

# MGB<sub>2</sub> CONDUCTORS FOR FUTURE DETECTOR MAGNETS

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## SUPERCONDUCTING MAGNETS FOR PARTICLE DETECTORS

Main characteristics:

- Large volume
- Moderate magnetic field (0.5 to 4 T)
- Transparency to particles is often required
- Generally, solenoidal or toroidal shape



At present, only Al stabilised NbTi conductors are used for detector magnets.

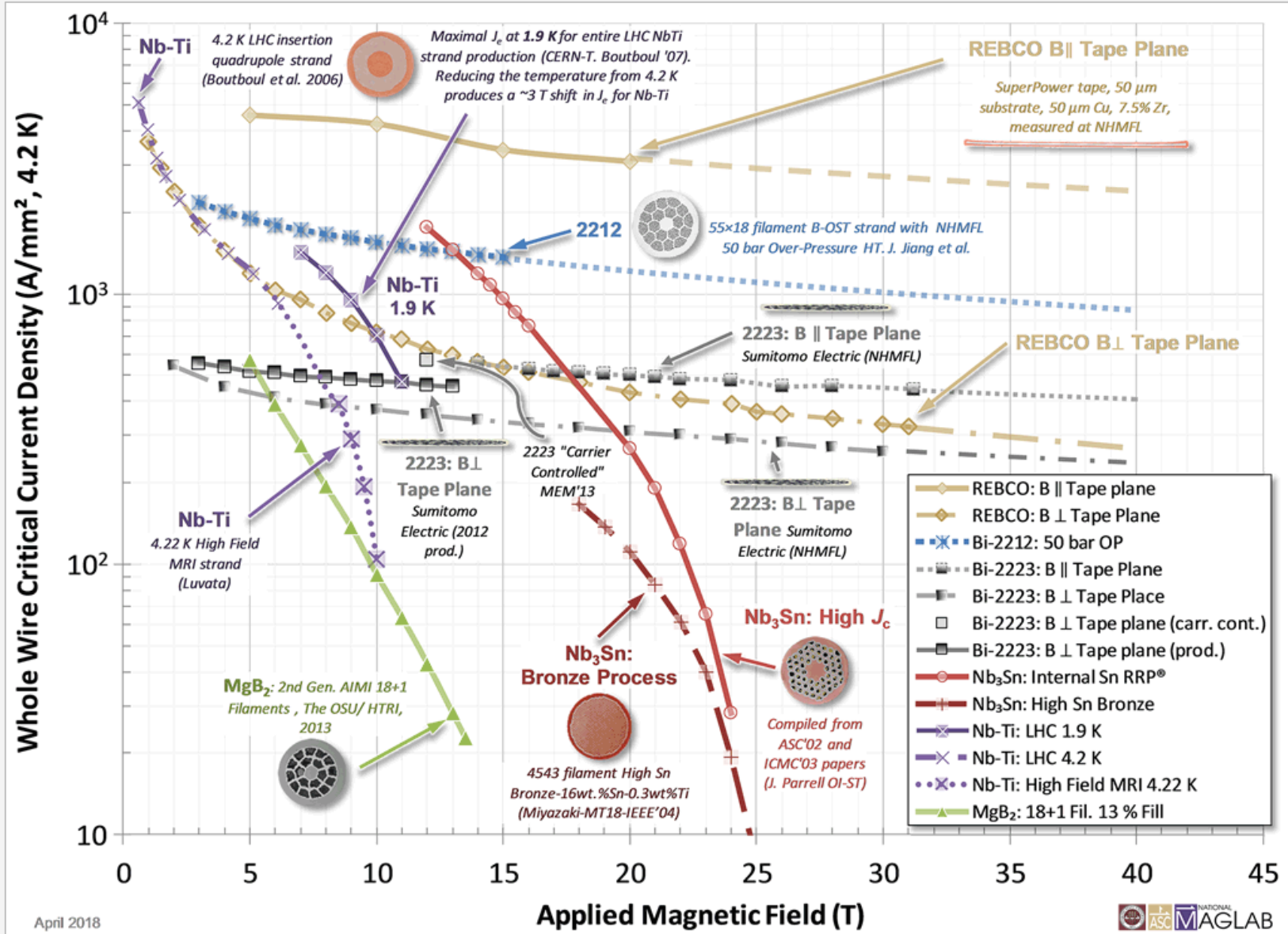
NbTi is ductile, relatively cheap and robust ( $J_C$  is not affected by mechanical stress).  
Al ensures high heat capacity per unit length and low resistance path for current.

However, fabrication of conductors requires cabling and co-extrusion.

Co-extrusion is an expensive and delicate industrial process.

Very few firms have the expertise to perform co-extrusion.

Would it make sense to use other superconductors ?



Other technical superconductors

REBCO (tape)  $T_c = 92 K$

BiSCCO 2223 (tape – Ag matrix)  $T_c = 108 K$

BiSCCO 2212 (Ag matrix)  $T_c = 96 K$

Nb<sub>3</sub>Sn  $T_c = 18 K$

MgB<sub>2</sub>  $T_c = 39 K$



MgB<sub>2</sub> is more expensive than NbTi but much cheaper respect to REBCO and BiSCCO

In situ: wires are prepared by powder-in-tube method using the precursors. MgB<sub>2</sub> is then obtained inside the wire by suitable heat treatment (about 700°C for a few tens of minutes)

Ex situ: wires are prepared by powder-in-tube method directly using MgB<sub>2</sub> powders.



MgB<sub>2</sub> has low reversibility field  $B_{irr}$  (if  $B \geq B_{irr}$  then  $J_c = 0$ )

Pure MgB<sub>2</sub>:  $B_{irr} \approx 12 T$

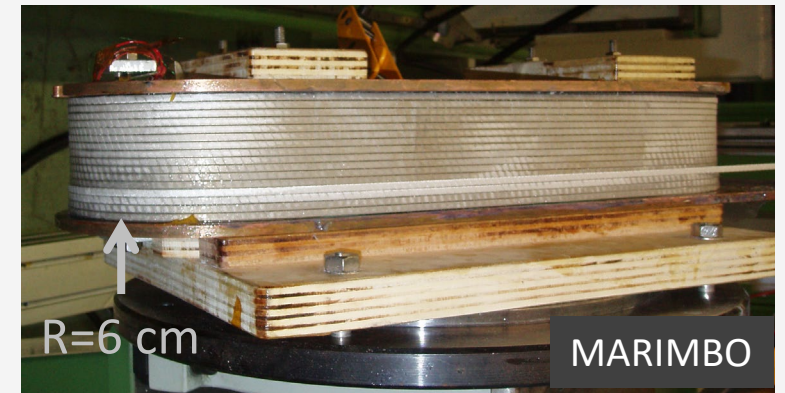
Doping increases  $B_{irr}$

But detector magnets must not generate high magnetic field

Generally  $B < 4 T$

Like all technical superconductors except NbTi, MgB<sub>2</sub> is brittle:  
for a given MgB<sub>2</sub> composite conductor, a critical bending radius does exist (order of few cm for a 0.65 mm thick tape).

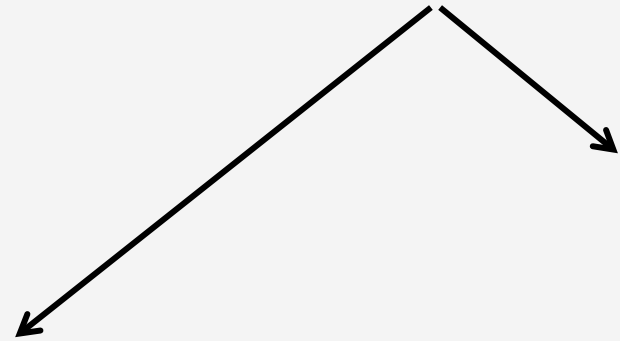
Not an issue for large magnets!



Winding of a racetrack coil  
with ex-situ MgB<sub>2</sub> tape



MgB<sub>2</sub> would allow operating the magnet at  $T > 10\text{ K}$  ( $T_c = 39\text{ K}$ )



More efficient cryogenics

Higher COP

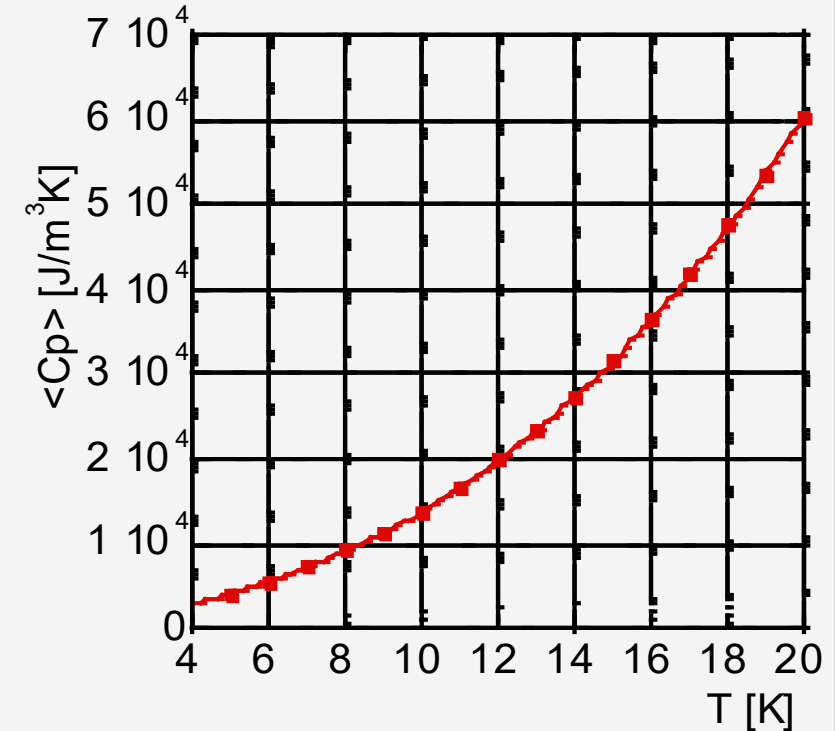
Better conduction cooling

$$\frac{K_{Al6061}@12\text{ K}}{K_{Al6061}@4.2\text{ K}} \approx 3$$

Higher energy density margin

$$\Delta e_{max} = \int_{T_{op}}^{T_{max}} c_{cond} dT$$

$$c_{cond} \propto \left(\frac{T}{\theta_D}\right)^3$$



Aluminium matrix is not necessary for stabilization.  
 It can be necessary/useful for quench protection.



First proposals about MgB<sub>2</sub> conductors coupled with Aluminium were related to space applications due to low weight requirement

P. Spillantini,

Superconducting magnets and mission strategies for protection from ionizing radiation in interplanetary manned missions and interplanetary habitats

Acta Astronautica, 68 (9–10), 2011, 1430-1439

R. Battiston, W. J. Burger, V. Calvelli, V. I. Datskov, S. Farinon, and R. Musenich

Superconducting Magnets for Astroparticle Shielding in Interplanetary Manned Missions

IEEE Trans. on Appl. Supercond., 23 (3), 2013, 4101604



EU FP7 project to study superconducting shields to protect astronauts from space radiation

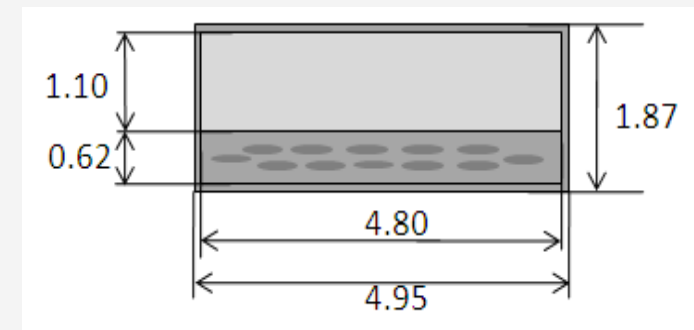
Conductor: Titanium clad MgB<sub>2</sub> tape + Aluminium strip

Ti/MgB<sub>2</sub> ratio 2.7/1.

75 μm thick insulation.

Total conductor cross section: 9.25 mm<sup>2</sup>.

Average mass density : 3000 kg/m<sup>3</sup>.



# Development of SR2S conductor prototype



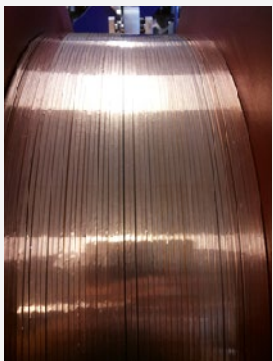
360 m Ti-MgB<sub>2</sub>



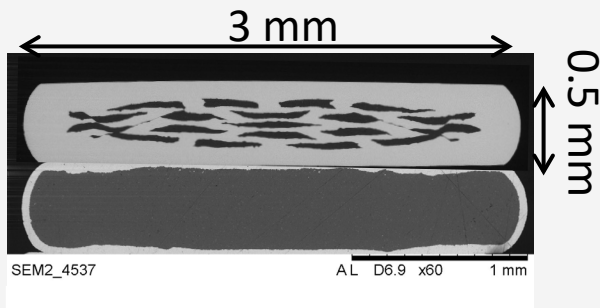
Ti-MgB<sub>2</sub> tape during copper plating



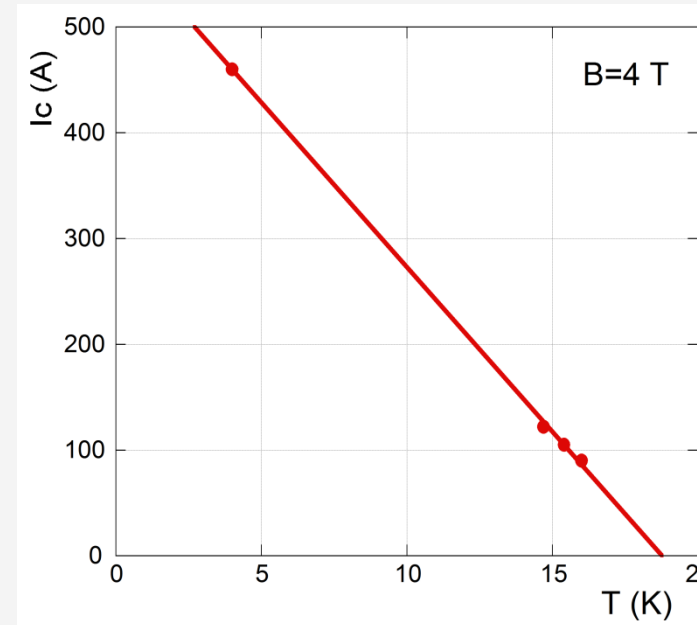
copper plated Ti-MgB<sub>2</sub> tape



Cu-Ti-MgB<sub>2</sub> tape



now



Problems occurred during aluminium tape soldering due to different thermal contractions. Due to tight schedule and limited funds, no further attempts were made to solder the aluminum tape.

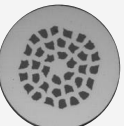


# Present status of ex-situ MgB<sub>2</sub> conductors

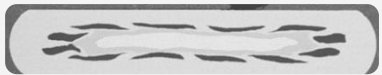
Wire 1



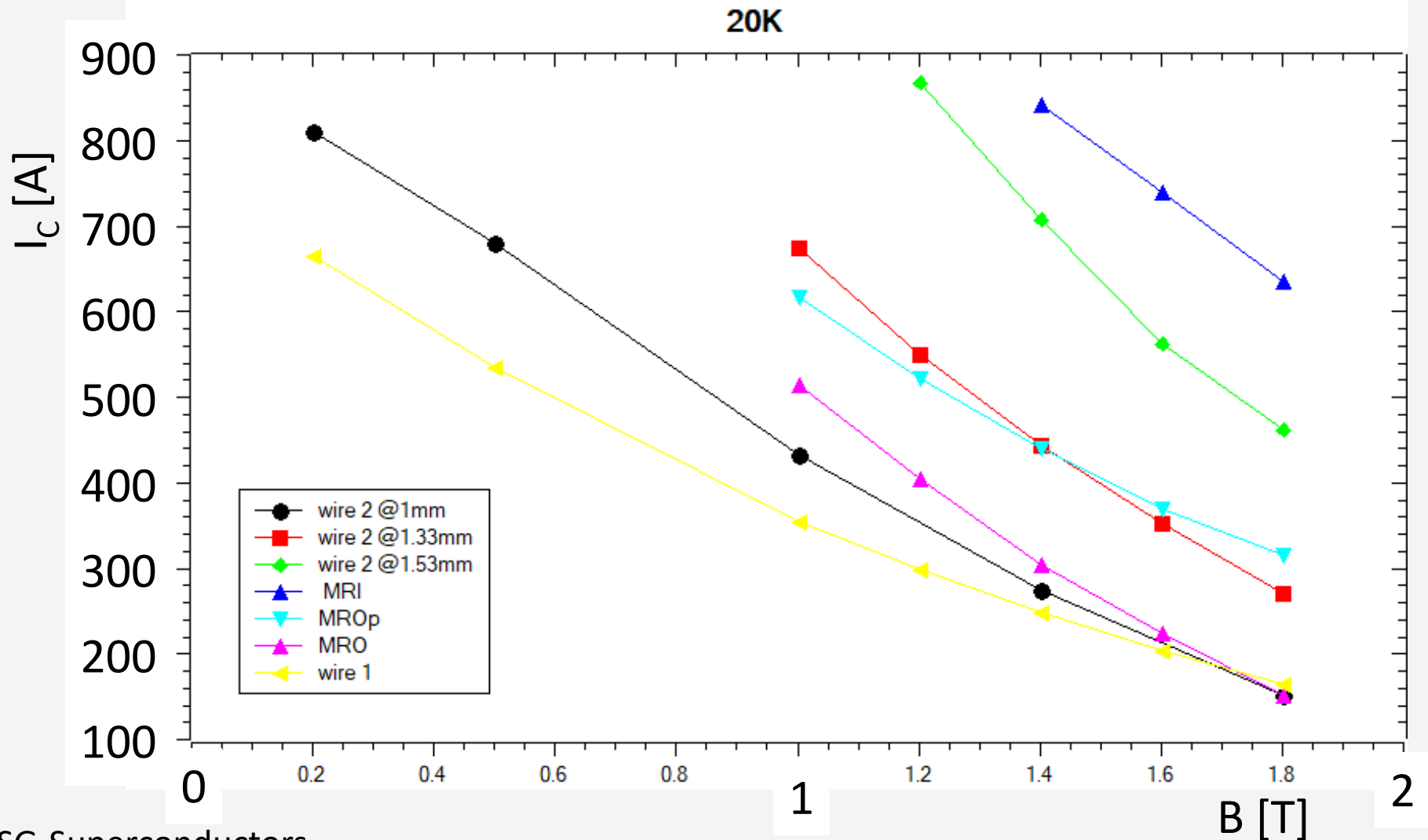
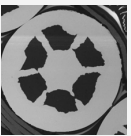
Wire 2

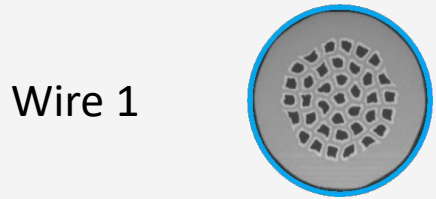


MRO/MRO+

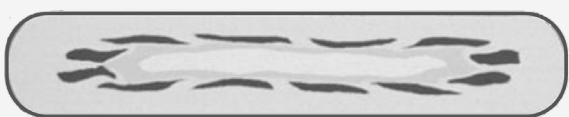


MRI (1,53 mm)

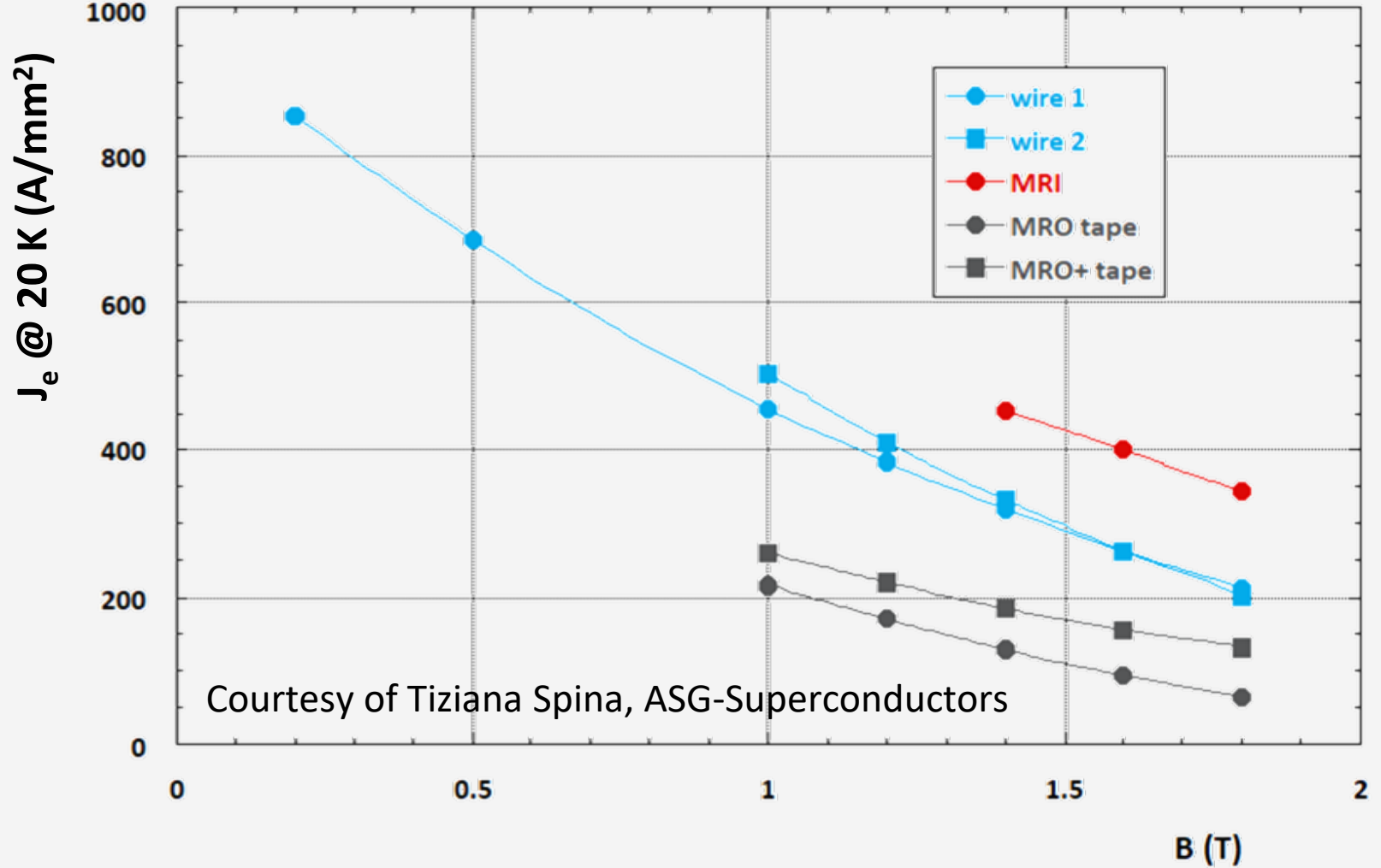




MRO/MRO+

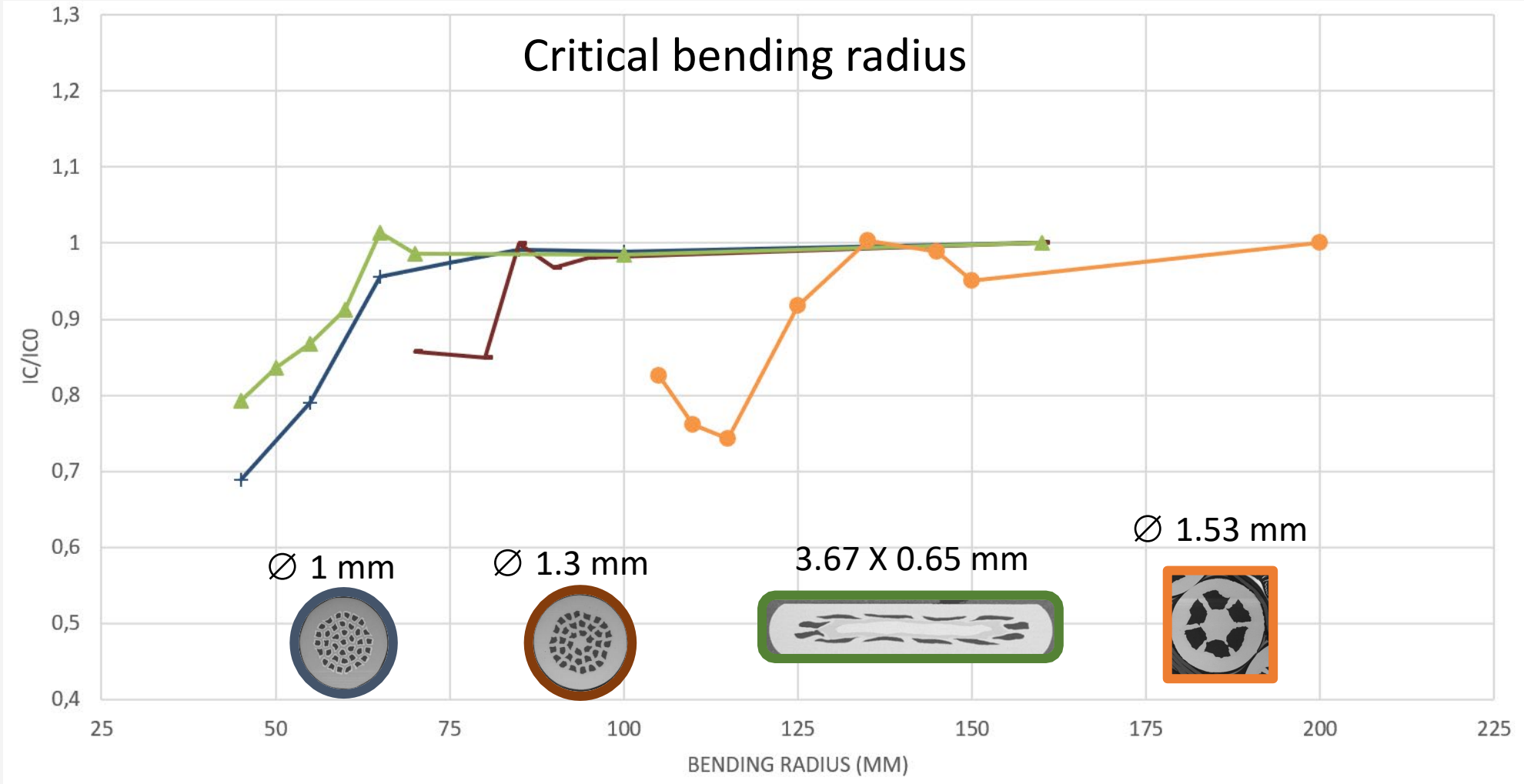


### Present status of ex-situ MgB<sub>2</sub> conductors



Courtesy of Tiziana Spina, ASG-Superconductors

$$J_e(15K, 2T) \approx 400 - 600 \text{ A/mm}^2$$



Courtesy of Tiziana Spina, ASG-Superconductors

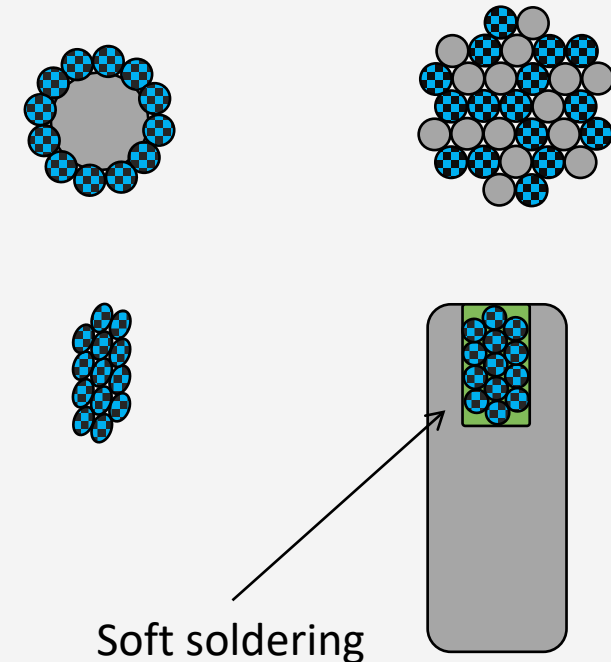
In MgB<sub>2</sub> magnets operating at  $T > 10 K$  stability is due to the high specific heat

Aluminium in parallel is for protection:

- Good bonding between cable and aluminium is not necessary (no co-extrusion)
- High purity aluminium is not necessary

In principle, it is possible to use conductors obtained by cabling MgB<sub>2</sub> wires and aluminium wires

Limited deformation is possible before heat treatment to obtain an almost flat cable

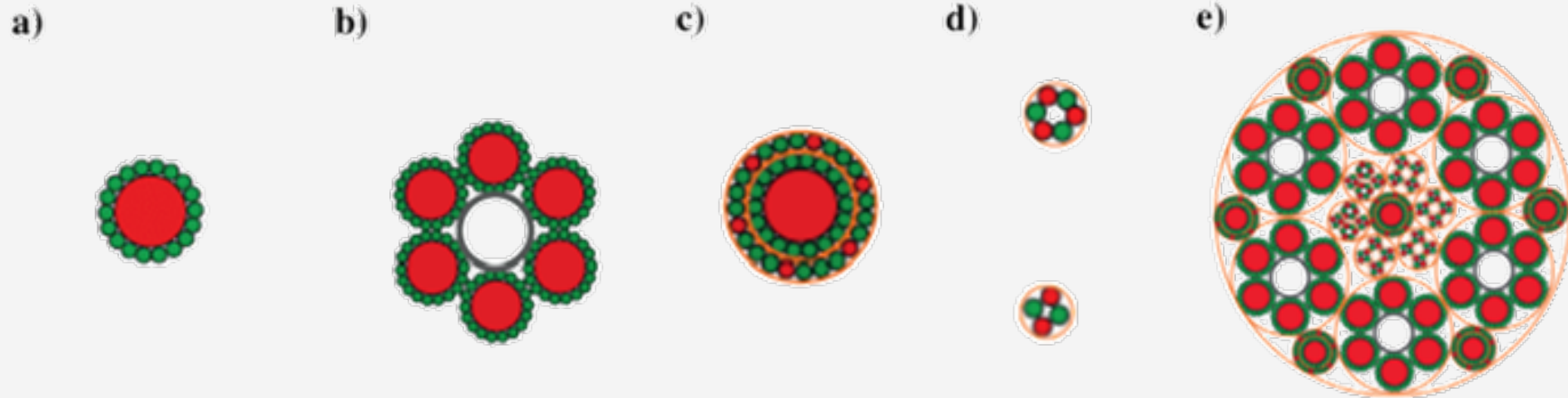




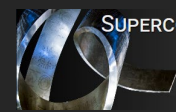
A remarkable example of MgB<sub>2</sub> wire cabling:  
 the LHC superconducting links



A. Ballarino, Supercond. Sci. Technol. 27 (2014) 044024



**Figure 5.** Cables made with MgB<sub>2</sub> round wire. (a) Sub-unit of 20 kA cable,  $\Phi \sim 6.5$  mm; (b) 20 kA cable,  $\Phi \sim 19.5$  mm; (c) concentric 2×3 kA cable,  $\Phi \sim 8.5$  mm; (d) 0.4 kA cable (top) and 0.12 kA cable (bottom),  $\Phi < 3$  mm; (e) 165 kA cable assembly for LHC P1 and P5 (6×20 kA, 7×2×3 kA, 4×0.4 kA, 18×0.12 kA),  $\Phi \sim 65$  mm.



## Summary

MgB<sub>2</sub> could be an excellent candidate to replace NbTi in detector magnets

Detector magnets based on MgB<sub>2</sub> conductors can be operated at  $T > 10K$

Consequences of higher operative temperature are:

- higher stability (aluminium is required for protection, not as stabiliser)
- higher thermal conductivity (better indirect cooling)
- higher refrigerator COP

R&D is necessary to develop suitable conductors.

Detector magnet design should be rethought based on MgB<sub>2</sub> conductor features (as an example, the quench issue of MgB<sub>2</sub> detector magnets could be faced via controlled insulation technique.)