Isolating the Sound of Dark Matter

Our HELIOS Suspension

Noah Baker, CASST 2022 Presentation



N. Baker^{1*}, M. Hirschel¹, V. Vadakkumbatt¹, J. Manley², S. Singh² and J. P. Davis¹

Department of Physics, University of Alberta, Edmonton, Alberta, Canada, T6G 2E9

²Department of Electrical and Computer Engineering, University of Delaware, Newark, Delaware, US



Ielium Pressure [a.u Ultralight Scalar Dark Matter Time-dependent variations in the fine structure A detectable, isotropic strain constant and fermion mass according to their induced on all condensed respective DM coupling constants g [1]: objects [2-4]: $\alpha \to \frac{\alpha}{1 - g_{\gamma}\phi} \approx \alpha(1 + g_{\gamma}\phi), \quad m_{\psi} \to m_{\psi} + g_{\psi}\phi$ $h(t) = \underbrace{d_{\rm DM} \frac{\sqrt{8\pi G\varrho}}{\omega c}}_{h_0} \cos(\omega t)$ Modulation of the atoms' Bohr radius [2-3]: $a_0(t) = \frac{n}{c m_e(t) \alpha(t)}$ (nucleus)-

Circuit Modelling

- Mechanical suspension systems generally **simulated directly**.
- Can actually map mechanical quantities to electrical ones.
 - Reduces the problem to a **circuit** which can be **solved analytically** [5].

 $|\mathbf{C}| = |\mathbf{m}|$

IABLE I. Table of corresponding electrical and mechanical quantities.					
Electrical		Mechanical		m	>
Variable	Symbol	Variable	Symbol		
Current	I (A)	Force	F (N)		· · · · · · ·
Voltage	U (V)	Velocity	v(m/s)	.	L =]
Impedance	$Z(\Omega)$	Admittance	Y(s/kg)	k >	
Admittance	$Y(1/\Omega)$	Impedance	Z(kg/s)	<	
Resistance	$R(\Omega)$	Responsiveness	1/D (s/kg)		>
Inductance	L (H)	Elasticity	1/k(m/N)		
Capacitance	C (F)	Mass	m (kg)	<	



Direct Implementation Issues

k = 398 W | m. K

= 15 W m.

MRFM



 We had 10-11 cm in vertical height to fit the entire suspension. Just one stage was 7.7 cm long. Since more stages means more attenuation, we needed a new design.



Copper Catherine Wheel Springs

- These springs have a **drastically smaller** rest length.
- As the oscillations are also very small, they take up almost no vertical height.
- Since they're also **made out of copper**, additional heat conducting wires are rendered **unnecessary**.







Mapping Springs to Cantilever Arms



Want deflection δ to be equal to deflection x in equivalent spring: $x = -\frac{F}{k} = \delta = -\frac{4L^3F}{EwT^3} \Leftrightarrow k = \frac{EwT^3}{4L^3}$

Thermal Conductivity Through the Arms

The **rate of heat flow** through a beam of length *L* with area *A* is given by [6]:

with $k_e \approx \frac{RRR}{0.76} T$, $[k_e] = W/m \cdot K$

$$\dot{Q} \approx \frac{A}{L}k_e(T)\Delta T$$

Thermal Conductivity
Temperature Gradient

The **Residual Resistivity Ratio** (RRR) of copper ranges from 10 – 2000.

$$\Rightarrow \dot{Q}_{stage} = 3\dot{Q}_{arm} \approx \begin{cases} 3.9 \times 10^{-8} W \ (RRR = 10) \\ 7.6 \times 10^{-6} W \ (RRR = 2000) \end{cases}$$

By these estimates, even the **minimum possible heat flow rate** would be sufficient to cool the detector to the 10 **mK range**. We also used **OFHC copper**, meaning an **even higher heat flow rate**.

Suspension Performance

- 1-2 orders of magnitude of attenuation in desired frequency range (~2 kHz).
- Performance on par with the suspension built in the paper.
- Need to test in proper environment (at low temp. on fridge) to definitively say.



Outlook and Future Plans

- The suspension **appears to work**, though **proper characterization** and **resonance identification** must still be performed.
- **Proper thermal characterization** is still to come.
- **Optimization** of the material (**brass screws**, **gold plating** the copper, etc.).

- Detect dark matter.

Thank you!

References

[1] D. Antypas, et al., *arXiv preprint*, 2203.14915 (2022).
[2] A. Derevianko, *Phys. Rev. A* 97, 042506 (2018).
[3] A. Arvanitaki et al., *Phys. Rev. Lett.* 116, 031102 (2016).
[4] J. Manley et al., *Phys. Rev. Lett.* 124, 151301 (2020).
[5] M. de Wit et al., *Rev. Sci. Instrum.* 90, 015112 (2019).
[6] F. Pobell, *Matter and Methods at Low Temperatures, Second Edition*, Springer (1996).