# Usage of manifolds in electromagnetism and superconductor modelling

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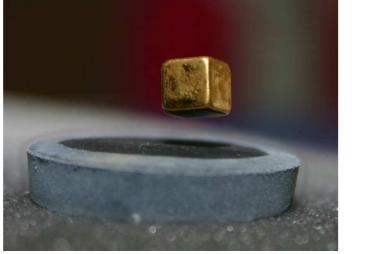


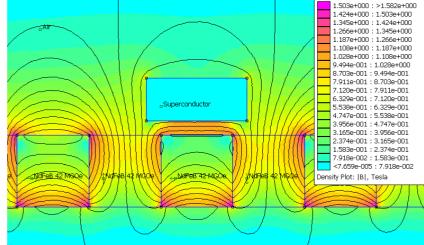


#### Contents

- Motivation of the topic / Introduction
- Manifolds
- Practical examples
- Symmetry in field problems (especially helicoidal)
- Modelling twisted conductors in 2D without loss of any information
  - Magnetostatics: defining critical current of conductor in self-field
  - Eddy current problems: hysteresis losses of a conductor
- Summary

• Phenomena are not coordinate dependent, but only evaluation in computations requires coordinates, or parametrizations, to present the problem.





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• Phenomena do not depend on metric, but material characterization is done in predetermined metric, because it enables comparison and unified approach.



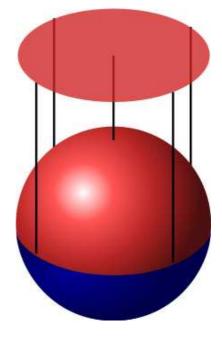
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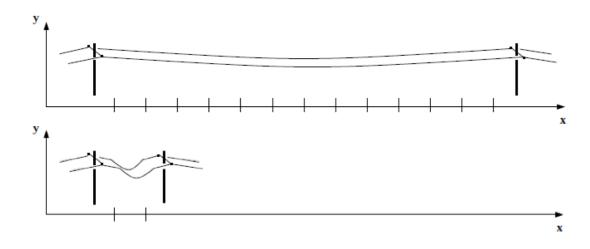
Loosely: A generalization of some coordinate system, like cartesian or cylindrical, is known in mathematics by name **manifold**.

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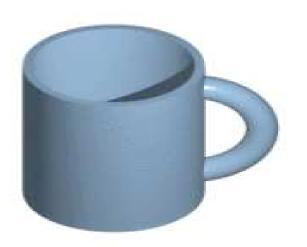


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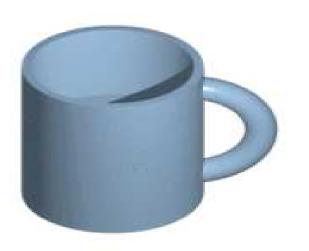


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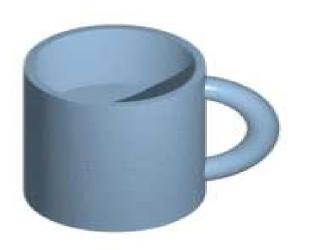
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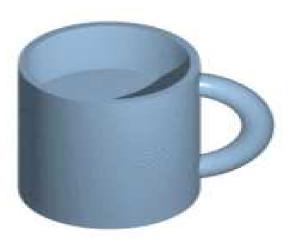
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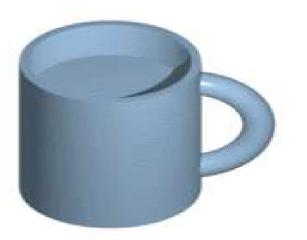
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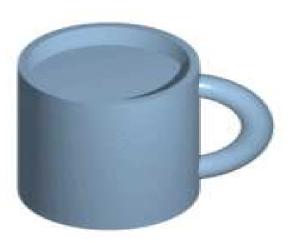
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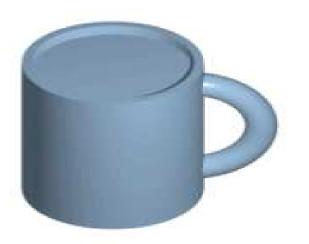
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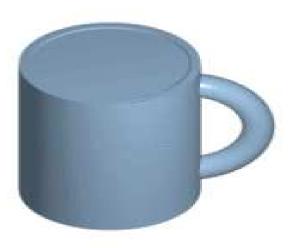
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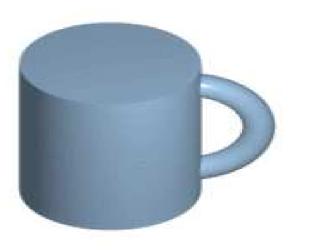
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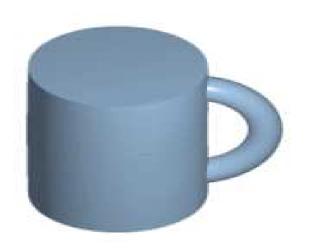
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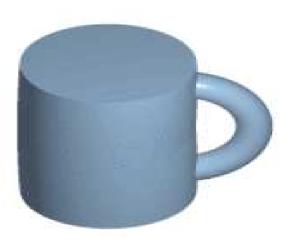
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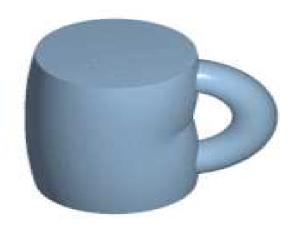
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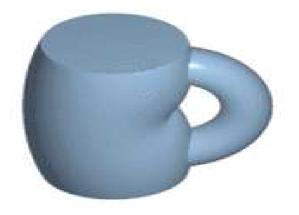
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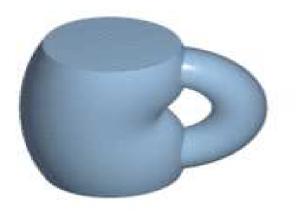
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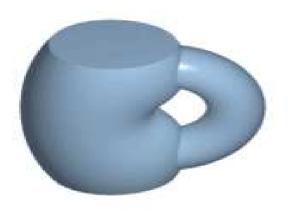
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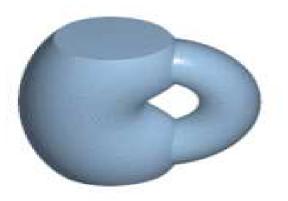
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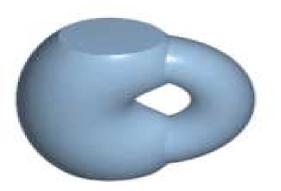
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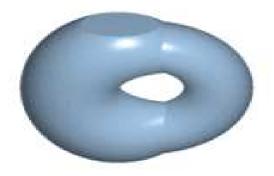
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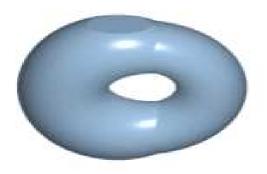
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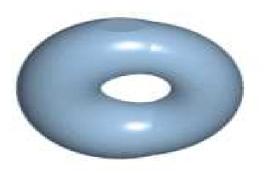
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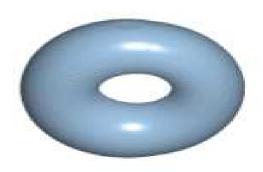
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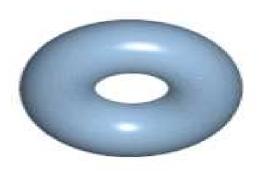
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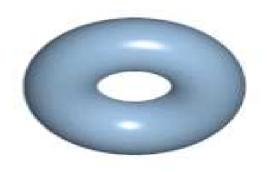
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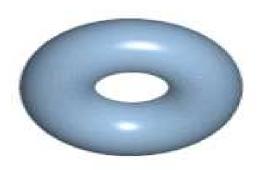
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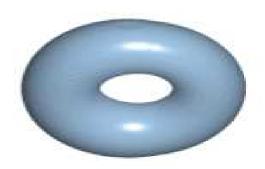
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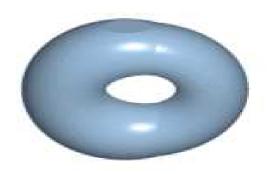
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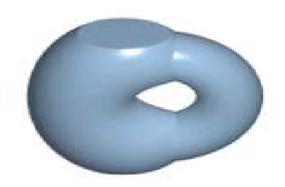
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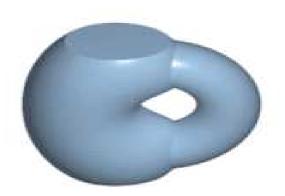
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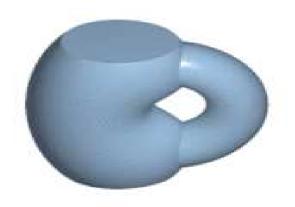
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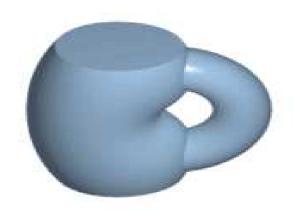
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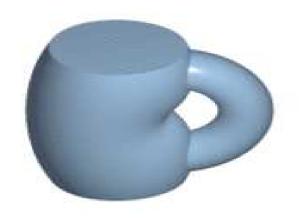
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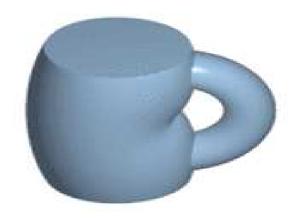
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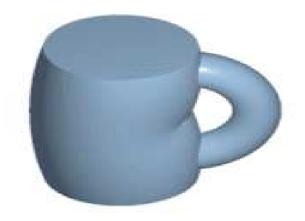
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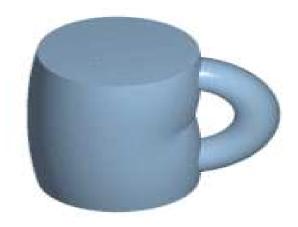
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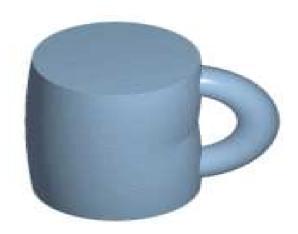
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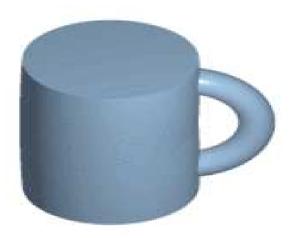
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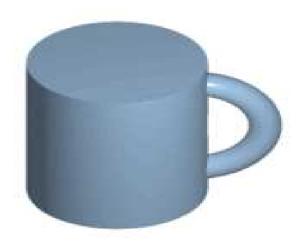
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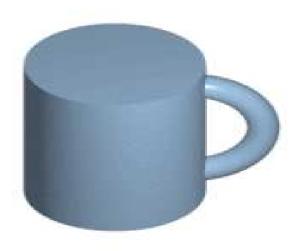
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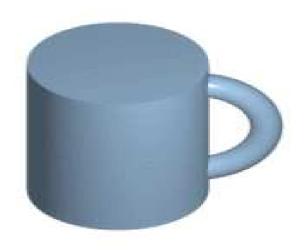
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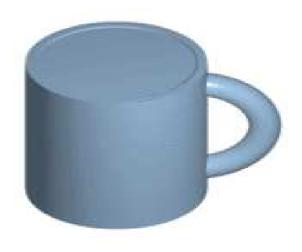
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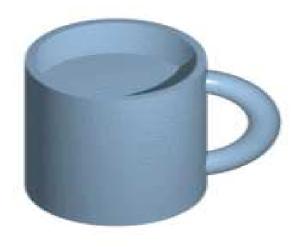
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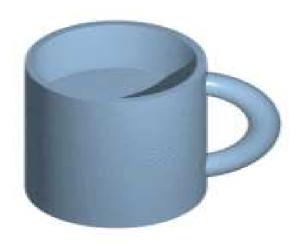
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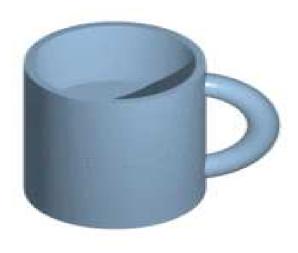
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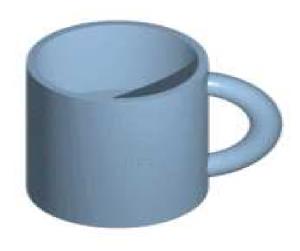
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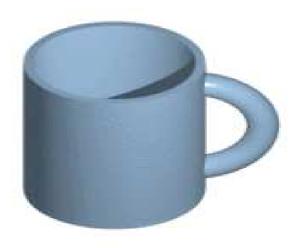
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- The shape does not play that big role in manifold, only topology and ...



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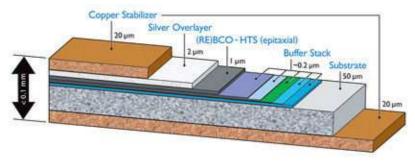


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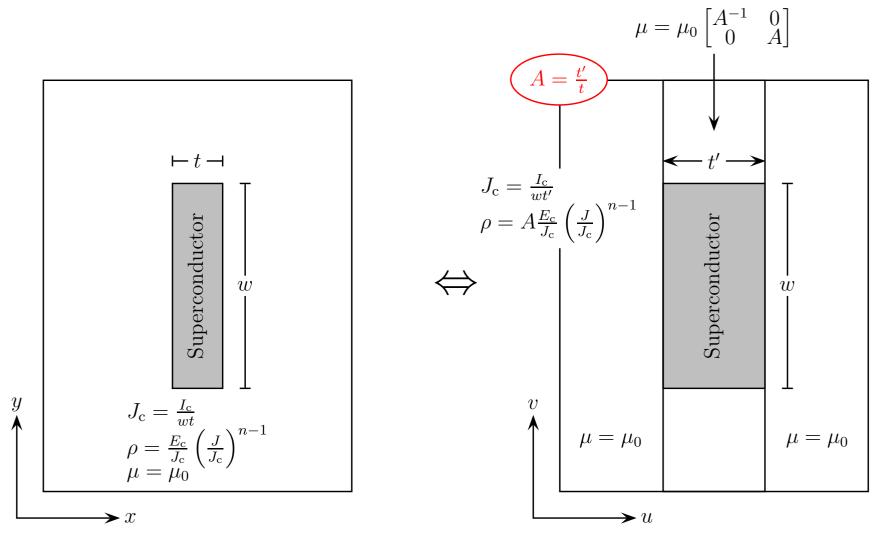
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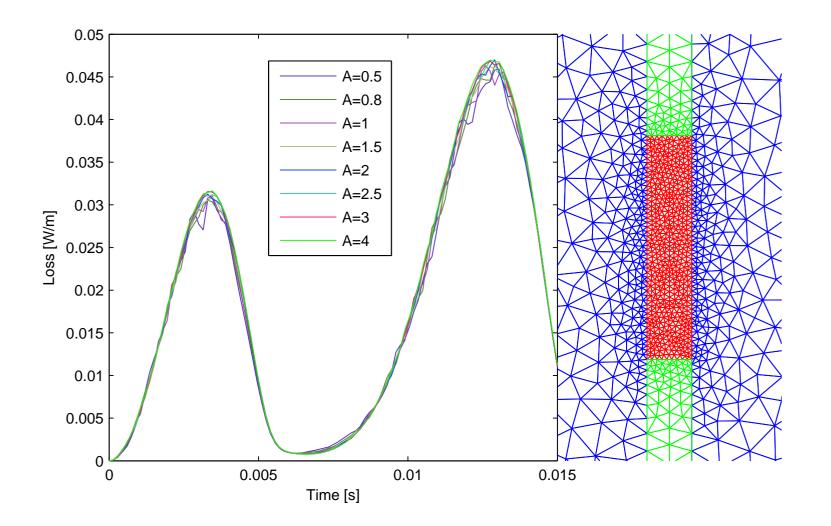
[SuperPower]

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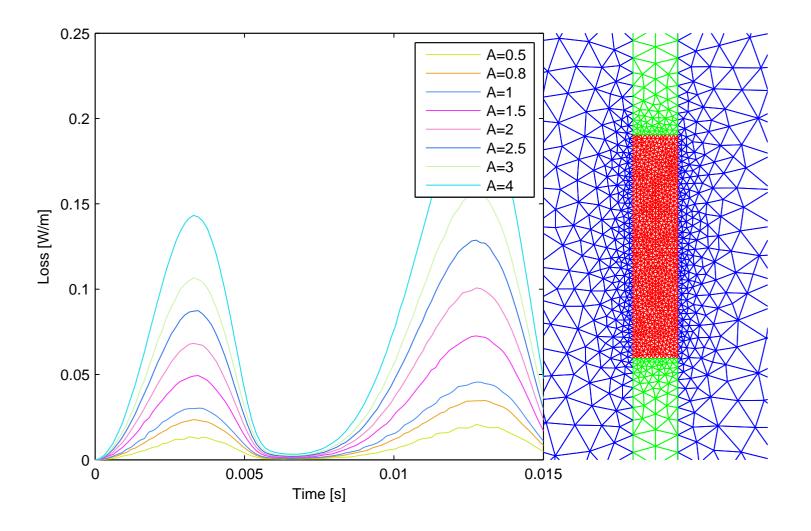
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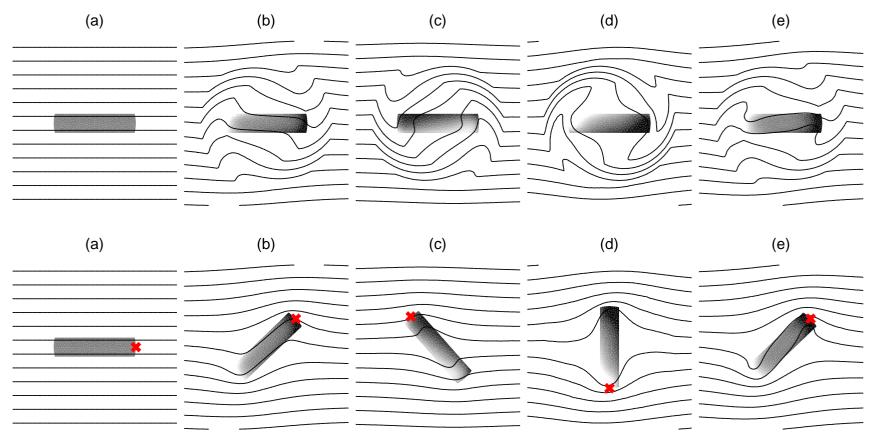
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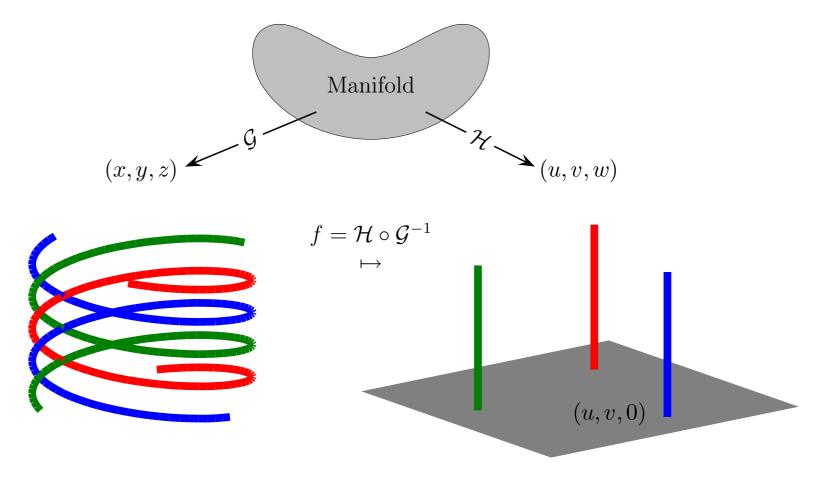
# **Examples of using manifold originating modelling**

- In general: modelling is not restricted to what we see and as we see it.
- Simulation of movement with rigid meshes.



# **Examples of using manifold originating modelling**

- In general: modelling is not restricted to what we see and as we see it.
- Being helicoidal is not absolute (compare being a doughnut or a mug).



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- Symmetry does not require that certain field components vanish at certain coordinate frames.

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• Example: translation symmetry  $F(x, y, z) = F(x, y, z + a) \quad \forall a \in \mathbb{R}$ 

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• Example: reflection symmetry F(x, y, z) = F(-x, y, z)

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• Example: combination of translation and rotation symmetry in a helicoidal structure in Cartesian coordinates  $F(x,y,0) = F(x\cos(\alpha z) + y\sin(\alpha z), -x\sin(\alpha z) + y\cos(\alpha z), z) \quad \forall z \in \mathbb{R}$ 

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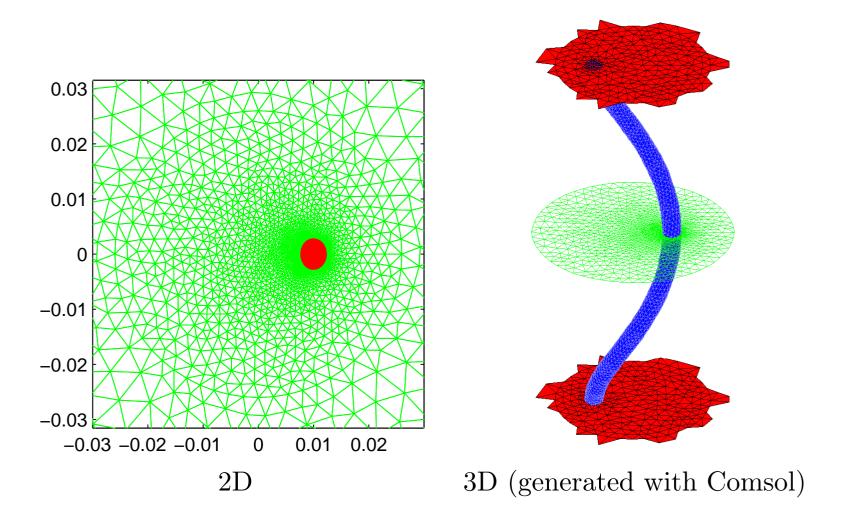
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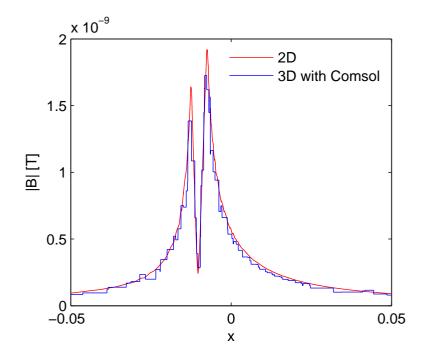
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- Presentation of the domain in another coordinates than Cartesian can be more convenient for computations → we get rid of rotation and work only with translation symmetry.

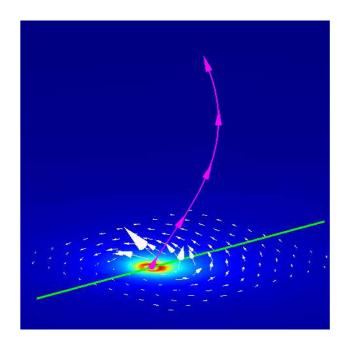
Theory of Riemannian manifolds tells us how to express with numbers the material properties in this new coordinate system.

#### SYMMETRY ANIMATION

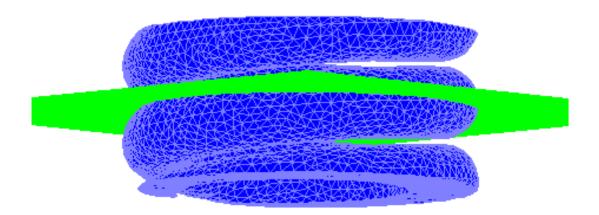
Twist pitch = 10 cm, filament/conductor radius = 2.5 mm

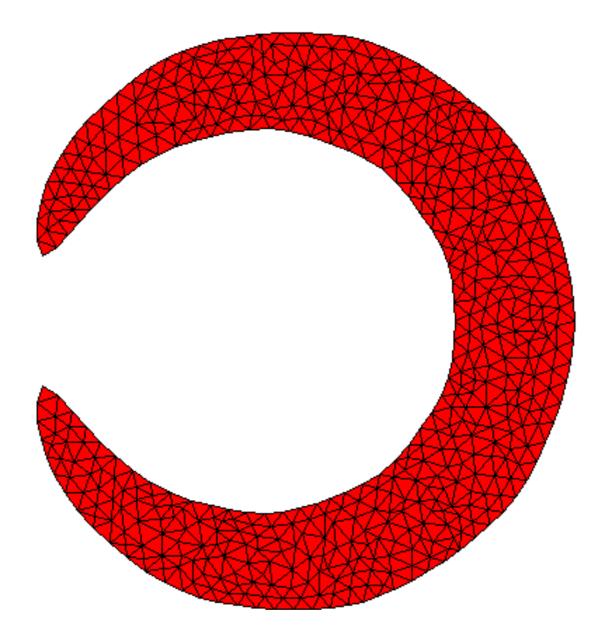


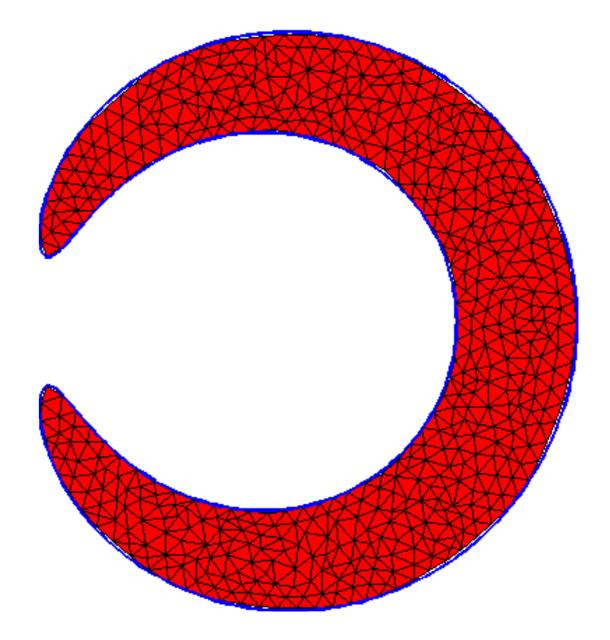


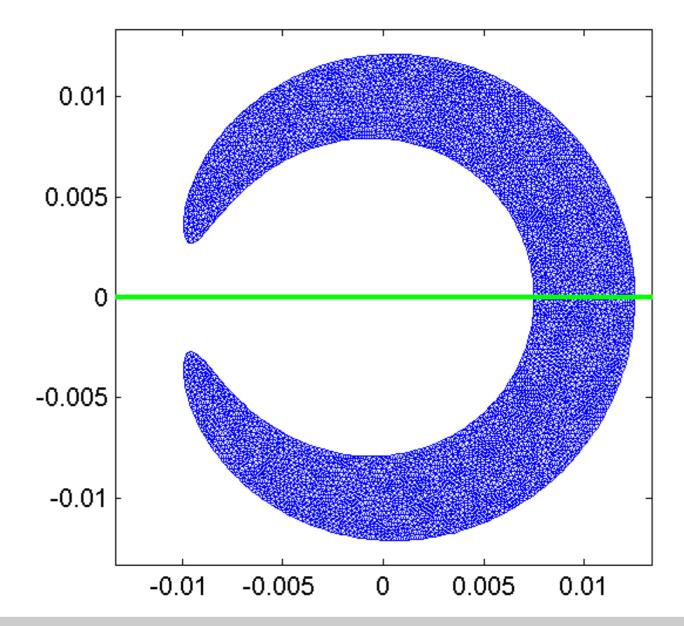


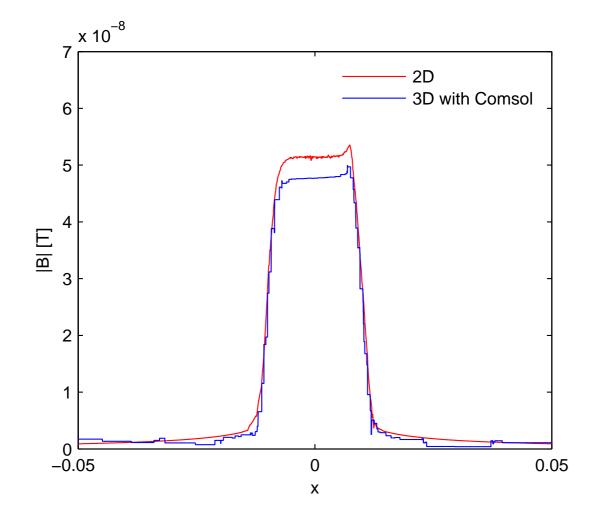
Twist pitch = 5.5 mm

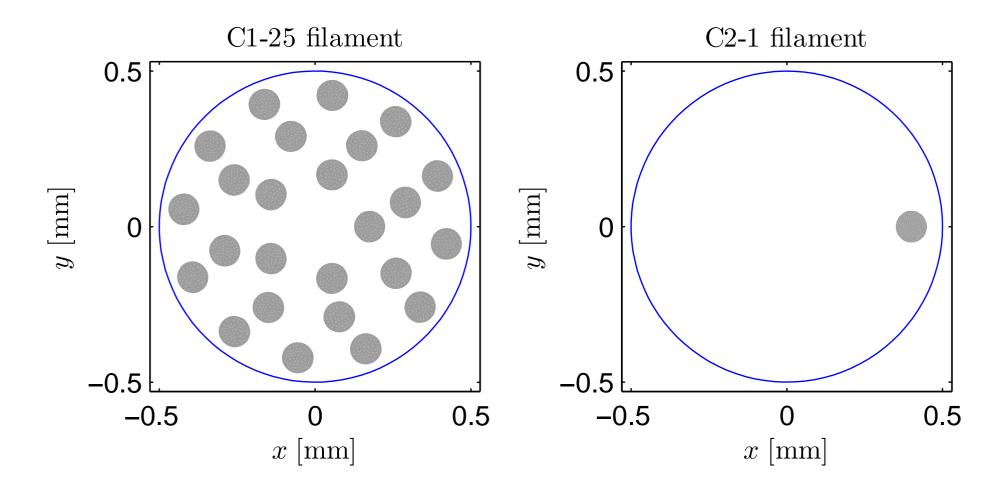


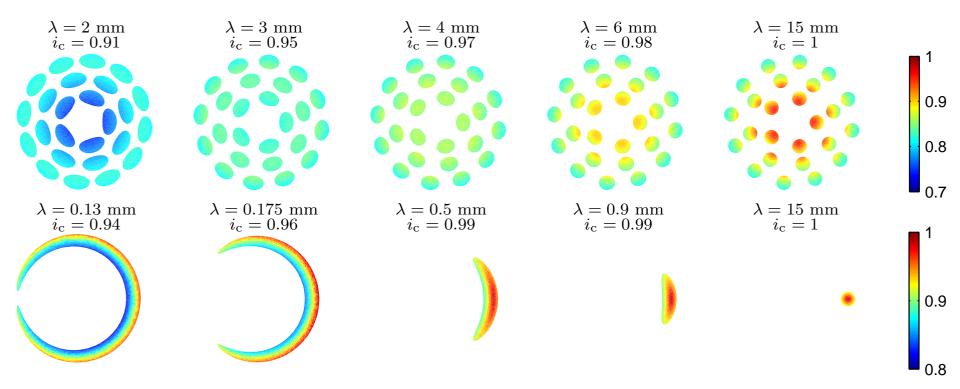




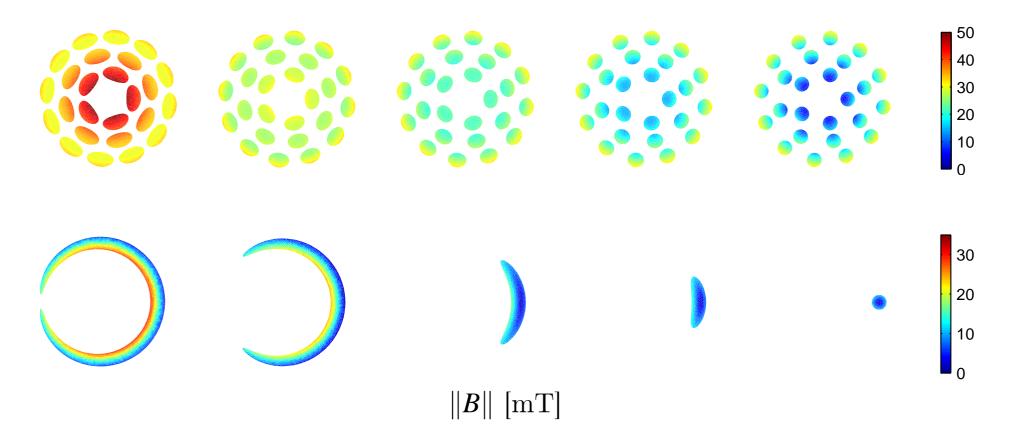


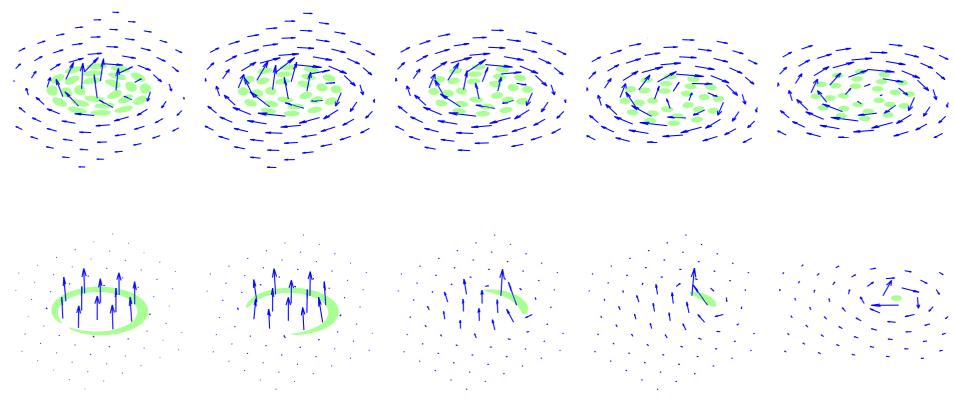






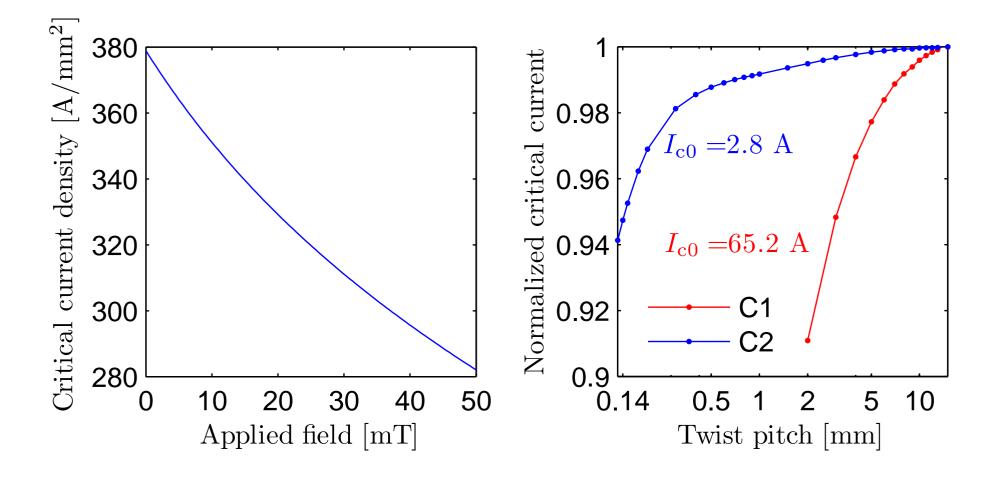
Local critical current density normalized to zero field  $J_c$  at saturation state.





Magnetic flux density vectors

## **Application to superconductors:** $I_c$ computations



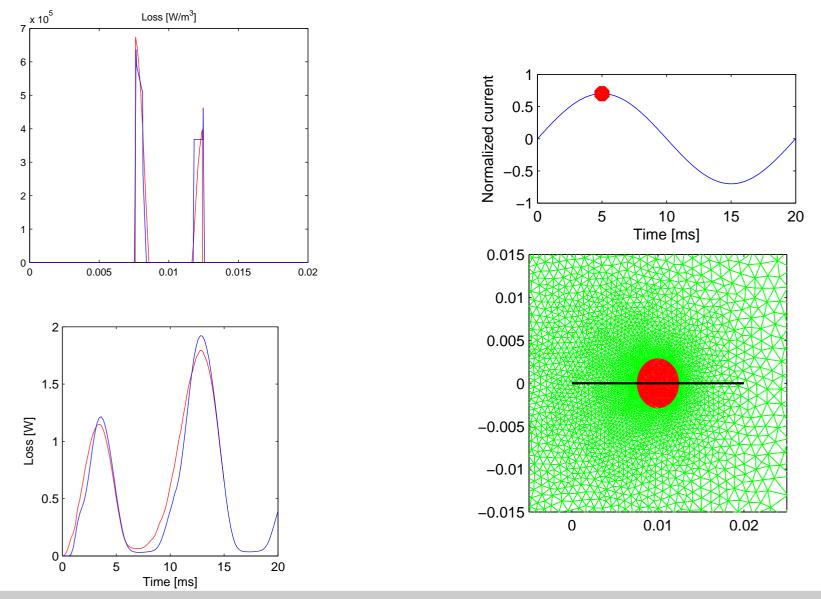
- Starting point: eddy current formulation and non-linear power-law resistivity in superconducting region.
- Two approaches: *H*-formulation in 3D (previous talk) and mixed A-V-J-H-formulation in 2D utilizing the symmetry.
- First assumption in 2D model: currents flow only helicoidally.
- Same geometry as earlier (twist pitch = 10 cm),
  - $J_{\rm c} = 100 \ {\rm A/mm^2}$
  - n-value = 19
  - operation current  $0.5I_c$ ,  $0.7I_c$ ,  $0.9I_c$  ( $I_c = 1965$  A)

• Comparison of computed losses (mJ) per twist per cycle

i	3D	$2\mathrm{D}$	Norris loss <sup>*</sup>
0.5	$3.85^{\#}$	$5.19^{\#}$	4.41
0.7	14.2	15.3	14.5
0.9	35.2	36.0	41.0

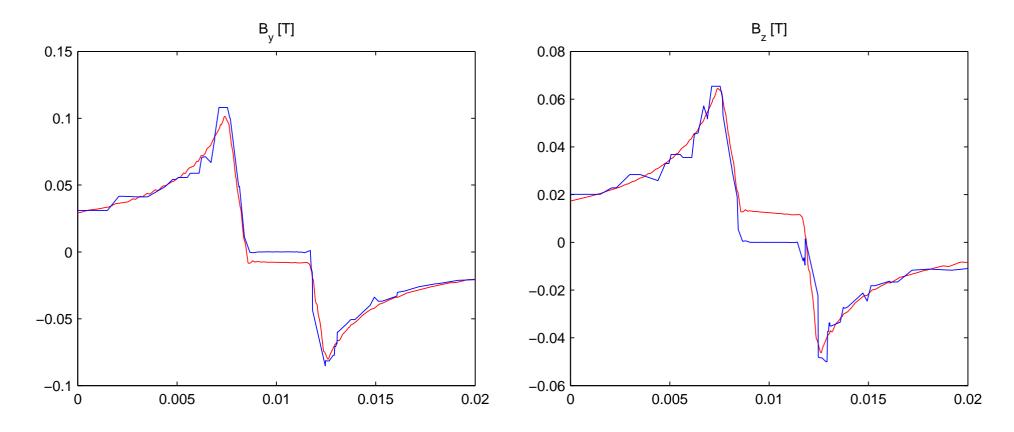
\*Norris loss computed using Norris ellipse formula and multiplied by conductor length in one twist pitch (slightly over 10 cm). This is not the analytical solution of the problem! # It is (well) known that clearly below  $I_c A - V$ -based FEM formulations produce too high loss values. Eddy current based methods result into too low losses when mesh is sparse and current amplitude is low.

• Comparison of field profiles solved in **2D** and **3D** programs (i=0.7)

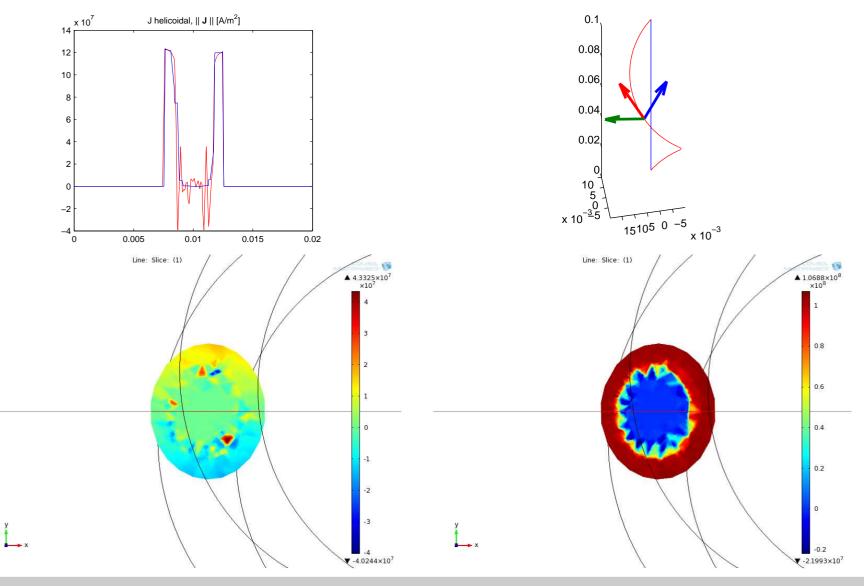


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- In a twisted conductor, current does not flow helicoidally, otherwise center of the conductor is not field free below  $I_c$ .
- It should be possible to also include on plane currents to 2D model, this work is underway.
- Unknown issue:
  - When  $\mathbf{B} \perp \mathbf{J}$  does not hold, how constitutive law or  $J_c$  should be addressed?

# Summary

- Real world physics do not depend on our modelling results or on measurement results.
- In modelling, everything does not need to be like we see.
- Models can be done in many practical equivalent ways.
- Thinking via manifolds can increase one's toolbox of implementing intuitive concepts which seem difficult at first clance.
- Finally, we used some of these ideas to simulate critical current and AC-losses in a helicoidal structures.

# Thank you!

This presentation is also available in my home page: http://antti.stenvall.fi Look for Material → Presentations