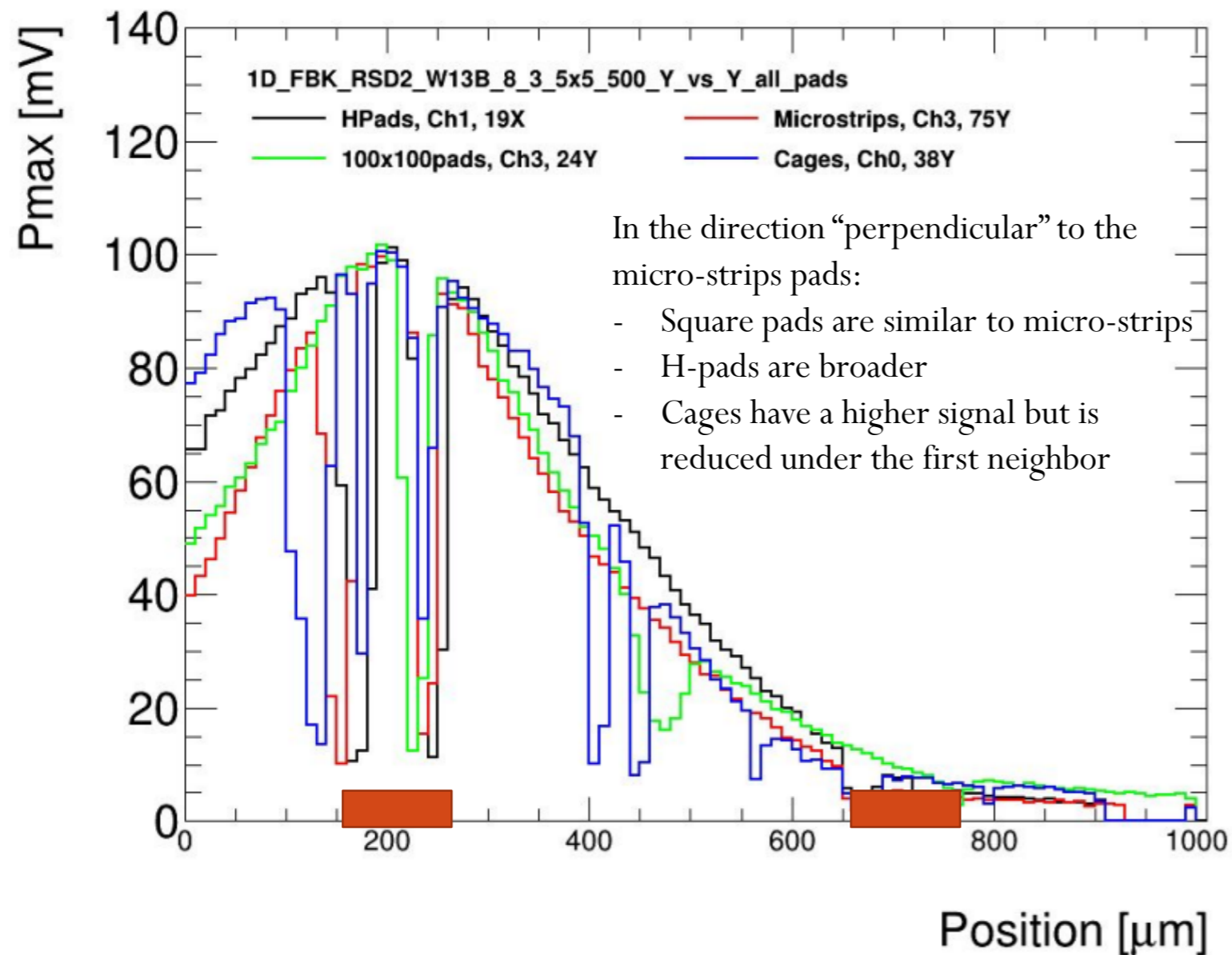


# AC-LGAD 500x500 $\mu\text{m}$ cages

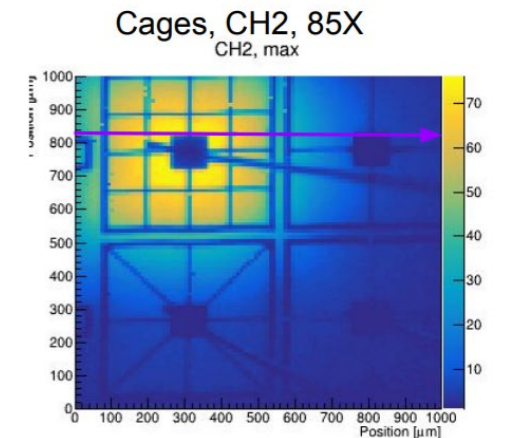
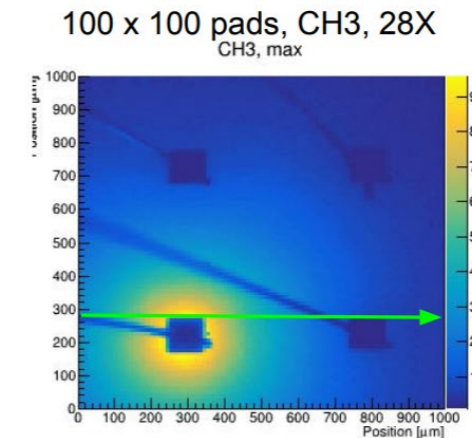
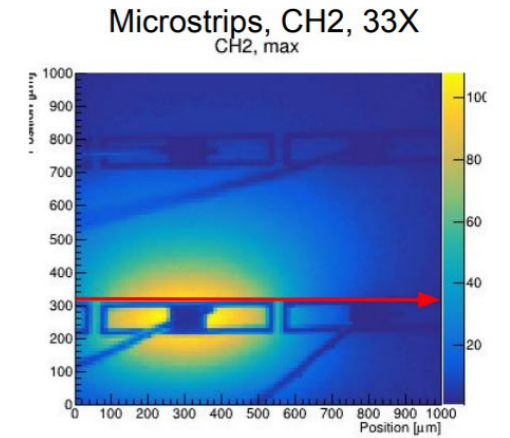
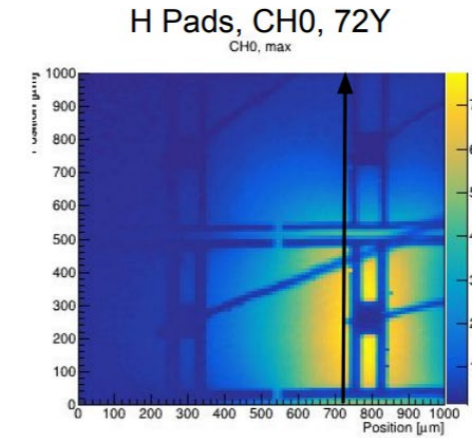
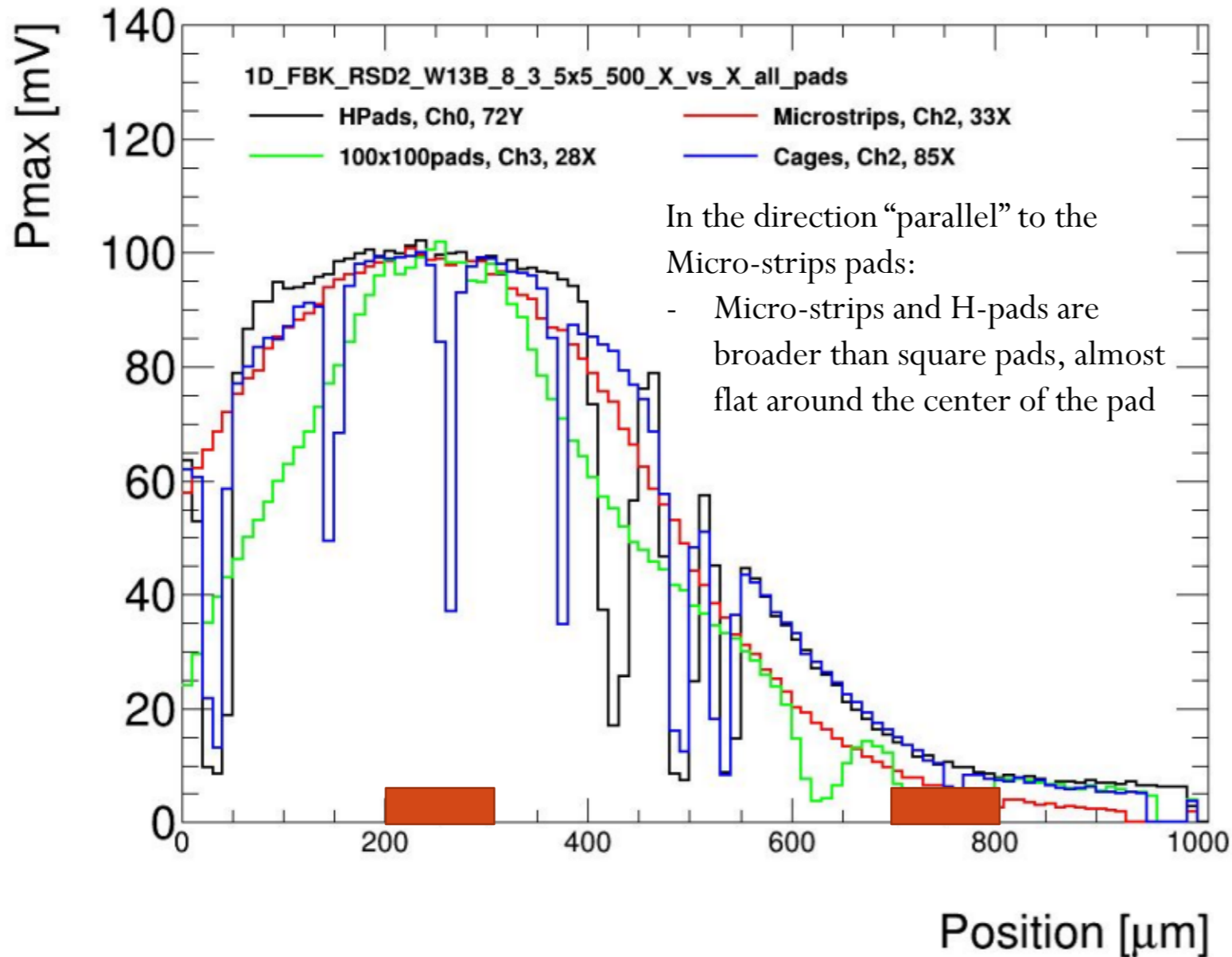
- Pro
  - Bigger signal
- Cons
  - Increased input capacitance
  - Unclear position resolution



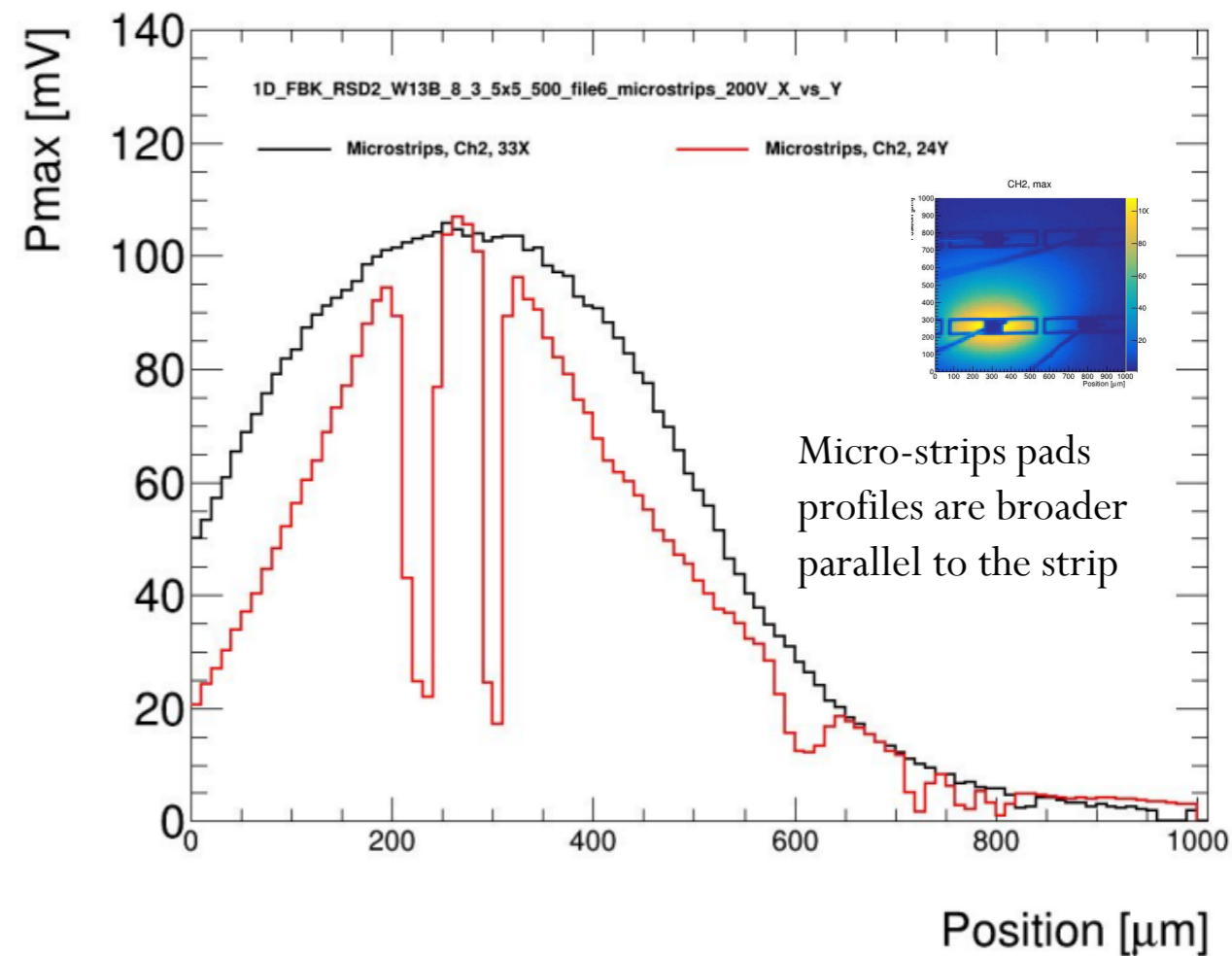
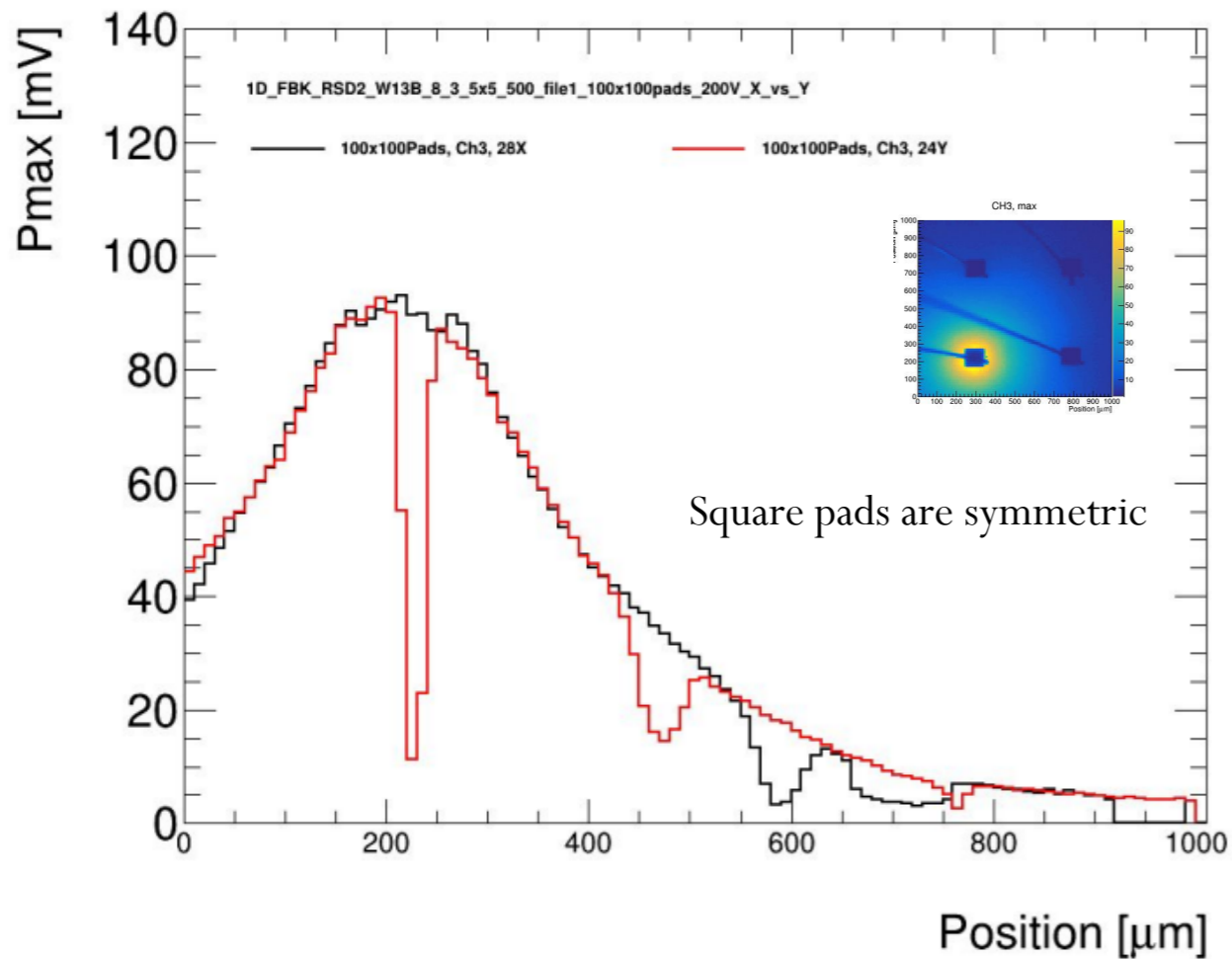
# Comparison of 1D profiles, all pads - Y



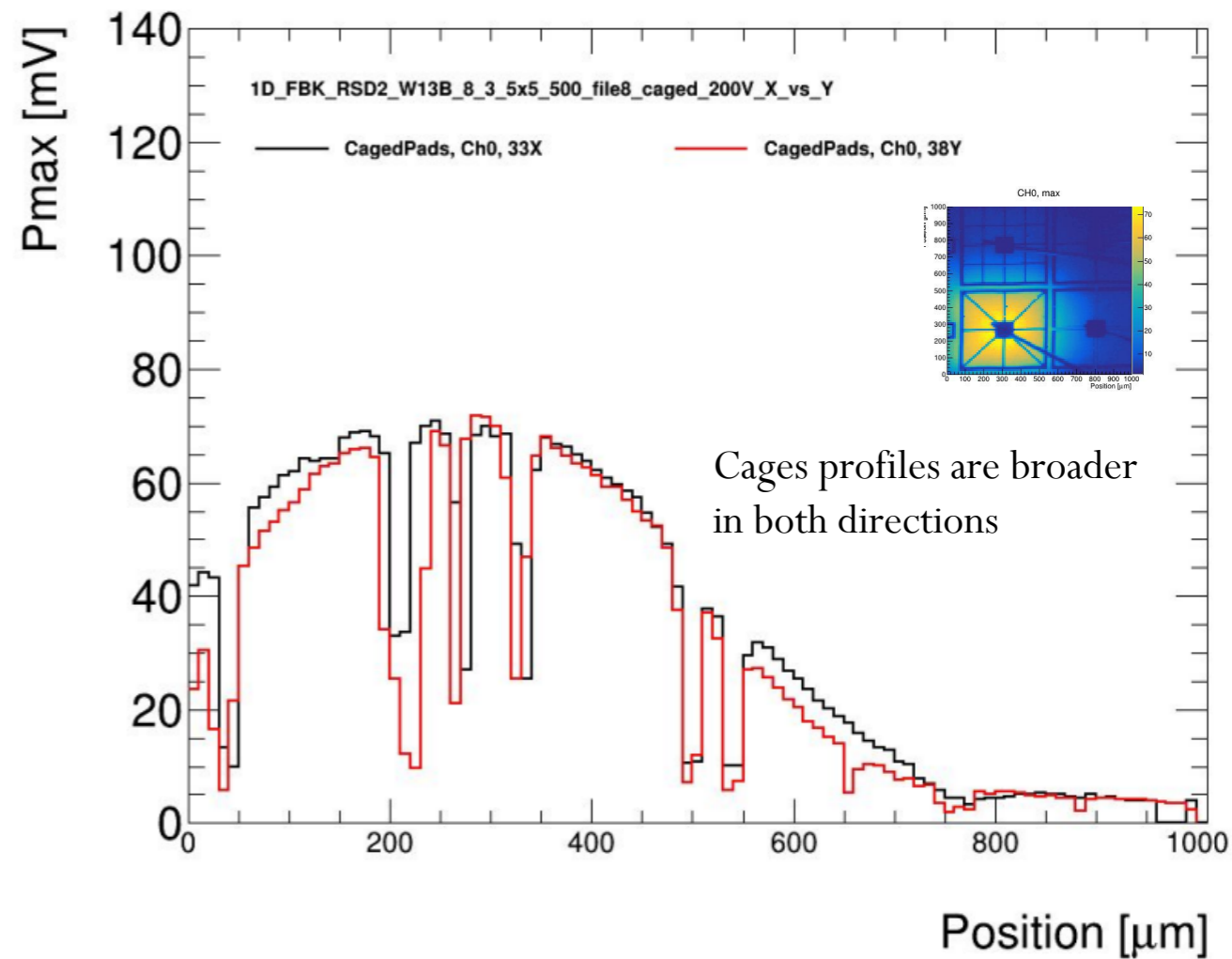
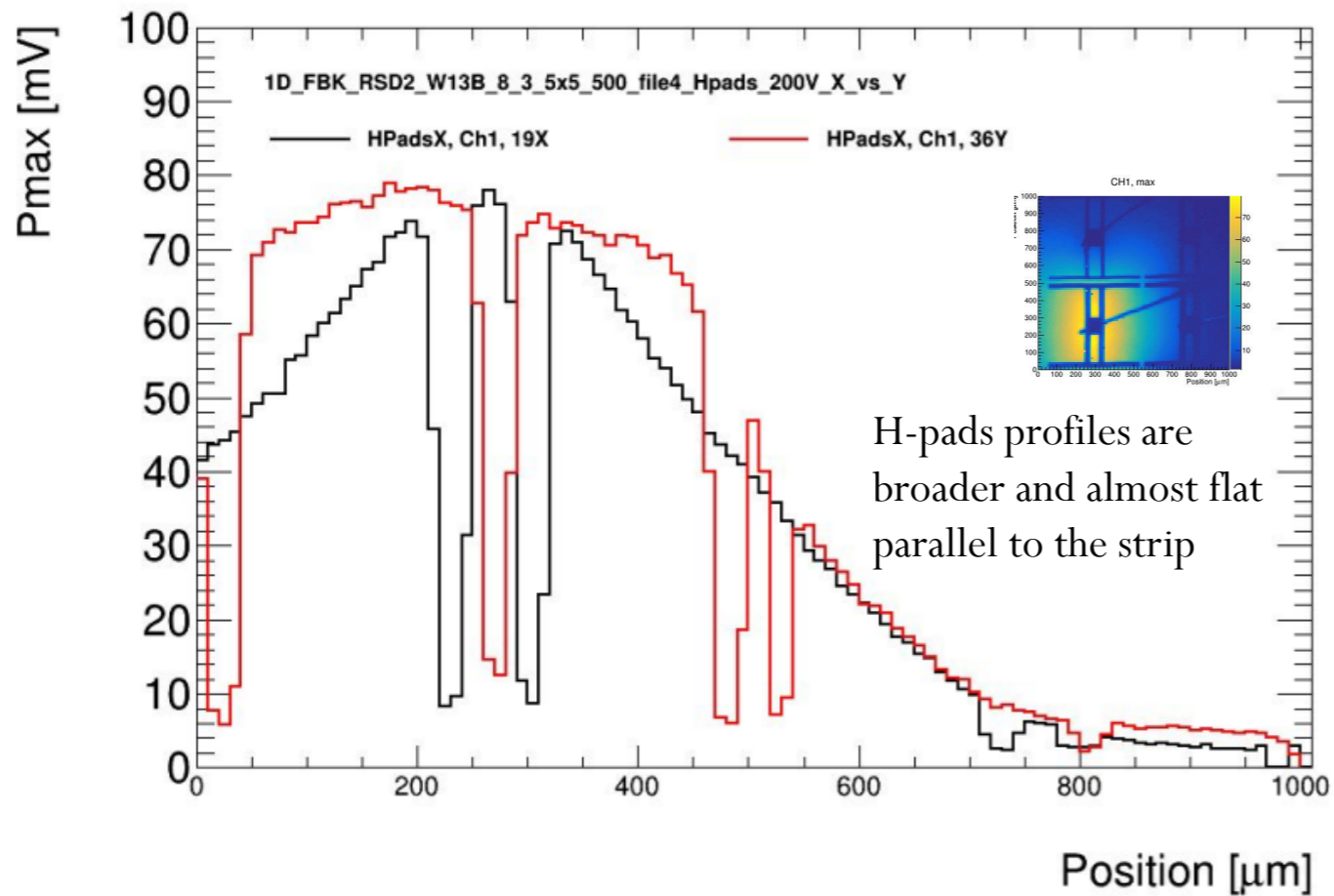
# Comparison of 1D profiles, all pads - X



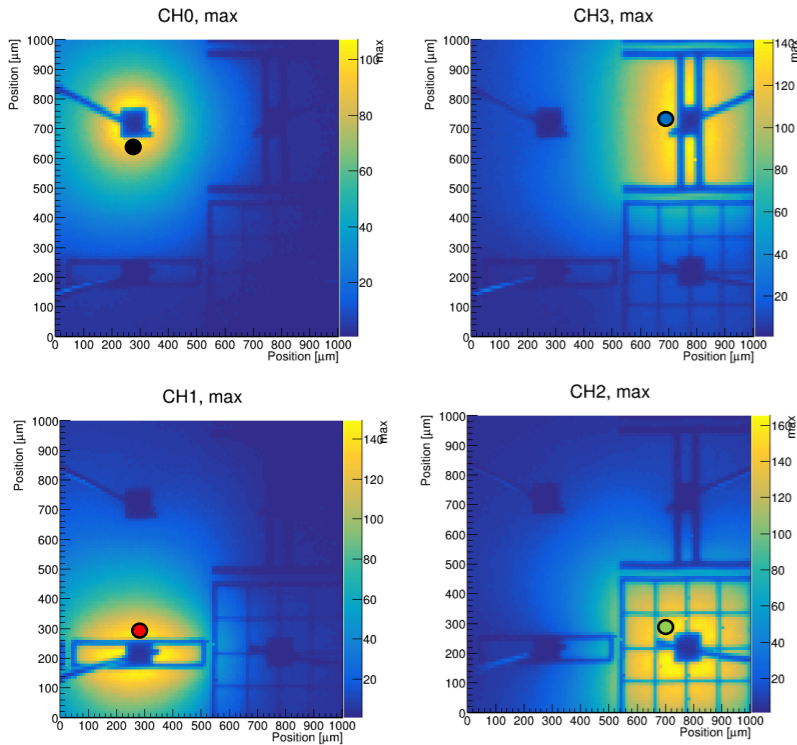
# Comparison of 1D profiles, all pads – X vs Y



# Comparison of 1D profiles, all pads – X vs Y



# Signal from all types of pads

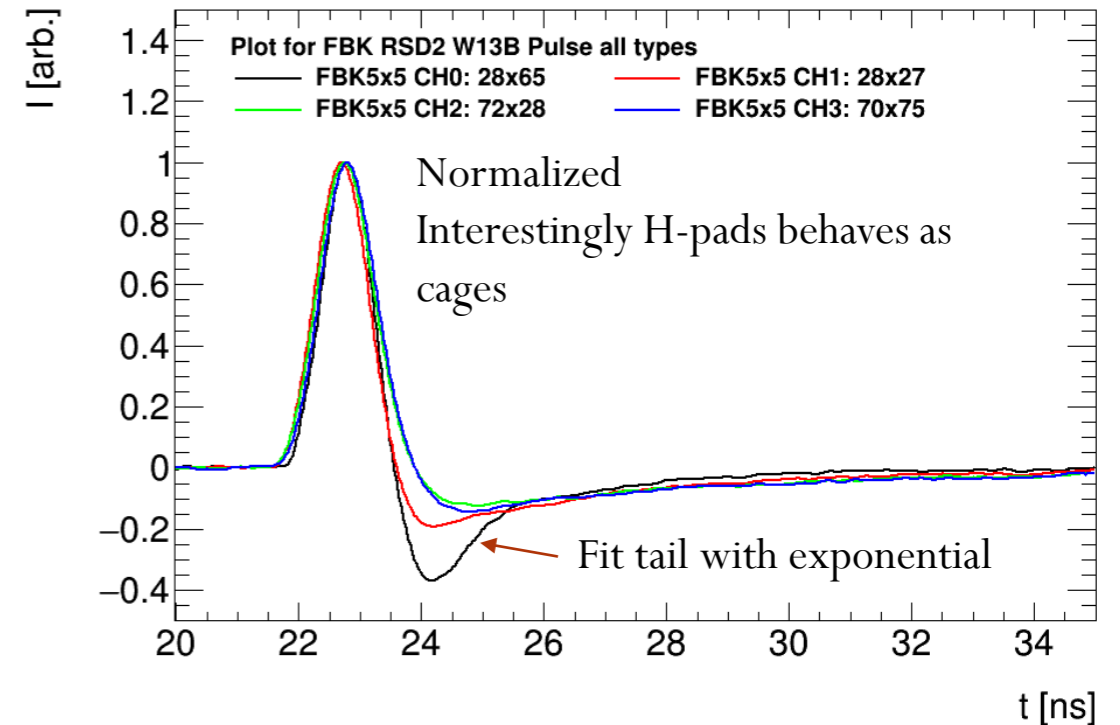
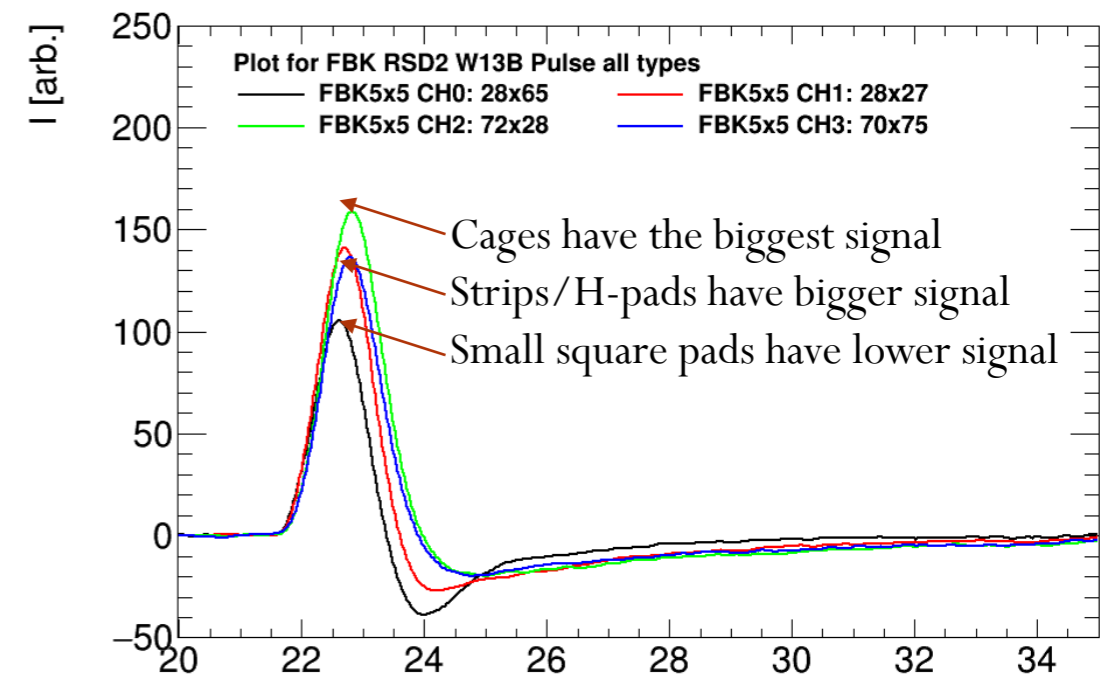


Positive pole of the signal is the same for all pad types

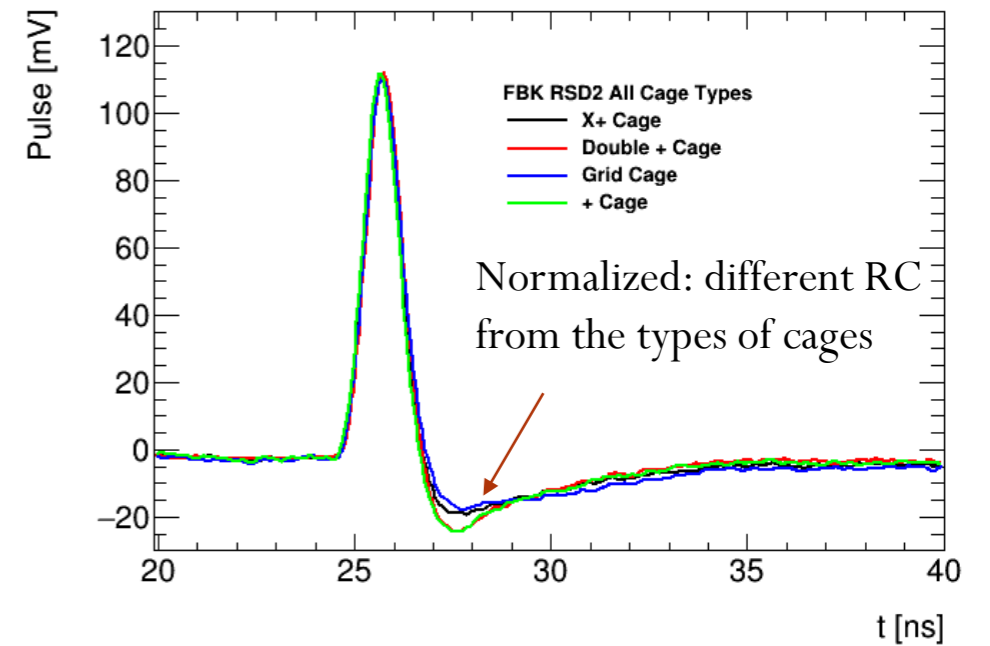
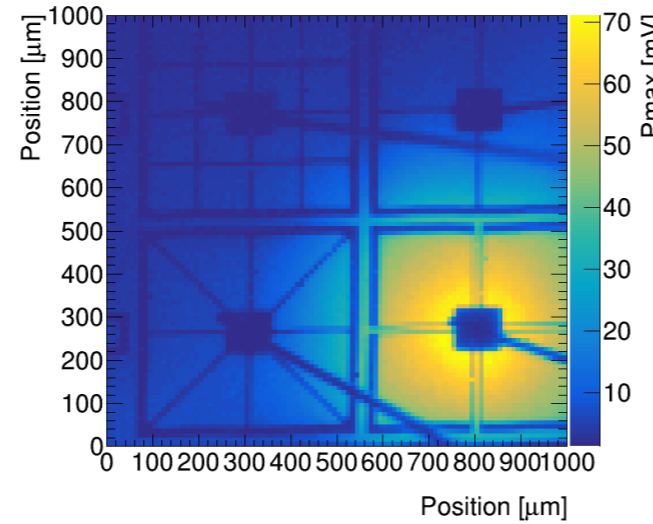
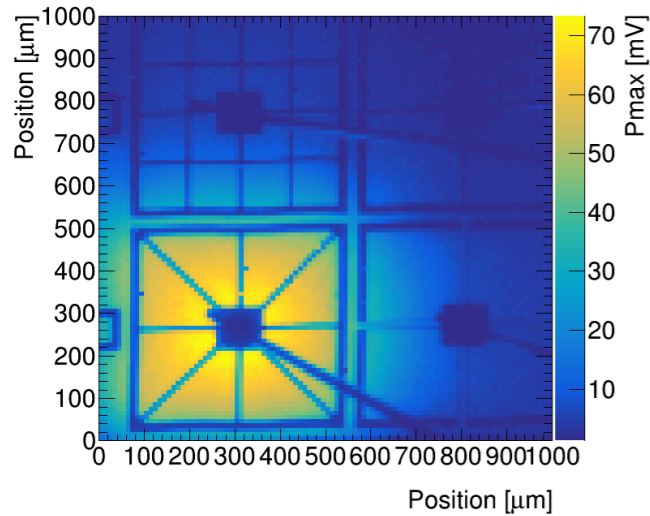
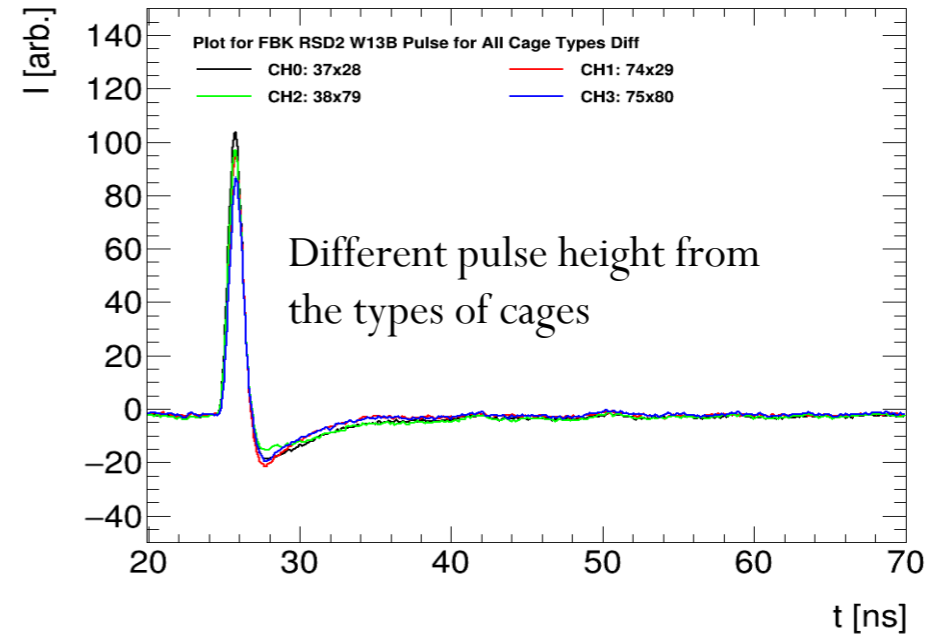
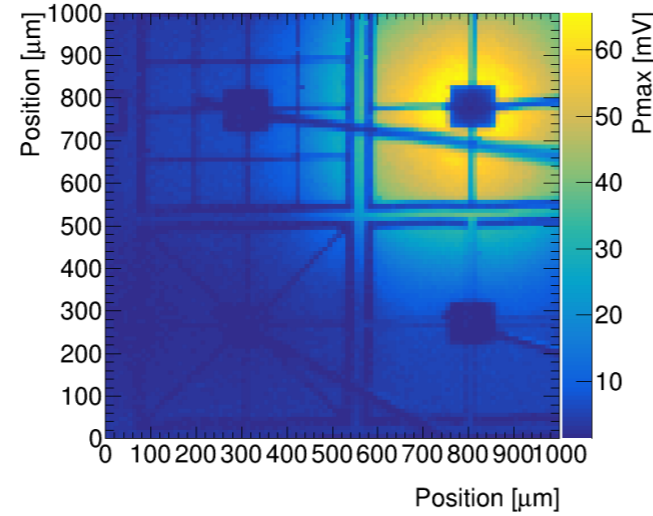
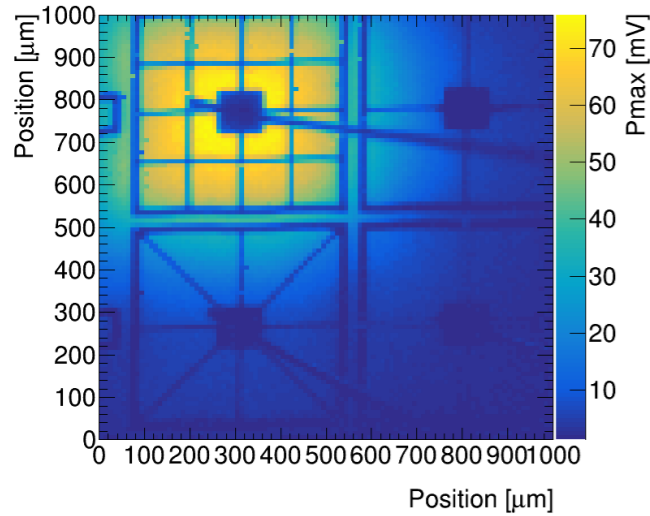
However they have different RC constant and return to baseline

Unclear why it doesn't scale directly with the capacitance of the pad

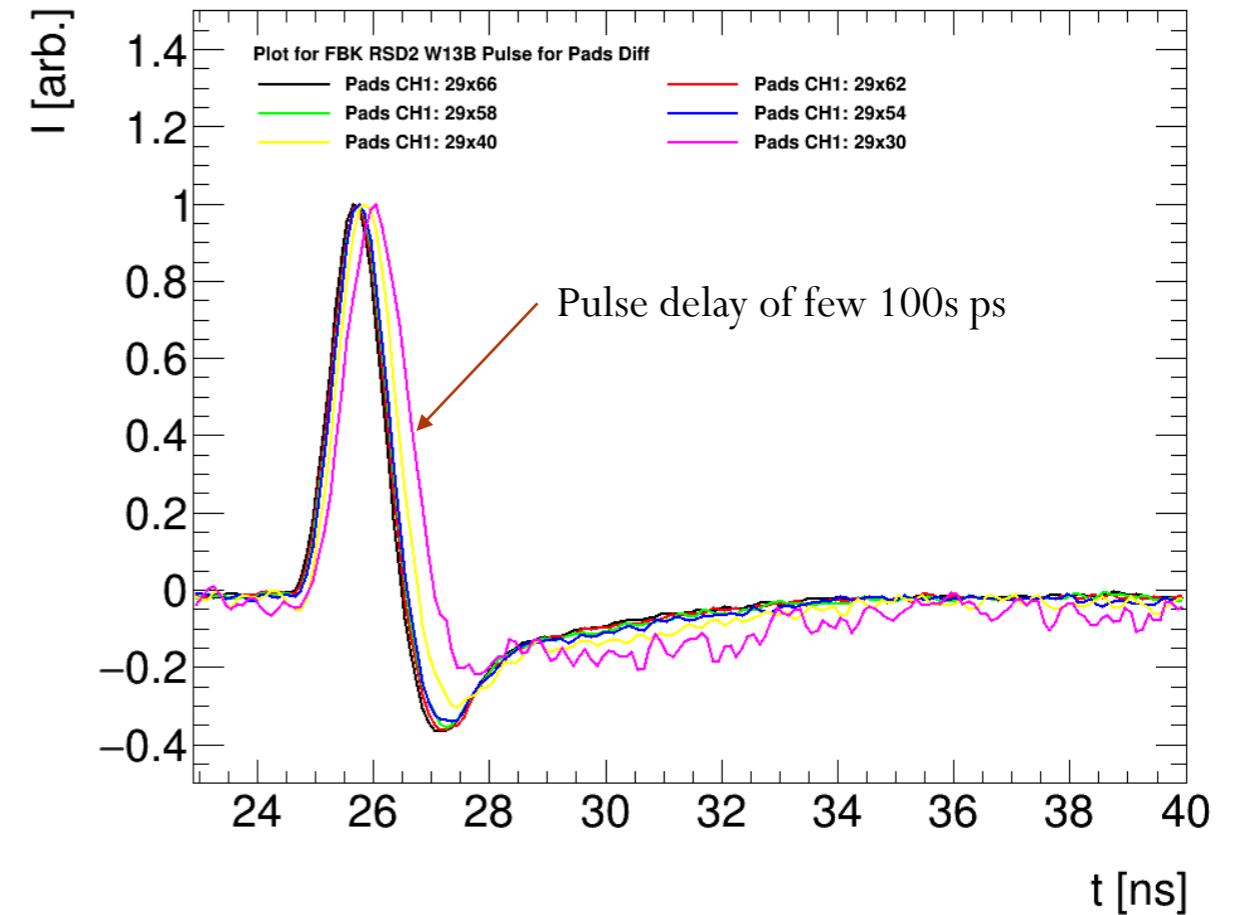
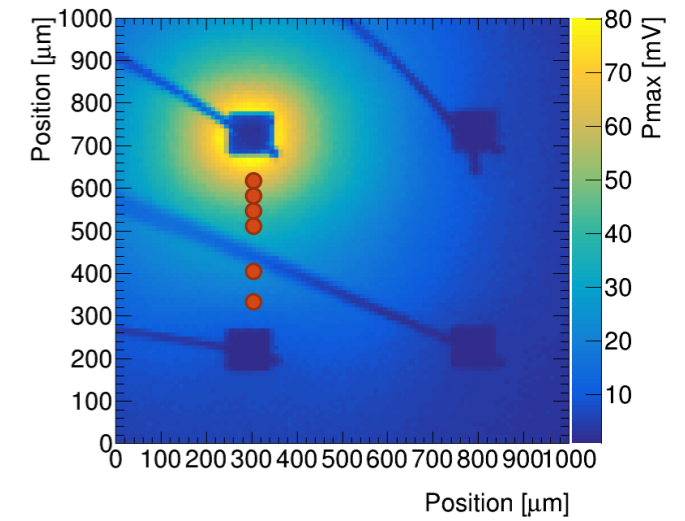
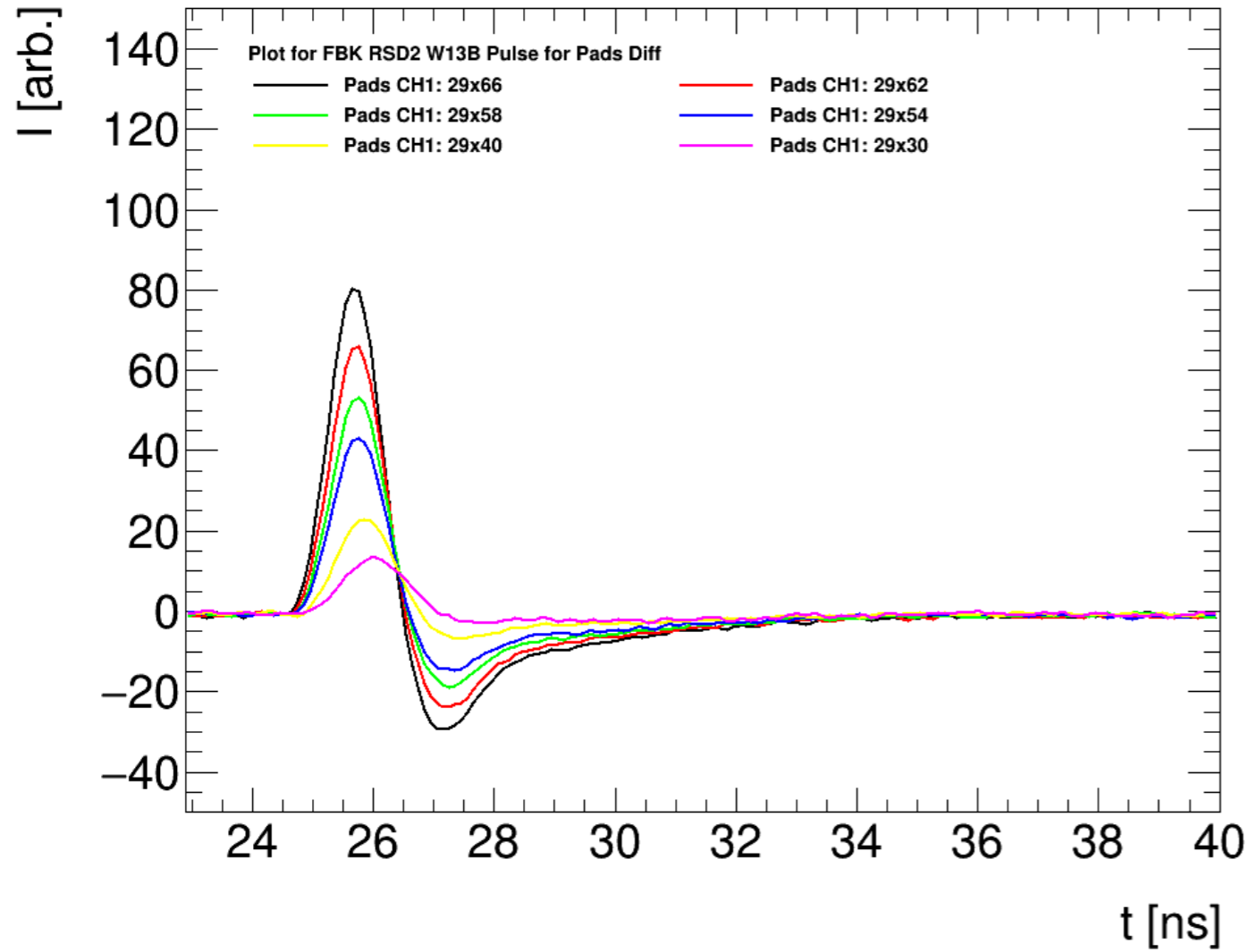
Pad type	Exponential RC constant	Capacitance
Square pads	0.61	94 fF
Micro-strips	0.28	299 fF
H-pads	0.19	639 fF
Cage	0.19	801 fF



# Signal from different types of “cages”

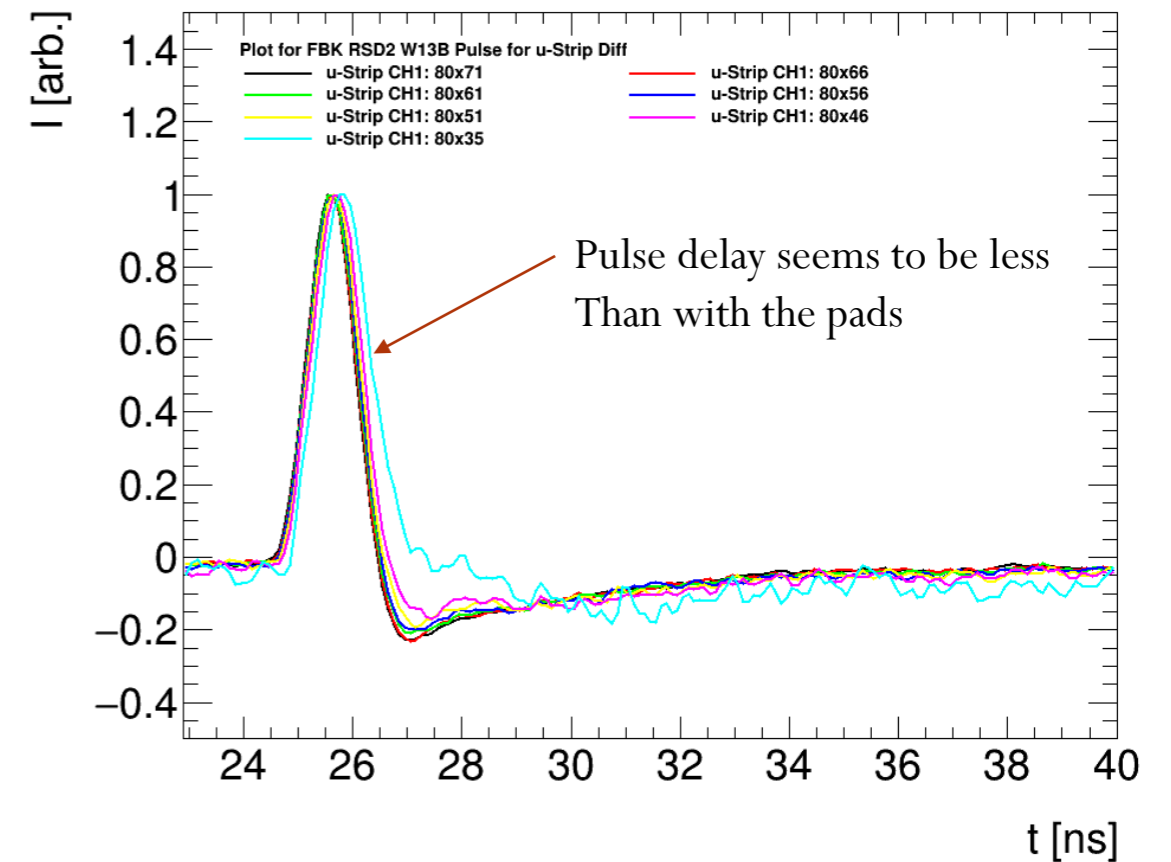
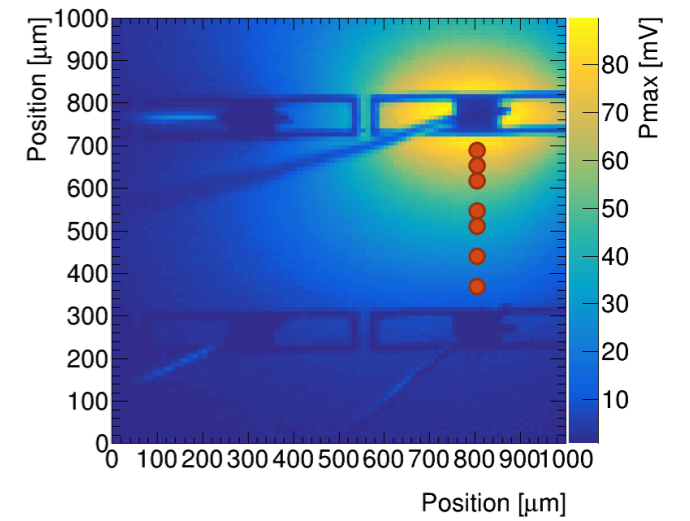
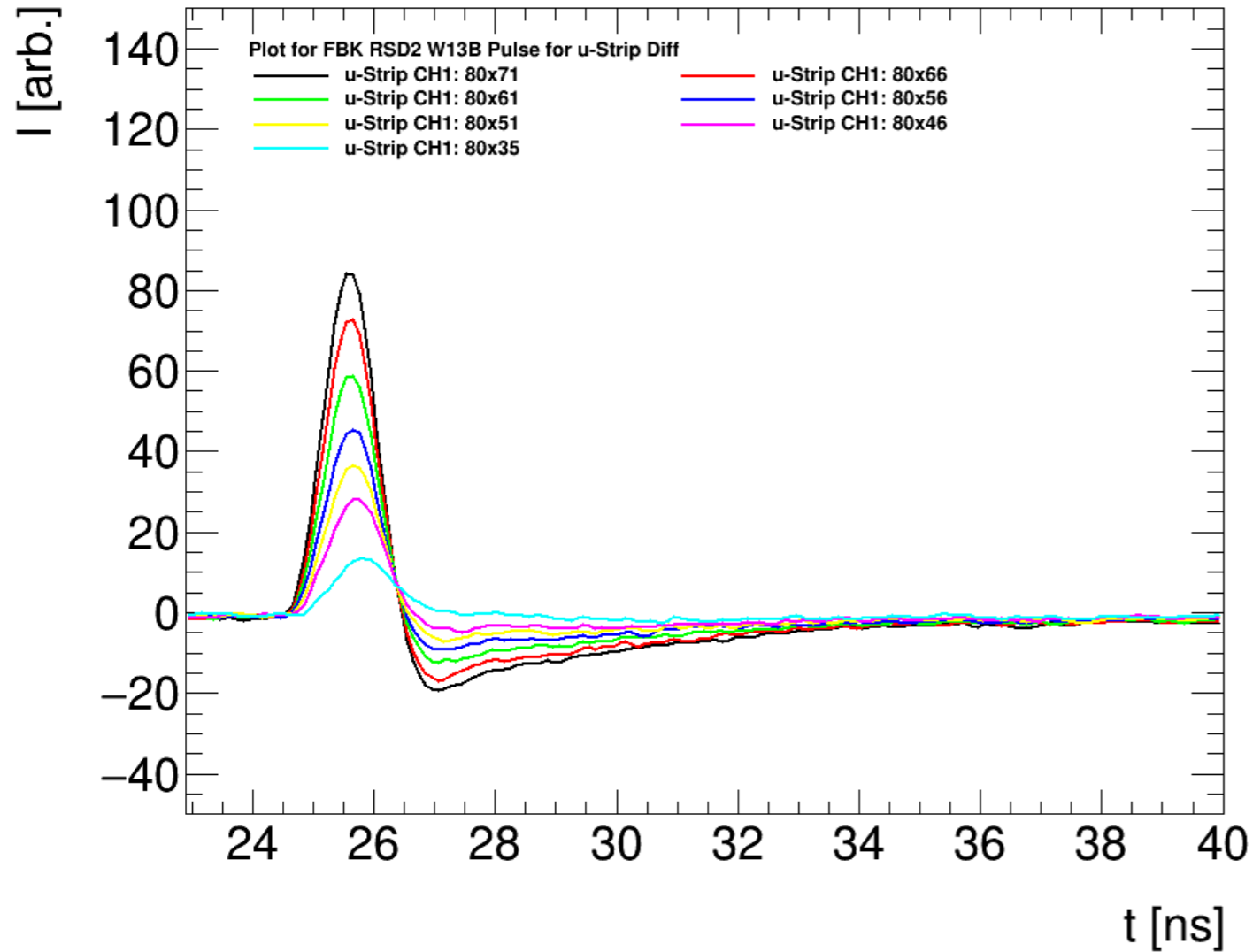


# AC-LGAD 100x100 um pads pulses

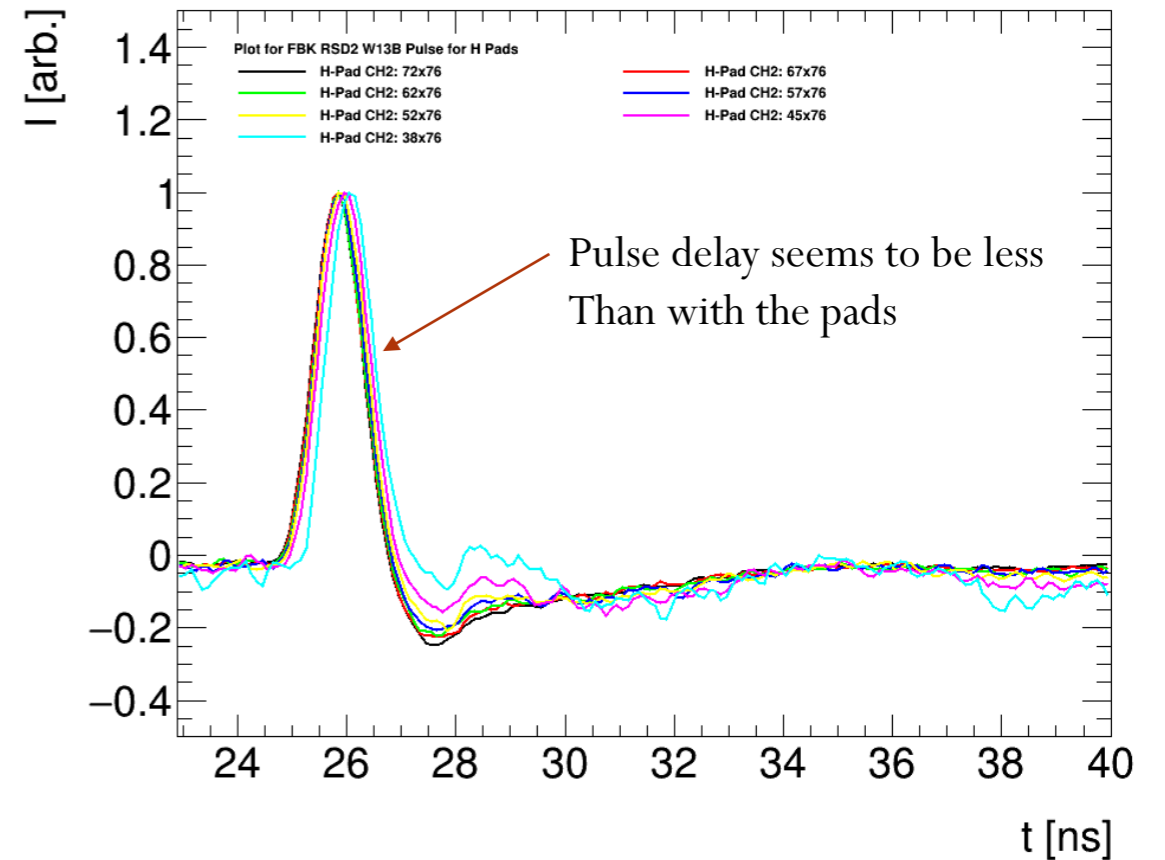
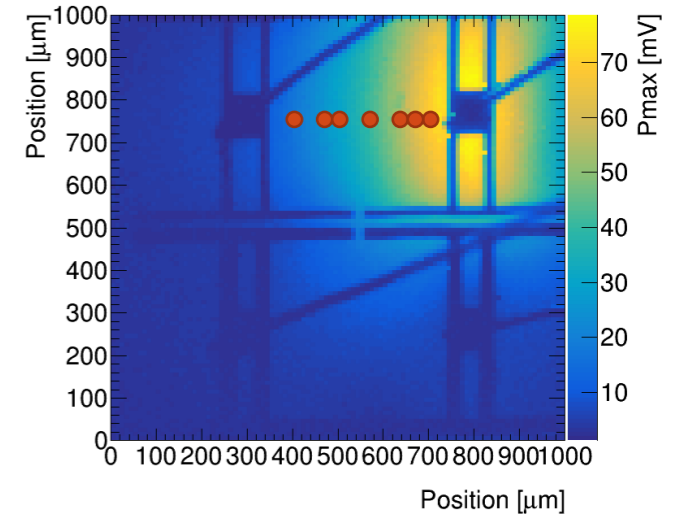
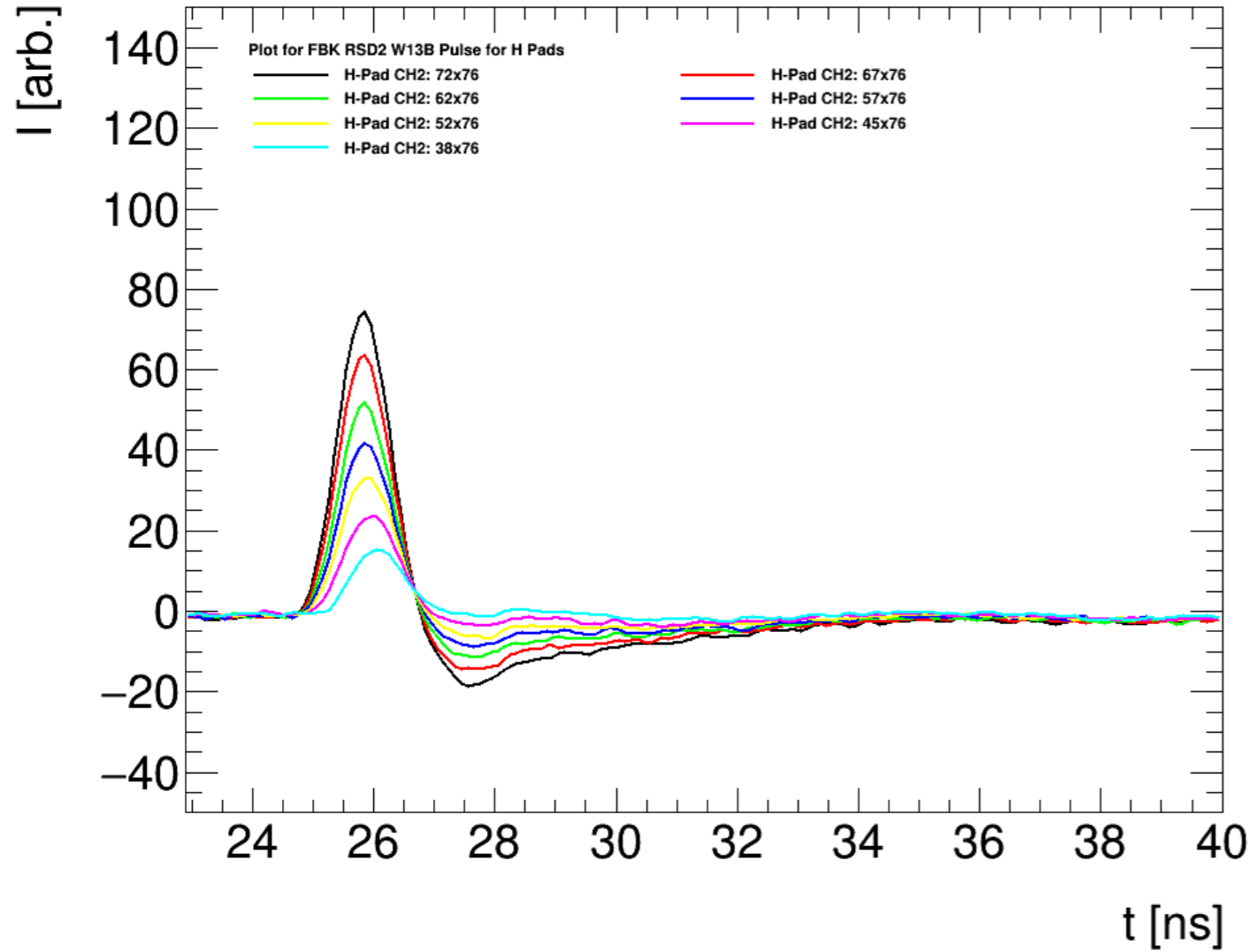




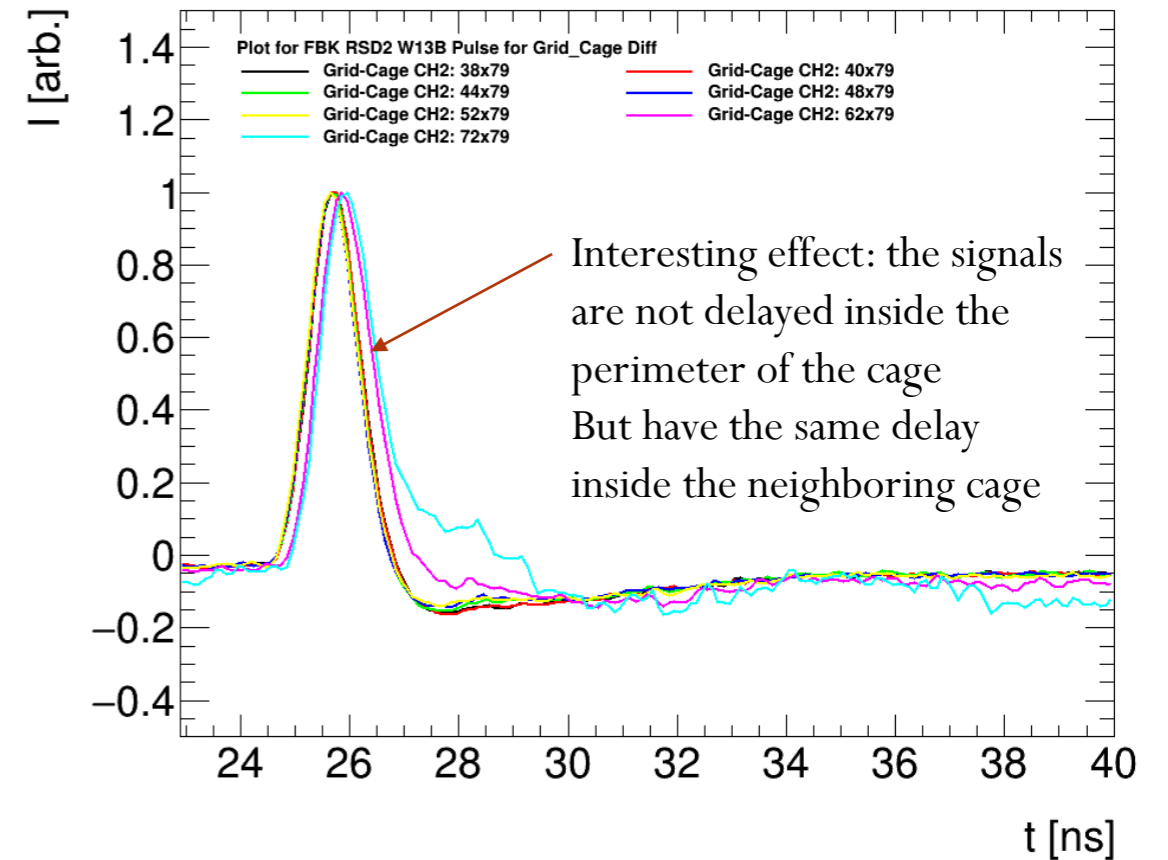
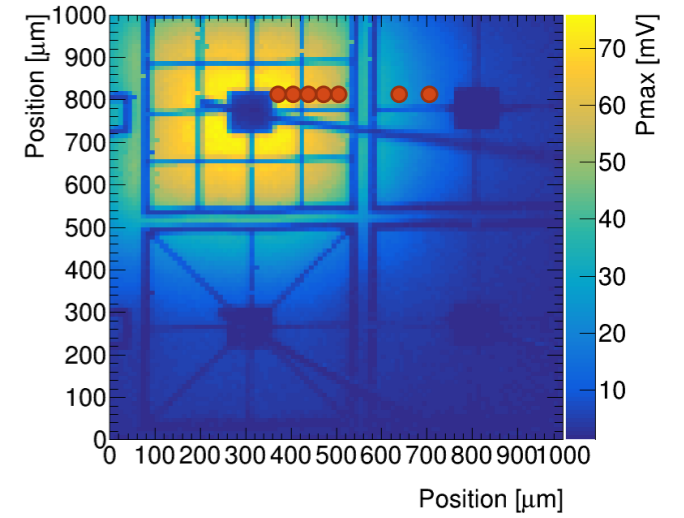
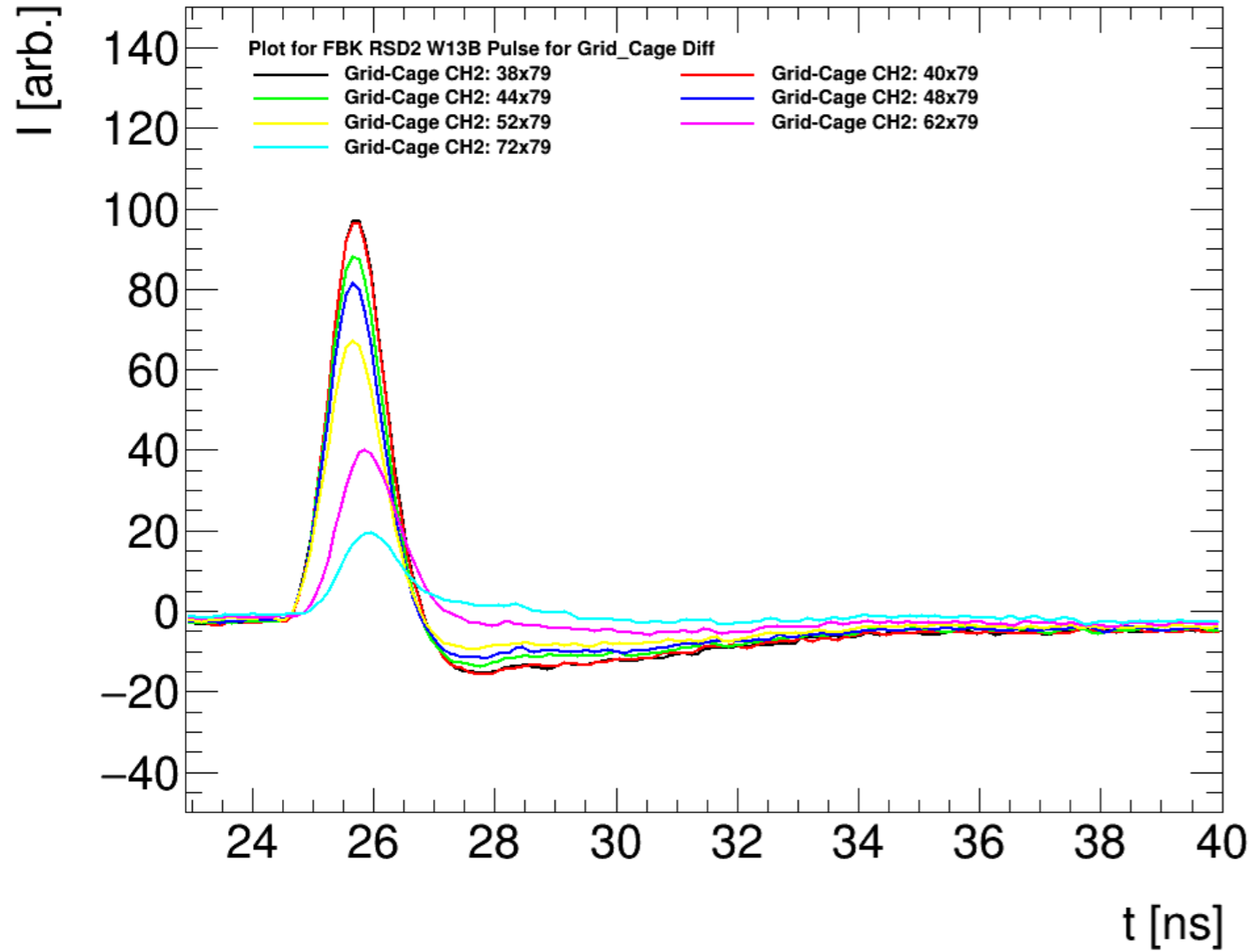
# AC-LGAD micro strips pulses



# AC-LGAD H pads pulses

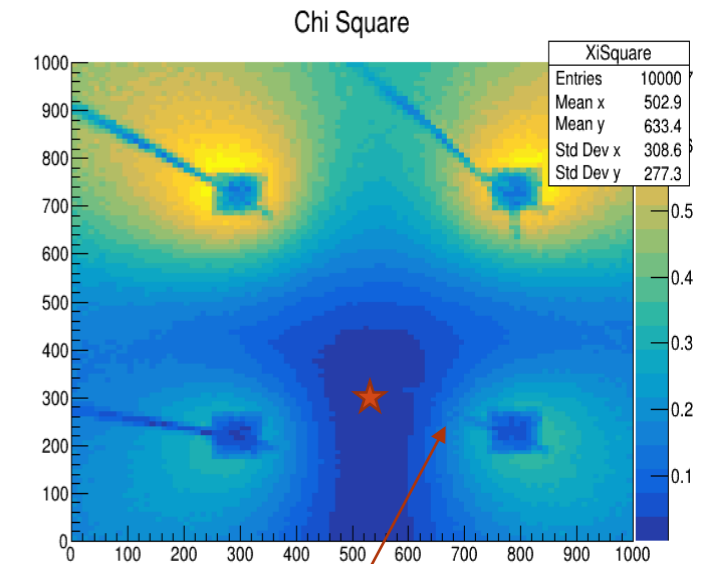
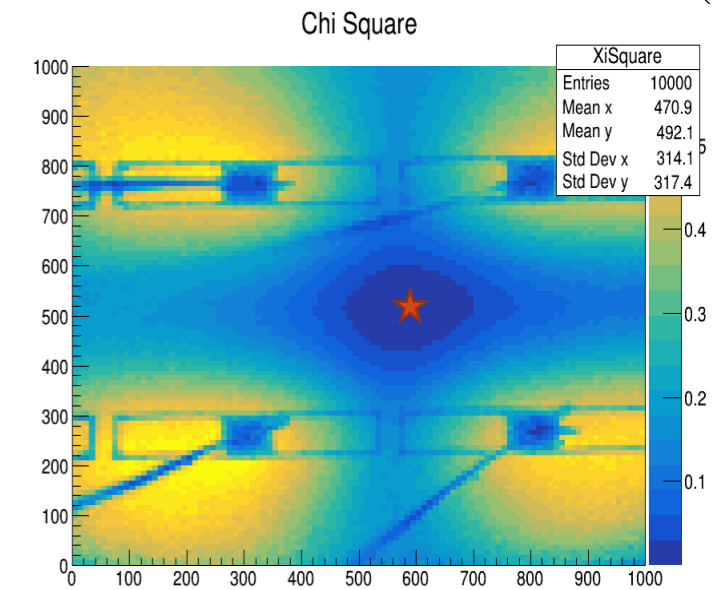


# AC-LGAD cages pulses



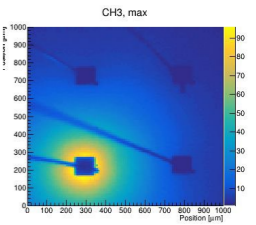
# Position reconstruction technique

- Position reconstruction is made by generating a reference file on the detector itself
  - Fine scan of the area averaging waveforms in each position using the TCT laser (using 2GHz scope)
  - From this reference file a fraction map is calculated for each of the 4 channels
- Then several single events are taken for each of the test positions
  - The position of each event is calculated by doing a  $\chi^2$  of the fractions in the event and the fraction maps from the average scan (using a 16ch CAEN digitizer based on DRS4)
  - The minimum  $\chi^2$  is taken as the reconstructed position (for now limited to the fine scan binning of  $\sim 10\mu\text{m}$ , so anything under  $5\mu\text{m}$  of precision is not fully accurate)
- **Reconstruction not based on master formula or charge imbalance** since it's not trivial to model these geometries
- Jitter is evaluated on the sigma of a Gaussian fit of the distribution of CFD 50% timestamps with the trigger signal
  - The timestamp is calculated using 4 channels weighted with the  $P_{\text{max}}^2$
  - Jitter seems to be higher than expected, might be because of the low bandwidth of the CAEN digitizer
  - Caveat: the time delay is not taken into account, to have a correct timestamp it needs to be considered. If the position resolution is high the effect should be small.



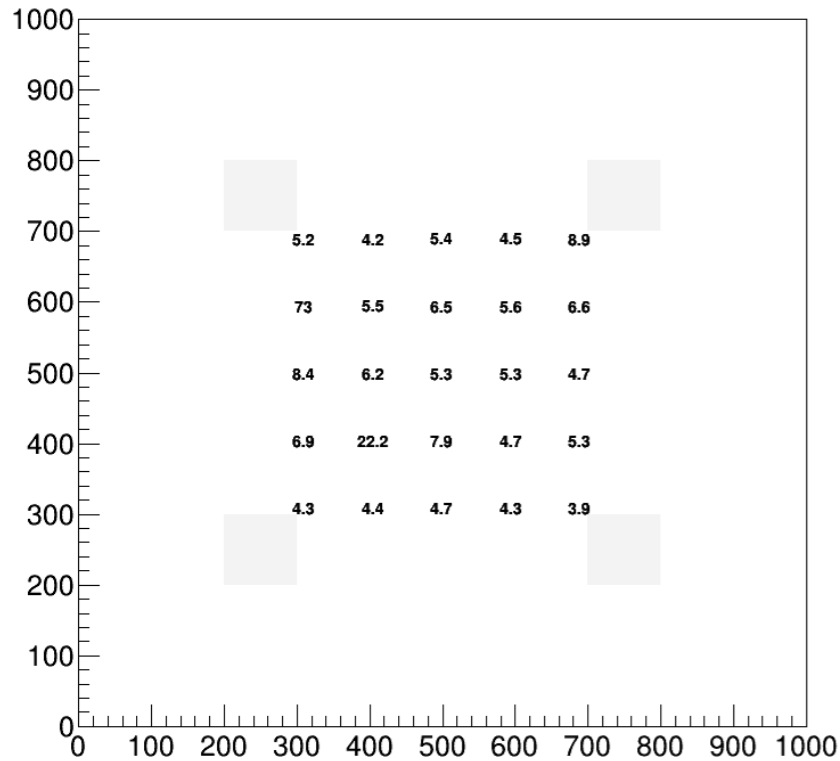
Note: some position are close to the wire bond so the reconstruction might fail

# Reconstructed position resolution – small pads

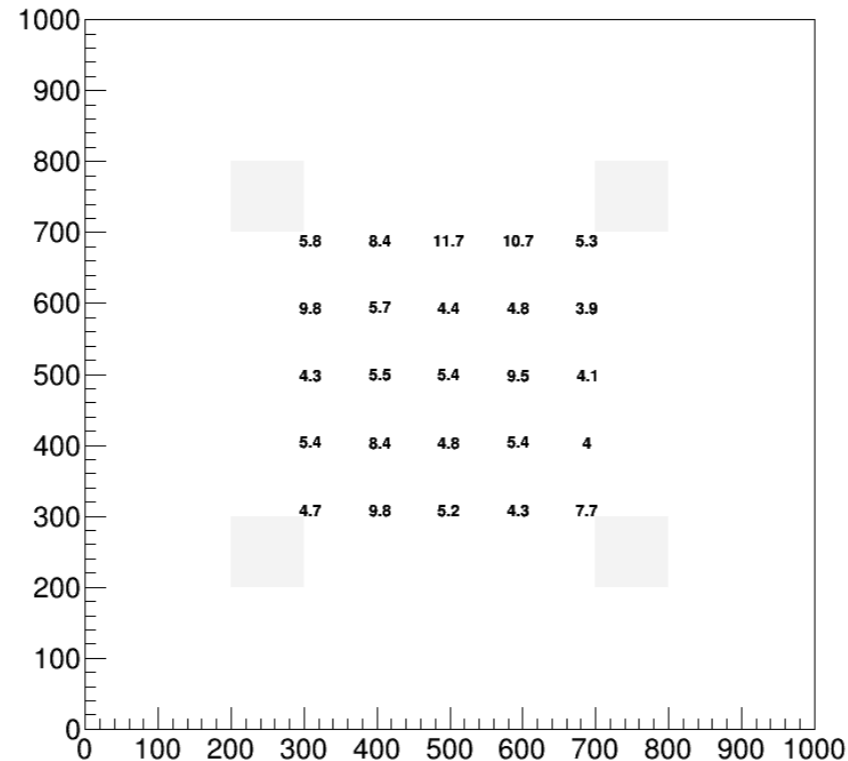


No characteristic ‘pincushion’ shape since reference is taken from the sensor itself

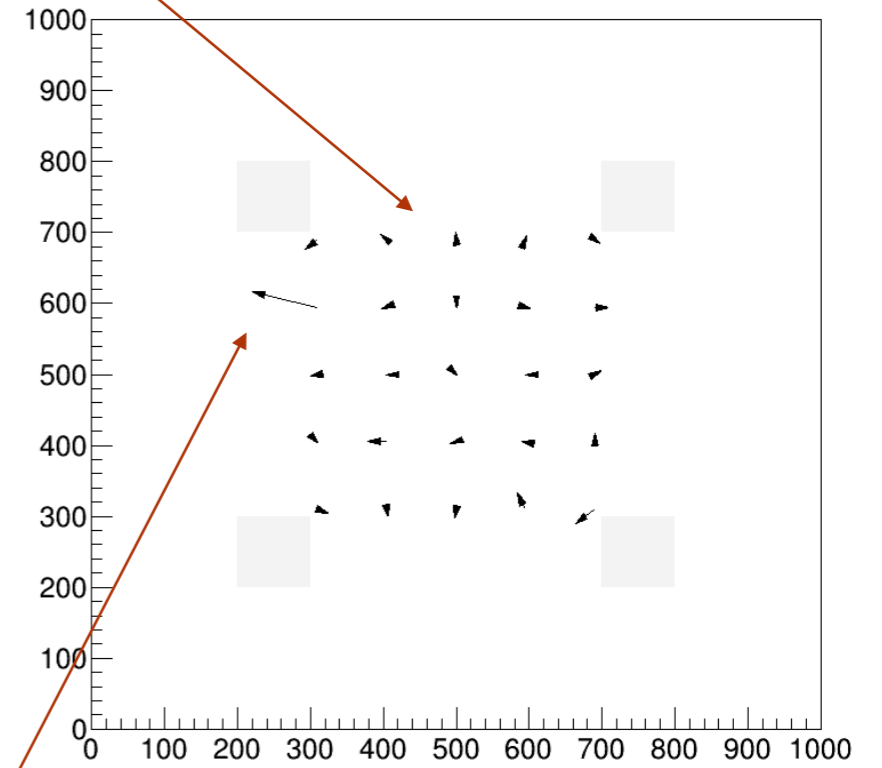
$\sigma_x$  [ $\mu\text{m}$ ]



$\sigma_y$  [ $\mu\text{m}$ ]

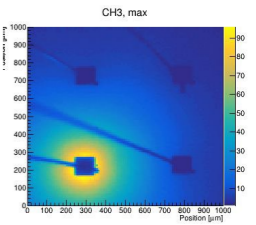


$\Delta_{\text{pos}}$  [ $\mu\text{m}$ ]



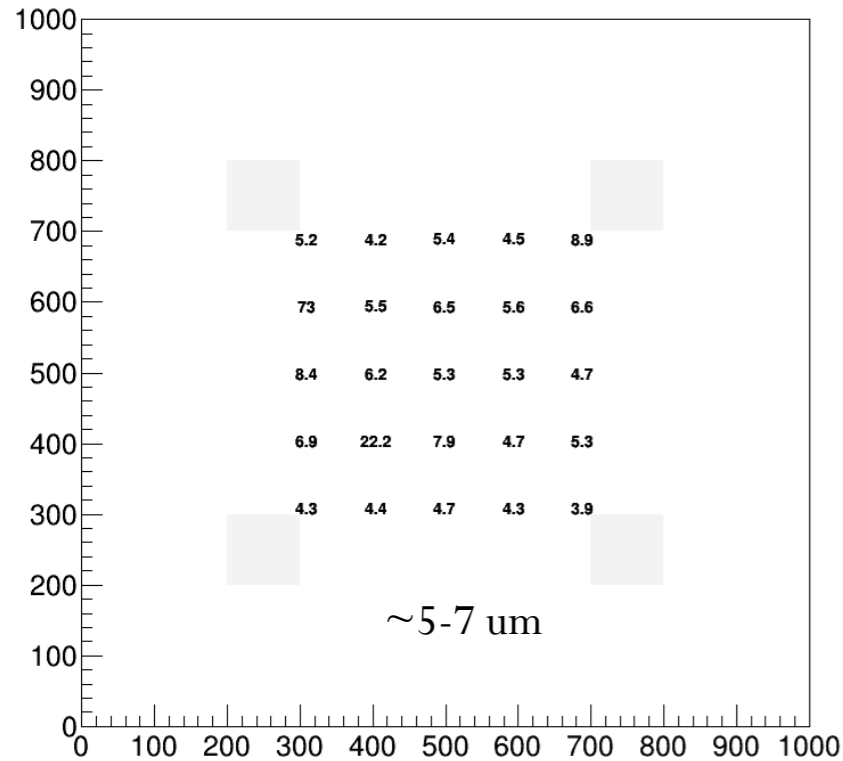
However at the edges the reconstruction can fail!

# Reconstructed position resolution – small pads



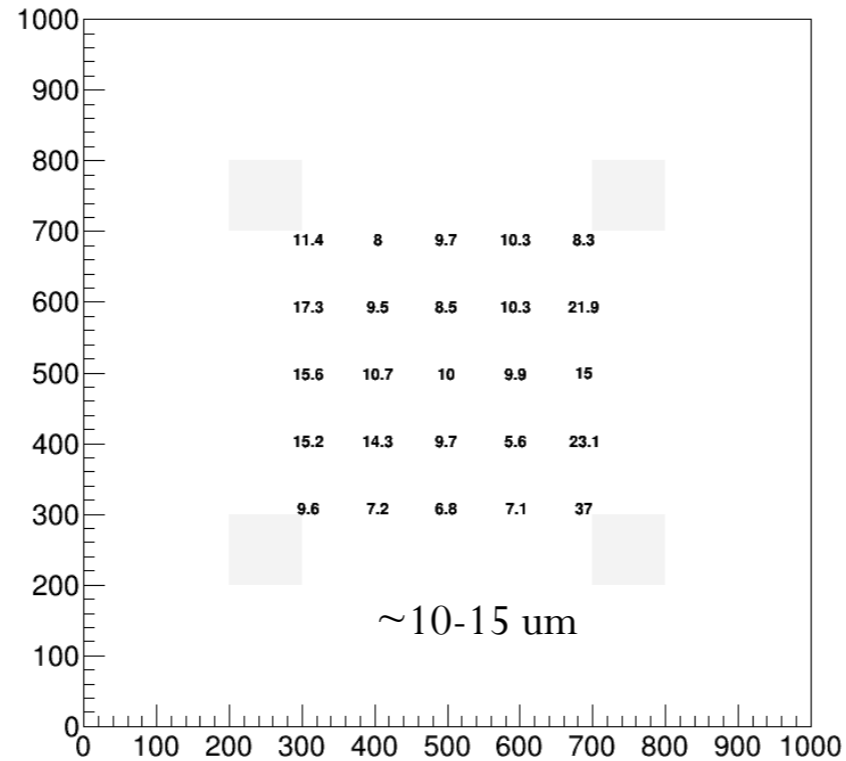
**250V**

$\sigma_x$  [um]



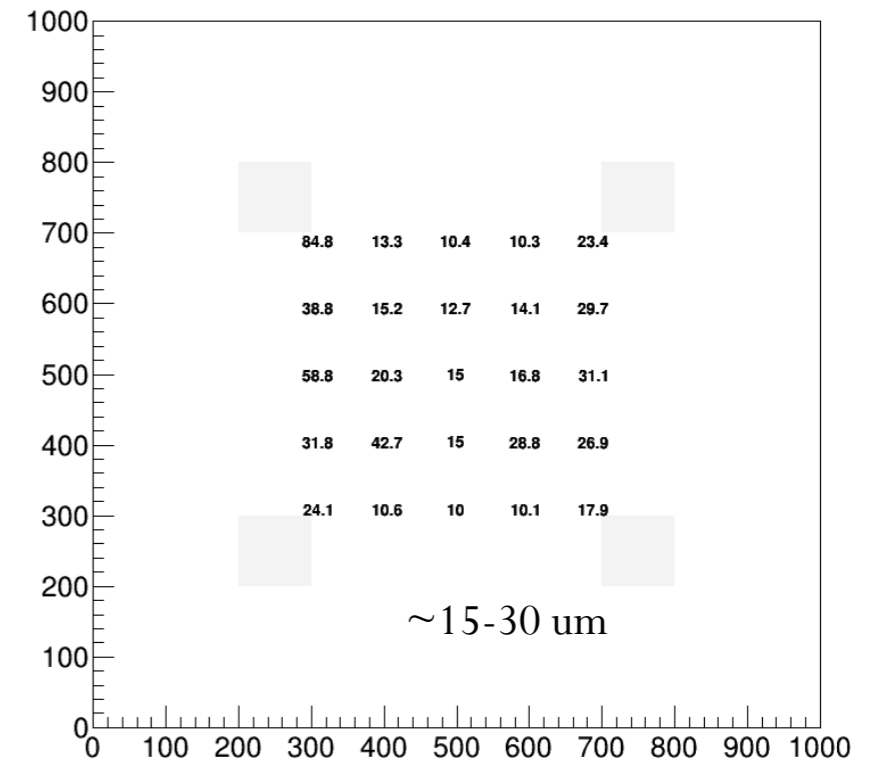
**200V**

$\sigma_x$  [um]



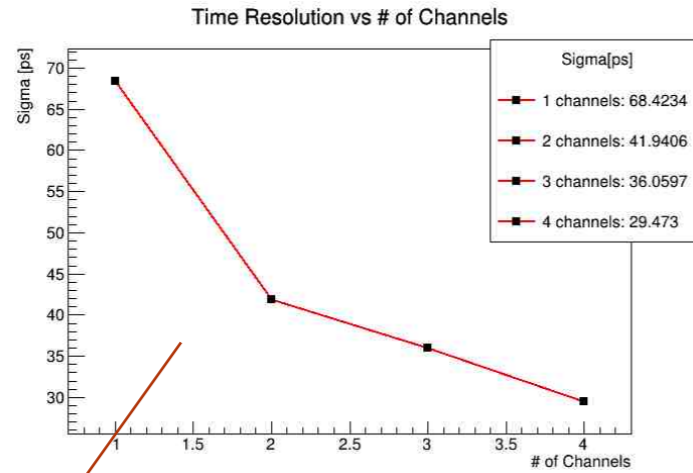
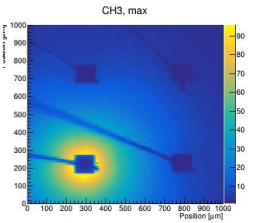
**150V**

$\sigma_x$  [um]



As expected the resolution is worse at lower gain

# Jitter – small pads



250V

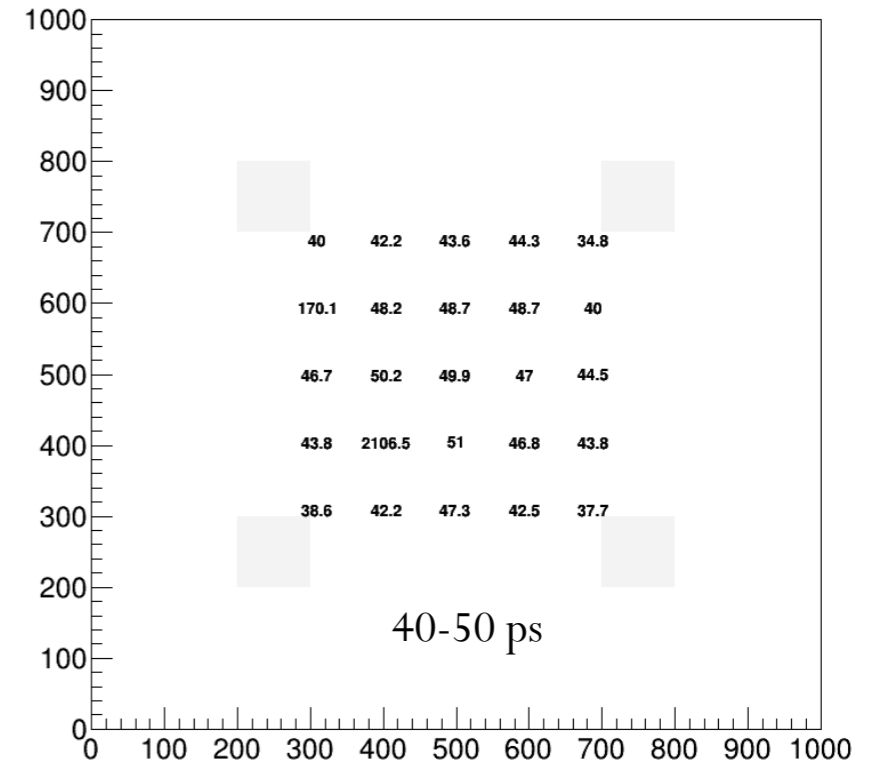
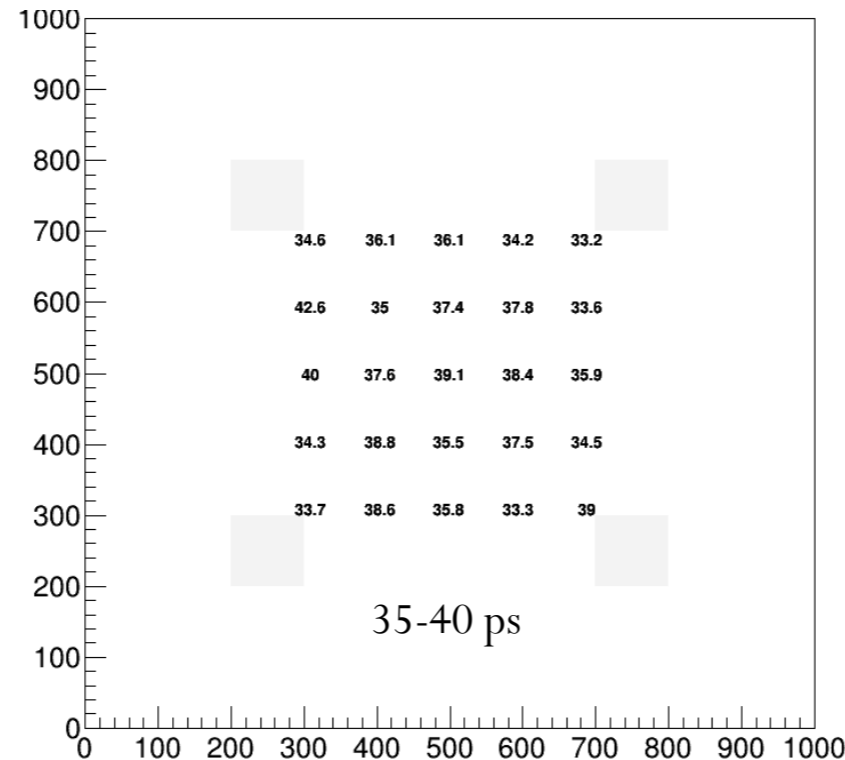
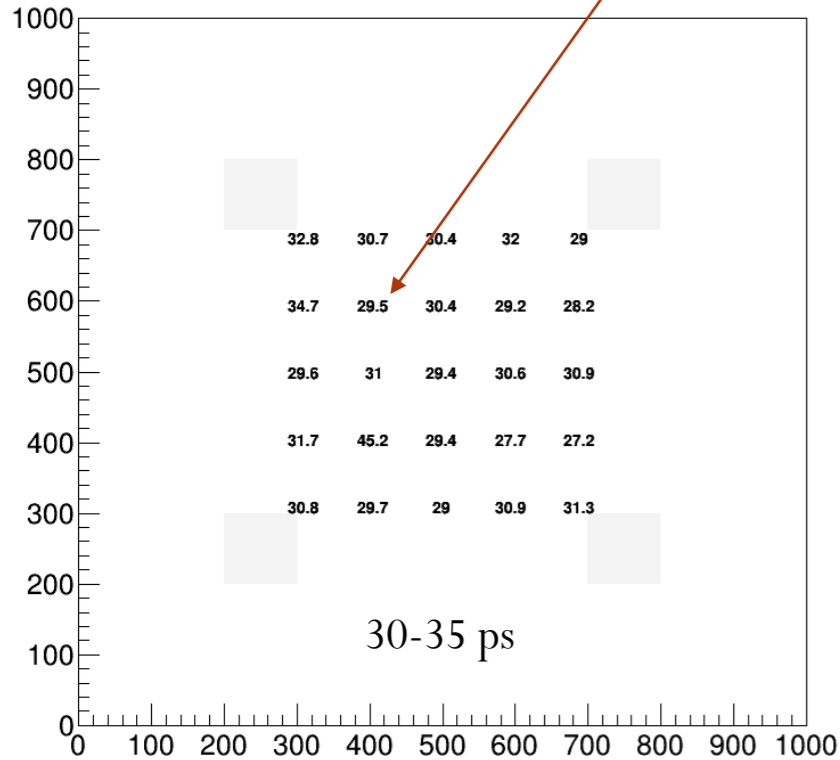
$\sigma_T$  [ps]

200V

$\sigma_T$  [ps]

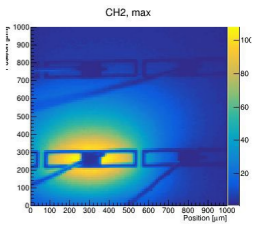
150V

$\sigma_T$  [ps]



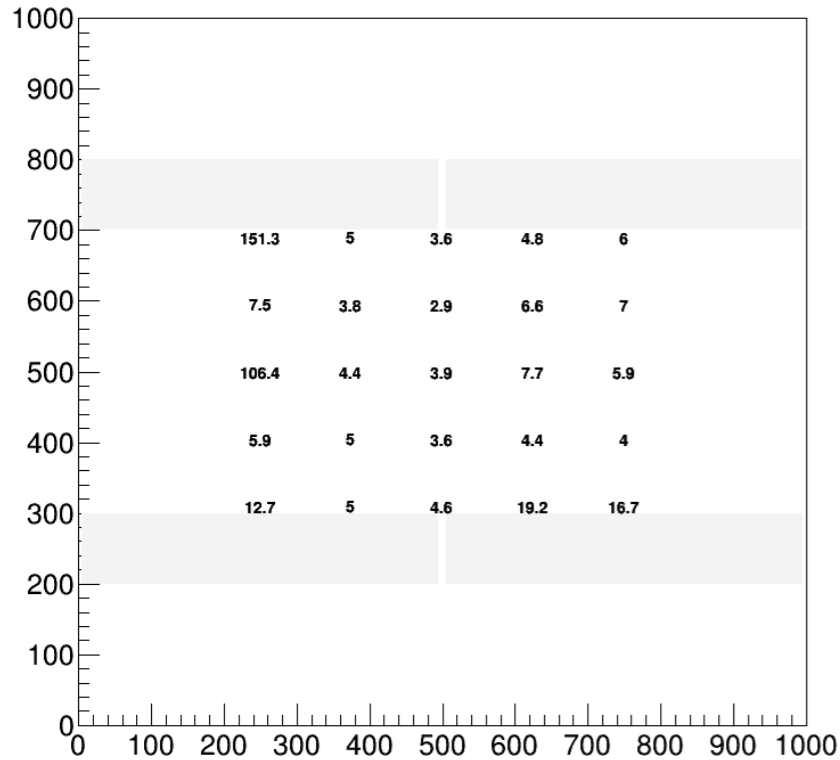
Jitter using the 4 channel combination is fairly constant in the region in between pads

# Reconstructed position resolution – microstrips

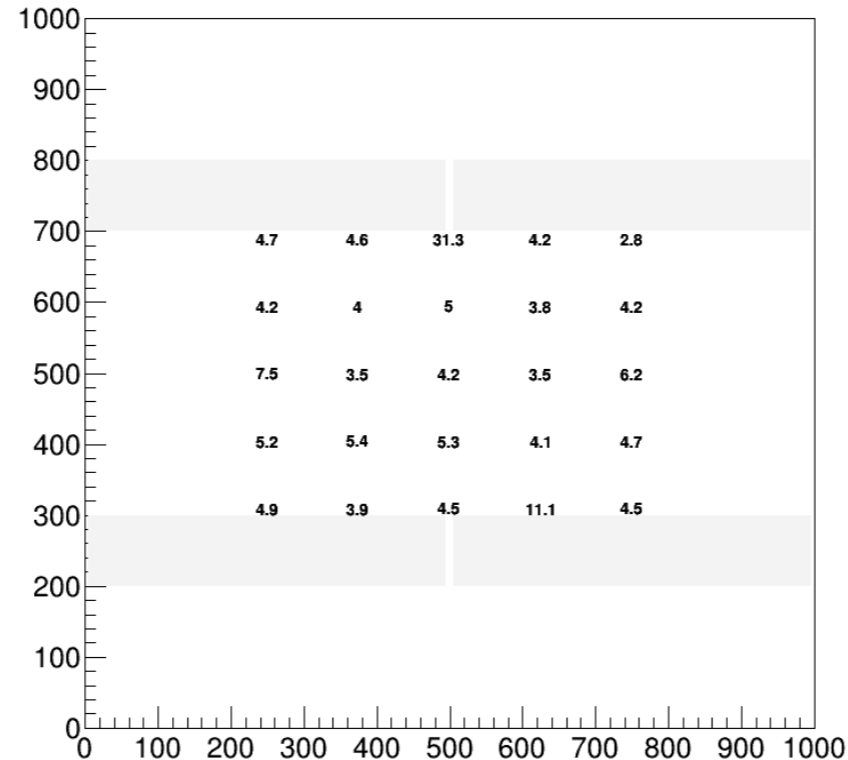


As expected better reconstruction in Y than in X, especially at the edges

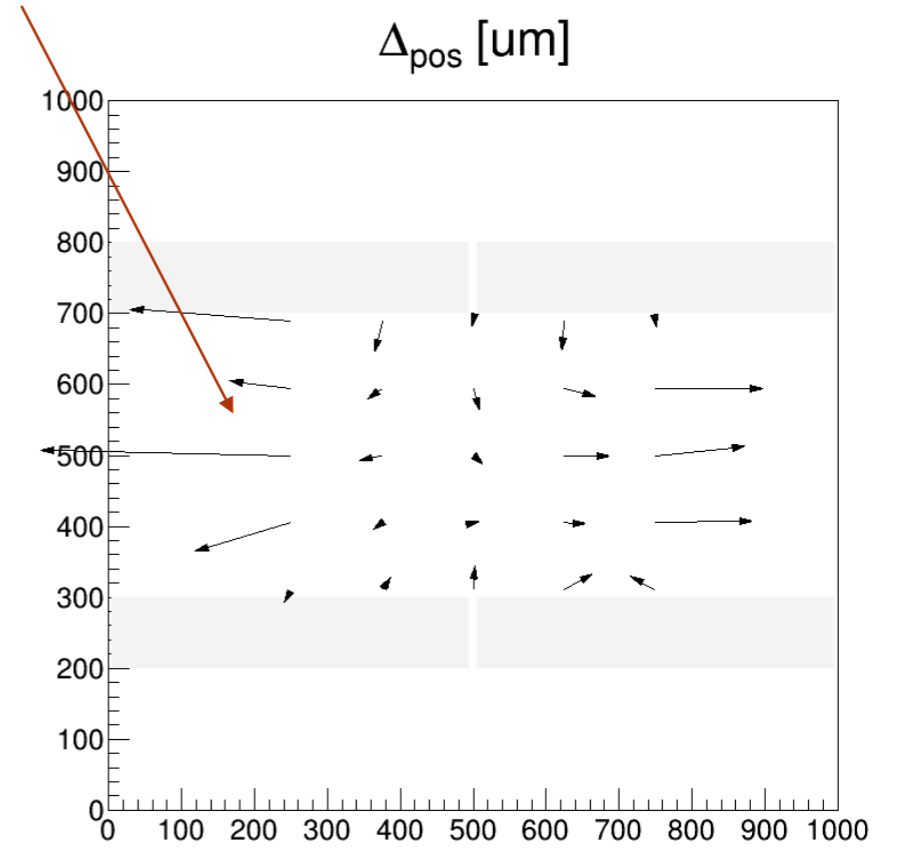
$\sigma_X$  [ $\mu\text{m}$ ]



$\sigma_Y$  [ $\mu\text{m}$ ]

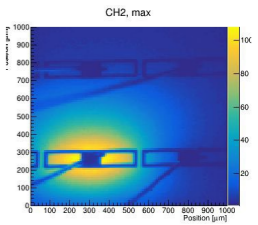


$\Delta_{\text{pos}}$  [ $\mu\text{m}$ ]



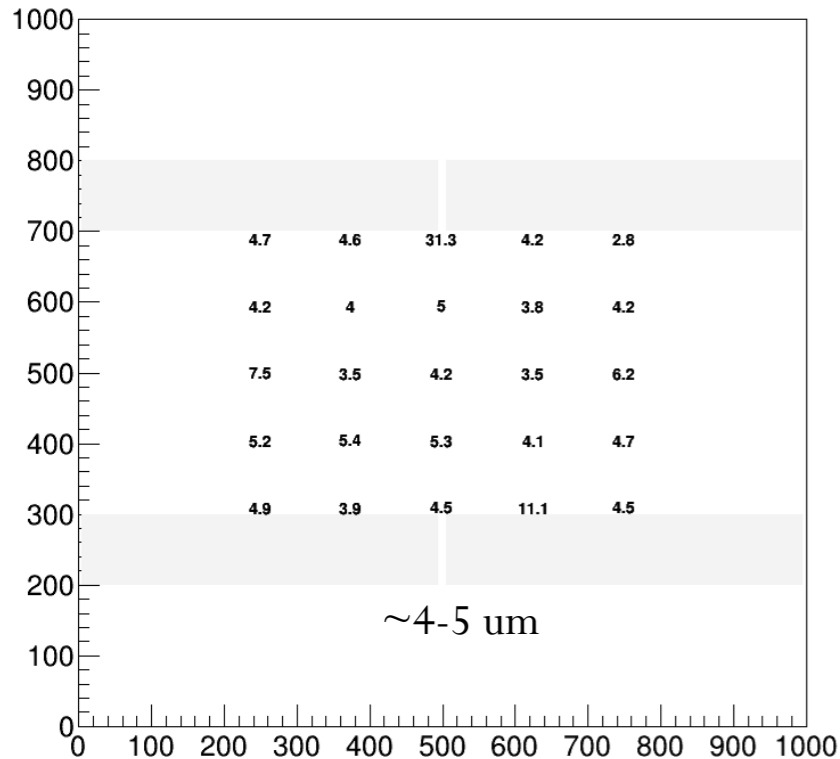


# Reconstructed position resolution – microstrips



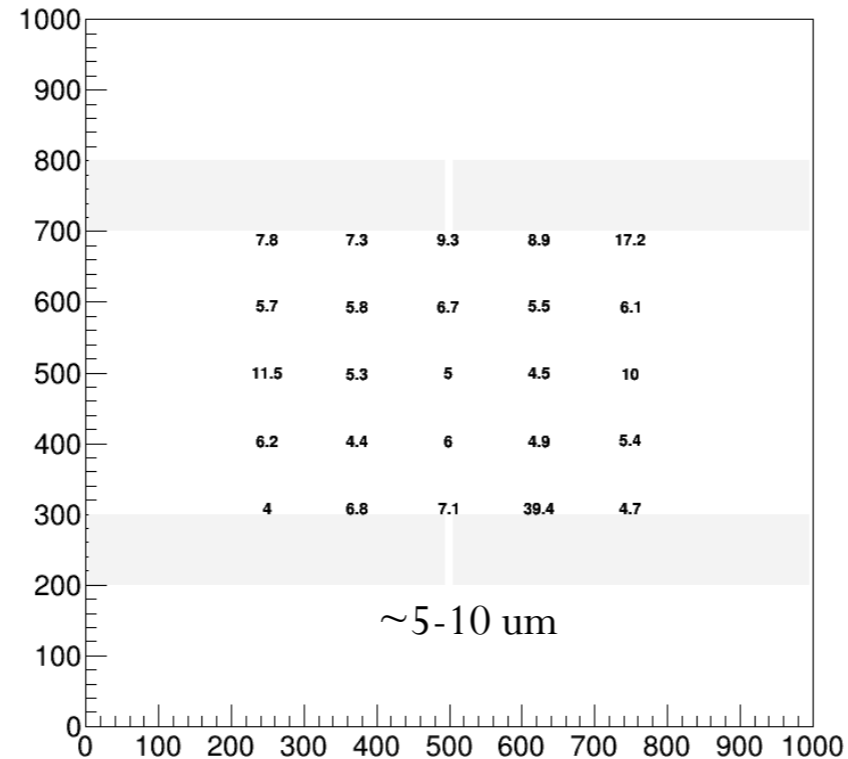
250V

$\sigma_Y$  [um]



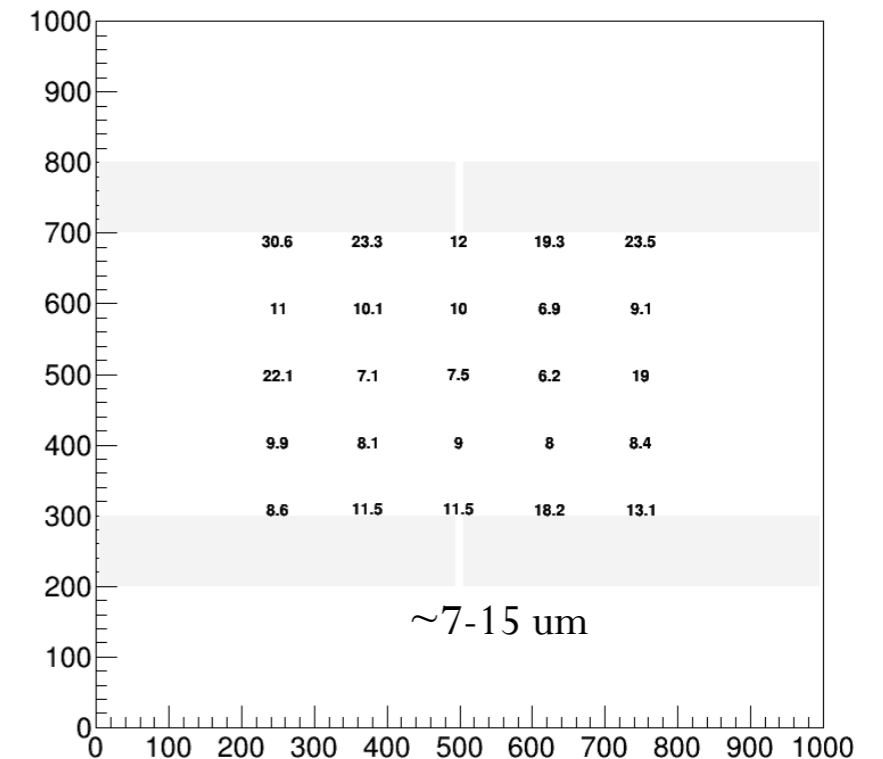
200V

$\sigma_Y$  [um]



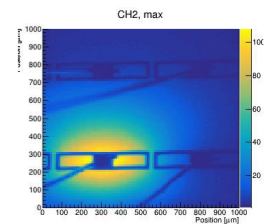
150V

$\sigma_Y$  [um]



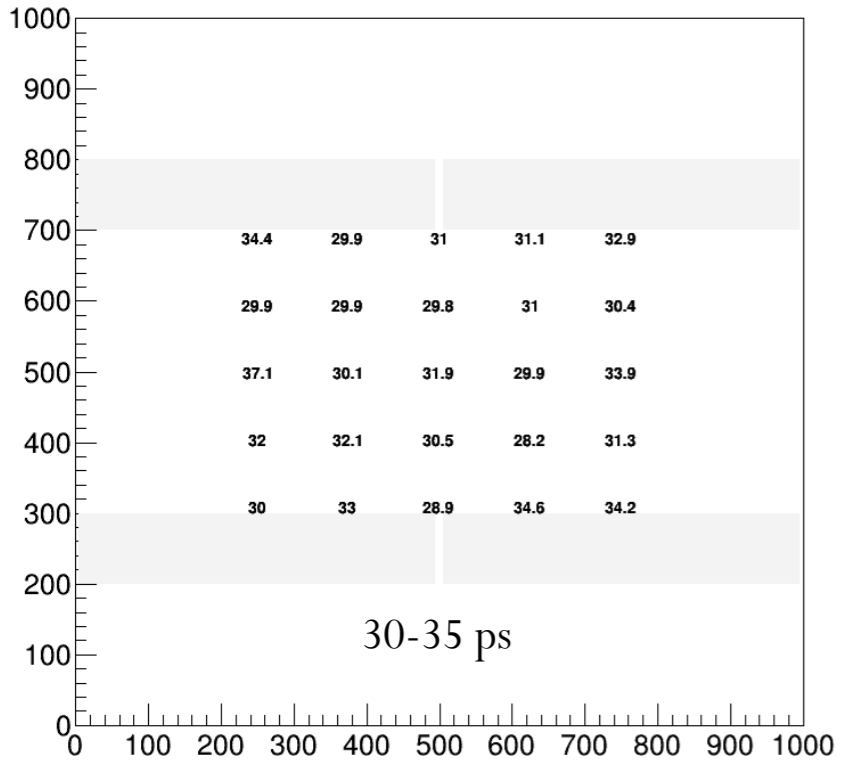
Resolution is worse at lower gain, but better than in the small pads case

# Jitter – microstrips



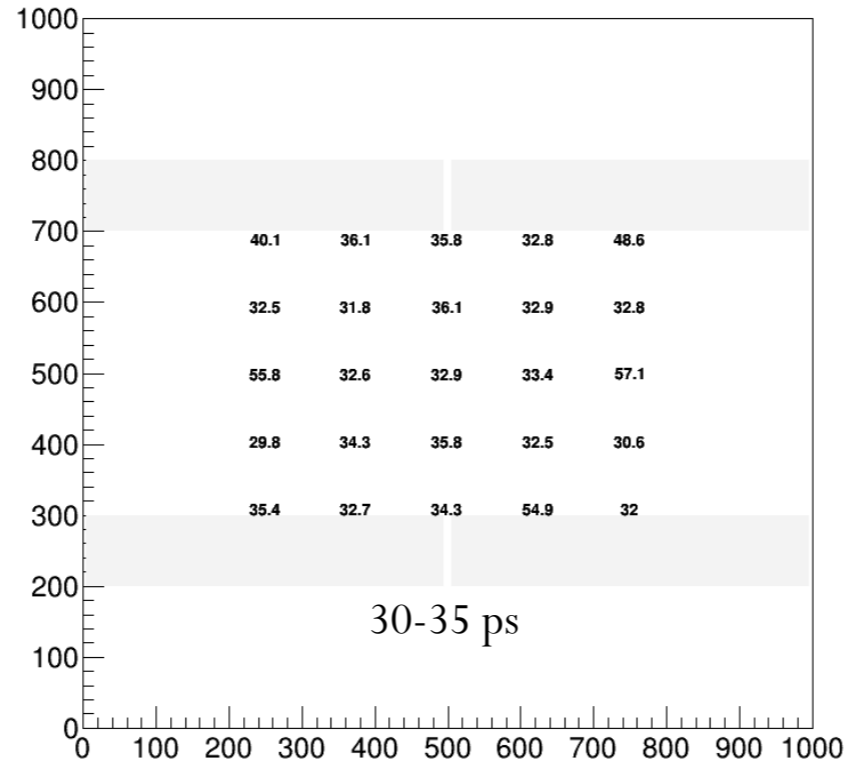
250V

$\sigma_T$  [ps]



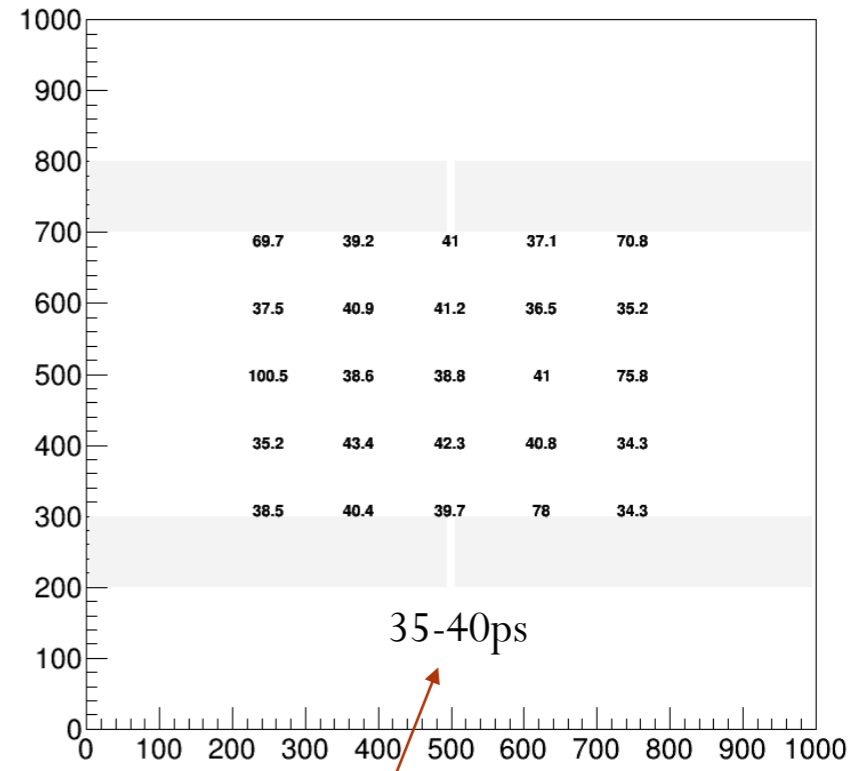
200V

$\sigma_T$  [ps]



150V

$\sigma_T$  [ps]



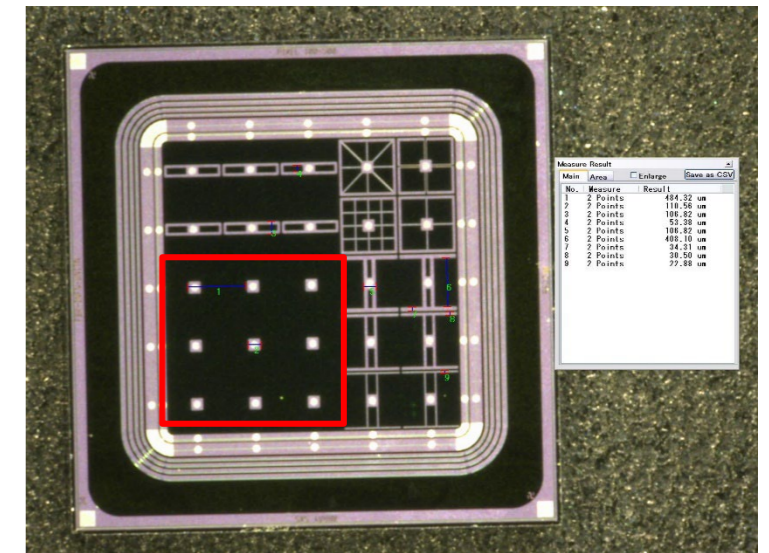
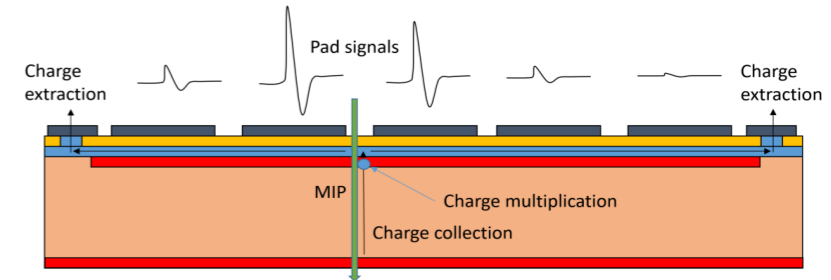
Better time resolution than with pads, related to higher S/N

# Conclusions – AC-LGAD geometries

- AC-LGADs need fine tuning of parameters for each application
  - The effect of different metal shapes have been studied for this contribution

Some questions answered:

- Does the metal structure influence the capacitance to the amplifier? **Yes**, it scales pretty well with the metal area
- Does the metal structure influence the charge sharing profile in X and Y? **Yes**, it depends on the metal shape
  - It also influence the amount of signal picked up, a larger metal structure has a higher signal
  - The the signal is also delayed in a different way
  - **Signal induction on the metal pad is not trivial to understand**
- Is there a difference in position resolution of the reconstructed events? **Yes**, but it's not as clear to understand.
  - The Jitter is lower for bigger metal structures, likely due to the increased S/N
- Reconstruction technique used is rudimental but it seems effective, **next step** is to make it more robust
  - Fully map the position resolution and Jitter for all types of pads
  - Also increase the number of channels used in the reconstruction (e.g. all 3x3 small pads)

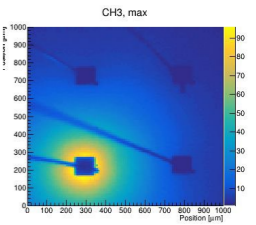




Thanks for the attention

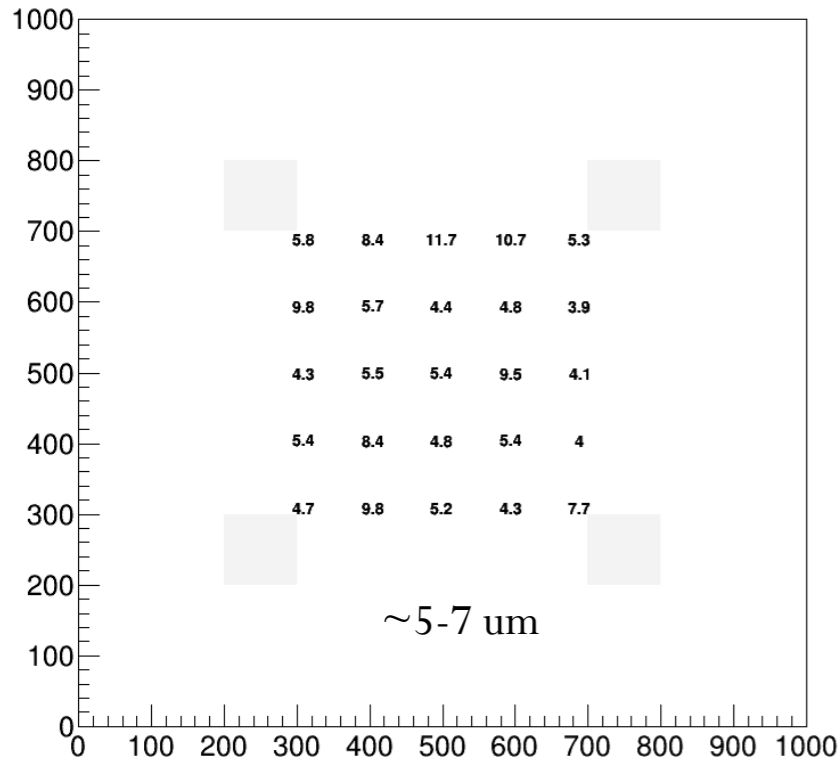


# Reconstructed position resolution – small pads



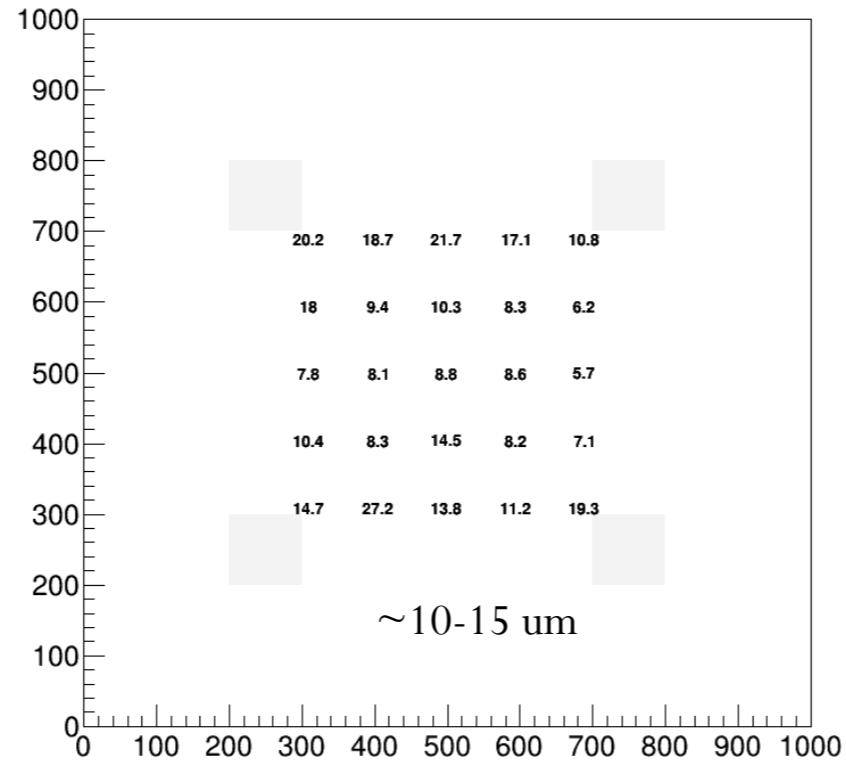
**250V**

$\sigma_Y$  [um]



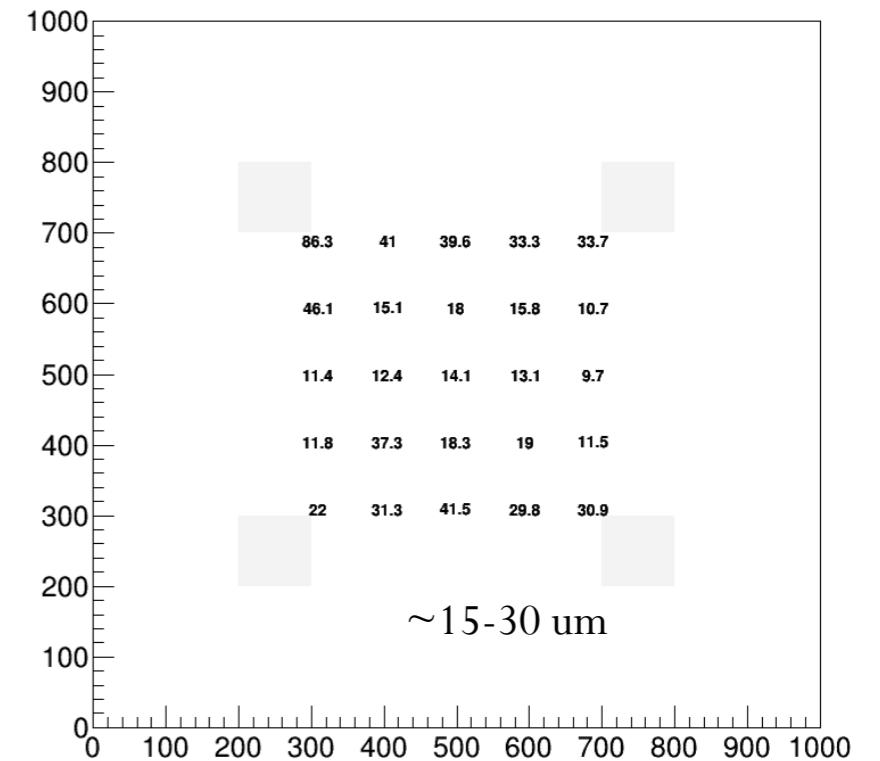
**200V**

$\sigma_Y$  [um]



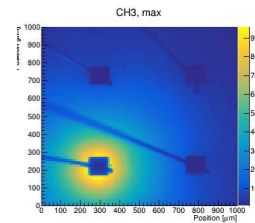
**150V**

$\sigma_Y$  [um]



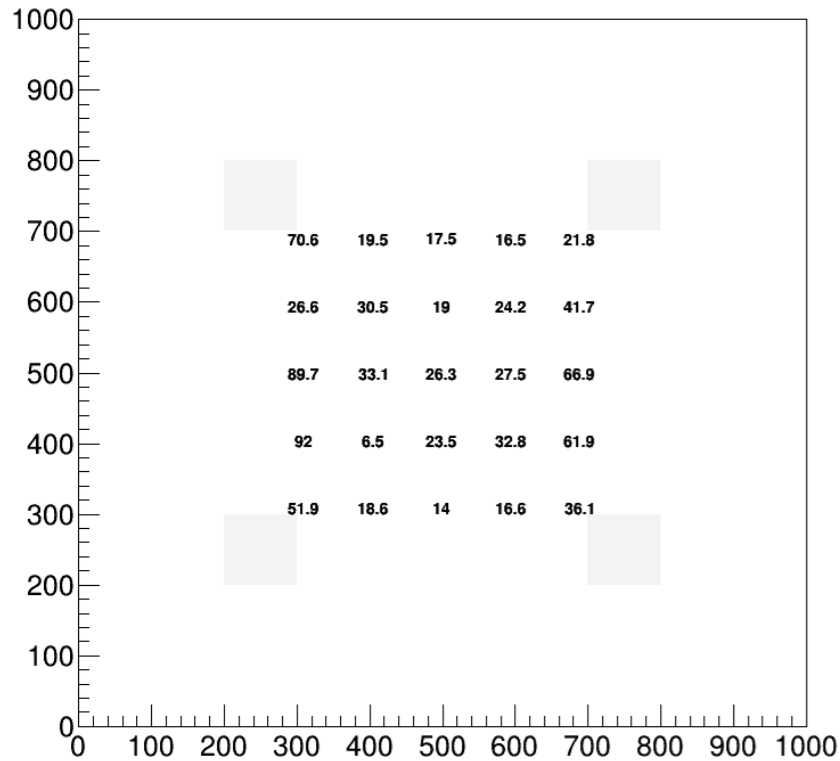
As expected the resolution is worse at lower gain

# Reconstructed position resolution – small pads



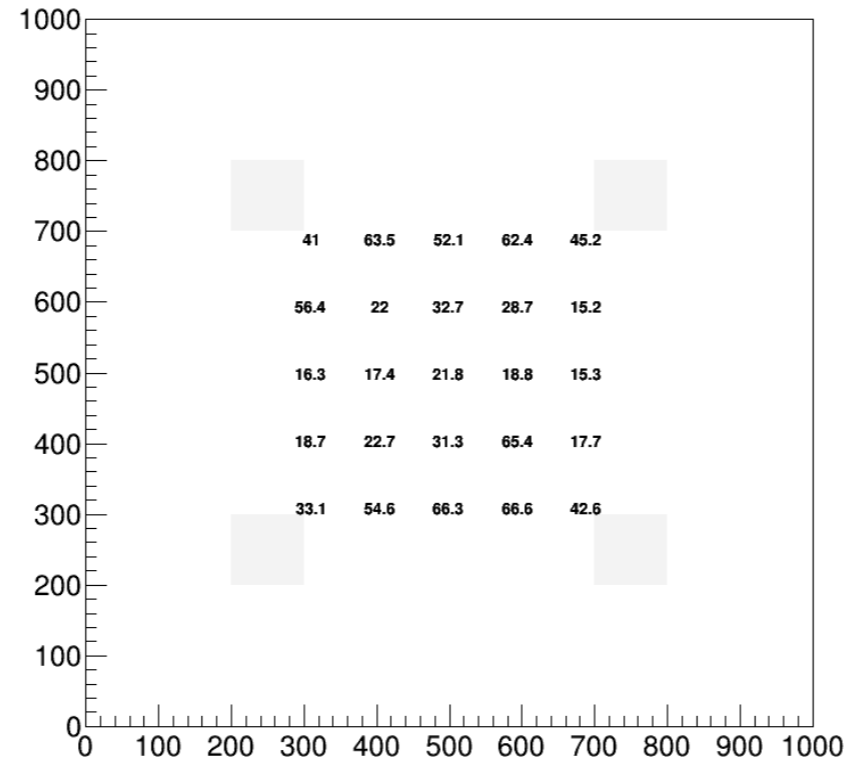
100V

$\sigma_x$  [um]



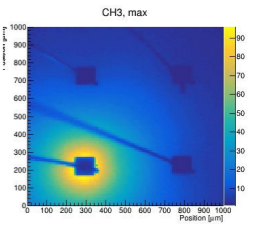
100V

$\sigma_y$  [um]



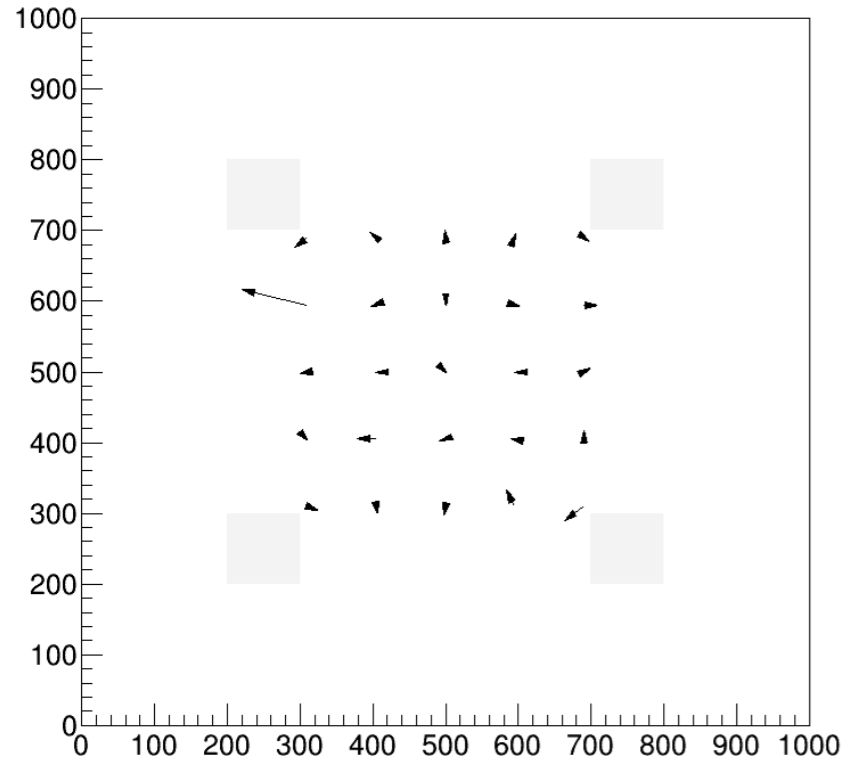
As expected the resolution is worse at lower gain

# Reconstructed position resolution – small pads



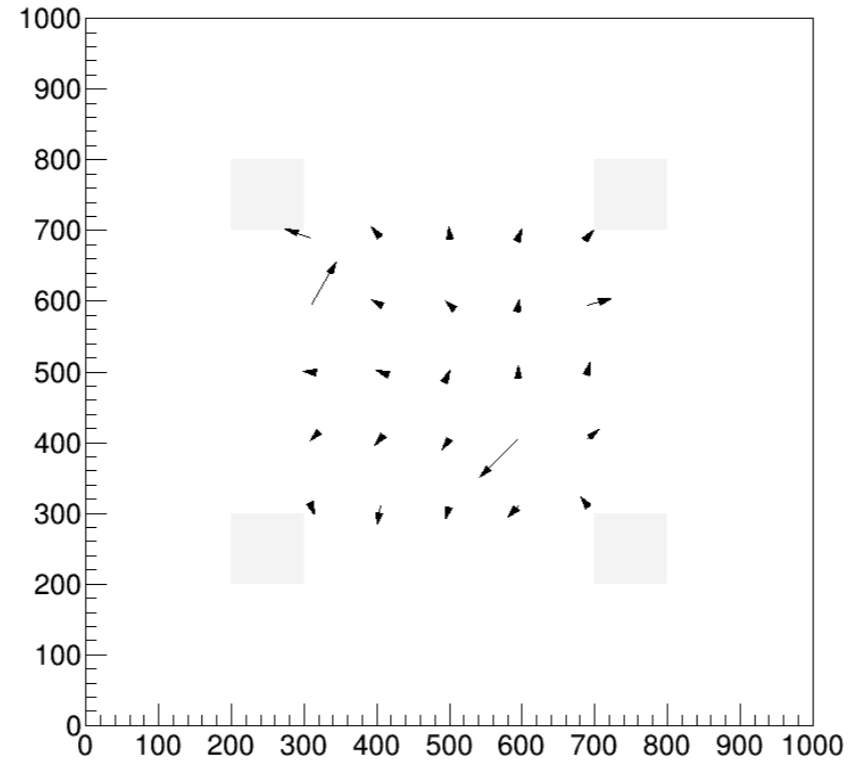
250V

$\Delta_{\text{pos}}$  [um]



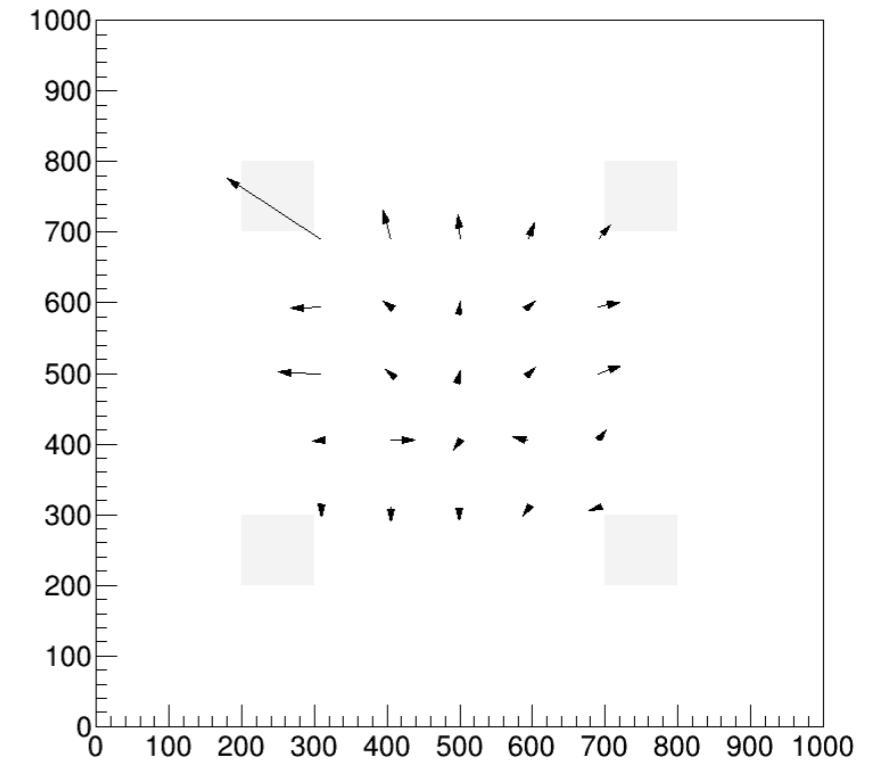
200V

$\Delta_{\text{pos}}$  [um]



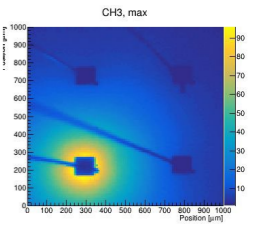
150V

$\Delta_{\text{pos}}$  [um]



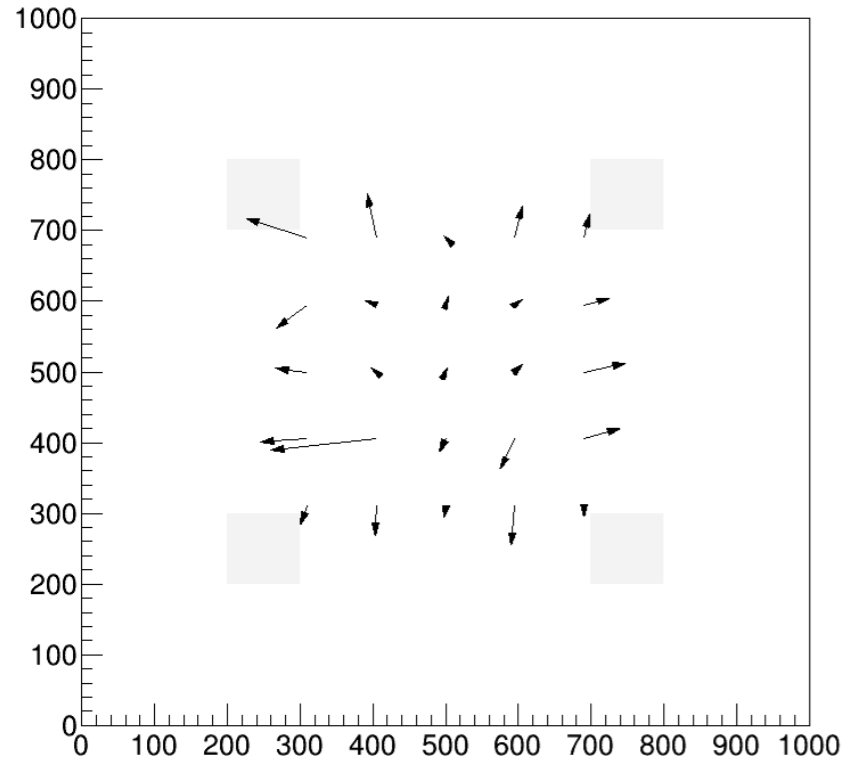
As expected the resolution is worse at lower gain

# Reconstructed position resolution – small pads



100V

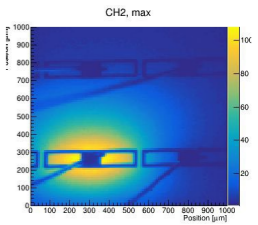
$\Delta_{\text{pos}}$  [um]



As expected the resolution is worse at lower gain

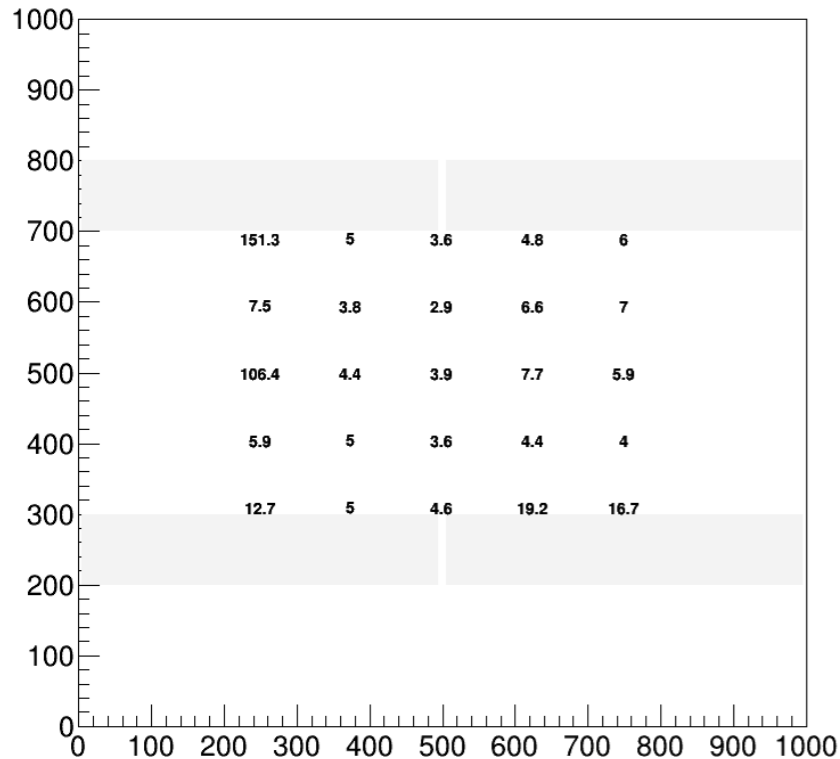


# Reconstructed position resolution – microstrips



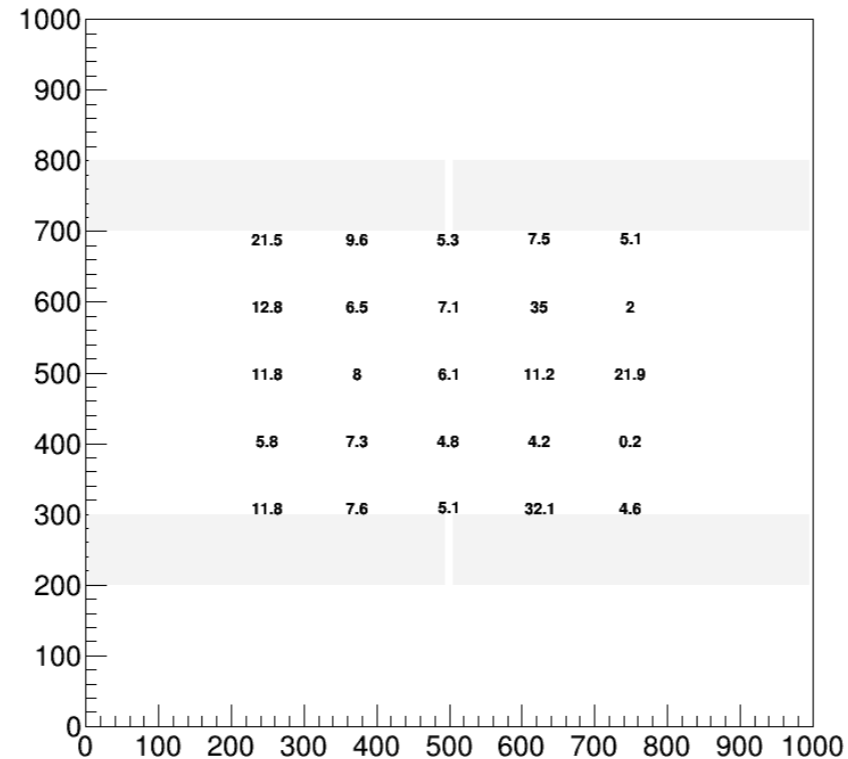
250V

$\sigma_x$  [um]



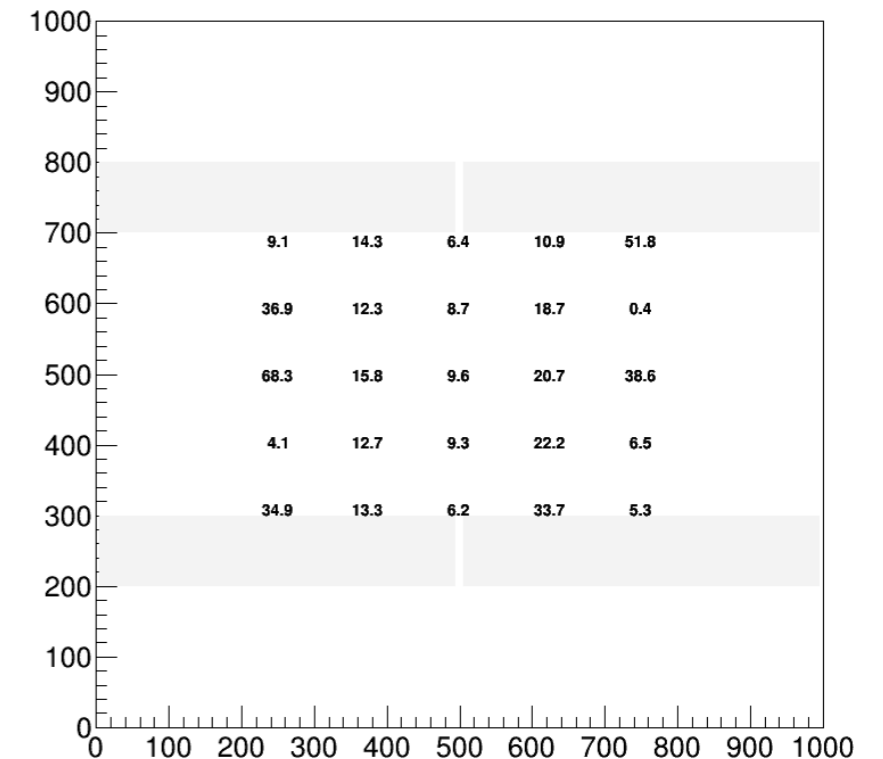
200V

$\sigma_x$  [um]



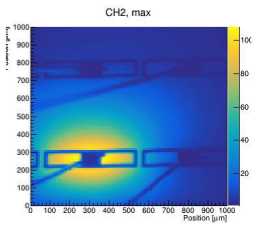
150V

$\sigma_x$  [um]



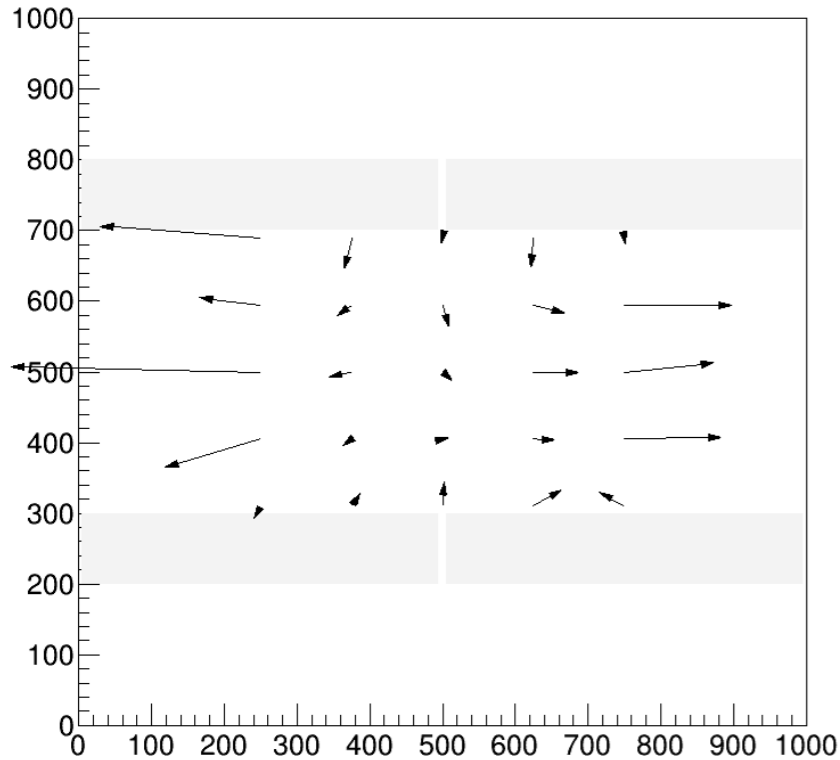
Resolution is worse at lower gain, but better than in the small pads case

# Reconstructed position resolution – microstrips



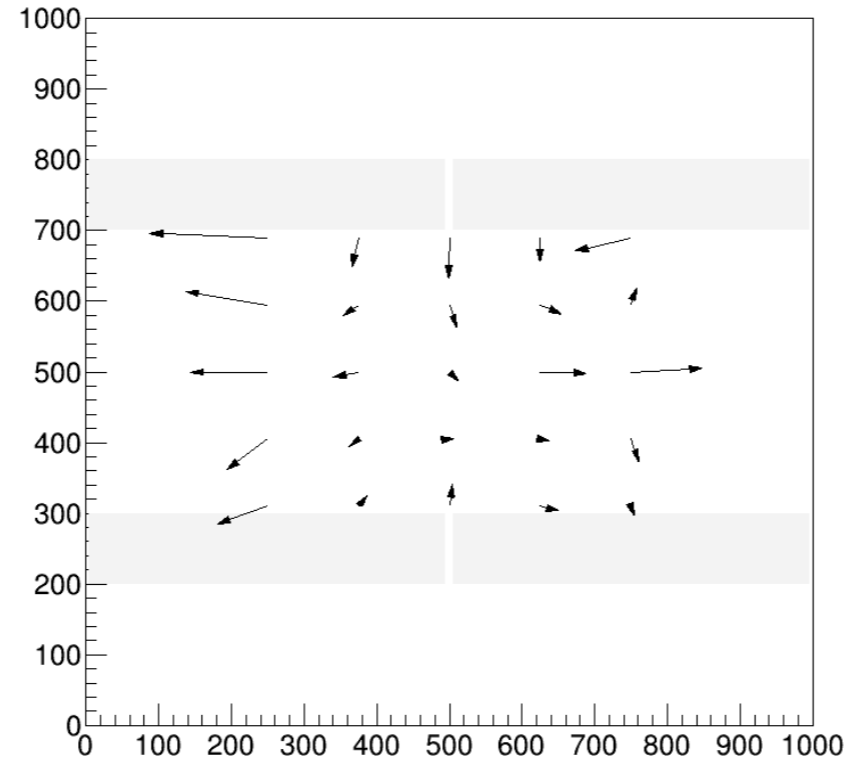
250V

$\Delta_{\text{pos}}$  [um]



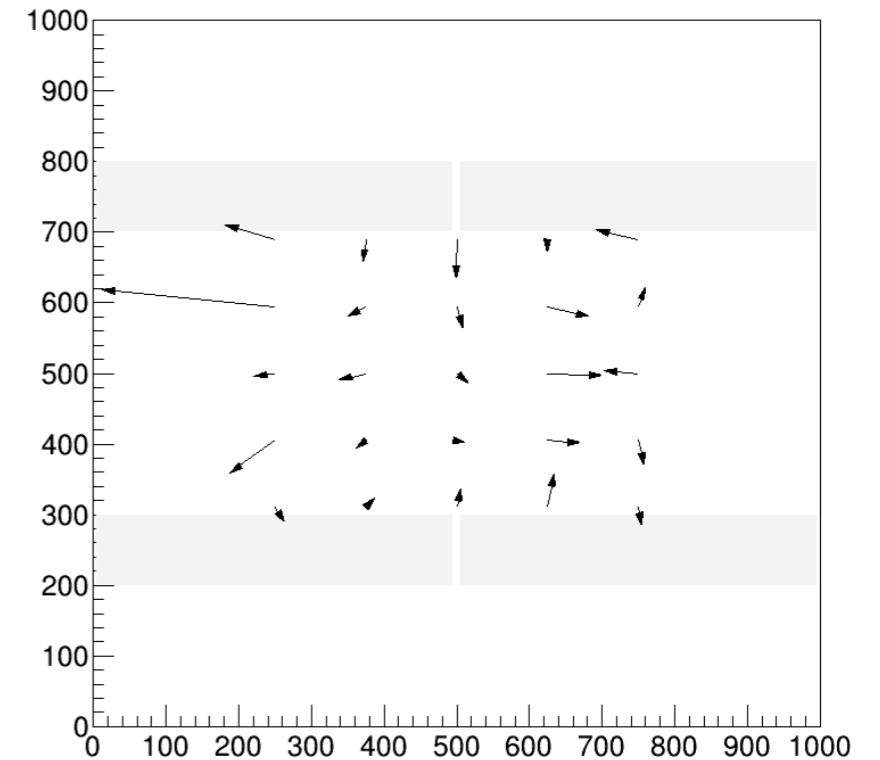
200V

$\Delta_{\text{pos}}$  [um]



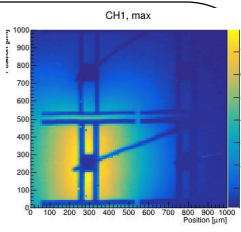
150V

$\Delta_{\text{pos}}$  [um]

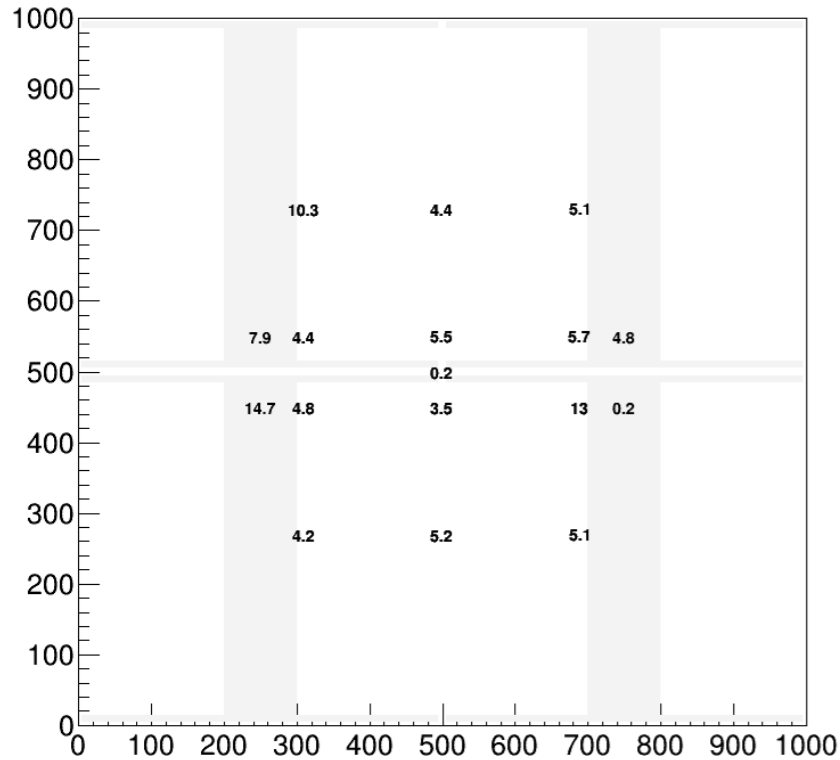


Resolution is worse at lower gain, but better than in the small pads case

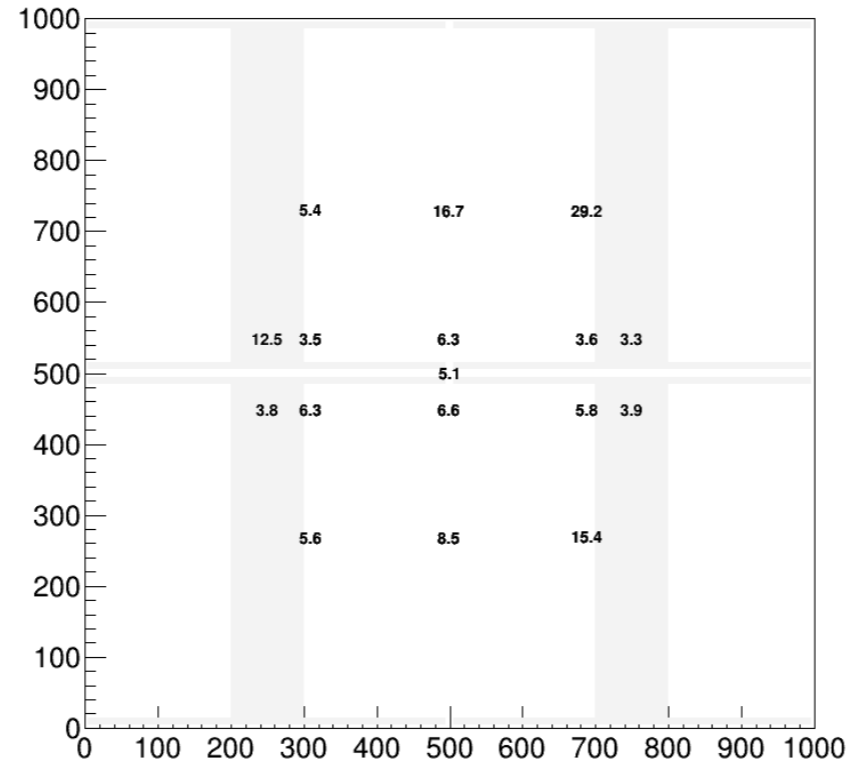
# Reconstructed position resolution – H pads



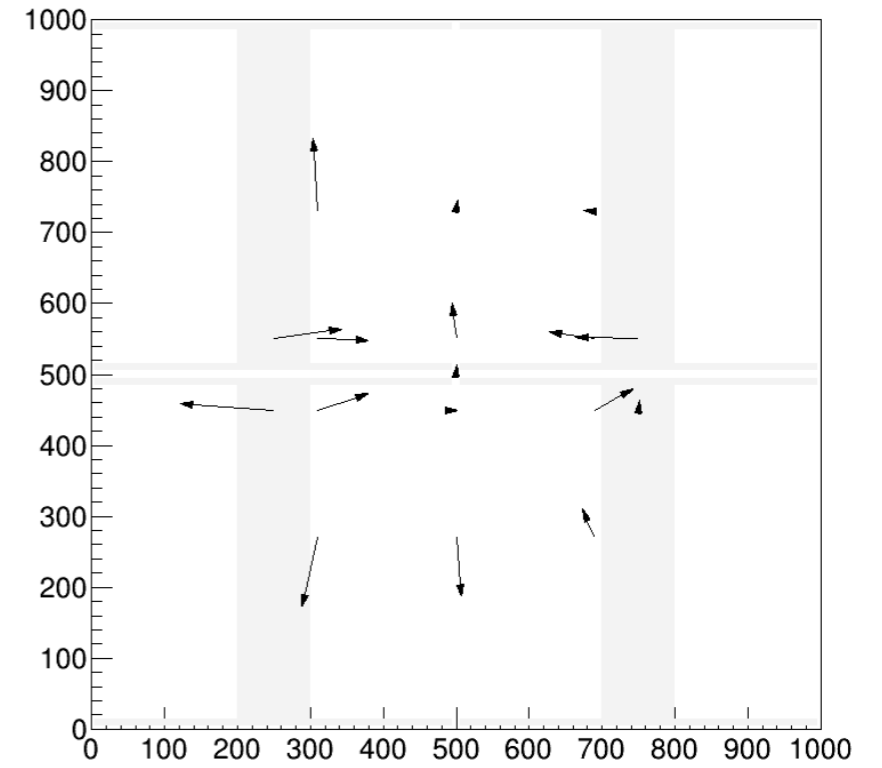
$\sigma_x$  [ $\mu\text{m}$ ]



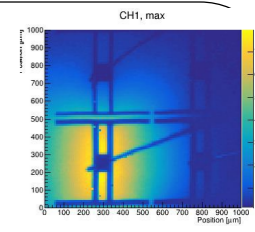
$\sigma_y$  [ $\mu\text{m}$ ]



$\Delta_{\text{pos}}$  [ $\mu\text{m}$ ]

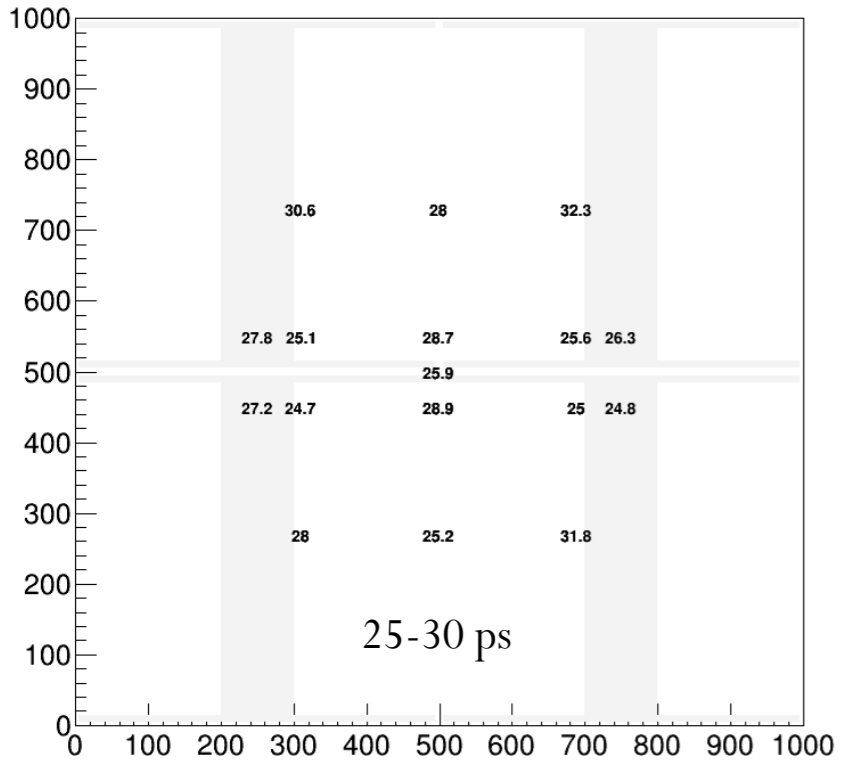


# Jitter - H pads



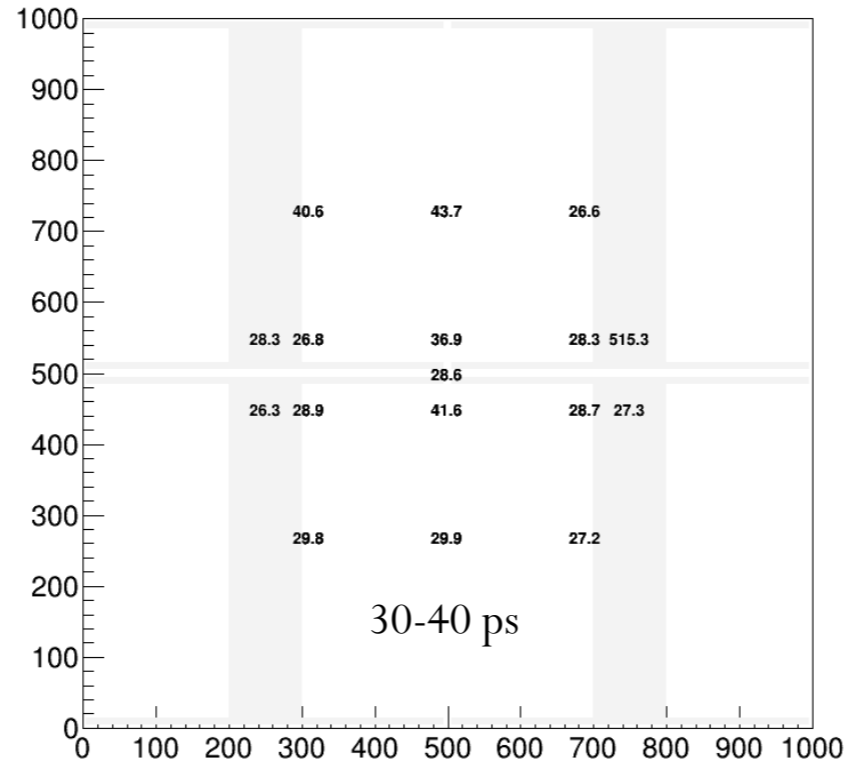
**250V**

$\sigma_T$  [ps]



**200V**

$\sigma_T$  [ps]



**150V**

$\sigma_T$  [ps]

