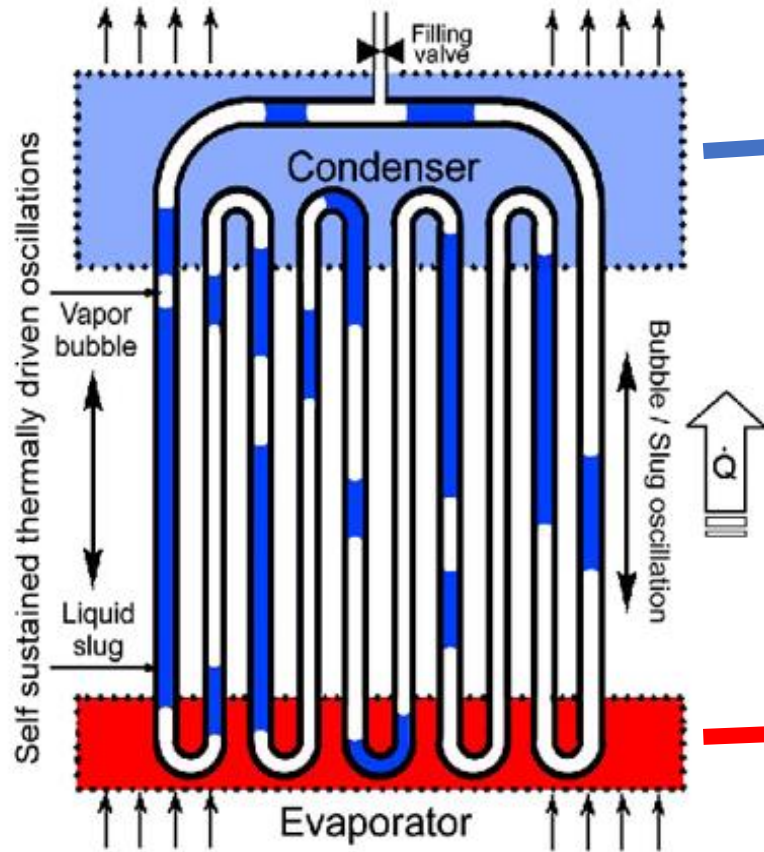


Nitrogen-based Pulsating Heat Pipes with Varied Configurations

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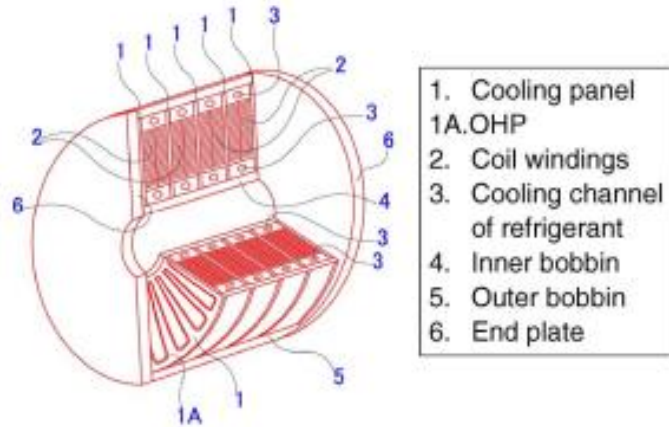
What is a Pulsating Heat Pipe



Schematic of a Pulsating Heat Pipes (PHP) [1]

- When the vapor bubble flows into the condenser section, it condenses into liquid resulting in a **pressure decrease**.
- When heat is applied on the evaporator, the pressure of the vapor plug is increased.
- The **increased vapor pressure** helps the fluid overcome the capillary forces, gravitational forces.

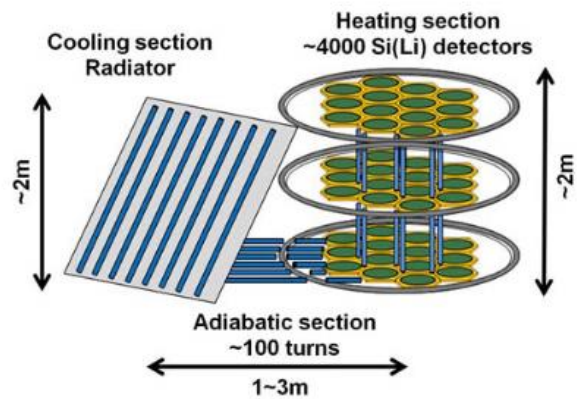
Application



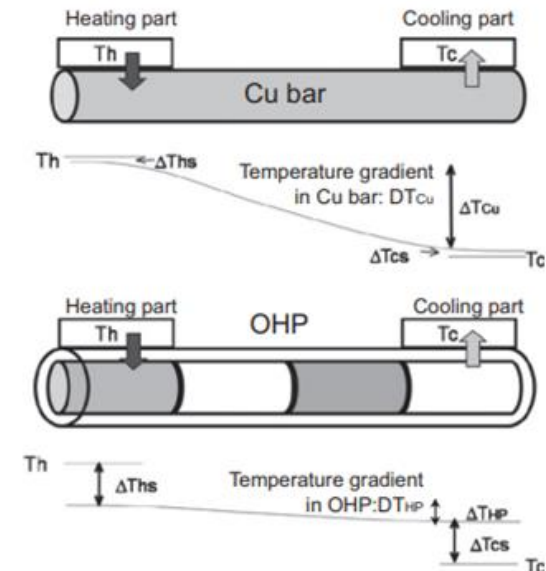
The PHP embedded in the HTS magnet [2]



MRI

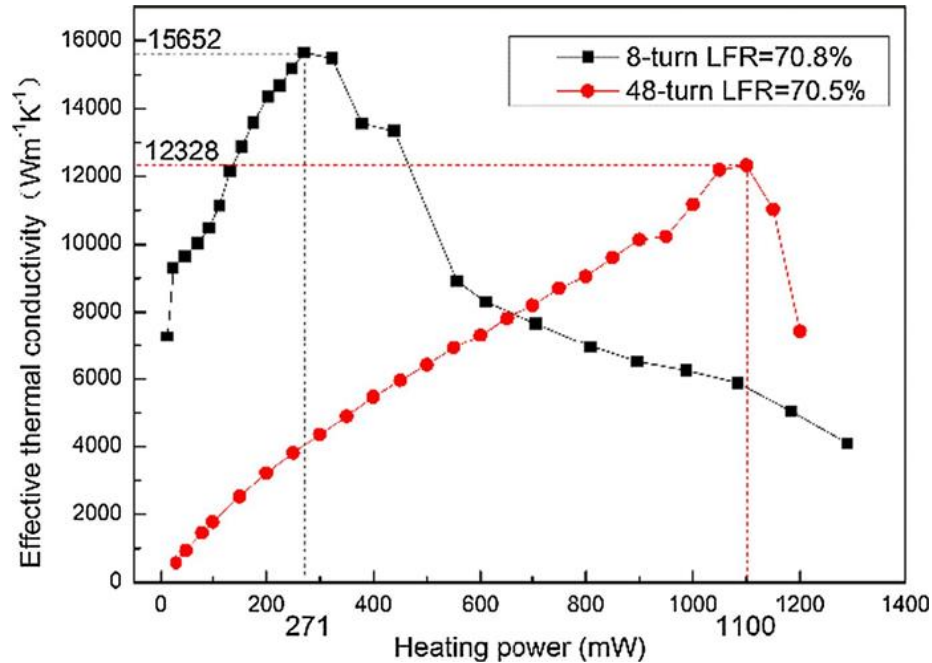


The PHP prototype cools down the spectrometer

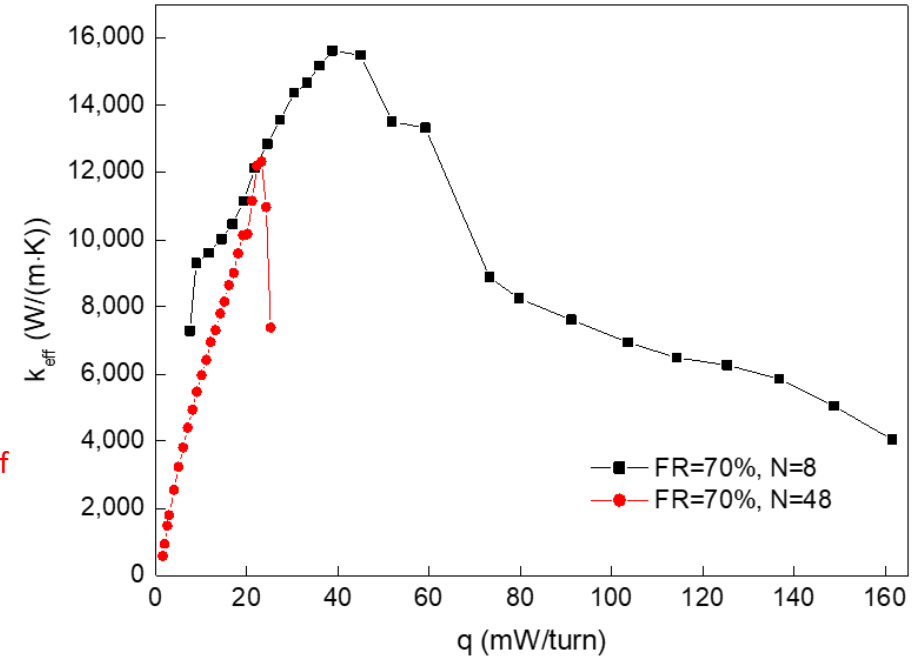


PHP has a much lower ΔT [3]

Motivation



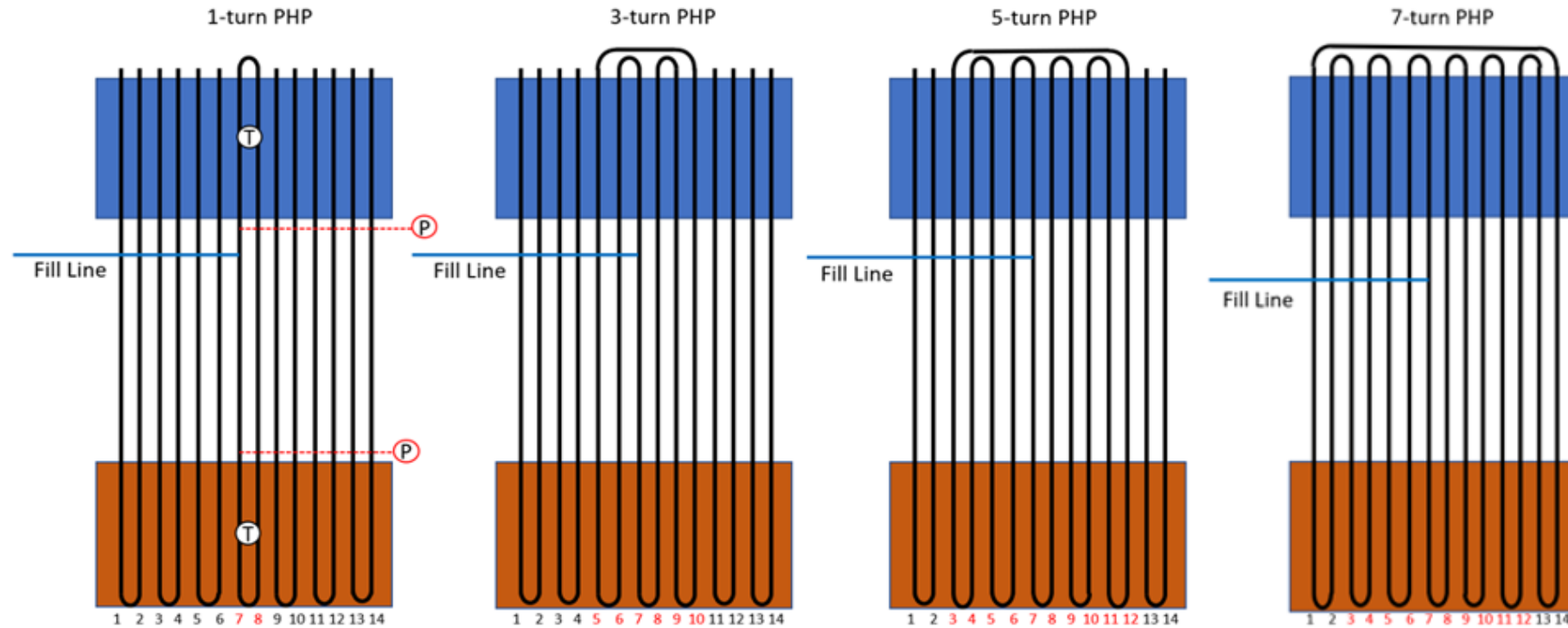
The x-axis is in terms of head load per turn



PHP with a small number of turns has good thermal performance at a lower heat load while a PHP with a large number of turns has a good heat transfer performance at a higher heat load.

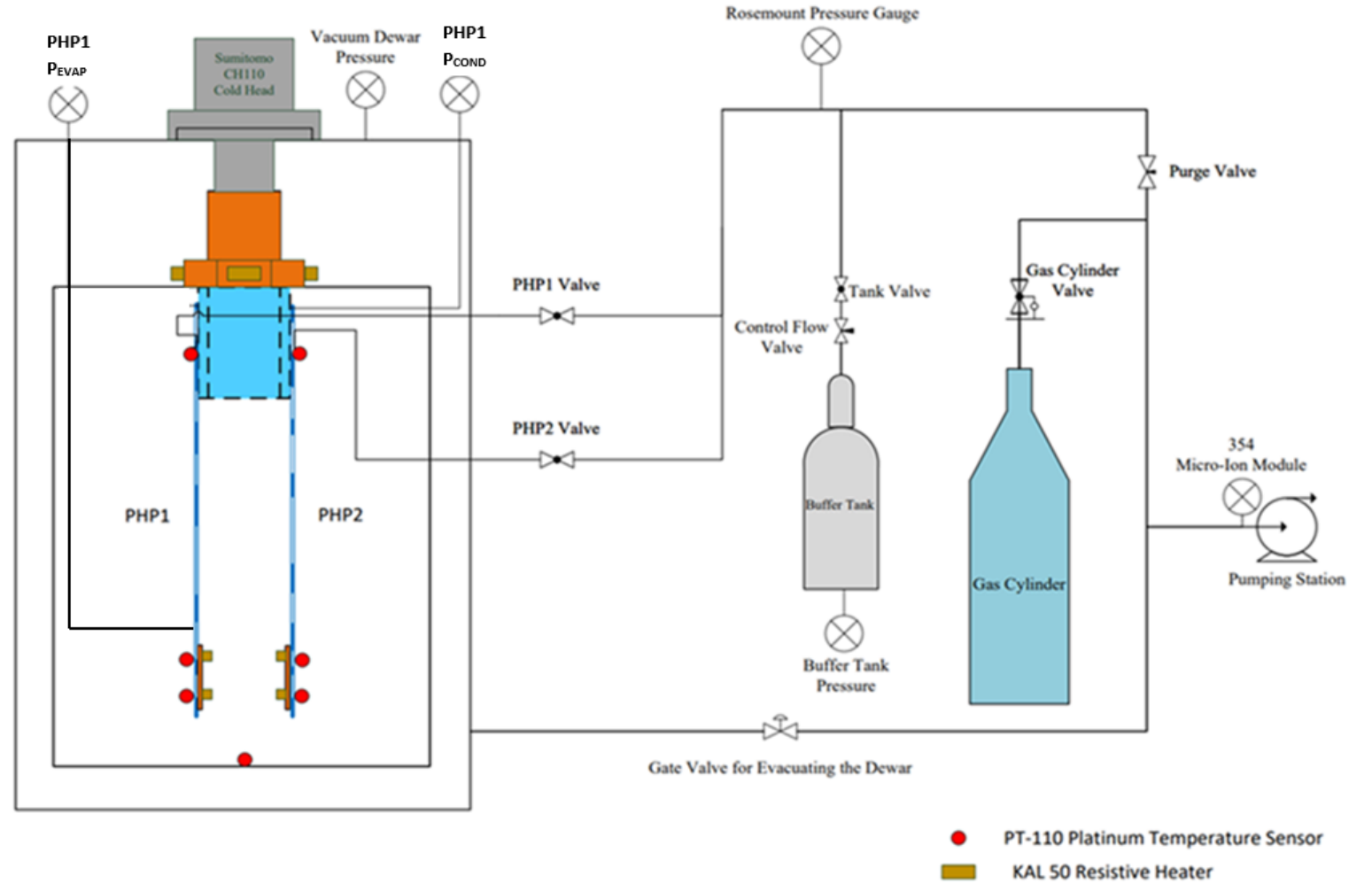
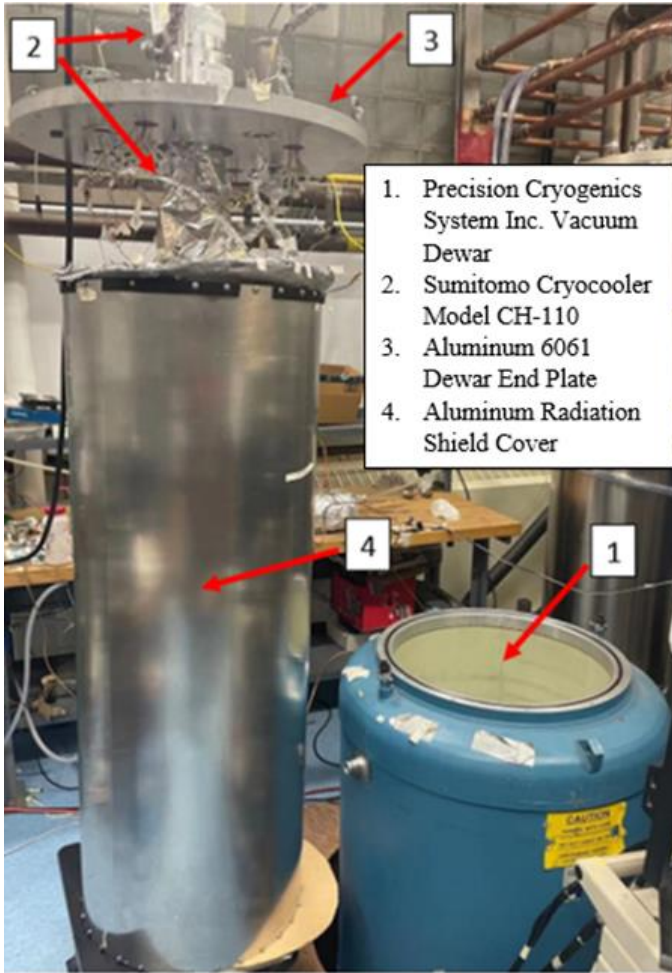
Although 48-turn can achieve maximum heat capacity at 1200[mW], but if we split 1200[mW] on a total of 48 turns, each turn only takes around 25[mW].

Motivation

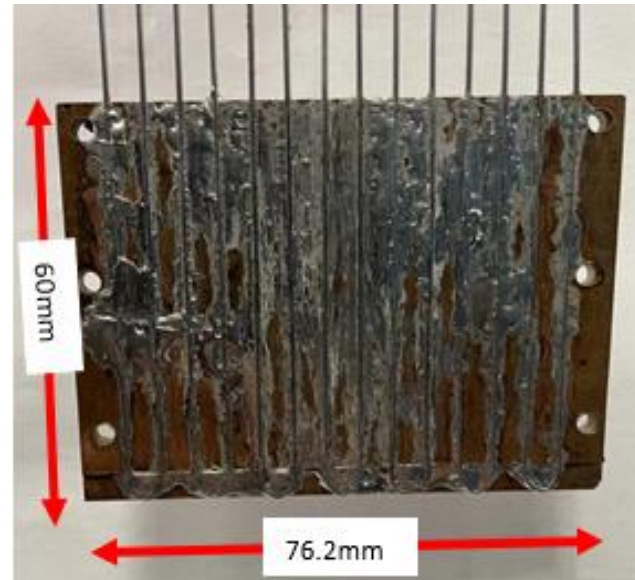
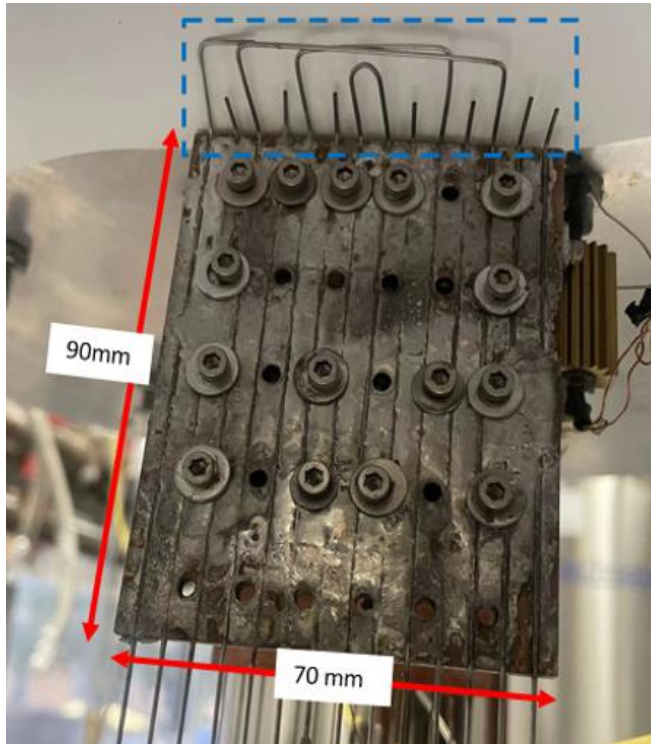


The number of turns of my PHP can change from 1 to 3 to 5 and 7 turns. With this design, we will be able to determine the optimal heat transfer per turn for a nitrogen PHP.

Experimental Setup

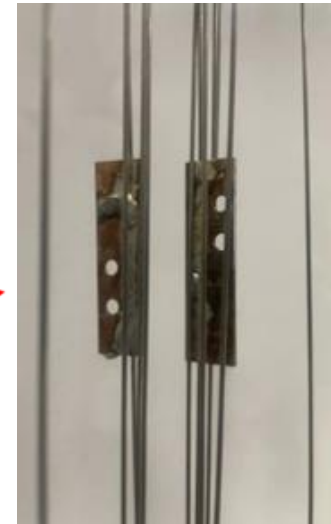
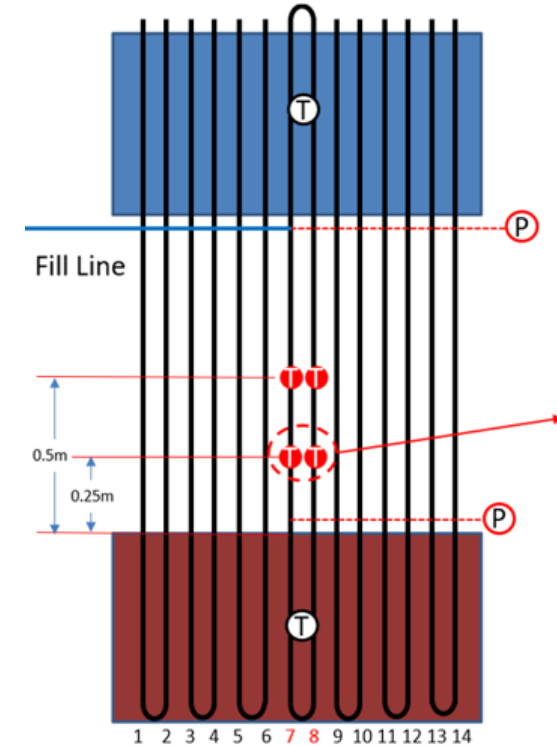


Experimental Setup



The Condenser (left) and Evaporator (right) sections

- The adiabatic section between the condenser and evaporator is 1m.
- The capillary tube is made from 304 stainless steel with an I.D. of 0.5mm and an O.D. of 0.8mm.



Locations of PRTs on each PHP are marked as 'T' and the locations of the pressure sensors are marked as 'P' in the schematic. Only PHP1 has pressure transducers installed. The locations

Experimental Conditions

Experimental Test	T _{cond} [K]	Initial Fill Ratio [%]
1	84.5	50
2	84.5	63
3	84.5	75
4	77.4	50
5	77.4	63
6	77.4	75

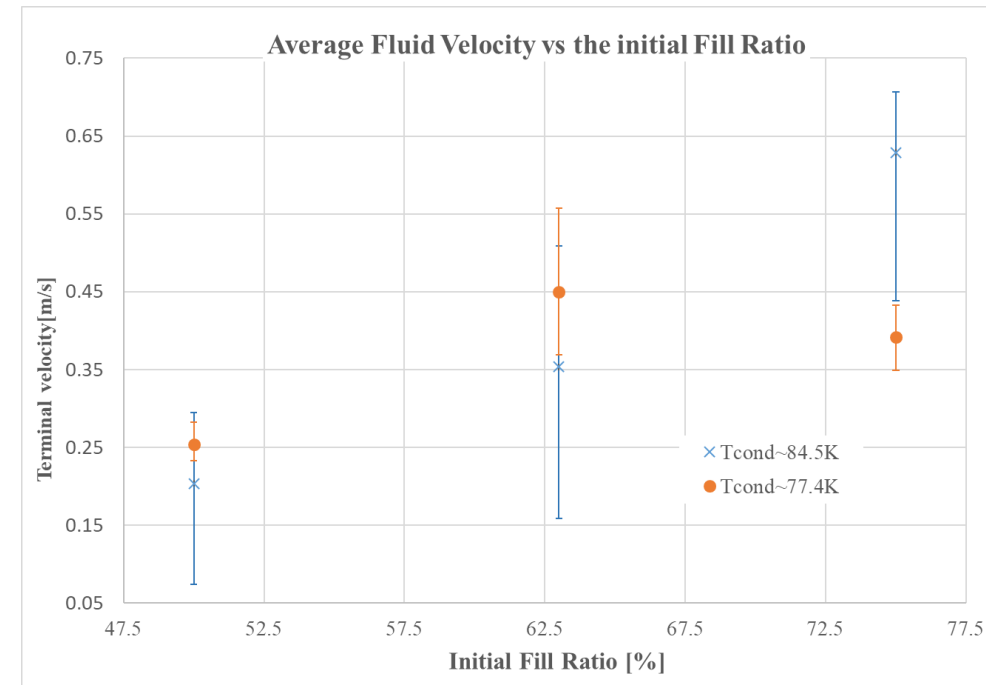
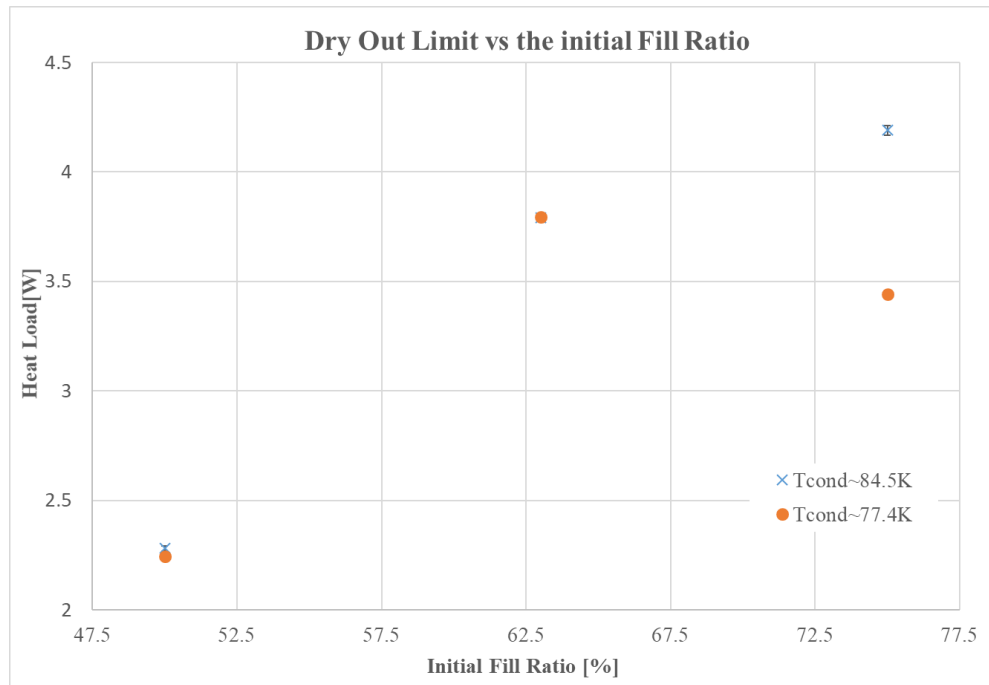
$$\text{Fill Ratio: } FR = \frac{Vol_{liquid}}{Vol_{PHP}}$$

A total of six experimental tests have been conducted on the PHP with two different condenser temperatures and three different fill ratios.

The heat transfer performance of the PHP is evaluated by the effective thermal conductivity:

$$k_{eff} = \frac{QL}{NA_c(\bar{T}_e - \bar{T}_c)}$$

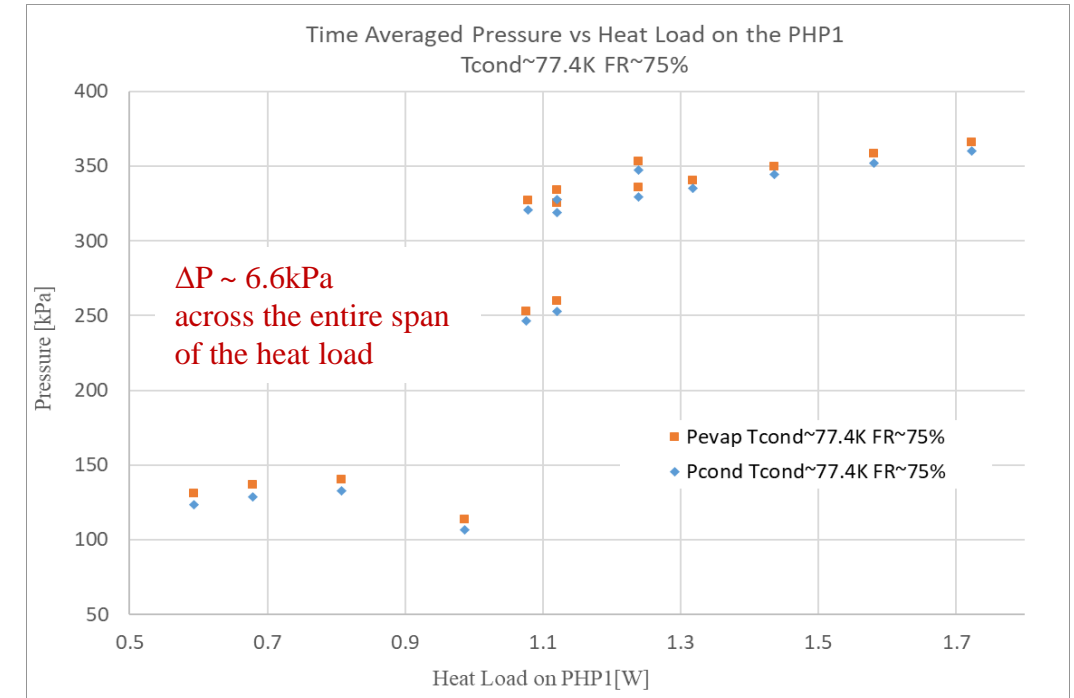
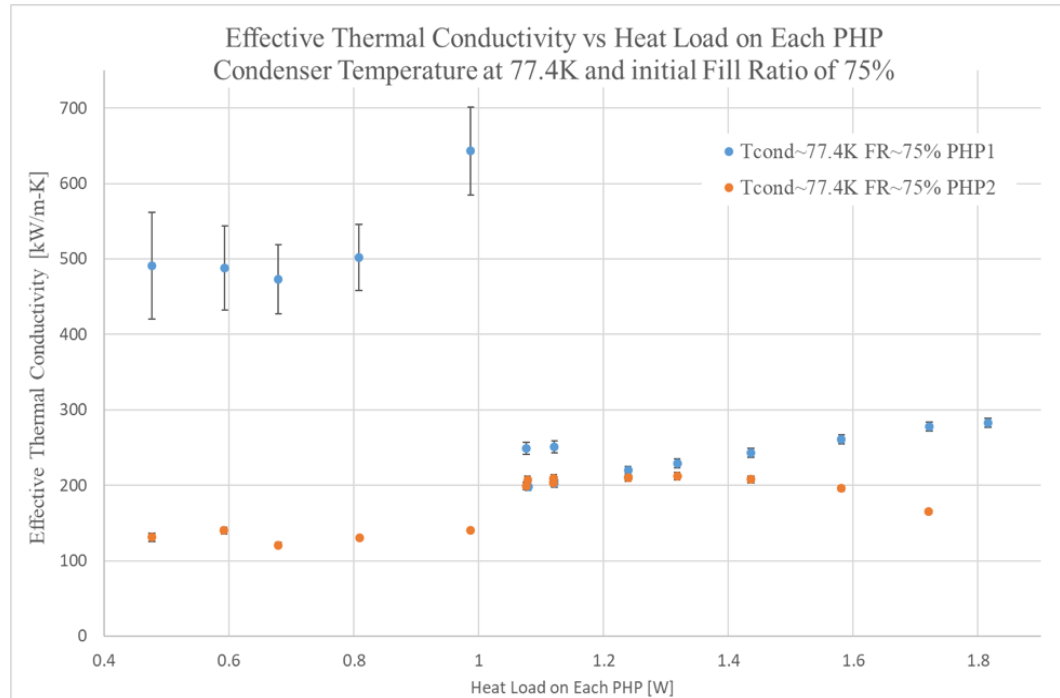
Experimental Results



- The maximum dry-out limit of the PHP assembly is observed at **4.19 W** of total heat load at the condenser temperature of 84.5 K and the initial fill ratio of 75%
- The optimal effective thermal conductivity of PHP1 is **1,048,000 W/m-K** when 0.81 W is applied on each PHP (a total of 1.62 W on the PHP assembly) at the condenser temperature of 84.5 K and the initial fill ratio of 63%.
- The optimal effective thermal conductivity of PHP2 is **838000 W/m-K** when 1.32 W is applied on each PHP (a total of 2.64 W on the PHP assembly) at the condenser temperature of 84.5 K and the initial fill ratio of 63%..

Experimental Results

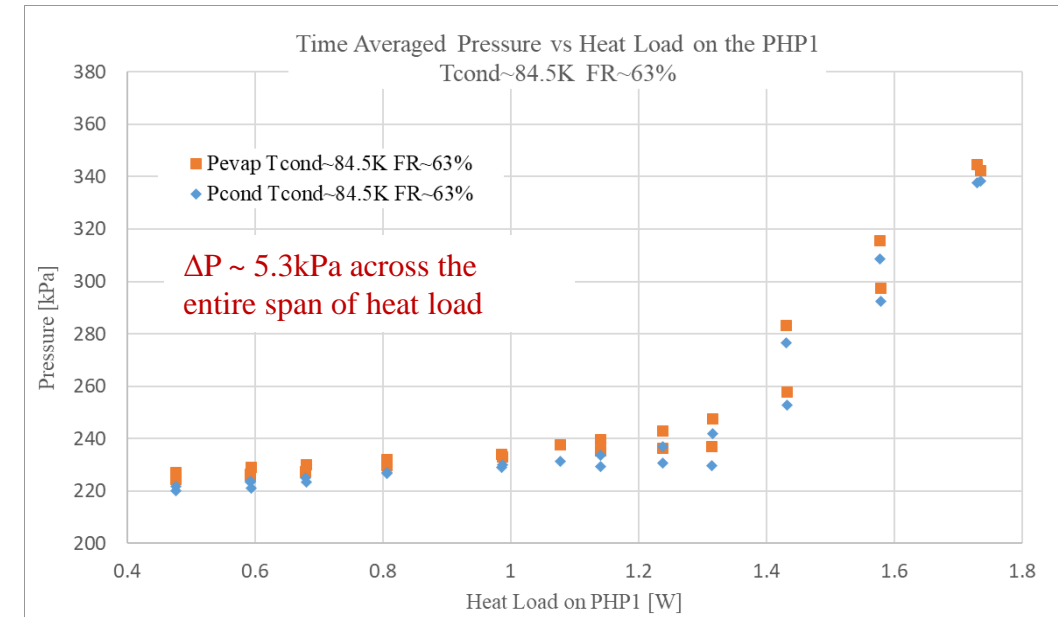
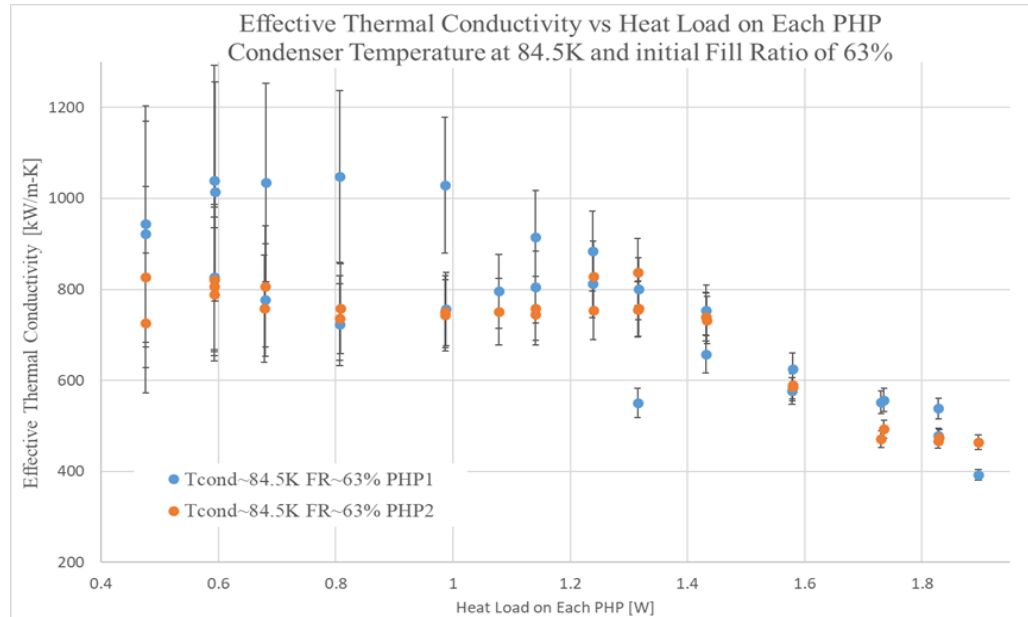
Condenser temperature of 77.4K and initial Fill Ratio of 75%



- The PHP reaches dry-out and is then **re-booted** at the heat load of 1.08 W for each PHP.
- In the reboot run, both PHP subsections can operate with the heat load on each PHP from 1.08 W to 1.72 W. PHP2 dries out at a heat load of 1.82 W.
- After the reboot, the difference in the effective thermal conductivity between PHP1 and PHP2 is much smaller. Between 1.08 W and 1.32 W, the percentage difference is less than 10%.

Experimental Results

Condenser temperature of 84.5K and initial Fill Ratio of 63%



- PHP1 exhibited dry-out behavior and rebooted at both 1.32 W and 1.43 W on each PHP.
- After the dry-out limit was reached, various experiment runs at heat load levels of 0.48 W, 0.60 W, 0.68 W, 0.81 W, 0.99 W, 1.32 W, 1.43 W, and 1.73 W were repeated.
- The difference in the time-averaged mean pressure between the original and repeated runs is insignificant, even though the difference in effective thermal conductivity of PHP1 is significant.

Summary

- The maximum dry-out limit of the PHP assembly is observed at 4.19W of total heat load at the condenser temperature of 84.5K and initial FR of 75%
- PHP subsection dries out at moderate heat load but can be rebooted with continued performance to higher heat loads.
- The effective thermal conductivity of the PHP subsection differs drastically before and after the reboot process.
- Gradual increase in the overall system pressure is observed in the FR of 50% and 63% fill ratio tests. The huge leap in the overall system pressure after the PHP reboot is observed in the 75% fill ratio runs.
- For future measurements, the PHP test rig will be modified to operate with 3-turn, 5-turn, and 7-turn PHPs in the parallel configuration but using the same condenser temperature and fill ratio conditions as with the single-turn PHP.

Thank You

Any Question?

This project is done under the support of Sumitomo (SHI)Cryogenics America.

- [1] P. Charoensawan, S. Khandekar, M. Groll and P. Terdtoon, "Closed loop pulsating heat pipes: Part A: parametric experimental investigations," *Applied Thermal Engineering*, vol. 23, no. 16, pp. 2009-2020, 2003.
- [2] K. Natsume, K. Mito, N. Yanagi and H. Tamura, "Development of a flat-plate cryogenic oscillating heat pipe for improving HTS Magnet Cooling," *Physics Procedia*, vol. 45, pp. 233-236, 2013.
- [3] Natsume, Kyohei, et al. "Heat transfer performance of cryogenic oscillating heat pipes for effective cooling of superconducting magnets." *Cryogenics* 51.6 (2011): 309-314.
- [4] Li, Monan, Laifeng Li, and Dong Xu. "Effect of number of turns and configurations on the heat transfer performance of helium cryogenic pulsating heat pipe." *Cryogenics* 96 (2018): 159-165.