



Cooling windows/absorber

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Muon Collider Collaboration Meeting - October 2022

Outline

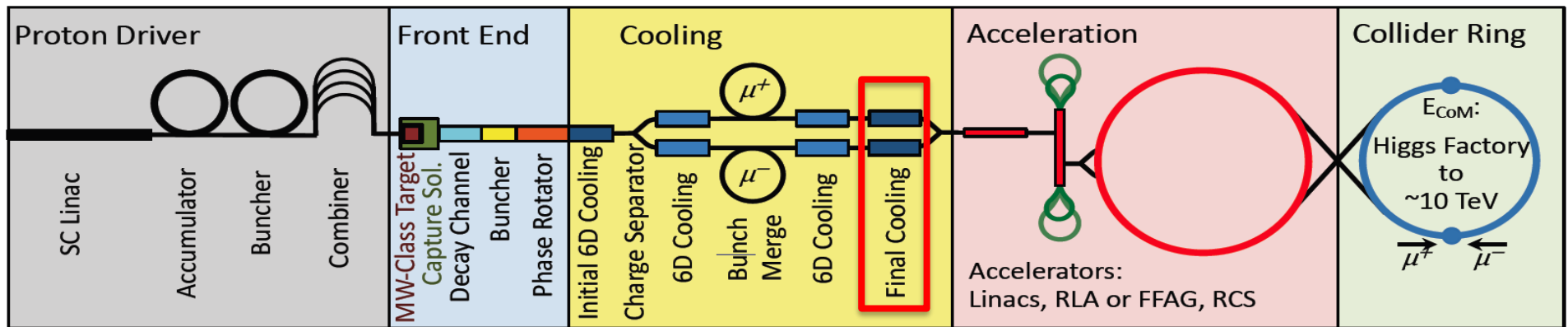
- Introduction: Final cooling
- Thin windows
- Absorber length and pressure
- Other concepts
- Summary

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Introduction

Fully driven by muon lifetime, otherwise would be easy



Short, intense proton bunch

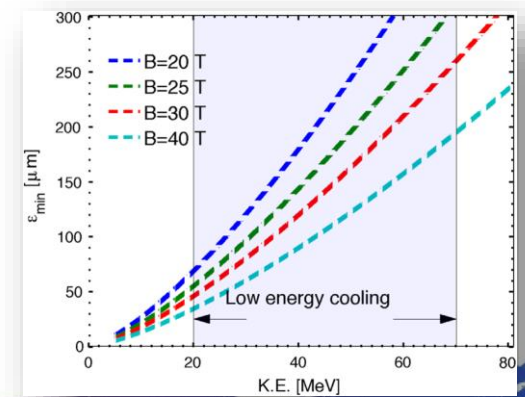
Ionization cooling of muon in matter

Acceleration to collision energy

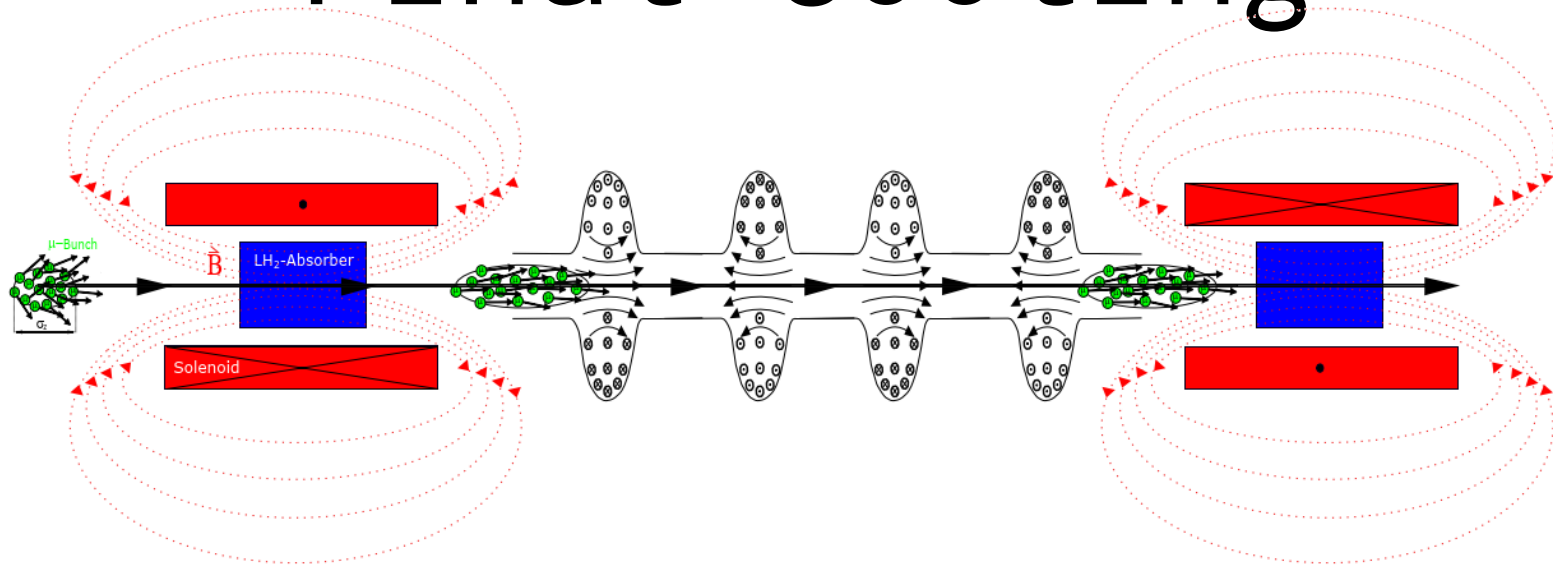
Collision

Protons produce pions which decay into muons. muons are captured

muon kinetic energy from 20 to 5 MeV (last window) [1][2]



Final Cooling



[10]

- ❑ Absorber → H₂ best candidate
- ❑ For liquid/gas absorber → Vacuum windows are required
- ❑ Low energy → Thin windows

TABLE II. Parameters of the high-field low-energy cooling channel.

| Stage | P | Energy spread | LH ₂ thickness | Drift length | rf length | rf frequency | Field flip |
|-------|---------|------------------|---------------------------|--------------|-----------|--------------|------------|
| [N] | [MeV/c] | σ_E [MeV] | [cm] | [m] | [m] | [MHz] | |
| 1 | 135.0 | 2.29 | 65 | 0.434 | 2.25 | 325 | Yes |
| 2 | 130.0 | 2.48 | 60 | 0.459 | 2.25 | 250 | Yes |
| 3 | 129.0 | 2.78 | 60 | 0.450 | 2.5 | 220 | No |
| 4 | 129.0 | 3.10 | 59 | 0.458 | 2.5 | 201 | No |
| 5 | 122.0 | 3.60 | 57 | 1.629 | 5.0 | 201 | Yes |
| 6 | 124.0 | 4.90 | 53 | 2.22 | 4.5 | 180 | No |
| 7 | 116.0 | 3.40 | 42 | 2.21 | 3.25 | 150 | No |
| 8 | 111.0 | 3.90 | 40 | 2.0 | 3.5 | 150 | No |
| 9 | 106.0 | 3.50 | 40 | 3.13 | 5.0 | 125 | Yes |
| 10 | 98.0 | 3.07 | 35 | 3.13 | 5.0 | 120 | No |
| 11 | 89.4 | 3.11 | 20 | 3.12 | 5.0 | 110 | No |
| 12 | 87.9 | 2.76 | 20 | 3.1 | 8.0 | 100 | No |
| 13 | 85.9 | 2.67 | 20 | 3.0 | 7.5 | 100 | Yes |
| 14 | 79.7 | 3.08 | 15 | 2.7 | 7.0 | 70 | No |
| 15 | 71.1 | 4.0 | 15 | 2.6 | 6.0 | 50 | No |
| 16 | 71.0 | 3.80 | 13 | 2.5 | 6.0 | 20 | No |
| 17 | 70.0 | 3.80 | 10 | ... | ... | 20 | ... |



[1]

| Initial Momentum (MeV) | Initial kinetic energy (MeV) | Final kinetic energy MeV |
|------------------------|------------------------------|--------------------------|
| 135 | 65.8 | 39.3 |
| 130 | 61.9 | 36.7 |
| 129 | 61.1 | 35.7 |
| 129 | 61.1 | 36.2 |
| 122 | 55.7 | 30.1 |
| 124 | 57.3 | 34.2 |
| 116 | 51.2 | 32.1 |
| 111 | 47.6 | 28.5 |
| 106 | 44.0 | 23.5 |
| 98 | 38.5 | 18.6 |
| 89.4 | 32.7 | 21.1 |
| 87.9 | 31.8 | 19.8 |
| 85.9 | 30.5 | 18.0 |
| 79.7 | 26.7 | 16.6 |
| 71.1 | 21.7 | 8.8 |
| 71 | 21.6 | 11.0 |
| 70 | 21.1 | 13.2 |

Parameters:

- 20 to 5 MeV cooling
- 4e12 muons/pulse
- 5 Hz repetition rate
- $\sigma_{RMS}=0.6$ mm

Outline

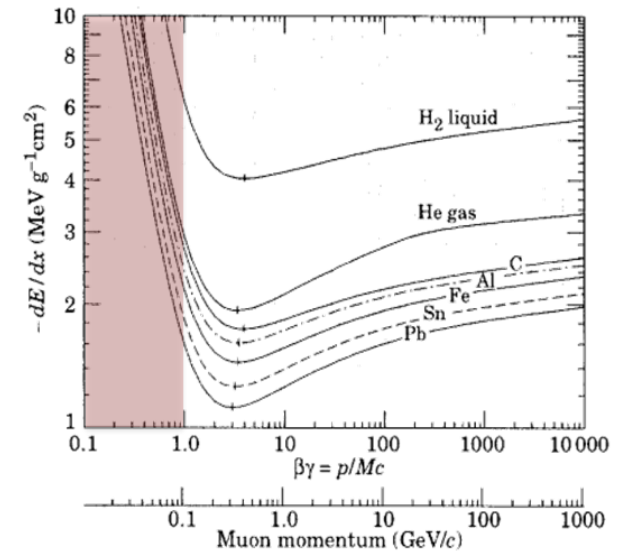
- Introduction: Final cooling
- **Thin windows**
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Thin windows

- Possible materials:
 - Be, Si₃N₄, C, SiC, etc.
- Limit beam perturbation <15μm (approx. <1% of power absorbed in the window for 3keV/μm)
- Thin window → Small window → 10×σ_{RMS}

$$\left\langle -\frac{dE}{dx} \right\rangle_{\text{electronic}} = K \frac{Z}{A} \frac{1}{\beta^2} \left[\frac{1}{2} \ln \frac{2m_e c^2 \beta^2 \gamma^2 Q_{\text{max}}}{I^2} - \beta^2 - \frac{\delta}{2} + \frac{1}{8} \frac{Q_{\text{max}}^2}{(\gamma M c^2)^2} \right] + \Delta \left| \frac{dE}{dx} \right|$$

| | | 5 MeV | 20 MeV |
|--------------------------------|---|-------|--------|
| Be | Stopping power [MeV×cm ² /g] | 11.2 | 4.0 |
| | Linear stopping power [keV/μm] | 2.1 | 0.7 |
| Si ₃ N ₄ | Stopping power [MeV×cm ² /g] | 11.2 | 4.0 |
| | Linear stopping power [keV/μm] | 3.1 | 1.1 |
| C | Stopping power [MeV×cm ² /g] | 12.2 | 4.3 |
| | Linear stopping power [keV/μm] | 2.7 | 1.0 |
| SiC | Stopping power [MeV×cm ² /g] | 11.1 | 4.0 |
| | Linear stopping power [keV/μm] | 3.5 | 1.3 |



Thin windows: Be

- ❑ Well known material
- ❑ As thin as 8 μm in commercial x-ray windows[3]
- ❑ Aperture 7 mm
- ❑ $\Delta P > 1$ bar



Figure 1 Typical Assembly of Beryllium Window

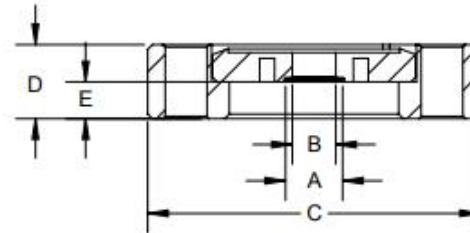


Figure 2 Conflat Flange Geometry

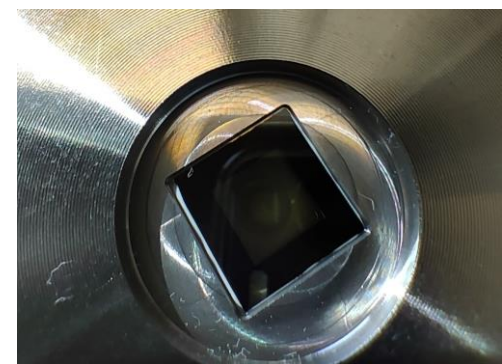
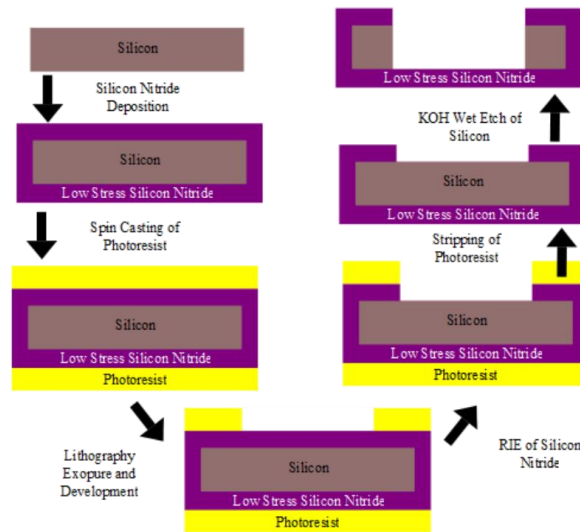
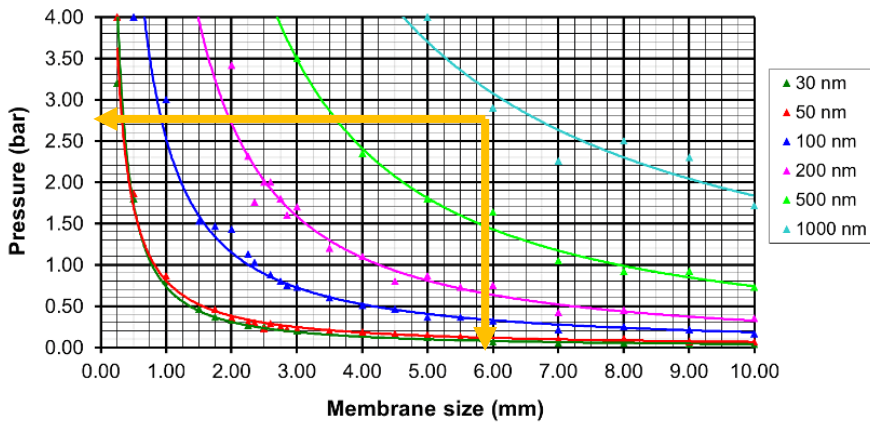


| Table 1 Dimensions of Conflat Flange Options (Refer to Figure 2 above) | | | | | | | | |
|--|----------------------------------|------------------------|--------------------------------|----------------------------|-----------------------|------------------------|---------------|--------------------|
| CF | Foil Thickness (μm) | Foil Diameter (mm) - A | Through Hole Diameter (mm) - B | CF Outer Diameter (mm) - C | CF Thickness (mm) - D | Window Height (mm) - E | Coating | Part ID |
| 1-1/3" OD | 8.0 | 9.2 | 7.0 | 33.8 | 7.2 | 0.5 | DuraCoat Plus | DBM-08-9.2-CF1.3-P |
| | 25.0 | 16.0 | 13.0 | 33.8 | 7.2 | 0.5 | DuraCoat | DBM-25-16.0-CF1.3 |
| 2-1/8" OD | 8.0 | 9.2 | 7.0 | 53.6 | 11.9 | 6.5 | DuraCoat Plus | DBM-08-9.2-CF2.1-P |
| | 25.0 | 16.0 | 13.0 | 53.6 | 11.9 | 6.5 | DuraCoat | DBM-25-16.0-CF2.1 |

Thin windows: Si_3N_4

- ❑ Commercially available: Xray windows i.e. [4]
- ❑ Thickness $< 1 \mu\text{m}$
- ❑ It can work at cryogenic temperature [11]
- ❑ Bulk material has excellent mechanical properties [5]
- ❑ $1 \mu\text{m}$ $6 \times 6 \text{mm}$ window $\rightarrow \approx 5 \text{ bar}$ pressure

Maximum differential pressure v membrane size
(membrane thickness 30 nm to 1000 nm)



Thin windows: C

- ❑ Thickness $< 1 \mu\text{m}$
- ❑ Different options: Graphenic carbon [12] or diamond [13]

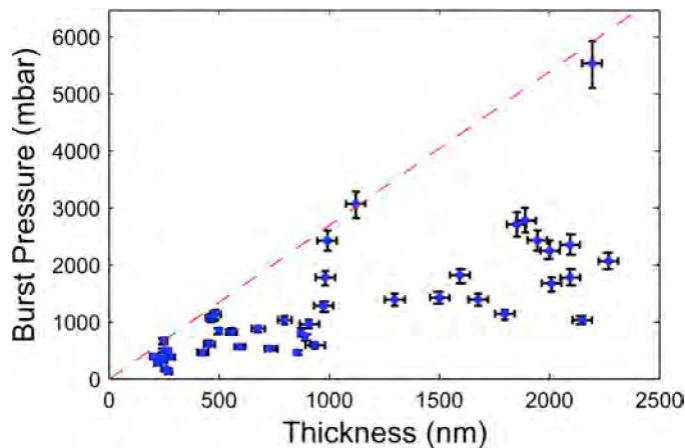


Fig. 4. Measured thickness dependent burst strength of fabricated GC transmission windows with a diameter of 7 mm.

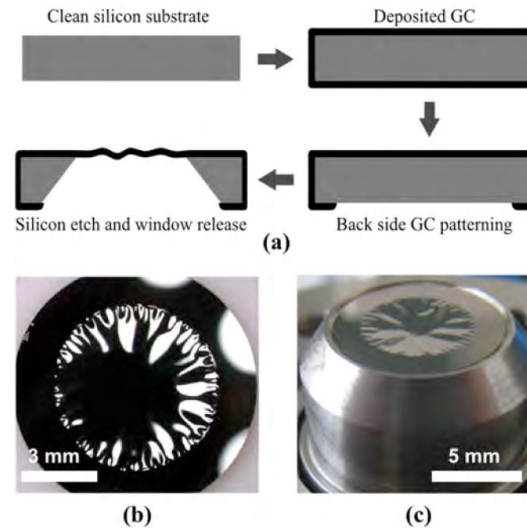


Fig. 2. (a) sketches the fabrication process of the transmission window. (b) shows a top view image of a fabricated GC window. (c) depicts a TO8 housing with a GC window glued into the top of the housing

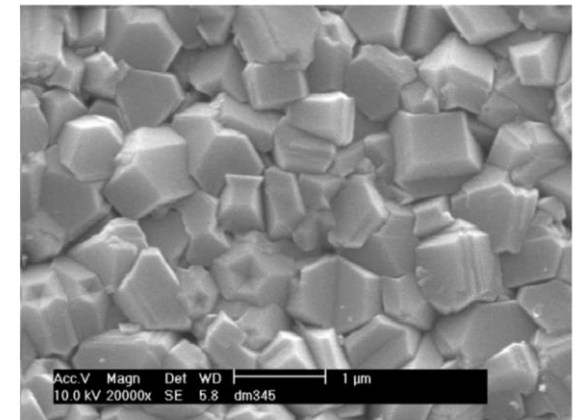
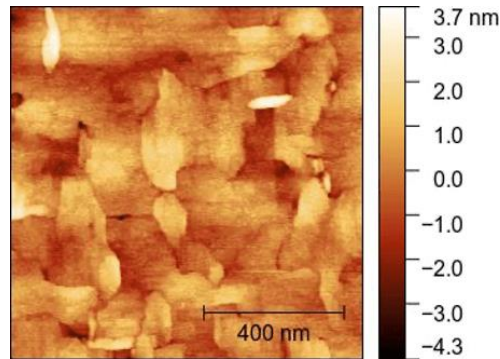


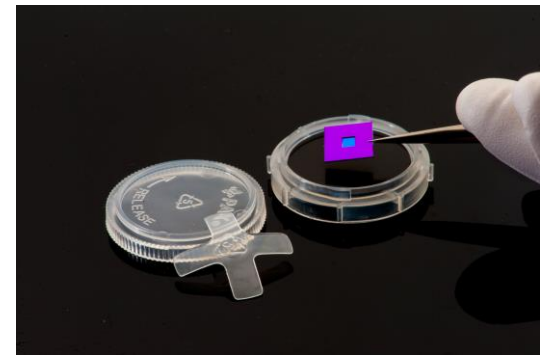
Fig. 4. SEM picture of the diamond film 345#.

Thin windows: SiC

- ❑ Thickness $< 1 \mu\text{m}$
- ❑ Bulk material has excellent mechanical properties
- ❑ No many commercial suppliers [6]



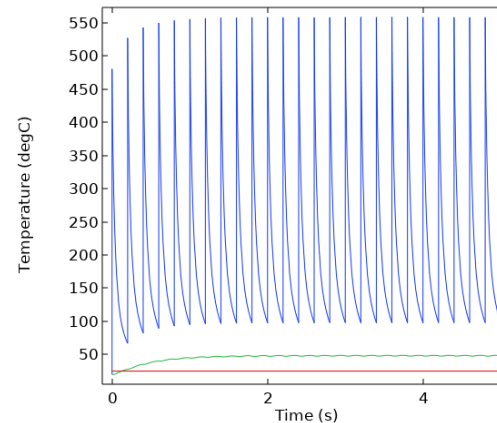
Silson



Thin windows

- Approx 1 mm stops the beam completely at 5MeV (1.3 mm for Be)
- Several candidates for thin windows
- Better characterization and evaluation required but first numbers look promising
- Measure mechanical properties (cryogenic to high temperature) for precise thermomechanical simulations. Bulge test [14] with interferometry?
- Pressure in the absorber is critical for the window definition

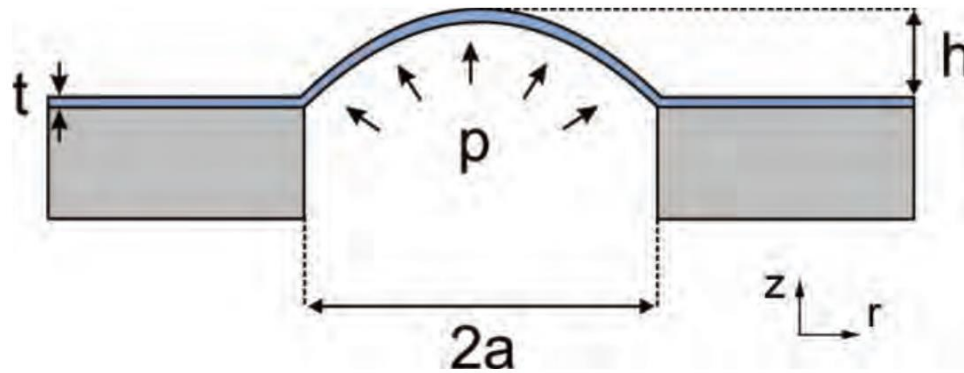
| | | 5 MeV | 20 MeV |
|-----------|-----------------------------|-------|--------|
| Be | ΔT_{inst} [K] | 174 | 61 |
| | Cyclic Thermal Stress (MPa) | 485 | 171 |
| Si_3N_4 | ΔT_{inst} [K] | 470 | 169 |
| | Cyclic Thermal Stress (MPa) | 228 | 82 |
| C | ΔT_{inst} [K] | 507 | 180 |
| | Cyclic Thermal Stress (MPa) | 1013 | 360 |
| SiC | ΔT_{inst} [K] | 467 | 168 |
| | Cyclic Thermal Stress (MPa) | 224 | 81 |



Si_3N_4 \varnothing 7 mm $1\mu m$ at
 5 MeV - 0.6 mm
 gaussian beam
 Only room
 temperature ambient
 radiation

$$\sigma_{cyc} \approx \frac{1}{2} \alpha E \Delta T \quad \Delta T_{inst} = \left(\frac{dE}{dx} \right) \frac{N}{2\pi\sigma^2\rho c}$$

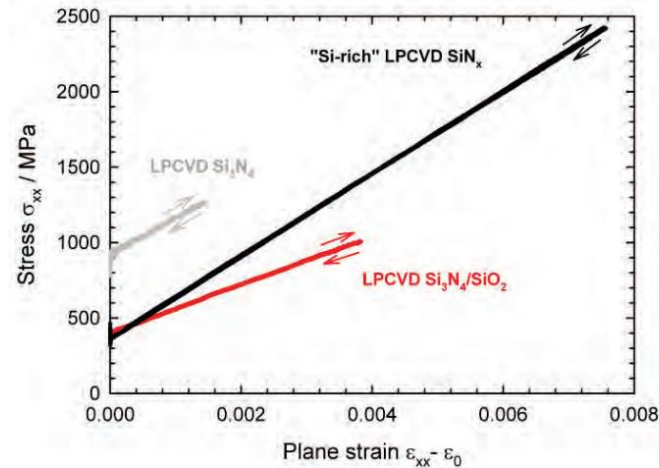
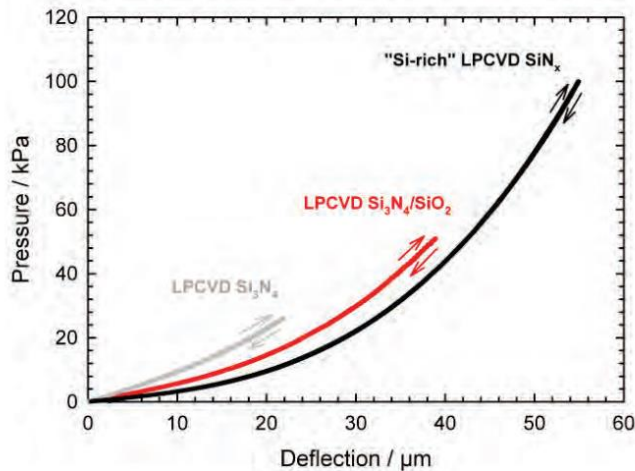
Thin windows



$$\sigma_r = \frac{pa^2}{4ht}$$

$$\epsilon_r = \frac{2h^2}{3a^2} + \epsilon_0$$

$$p = 4\sigma_0 t \frac{h}{a^2} + \frac{8}{3} \frac{E}{1-\nu} t \frac{h^3}{a^4}$$



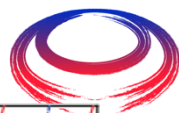
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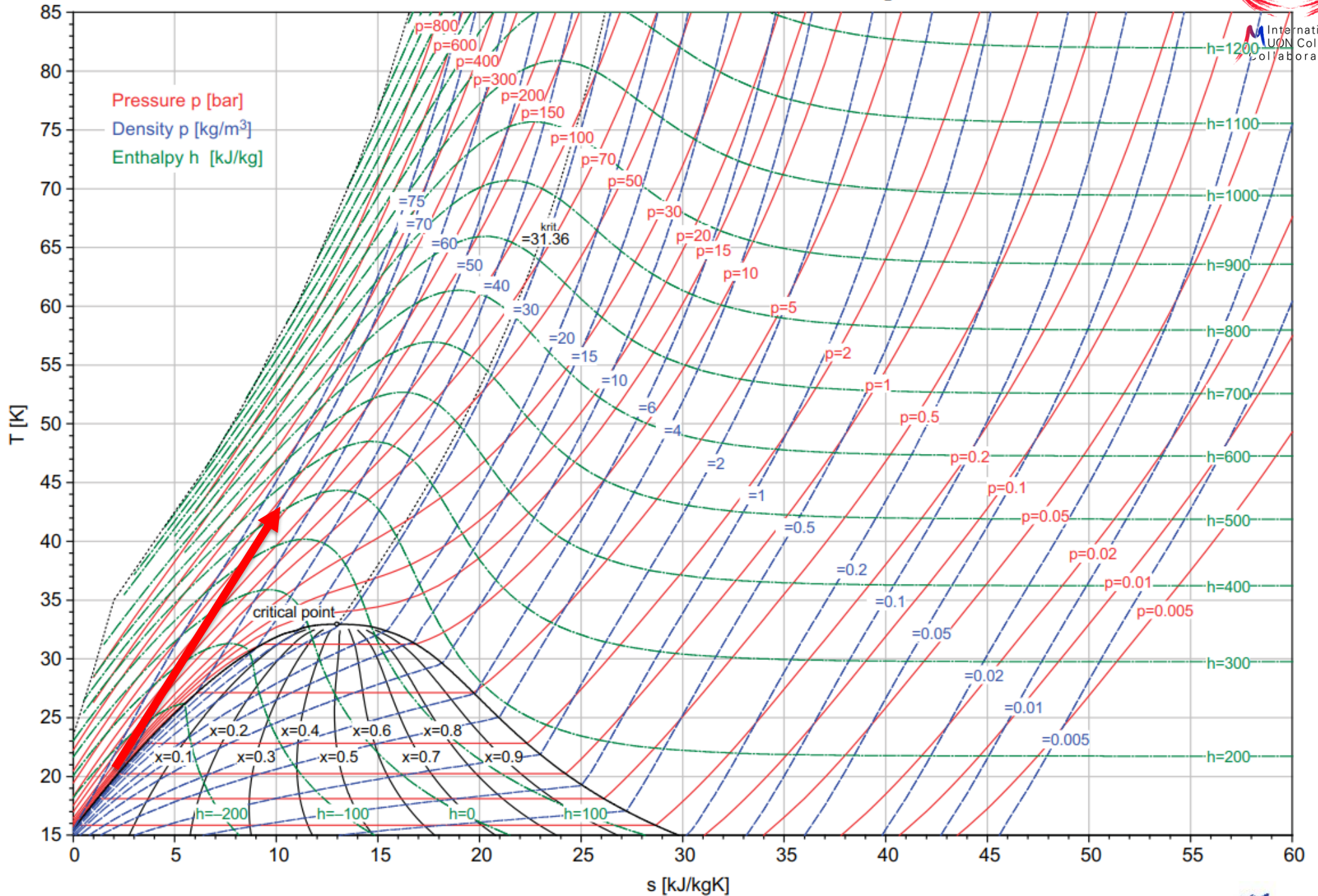
Adsorber

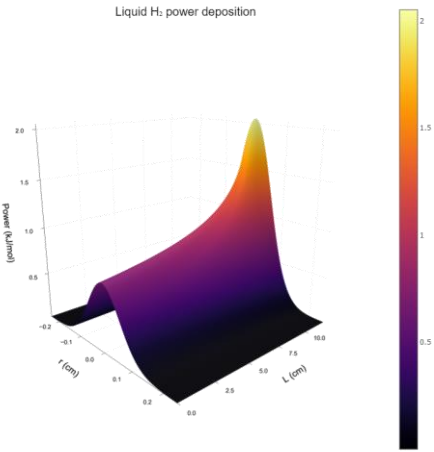
$$\epsilon_{min,N} \propto \frac{E}{BL_R(dE/ds)} \quad [1]$$

- H₂ best absorber material
- What is the required density?
- Which length can we expect?



Ts-Diagram for Hydrogen (Equilibrium H₂)





Absorber length

20 → 5 MeV from [8][15]. 9.6 J, not including heat load from muon decay

| H ₂ Absorber | Length | Max P (bar) | Max T (K) | P assuming power deposited in $3\times\sigma_{\text{RMS}}$ (bar) | K assuming power deposited in $3\times\sigma_{\text{RMS}}$ (K) |
|-------------------------|--------|-------------|-----------|--|--|
| RT@1bar | 124 m | 1.3 | 373 | 1.04 | 303 |
| RT@4bar | 31 m | 5.2 | 373 | 4.18 | 303 |
| 20.3K@1bar vapor | 8 m | 7.5 | 140 | 1.8 | 34 |
| 26.1K@4bar vapor | 2.1 m | 29.2 | 143 | 7 | 40 |
| 20.3K@1bar liquid | 15 cm | 833 | 128 | 125 | 35 |

Is the H₂ absorber compatible with a thin window?
Is there any concept to make both compatible?

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Other concepts? Solid?

- ❑ Solid hydrogen can be produced in small pellets
- ❑ It is possible to produce 6 mm diameter >10 mm long pellets [16][17]
- ❑ Very likely there is a limit to the length of the solid plug produced by condensation → Several plugs in the same tube?
- ❑ It will allow to decouple the window from the absorber (vacuum space)

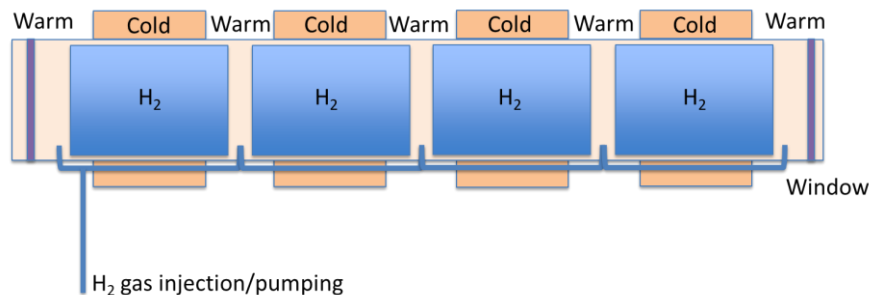
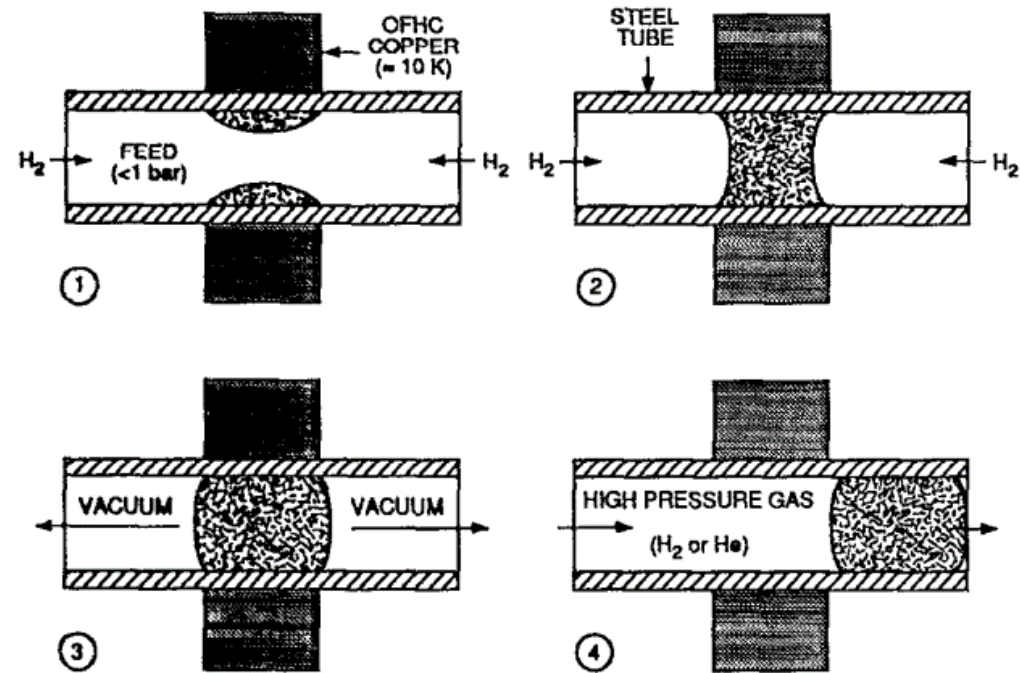


FIG. 1. Principles of operation for a “pipe-gun” pellet injector: (1) introduction of room-temperature gas (pure H_2 , D_2 , T_2 , or a mixture) initiates the solidification process, (2) freezing process continues, filling in the center of the pellet within a few minutes, (3) residual gas is pumped away after sufficient freezing time, and (4) high-pressure gas is admitted at the breech to accelerate the frozen pellet in the tube.

Other concepts? Solid?

- Power deposition \rightarrow H_2 will be melted and heat up (>100s bars)
- Will part of this fluid be expelled into the vacuum volume?
- Is there enough time between pulses to recondense the gas produced during the shot?
- Will the shape be preserved?

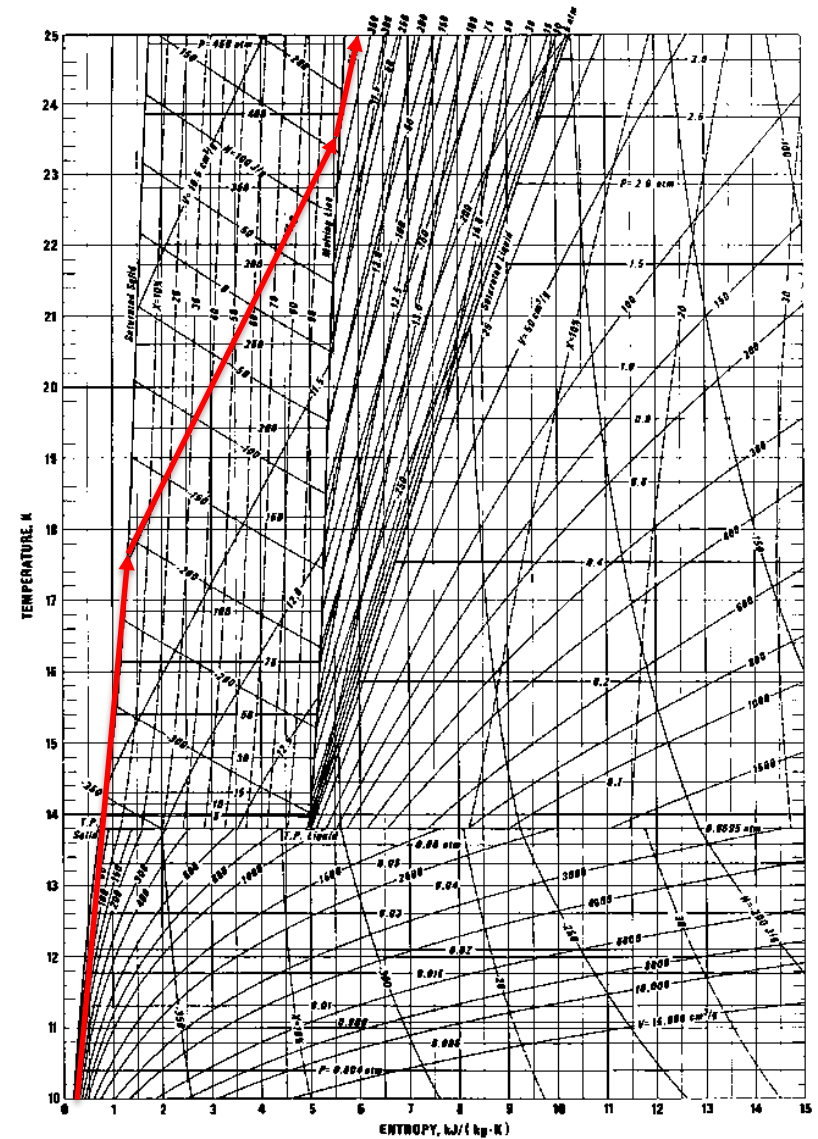
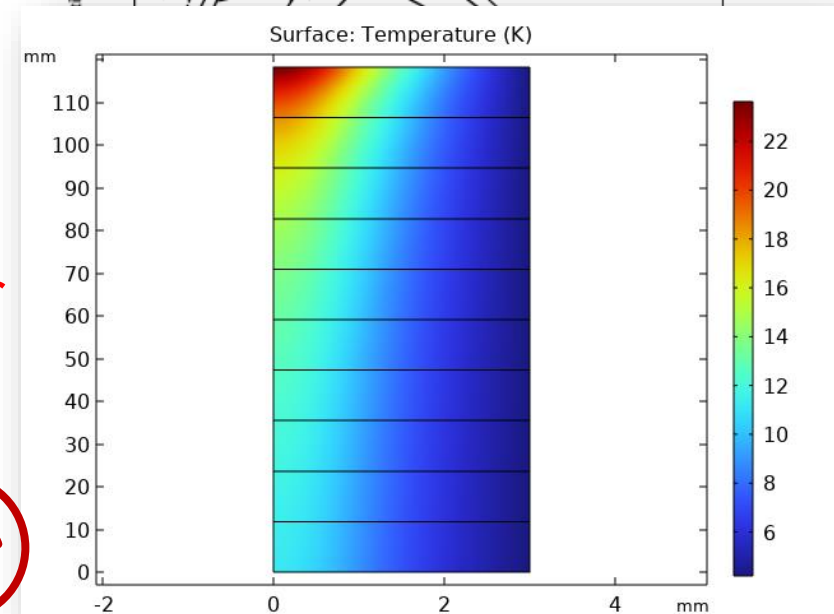
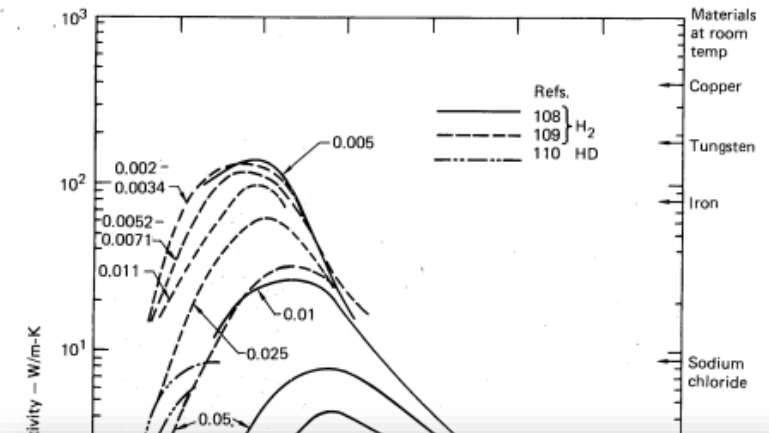


FIGURE 43. Parahydrogen, temperature-entropy diagram (10 to 25 K).

Other concepts? Solid?

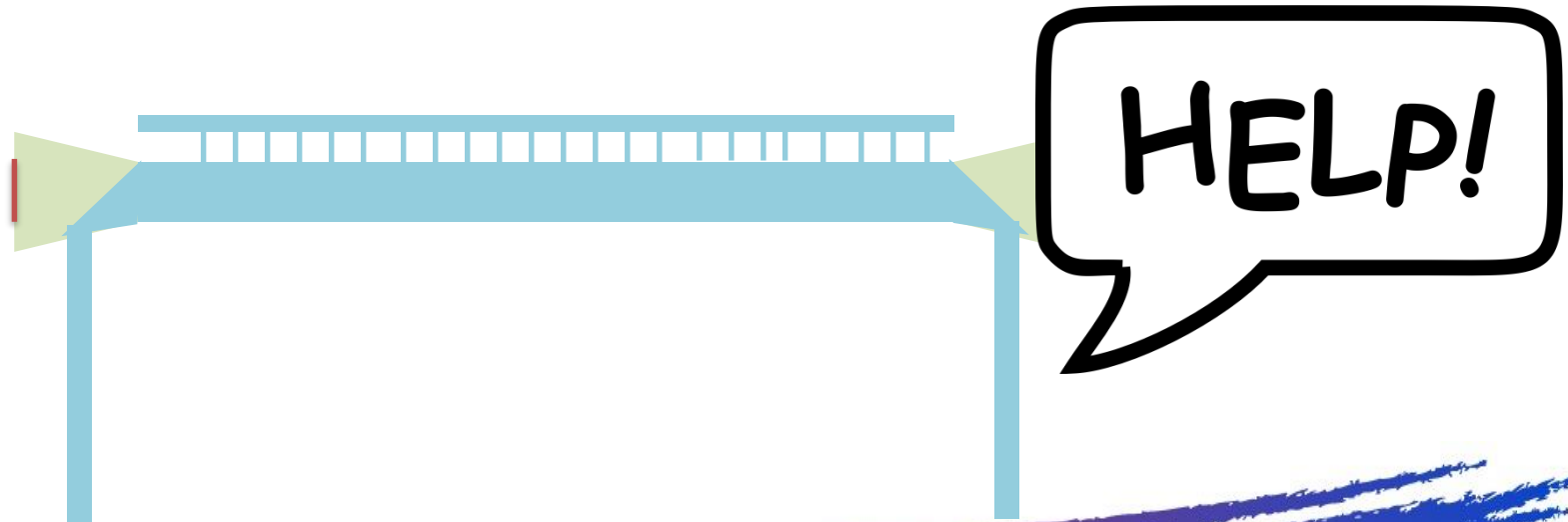
- ❑ Assuming 10 W/m/K
- ❑ From 20 to 5 MeV
- ❑ Radius = $5\sigma_{rms}$
- ❑ 10 segments with adiabatic boundaries (12 mm long)
- ❑ Boundary at 4.2K

- ❑ Last section of the cooling too hot (no longer solid)



Other concepts?

- How to implement inside a small magnet bore?
- Is it possible to take the windows out of the solenoid?
- At 14.5K vapor pressure 100 mbar → Lower ΔP
- Liquid curtain?
- Shutter to expose the liquid for a fraction of time?
- Keep bubble in front of window (extra heat load to absorber)?
- Reproducibility of absorber length?



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- ❑ Several window candidates for final cooling.
 - ❑ Systematic study of the different candidates
 - ❑ Measurement of mechanical properties at working temperature
 - ❑ Thermomechanical simulations
 - ❑ Validation in proton facilities with equivalent power deposition

- ❑ High density absorber required to have a short solenoid, but power deposition → High pressure. Compatible with thin window?

- ❑ Shock wave and phase change after power deposition in liquid hydrogen → Very challenging CFD problem out of reach of commercial codes

- ❑ Possible mitigations?:
 - ❑ Repetition rate
 - ❑ Lower density (long solenoid)
 - ❑ Higher energy
 - ❑ Decouple window and absorber → new concept

References

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