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Guard-ring design optimization in thin UFSD

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Outline

- > Four Guard-Ring (GR) designs have been implemented in UFSD4 production by FBK
- Guard-ring designs investigated in simulation
- Characterization of new PiN diodes and irradiated LGAD (neutrons; Ø=1.5·10¹⁵ n_{eq}/cm²)
 - PiN diodes: measurement of breakdown voltage
 - Irradiated LGAD: measurement of GR current
- Characterization of Noise due to different GR design in irradiated LGAD (neutrons up to Ø=1.5·10¹⁵ n_{eq}/cm²)

Design: GR5_STD (Multi floating Guard-Ring)



- \succ Edge width of 500 μ m
- One grounded Guard-ring
- ➤ 4 floating Guard-ring
- > One p-stop between the last GR and the cut line

Design: GR3_0 (Zero floating Guard-Ring)





- \succ Edge width of 300 μ m
- One grounded Guard-ring
- > No floating Guard-ring
- > No p-stop between the GR and the cut line

Design: GR3_1 (One floating Guard-Ring)





- Edge width of 300 μm
- One grounded Guard-ring
- ➤ 1 floating Guard-ring
- > No p-stop between the floating GR and the cut line



- \succ Edge width of 300 μ m
- One grounded Guard-ring
- No floating Guard-ring
- Double p-stop between the floating GR and the cut line

Summary of guard-ring tested





Simulations of different guard-ring designs in 45 μ m-thick LGAD



On the region between innermost GR and the sensor edge:

- Electric field drop localised between the innermost GR and the first floating one or first p-stop implant
- Negligible electric field drop in the region beyond the first floating GR
- Electric field drop smoother in design with no-floating GR than with floating one



No-floating guard-ring + double p-stop design



Evaluation method

The different guard-ring structures have been tested using the following measurements:

- Breakdown of new PIN structures
- Current and breakdown in irradiated structures
- Presence of spurious signals (macro-discharges) due to guard-ring structure instability

Breakdown of PiN diodes with different GR designs



Breakdown measurement performed on PiN diodes unirradiated

Breakdown:

- Edge breakdowns between 600 V and 700 V
- Slight dependence on guard-ring design
- Designs with no floating GR are the most robust
- Design with multi-floating GR is the least robust
- The edge width does not affect the breakdown

Breakdown vs # of edge implants (guard-ring and p-stop)



Relationship between the breakdown voltage and the number of implants beyond the innermost guard-ring

Guard-ring currents in irradiated LGAD at $Ø=1.5\cdot10^{15} n_{eq}/cm^2$



Guard-ring designs investigated on 2x2 LGAD: GR3_0 GR3_1 GR5_STI

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1	GR5_STD

In presence of bulk damage:

- Multi guard-ring design has a steeper increase of the edge current
- Zero and one-floating guard-ring designs are more robust than multi GR design

The effect of surface damage must be investigated

Characterization of Noise – Macro discharges

Macro Discharge (MD) phenomenon has been observed for the first time in multi guardring irradiated LGAD (\emptyset >1·10¹⁵ n_{eq}/cm²), working at high bias (Bias > 450V)



- (MDs) were observed by triggering the sensor noise in absence of external source of signal (beta, laser etc...)
- Measurements were done in climatic chamber at -25°C with a readout chain based on SC-Board + a 20dB second stage amplifier (Cividec BroadBand)
- > Macro discharge phenomenon, main characteristics:
 - Bias dependent
 - Irradiation level dependent
 - Discharges of different amplitude and time duration

Characterization of Noise – Macro discharges



Macro discharges in different guard-ring devices

Macro discharges investigated in irradiated LGAD with different guard-ring designs

Guard-ring design investigated:

- Multi floating guard-rings (GR5_STD)
- One floating guard-ring (GR3_1)
- Zero floating Guard-ring (GR3_0)



Bias table at witch macro-discharges appear

	GR5_STD	GR3_1	GR3_0
$\emptyset = 1.10^{15} n_{eq}/cm^2$	450–500 V	/	/
$\emptyset = 1.5 \cdot 10^{15} n_{eq}/cm^2$	450–500 V	550–600 V	/

Macro-discharge is guard-ring design dependent:

- ➢ GR5_STD design: Macro-discharges appear in the safe working bias (Bias < 500V) of sensors</p>
- GR3_1 design: Macro-discharges appear above fluence of 1.5·10¹⁵ n_{eq}/cm², beyond the safe working bias (Bias>550V) of sensors.
- GR3_0 design: Macro-discharges do not appear

Possible source of macro-discharge

Pocket of area limited within two implants collect charge and increase their voltage, until they discharge

Consistent with evidence:

- Faster charge-up in more irradiated sensors
- Faster charge-up at higher bias



Summary

- Four Guard-ring designs have been investigated in simulation and implemented in UFSD4 FBKproduction:
 - Multi floating Guard-Ring
 - One floating Guard-Ring
 - Zero floating Guard-Ring
 - Zero floating Guard-Ring + double p-stop
- From simulations and electrical characterizations pre and post neutrons irradiation, the designs with zero and one floating guard-ring are more robust than multi guard-ring design
- Noise characterization in irradiated LGAD showed Macro-Discharges correlated with the GR design:
 - In multi-GR design Macro-Discharges appear in the safe working bias (Bias<500V) range of sensors
 - In One-GR designs the Macro-Discharges appear beyond the safe working bias range (Bias>550V) of sensors
 - In Zero-GR designs the Macro-Discharges are absent up to 700V

Back up

Simulation parameters

- 45-μm-thick active substrates with 0.81-μm-thick oxide
- Edge contact at the same bias of the back
- Horizontal cutlines at 100 nm beneath the silicon/oxide interface
- Radiation damage models implementation (new Perugia, bulk damage)
- Unirradiated profiles plotted at breakdown
- Irradiated profiles plotted at 600 V

Simulations of Zero floating guard-ring + double p-stop in 45µmthick LGAD

Innermost GR

not irradiated at **411 V** (breakdown) irradiated at **600 V** (1 Mrad, 1e15 n_{eq} /cm²): $I \simeq 10 \mu A$

Double p-stop

Sensor edge



UFSD4 Reticle



Devices:

- Pair LGAD-PiN
- LGAD 1x2
- LGAD 2x2
- LGAD 5x5

Breakdown of irradiated LGADs

