

Italian National Agency for New Technologies, **Energy and Sustainable Economic Development** 

**Fusion and Technology for Nuclear Safety and Security Department (FSN)**

# **Liquid Heavy Metal applications for particle accelerators**

**C. Carrelli, M. Tarantino, ENEA FSN-PROIN 12/10/2022**



# **Summary**

Framework:

- Started collaboration with STI Group
- Reference people: M. Calviani, R. F. Ximenes

Summary:

- **Presentation**
- Liquid Heavy Metals
- Liquid Lead feasibility for BDF target
- Liquid Lead option for MuC target



# **Presentation – ENEA Brasimone**



#### Capabilities:

- Experiment design & ops
- Numerical simulations
- Corrosion and chem analysis **GEN IV LFR – ANN/ENEA ALFRED**

Research activities:

- Nuclear Fusion
	- Nuclear Fission Gen-IV  $\longrightarrow$  •



#### **Nuclear Fission Technology**

Main focus:

- Tritium Breeding from liquid Pb-Li
	- Lead/LBE-cooled Fast Reactors



**ITER / DEMO Nuclear Fusion Technology**



### **Presentation – Nuclear Gen-IV Experiments**





### **Presentation – Nuclear Fusion Experiments**



# **Heavy Liquid Metals**

#### Lead

Density: 10660~9000 kg m<sup>-3</sup> Melts: 600 K Boils: 2020 K

#### LBE

Density: 10100~8500 kg m-3 Melts: 398 K Boils: 1930 K

Technological aspects:

- Steel corrosion at  $T > 450^{\circ}$ C (slow process, 10<sup>3</sup> hrs)
- Stagnation areas in loop to be avoided  $(O<sub>2</sub>)$ accumulation, local freezing)
- Ambient pressure ops

Radiological aspects:

- Pb is neutron multiplier:  $n 2n$
- <sup>210</sup>Po production under neutron irradiation in pure lead is  $~10<sup>4</sup>$  less than in LBE<sup>1</sup>
- Studies are being conducted for MHYRRA ADS reactor to verify Polonium production under proton irradiation<sup>2</sup>

<sup>1</sup>[Toshinsky et al, 2020](https://www.scirp.org/journal/paperinformation.aspx?paperid=98300) 2[Choudhury et al, 2018](https://link.springer.com/content/pdf/10.1140/epja/i2018-12646-7.pdf)



# **Liquid Lead BDF Target**

SPS Beam Dump Facility Project

- ECN3 Complex
- Pulse: 1s spill every 7.2s,
- $P_{AVF}$ : 350kW
- Baseline: solid W + TZM

Liquid Lead Proposal

- Target: pure Pb, D150 x L2000 mm
- Loop with circulating pump, HX





## **BDF Target: CFD model**



- Inlet  $@$  400 °C, flow equi-current with beam
- Average velocity in the pipe:
	- 1 m/s (mfr 185 kg/s),
	- $\cdot$  0.5 m/s (mfr 96.5 kg/s)
	- 0.25 m/s (mfr 46.25 kg/s)
- ANSYS CFX, RANS model SST komega y+=1 (boundary layer fully resolved) Mesh 2.2MNodes
- Transient calculations time step 5∙10-4s
- Power map provided by CERN (BDF\_Pb\_heatLoad\_CFX.txt)



# **BDF Target: temperatures**



mfr 185 kg/s mfr 92.5 kg/s mfr 46.25 kg/s

The solution @185 kg/s (1 m/s in the target) ensures that at the beginning of next pulse (7.2s) the target is completely cooled at 400°C. For lower flow rates further investigation are needed to explore the behaviour in the 2° cycle. Mfr 46.25 is still 550°C below the boiling point for lead. Wall temperature is under control.



# **BDF Target: 46 kg/s**



#### mfr 46.25 kg/s (u=0.25 m/s)

- 
- C. Carrelli Liquid Heavy Metals application for particle accelerators
- Max internal temperature **1163°C**, with more than 600°C margin for boiling
- Max wall temperature about **520 °C** (at the end of 1s power deposition)
- These values are very comfortable from an engineering point of view for material resistance
- Lower flow rate better for loop engineering (pump, pressure losses, lead inventory)



### **BDF Target: wall temperature**





# **BDF Target: Lead Loop**

Ongoing activities:

- Loop components sizing
- **Target vessel**
- Loop integration

#### Challenges:

- Housing of components
- High-radiation environment





# **Liquid Lead MuC target**

- Pulse: 2ns every 0.2s,
- $P_{AVF}$ : 2 MW
- Target volume: D30 x L509 mm

- Very high power density
- Limited available space
- MHD losses
- Risk of local lead vaporization





## **MuC target: temperatures**

Thermal map calculated accounting for temperature-dependent properties: maximum temperature expected to be about 25 K below the boiling point. A beam 1.6% more powerful likely to flash the lead at the power peak. Opted for flow equicurrent with beam direction to achieve dilution before high-temperature lead hit walls

At 2000 K (close to boiling point) lead increase by 20% in volume from 400°C.

Average lead volume temperature increase is about 190 K.





#### **MuC target: temperatures**





## **MuC target: wall temperatures**

Adiabatic wall temperatures up to 650 °C (vessel), and 850 °C (beam window).







### **MuC target: wall temperatures**





# **MuC target: Challenges**

Thermo-mechanical:

- Vessel subjected to intense temperature gradient and values
- Regardless of flashing, likely pressure waves and vibrations due to quick lead thermal expansion.
- Beam window gets too hot for common vessel materials:
	- Beryllium?
	- Tungsten?
	- Interaction with Pb?

Integration:

- Limited space
- High radiation environment



## **MuC target: Next steps**

#### Thermo-mechanical:

- Start analysing vessel behaviour
- Try material combination

#### CFD:

- Pressure wave analysis
- Lead flashing analysis

#### MHD:

• MHD losses evaluation

Testing likely to be crucial in the development:

- Lead flashing effects on structures
- Material chemical compatibility

```
Magnetic Reynolds:
            Re_m =\mu_{0}σ
                        uL = 0.0955 \ll 1Where:
σ = electrical resistivity = (67.0 + 0.0471*T)*1e-8 [Ω m]
u = fluid velocity = 2.5 [m/s]
L = fluid typical length = 0.03 [m]
```
Estimated value of  $\text{Re}_{m}$  ensures there is no significant influence of fluid flow to the surrounding magnetic field



### **Conclusions**

Liquid Heavy Metals have potentials to act as particle targets:

- Known and proven technology
- Low radiation damage
- Loops allow to decouple functions

Ongoing collaboration activities:

- BFD target
- MuC HLM target
- Early stages

Thank you!



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