# From 32 T to the 40 T All-Superconducting Magnet

# **NATIONAL HIGH** MAGNETIC **FIELD LABORATORY**

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- 32 T All-superconducting magnet
	- *Timeline and development*
- 40 T All-superconducting magnet
	- *Technical challenges*
	- *Test coils*
		- *Insulated REBCO*
		- *Resistive Insulation REBCO*
- Outlook

#### The 32 T magnet

Key parameters:







15 T / 250 mm bore LTS magnet 17 T / 34 mm bore REBCO coils Separately powered, simultaneously ramped

REBCO: 2 double pancake coils Nb <sup>3</sup>Sn coils NbT<sub>i</sub> coils



#### 32 T Project Timeline and Development

• 2007 – 2008 IGC/SP test two test coils @NHMFL to 27 T (19 T background)



- 2008 NHMFL 33.4 T Test coil (31 T background)
- 2009 Initial funding of 32 T
- 2009 2012 Additional test coils



High Hoop-stress coils >760 MPa



42-62 Mark 1: 1<sup>st</sup> test coil



42-62 Mark 2: 2<sup>nd</sup> test coil





31 T + 2.4 T





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### 32 T Project Timeline and Development

• 2013 – 2014 Prototype test coils







2<sup>nd</sup> Full-featured **Prototype** 



### 32 T Project Timeline and Development

• 2015 – 2017 Construction and Testing



• 2020 Open for User Operations



### 40 T All-Superconducting Magnet Project

- National Science Foundation Funded Design Project through 2025
- Implementation/Construction Proposal to Follow
- Specifications:
	- Central field: 40 T
	- Operating temperature: 4.2 K
	- Cold bore diameter: ≥ 34 mm
	- Ramp rate: ≥ 0.5 T/min
	- Operating lifetime: 50,000 cycles or 20 years
	- Homogeneity: ≤ 500 ppm over a 1 cm DSV
	- 10 Gauss fringe field: < 5.4 m
	- Stabilization time: < 3 minutes
- Two design options are being considered
	- Insulated REBCO (I-REBCO)
	- Resistive Insulation REBCO (RI-REBCO)





#### 40 T Technical Challenges - Compactness

- Simple scaling of the 32 T to 40 T is not feasible
	- LTS outsert field / bore size too large
	- Most economical to design HTS coils to fit inside the commercially available 15 T LTS or 12 T LTS (with inner  $Nb<sub>3</sub>$ Sn coil removed)
	- Need to increase current density of HTS coils, *J eng, J cu*
		- For  $J_{eng}$  we need to increase  $f_{lc} = I_{op}/I_c$ 
			- Reduced screening currents and better quench management
			- Higher chance of finding conductor defects
			- Better knowledge of conductor properties are required  $(I_c(B, \theta)$ , ab-plane)
		- For *J cu*
			- 32 T:  $J_{cu} = 420 \text{ A/mm}^2$
			- I-REBCO goal:  $J_{cu}$  = 700 A/mm<sup>2</sup>
			- RI-REBCO goal:  $J_{cu} = 1500 \text{ A/mm}^2$



#### 40 T Technical Challenges - Compactness



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#### 40 T Technical Challenges – Stress Management

- It is critical to have precise knowledge of the conductor strain state
- We are working to improve accuracy of electromagnetic-screening current strain calculations
- An electromagnetic model (TA formulation) computes current & density is coupled with a structural model for strain and deformations. Iterated to recompute e-m with updated applied field angle from conductor deformations.







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#### 40 T Technical Challenges – Stress Management



 $\overline{1}$ 

400

500

popula



Critical Current of Conductor for the 32 T

This conductor is "TOO GOOD"

Operating margin is large:

- **Exceedingly stable**
- 130,000 J to protect 100 kg HTS coils
- 300 J to protect 1400 kg LTS coils



#### Calculated critical current (32 T) at full field

• Operating current is 1/10 to 1/3 of critical current



- Design approach is to maintain a constant fraction of critical current
- Example design of a 12-disk coil with maximum  $f_{1c}$  = 0.70 within a pancake
- Constant  $f_{1c}$  is achieved by varying a "standard" conductor critical current from 25 % - 90 %





- The angular tilt of the REBCO ab-plane shifts the  $I_c(\theta)$  peak
- Mixing up the "left" / "right" orientation can greatly affect the critical current of a module
- We are developing techniques to determine the angle and orientation of a tape's ab-plane
- See Lu, ASC2022 2MPo2A-04











#### 40 T, Small Scale Test Coils



PTC1 (Apr 2019)



(Apr 2019)



PTC2 (Jun 2019)



LBC-CO (Aug 2019)



PT1R (Oct 2019)



Mini fatigue coil – Off centered (Jun 2020)



PT3 (July 2020)





PTC4



Mini fatigue coil – centered (Mar 2021)



Axial pressure test coils (Mar 2021)



PTC5 (Mar 2021)



Axial pressure test coil: two in hand (April 2021)



PT<sub>6</sub> (June 202

#### 40 T, Mid-Scale Test Coils



- Most Recent Test Coils
	- I-REBCO: "TC2"
		- Single insert coil operated in the 45 T Outsert
		- Two-in-hand REBCO winding "MTI"
	- RI-REBCO: "RI-NC"
		- Two nested coils self field
		- Inner coil: 12 DP's
		- Outer coil: 18 DP's





#### I-REBCO Test Coil – TC2

- Single insert coil operated in the 45 T Outsert
- Central field: 25.4 T (11.4 T background)
- Current: 570 A
- Stored energy: 47 kJ
- Inductance: 289 mH
- Six conductor grades
- $J_{cu} = 650 \text{ A/mm}^2$
- Protected via pulsed forming network



#### I-REBCO Test Coil – TC2

- Fully characterized *I <sup>c</sup>* of each tape used in the test coil via torque magnetometry
	- See Jaroszynski ASC2022, 2MOr2B-01
- Critical surface of each spool is unique and not scalable based from single point measurements







Sinus Squared M3-505-3adj fit v M4-547-6 3 1661.25m

#### SinusSquared M3-505-3adj fit v M4-548-2 10 2100.06n





#### I-REBCO Test Coil – TC2

- The main purpose of TC2 was to study quench
- Quench modeling now includes deformation of conductors from screening currents, which affects critical current
- Very good agreement between predictions and measurements



#### RI-Nested Coils

- Two nested REBCO Coils
- Central field: 19.2 T (225 A)
- Stored energy: 0.105 MJ
- Inductance: 4.15 H
- Target  $R_c = 2.7$  m $\Omega$
- Mid-plane pressure = 60 MPa (coil 2)
- Self contained axial forces, designed to 245 kN
- Testing occurred late September



#### RI -Nested Coils

- Quench tests
	- Active protection system
	- Varied energy level of quench heaters to study discharge time and quench propagation
	- Quench initiated

• Coil 2, module 12



## RI -Nested Coil

- Quench moment
	- Module starts to transition
		- $\cdot$  t ~ 57 s
	- Voltage rises until exceeding threshold of 0.5 V for 5 ms
		- $t = 57.045 s$
	- Protection fires
		- $t = 57.046 s$
	- Other modules start to normalize within 10 ms
		- $t = 57.057 s$
- Comparisons with modeling are proceeding



#### RI-Nested Coils

- Contact resistance
	- Target  $R_c$  = 2.7 m $\Omega$
	- Measured:  $0.74 \text{ m}\Omega$ 
		- Using fast discharge method
	- Contact resistance remained constant through the testing



First discharge test

Final discharge test (after quench tests)



## **Outlook**

- Technical risks are being retired because of the results produced by the test coils and conductor characterizations – but there is still more to do
- Additional thermometry is being added to TC2, which will be retested in November
- RI-NC results are still being reviewed
- Within 1-year we will select the technology for the 40 T final design
- Final demonstration large scale coil testing to be performed based on final design